

Noninvasive dynamic output-feedback stabilization of multistable systems

Samuele Zoboli^{**} Andreu Cecilia^{*} Sophie Tarbouriech^{**}

^{*} *Universitat Politècnica de Catalunya, Avinguda Diagonal, 647, 08028 Barcelona, Spain, (e-mail: andreu.cecilia@upc.edu)*

^{**} *LAAS-CNRS, Université de Toulouse, CNRS, Toulouse, (e-mail: samuele.zoboli@laas.fr, sophie.tarbouriech@laas.fr)*

Abstract: Artificial intelligence, machine learning, engaging keywords.

Keywords: LMI, Controller design, Matrix inertia, Nonlinear systems, Contraction, k -contraction.

1. INTRODUCTION

To be written

Notation: $\mathbb{R}_{\geq 0}[0, \infty)$ and $\mathbb{N}\{0, 1, 2, \dots\}$. $|\cdot|$ denotes the standard Euclidean norm. Given $x \in \mathbb{R}^n$, $y \in \mathbb{R}^m$, we set $(x, y)(x^\top, y^\top)^\top$. The inertia of a matrix P is defined by the triplet of integers $(P)(\pi_-(P), \pi_0(P), \pi_+(P))$, where $\pi_-(P)$, $\pi_+(P)$ and $\pi_0(P)$ denote the numbers of eigenvalues of P with negative, positive and zero real part, respectively, counting multiplicities.

2. PROBLEM FORMULATION

We consider nonlinear systems of the form

$$\begin{aligned} \dot{x} &= Ax + D\phi(Ex) + Bu, \\ y &= Cx + G\phi(Ex), \end{aligned} \quad (1)$$

where $x \in \mathbb{R}^{n_x}$ is the state vector, $u \in \mathbb{R}^{n_u}$ the controlled input, $y \in \mathbb{R}^{n_y}$ the measured outputs and $\phi: \mathbb{R}^{n_v} \rightarrow \mathbb{R}^{n_v}$ is a sufficiently smooth vector field. Additionally, to recover efficiently solvable conditions, we assume the existence of known matrices $R = R^\top$, $Q = Q^\top$ and S such that

$$\begin{pmatrix} I_{n_x} \\ \frac{\partial \phi}{\partial x}(v) \end{pmatrix}^\top \begin{pmatrix} R & S^\top \\ S & Q \end{pmatrix} \begin{pmatrix} I_{n_x} \\ \frac{\partial \phi}{\partial x}(v) \end{pmatrix} \preceq 0 \quad (2)$$

holds for all $v \in \mathcal{V} \subseteq \mathbb{R}^{n_v}$ where $\mathcal{V} = \{v \in \mathbb{R}^{n_v} : v = Ex, x \in \mathcal{X} \subseteq \mathbb{R}^{n_x}\}$. We recall that such a class of nonlinearities includes common and interesting family of functions, such as (shifted) monotonic and differentially sector-bounded ones (Zoboli et al., 2024b). Finally, we assume that in the unforced case, namely when $u = 0$, system (1) presents a set of fixed points \mathcal{F}_x^* . More formally, we assume the existence of a nonempty set of equilibria

$$\mathcal{F}_x^* := \{x \in \mathbb{R}^{n_x} \mid Ax + D\phi(Ex) = 0\}. \quad (3)$$

We highlight that \mathcal{F}_x^* can include multiple elements, that is, system (1) may present multiple equilibrium points for the unforced case $u = 0$.

We aim to design a feedback control policy that makes (at least) one point $x^* \in \mathcal{F}_x^*$ asymptotically stable. In other

words, we want to make the set \mathcal{F}_x^* attractive and forward-invariant.

One possibility is to reformulate the problem as a standard stabilization one, see e.g. (Isidori, 2017). Differently put, the problem could be solved by selecting a specific point $x^* \in \mathcal{F}_x^*$ and designing a control law making x^* globally asymptotically stable. However, we highlight that the considered problem relaxes the more common stabilization problem in three directions. First, the goal is not to stabilize the system at a specific point in \mathcal{F}_x^* , we only need the system to converge to \mathcal{F}_x^* . Second, the proposed objective allows for the existence of multiple attractive equilibrium points for the closed-loop system. Third, the set of equilibrium points \mathcal{F}_x^* may be unknown to the designer. This third point is particularly relevant for feedback policies that include an integral action, e.g. (Astolfi and Praly, 2017; Giaccagli et al., 2023), which often require an unknown non-zero steady-state control signal to be generated by the integral component. Another possibility is to invoke set-stability approaches, e.g. (Shiriaev and Fradkov, 2000). However, we remark that \mathcal{F}_x^* may be disconnected. Moreover, its elements are given by the (possibly unknown) equilibria of the unforced system dynamics. These facts impose additional restrictions that can impact the effectiveness and applicability of set-stability approaches.

Given the abovementioned constraints, in what follows, we present a solution that does not require knowledge of the open-loop equilibria and guarantees their stability via 2-contraction (Li and Muldowney, 1995). Our approach is based on the recent findings in (Cecilia et al., 2023; Zoboli et al., 2024a) and inspired by the techniques of derivative control and washout filters.

3. MAIN RESULT

3.1 Proposed approach

We start by highlighting a necessary property controllers must satisfy to guarantee the open-loop equilibria are preserved by the closed loop. From (1), it is clear that for the closed-loop system to stabilize at $x^* \in \mathcal{F}_x^*$ the control

^{*} This research is carried out by the infinite utility of k -contraction

input must vanish at such point. We will denote a control policy that satisfies such a property as *noninvasive*, e.g. (Angeli et al., 2024).

Definition 1 (Noninvasive controller). *Consider the non-linear system*

$$\dot{x} = f(x, u), \quad y = h(x),$$

with $x \in \mathbb{R}^{n_x}, y \in \mathbb{R}^{n_y}$ and $u \in \mathbb{R}^{n_u}$. Let

$$\mathcal{F}^* \{x \in \mathbb{R}^{n_x} : f(x, 0) = 0\}.$$

The dynamic output-feedback law $u = \alpha(y, \xi)$ with state $\xi \in \mathbb{R}^{n_\xi}$ is said to be *noninvasive* if

$$\alpha(h(x^*), \xi^*) = 0, \quad \forall x^* \in \mathcal{F}^*, \quad (4)$$

where ξ^* is the controller equilibrium associated to x^* .

In this paper, we propose ensuring such a requirement via integral action. More specifically, we extend the dynamics of (1) as follows

$$\begin{aligned} \begin{pmatrix} \dot{x} \\ \dot{z} \end{pmatrix} &= \begin{pmatrix} A & 0 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ z \end{pmatrix} + \begin{pmatrix} B \\ I_{n_u} \end{pmatrix} u + \begin{pmatrix} D \\ 0 \end{pmatrix} \phi \left(\begin{pmatrix} E & 0 \end{pmatrix} \begin{pmatrix} x \\ z \end{pmatrix} \right), \\ \begin{pmatrix} \dot{y} \\ \dot{z} \end{pmatrix} &= \begin{pmatrix} C & 0 \\ 0 & I_{n_u} \end{pmatrix} \begin{pmatrix} x \\ z \end{pmatrix} + \begin{pmatrix} G \\ 0 \end{pmatrix} \phi \left(\begin{pmatrix} E & 0 \end{pmatrix} \begin{pmatrix} x \\ z \end{pmatrix} \right). \end{aligned} \quad (5)$$

At any equilibrium point (x^*, z^*) the z -dynamics impose $u = 0$, and thus $x^* \in \mathcal{F}_x^*$.

3.2 Controller design

Given the above discussion, we aim to design a dynamic-output feedback controller stabilizing the extended dynamics (5) to a (possibly nonunique) equilibrium. Moreover, we leverage 2-contraction to obtain local exponential stability of equilibria (Muldowney, 1990). In particular, we exploit the techniques of (Zoboli et al., 2024a) to efficiently design a noninvasive linear dynamic output-feedback controller guaranteeing 2-contractivity of the extended closed loop. More formally, we select $n_\xi = n_x + n_u$ and we consider the extended system

$$\begin{aligned} \dot{x} &= Ax + D\phi(Ex) + Bu, \\ y &= Cx + G\phi(Ex), \\ \dot{z} &= u, \\ \dot{\xi} &= M\xi + Ny + Fz, \\ u &= Ky + L\xi + Hz, \end{aligned} \quad (6)$$

which can be equivalently represented as

$$\dot{\eta} = f(\eta) = \mathbf{A}\eta + \mathbf{D}\phi(\mathbf{E}\eta) \quad (7a)$$

with $\eta = \text{col}(x, z, \xi) \in \mathbb{R}^{n_\eta}$, $n_\eta = n_x + n_u + n_\xi = 2n_\xi$ and

$$\begin{aligned} \mathbf{A} &= \begin{pmatrix} A + BKC & BH & BL \\ KC & H & L \\ NC & F & M \end{pmatrix}, \\ \mathbf{D} &= \begin{pmatrix} D + BKG \\ KG \\ NG \end{pmatrix}, \quad \mathbf{E} = (E \ 0 \ 0). \end{aligned} \quad (7b)$$

We also remark that (2) implies the existence of matrices $\mathbf{R}, \mathbf{S}, \mathbf{Q}$ such that

$$\begin{pmatrix} I_{n_\eta} \\ \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \end{pmatrix}^\top \begin{pmatrix} \mathbf{R} & \mathbf{S}^\top \\ \mathbf{S} & \mathbf{Q} \end{pmatrix} \begin{pmatrix} I_{n_\eta} \\ \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \end{pmatrix} \preceq 0 \quad (8)$$

holds for all $\eta \in \mathcal{S} \subseteq \mathbb{R}^{n_\eta}$ with $\mathcal{S} \{ \eta \in \mathbb{R}^{n_\eta} : \mathbf{E}\eta \in \mathcal{V} \}$, see (Zoboli et al., 2024a, Section 2.5). The following result proposes a design for noninvasive linear dynamic output-feedback controllers based on matrix inequalities.

Proposition 1. *Consider (7a) with (7b) and let (8) hold for all $x \in \mathcal{F}$ with given matrices R, S, Q . Select $Z \preceq 0$ such that $Z \preceq R$ and assume there exist $\bar{R}_{11} = \bar{R}^\top$, $\hat{R}_{11} = \hat{R}_{11}^\top$, $\hat{R}_{12}, \hat{R}_{22} = \hat{R}_{22}^\top$, $\hat{S}_1, \hat{S}_2, \hat{Q} = \hat{Q}^\top$, scalars $\alpha > 0, \beta_0 \in \mathbb{R}, \beta_1 < 0$, symmetric matrices $\Pi_1 = \Pi_1^\top, \Pi_2 = \Pi_2^\top \in \mathbb{R}^{n_\xi \times n_\xi}$, matrices $\hat{K} \in \mathbb{R}^{n_u \times n_y}$, $\hat{L} \in \mathbb{R}^{n_u \times n_\xi}$, $\hat{M} \in \mathbb{R}^{n_\xi \times n_\xi}$, $\hat{N} \in \mathbb{R}^{n_\xi \times n_\xi}$, matrices $\Gamma_1, \Gamma_2, \Gamma_3$ and $\Sigma = \Sigma^\top \succ 0$ such that*

- i) The matrix $R_Z \begin{pmatrix} \bar{R} & \alpha \Pi_2 Z \\ \star & \alpha Z \end{pmatrix}$ is negative semidefinite;
- ii) Inequality (9)¹ holds with $\beta_0 + \beta_1 < 0$;
- iii) $(\Gamma_2) = (1, 0, 2n_\xi - 1)$.

Then, there exist square invertible matrices $U, V \in \mathbb{R}^{n_\xi \times n_\xi}$ such that $UV^\top = I_{n_\xi} - \Pi_1 \Pi_2$ and a scalar $\Delta^* > 0$ such that the control matrices

$$\begin{aligned} (K \ H) &= \hat{K}, \\ (N \ F) &= U^{-1}(\hat{N} - \Pi_1 B \hat{K}), \\ L &= (\hat{L} - \hat{K} C \Pi_2) V^{-\top}, \\ M &= U^{-1} \begin{pmatrix} I_{n_\xi} \\ -\Pi_1 \end{pmatrix}^\top \begin{pmatrix} \hat{M} & \hat{N} C \\ B \hat{L} - A + B \hat{K} C \end{pmatrix} \begin{pmatrix} I_{n_\xi} \\ -\Pi_2 \end{pmatrix} V^{-\top} \end{aligned} \quad (10)$$

ensure all trajectories of any perturbed closed loop

$$\dot{\eta} = \tilde{f}(\eta) = \mathbf{A}\eta + \mathbf{D}\phi(\mathbf{E}\eta) + \delta(\eta) \quad (11)$$

evolving in a forward-invariant bounded compact set $\mathcal{K} \subseteq \mathcal{S}$ with $\delta(\eta) = \text{col}(\delta_x(\eta), 0, 0)$, $\delta_x(\eta) \in \mathcal{C}^1$, $|\frac{\partial \delta_x}{\partial \eta}(\eta)| < \Delta^*$ for all $\eta \in \mathcal{K}$, converge to an equilibrium $\eta^* \in \mathcal{F}_\eta^*$ with

$$\mathcal{F}_\eta^* \{ \eta \in \mathcal{K} : Ax + D\phi(Ex) + \delta_x(x) = 0 \}. \quad (12)$$

The proof of Proposition 1 is presented in Section 6.1.

Controllers issued from Proposition 1 ensure convergence of the closed-loop trajectories to open-loop equilibria even in the presence of (sufficiently slow-varying) state-dependent uncertainties. This robust noninvasive behavior differs from the one in (Angeli et al., 2024), where the open-loop dynamics must be perfectly known, or the derivative of the state must be measurable. Moreover, while the matrices R, S, Q in (2) (and therefore $\mathbf{R}, \mathbf{S}, \mathbf{Q}$ in (8)) are assumed to be known, extensions of Proposition 1 to cases of unknown quadratic abstractions can be proposed by following the results in (Zoboli et al., 2024a, Section 2).

Nonetheless, Proposition 1 presents two main drawbacks. Firstly, it requires imposing matrix inertia constraints, see item iii). A detailed discussion on methods to impose such constraints in the optimization problem is presented in (Zoboli et al., 2024a, Section 3). Secondly, it requires closed-loop trajectories to evolve in a forward invariant bounded compact set \mathcal{K} . This necessity arises from the fact that the proposed result is grounded on the notion of 2-contraction, which guarantees convergence to nonunique equilibria if the system evolves in forward invariant bounded compact sets (Li and Muldowney, 1995, Theorem 2.5), (Cecilia et al., 2023, Lemma 6). Therefore, we now present an LMI-based approach allowing the *a-posteriori* verification of such a requirement.

Proposition 2. *Consider (7a) and let $\mathbf{A} = \mathbf{A}_s + \tilde{\mathbf{A}}$ with \mathbf{A}_s Hurwitz. Suppose there exist matrices $\mathbf{X} = \mathbf{X}^\top, \mathbf{Y}$,*

¹ Given at the top of the next page.

$$\begin{aligned}
& A_e \begin{pmatrix} A & 0 \\ 0 & 0 \end{pmatrix}, \quad B_e \begin{pmatrix} B \\ I_{n_u} \end{pmatrix}, \quad C_e \begin{pmatrix} C & 0 \\ 0 & I_{n_u} \end{pmatrix}, \quad D_e \begin{pmatrix} D \\ 0 \end{pmatrix}, \quad G_e \begin{pmatrix} G \\ 0 \end{pmatrix}, \quad \Phi \begin{pmatrix} \Pi_2 & I_{n_\xi} \\ I_{n_\xi} & \Pi_1 \end{pmatrix}, \\
& \hat{A} \begin{pmatrix} A_e \Pi_2 + B_e \hat{L} & A_e + B_e \hat{K} C_e \\ \hat{M} & \Pi_1 A_e + \hat{N} C_e \end{pmatrix}, \quad \hat{D} \begin{pmatrix} D_e + B_e \hat{K} G_e \\ \Pi_1 D_e + \hat{N} G_e \end{pmatrix}, \quad \hat{R} \begin{pmatrix} \hat{R}_{11} & \hat{R}_{12}^\top \\ \star & \hat{R}_{22} \end{pmatrix}, \quad \hat{S}^\top \begin{pmatrix} \hat{S}_1^\top \\ \hat{S}_2^\top \end{pmatrix}, \\
& \begin{pmatrix} \hat{R}_{11} - \bar{R} & \hat{R}_{12}^\top - \alpha \Pi_2 R^\top & \hat{S}_1^\top - \alpha \Pi_2 S^\top \\ \star & \hat{R}_{22} - \alpha R & \hat{S}_2^\top - \alpha S^\top \\ \star & \star & \hat{Q} - \alpha Q \end{pmatrix} + \text{He} \left\{ \begin{pmatrix} \Upsilon_1 \\ \Upsilon_2 \\ \Upsilon_3 \end{pmatrix} \begin{pmatrix} \frac{\partial \phi}{\partial x}(v) & 0 & -I_{n_x} \end{pmatrix} \right\} \preceq 0, \quad \forall v \in \mathcal{V}, \\
& \begin{pmatrix} \text{He} \left\{ A_e \Pi_2 + B_e \hat{L} \right\} - 2\beta_1 \Pi_2 - \hat{R}_{11} & A_e + B_e \hat{K} C_e + \hat{M}^\top - 2\beta_1 I_{n_\xi} - \hat{R}_{12}^\top & D_e + B_e \hat{K} G_e - \hat{S}_1^\top \\ \star & \text{He} \left\{ \Pi_1 A_e + \hat{N} C_e \right\} - 2\beta_1 \Pi_1 - \hat{R}_{22} & \Pi_1 D_e + \hat{N} G_e - \hat{S}_2^\top \\ \star & \star & -\hat{Q} \end{pmatrix} \prec 0, \\
& \begin{pmatrix} -2\beta_0 \Sigma + \text{He} \left\{ \Gamma_1 \hat{A} \right\} - \hat{R} & \Sigma - \Gamma_1 \Phi + \hat{A}^\top \Gamma_2^\top & \Gamma_1 \hat{D} + \hat{A}^\top \Gamma_3^\top - \hat{S}^\top \\ \star & -\text{He} \left\{ \Gamma_2 \Phi \right\} & \Gamma_2 \hat{D} - \Phi \Gamma_3^\top \\ \star & \star & \text{He} \left\{ \Gamma_3 \hat{D} \right\} - \hat{Q} \end{pmatrix} \prec 0.
\end{aligned} \tag{9}$$

$$\begin{pmatrix} \tau_1 P_{\mathcal{E}_1} - \tau_2 P_{\mathcal{E}_2} + \mathbf{A}_s^\top P_{\mathcal{E}_1} + P_{\mathcal{E}_1} \mathbf{A}_s - \mathbf{X} & P_{\mathcal{E}_1} - \mathbf{Y}^\top & 0 \\ \star & -\mathbf{Z} & 0 \\ \star & \star & -\tau_1 + \tau_2 \end{pmatrix} \prec 0. \tag{13}$$

$\mathbf{Z} = \mathbf{Z}^\top$, a set $\mathcal{S} \subseteq \mathbb{R}^{n_\eta}$ and a vector $\eta^\star \in \mathcal{S}$ such that the local sector condition

$$\begin{pmatrix} \eta - \eta^\star \\ \psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^\star) \end{pmatrix}^\top \begin{pmatrix} \mathbf{X} & \mathbf{Y}^\top \\ \mathbf{Y} & \mathbf{Z} \end{pmatrix} \begin{pmatrix} \eta - \eta^\star \\ \psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^\star) \end{pmatrix} \leq 0 \tag{14}$$

holds for all $\eta \in \mathcal{S}$, with $\psi(v)\mathbf{D}\phi(v) + \tilde{\mathbf{A}}\eta$. If there exist positive scalars τ_1, τ_2 , two matrices $P_{\mathcal{E}_1} \succeq P_{\mathcal{E}_2} \succ 0$ and a matrix $\Omega \in \mathbb{R}^{n_\eta \times n_u}$ such that (13)² holds and such that the ellipsoidal set $\mathcal{E}_2\{\eta \in \mathbb{R}^{n_\eta} : (\eta - \eta^\star)^\top P_{\mathcal{E}_2}(\eta - \eta^\star) \leq 1\} \subseteq \mathcal{S}$, then $\mathcal{E}_1\{\eta \in \mathbb{R}^{n_\eta} : (\eta - \eta^\star)^\top P_{\mathcal{E}_1}(\eta - \eta^\star) \leq 1\}$ is attractive and forward invariant for (7a) with region of attraction including the non-empty set $\tilde{\mathcal{E}}\mathcal{E}_2 \setminus \mathcal{E}_1$, for all $\eta \in \mathcal{S}$.

The proof of Proposition 2 is presented in Section 6.2.

Remark 1. Note that the loop transformation $\mathbf{A} = \mathbf{A}_s + \tilde{\mathbf{A}}$, $\psi(v)\mathbf{D}\phi(v) + \tilde{\mathbf{A}}\eta$ is a necessary step for the satisfaction of (13). Indeed, after the removal of the quadratic abstraction entry \mathbf{X} , the top-left entry of (13) requires

$$\tau_1 P_{\mathcal{E}_1} - \tau_2 P_{\mathcal{E}_2} + \mathbf{A}_s^\top P_{\mathcal{E}_1} + P_{\mathcal{E}_1} \mathbf{A}_s \prec 0.$$

Since $P_{\mathcal{E}_1} \succeq P_{\mathcal{E}_2}$ this implies

$$(\tau_1 - \tau_2)P_{\mathcal{E}_1} + \mathbf{A}_s^\top P_{\mathcal{E}_1} + P_{\mathcal{E}_1} \mathbf{A}_s \prec 0,$$

which requires \mathbf{A}_s Hurwitz, given that $\tau_1 > \tau_2$ from the bottom-right entry of (13). Moreover, since the pair (\mathbf{A}, \mathbf{D}) may not be controllable, the more classical loop transformation involving the addition and subtraction of a virtual stabilizing input $u_s = \mathbf{K}\eta$ and the definition of a reshaped nonlinearity $\psi(v) = \phi(v) - \mathbf{K}\eta$ may not be applicable. Thus, $\psi(v)$ must include \mathbf{D} in its definition.

While useful, the results of Proposition 2 present two main drawbacks. First, they require the knowledge of a nondifferential quadratic abstraction (14) for the *reshaped closed loop*. Second, they do not guarantee the outer ellipsoid $\mathcal{E}_2 \subseteq \mathcal{S}$. We first address the issues emerging from the loop transformation by proposing a result connecting quadratic abstractions on the original system to ones on the reshaped loop.

Lemma 1. Consider (7a) and suppose there exist matrices $X = X, Y, Z = Z$, a set $\mathcal{S} \subseteq \mathbb{R}^{n_\eta}$ and a vector $\eta^\star \in \mathcal{S}$ such that the local sector condition

$$\begin{pmatrix} \eta - \eta^\star \\ \phi(\mathbf{E}\eta) - \phi(\mathbf{E}\eta^\star) \end{pmatrix}^\top \begin{pmatrix} X & Y^\top \\ Y & Z \end{pmatrix} \begin{pmatrix} \eta - \eta^\star \\ \phi(\mathbf{E}\eta) - \phi(\mathbf{E}\eta^\star) \end{pmatrix} \leq 0 \tag{15}$$

holds for all $\eta \in \mathcal{S}$. If there exists a matrix $\Omega \in \mathbb{R}^{n_\eta \times n_u}$ such that

$$\begin{pmatrix} \mathbf{D}^\top \Omega + \Omega^\top \mathbf{D} & \Omega^\top \\ \star & I_{n_u} \end{pmatrix} \succ 0, \tag{16}$$

then $\mathbf{D}^\top \mathbf{D} \succ 0$ and (14) holds with

$$\begin{aligned}
\bar{\mathbf{D}} &= (\mathbf{D}^\top \mathbf{D})^{-1} \mathbf{D}^\top, \\
\mathbf{X} &= X - Y^\top \bar{\mathbf{D}} \tilde{\mathbf{A}} - \tilde{\mathbf{A}}^\top \bar{\mathbf{D}}^\top Y - \tilde{\mathbf{A}}^\top \bar{\mathbf{D}}^\top Z \bar{\mathbf{D}} \tilde{\mathbf{A}}, \\
\mathbf{Y} &= \bar{\mathbf{D}} Y + \bar{\mathbf{D}}^\top Z \bar{\mathbf{D}} \tilde{\mathbf{A}}, \\
\mathbf{Z} &= \bar{\mathbf{D}}^\top Z \bar{\mathbf{D}}.
\end{aligned} \tag{17}$$

The proof of Lemma 1 is presented in Section 6.3.

Lemma 1 allows translating quadratic abstractions for the original closed loop to abstractions for the transformed one. We highlight that constraint (16) can be dropped by assuming \mathbf{D} has full column rank.

While representing an important step in improving the applicability of Proposition 2, Lemma 1 requires knowledge of matrices X, Y, Z in (15) and it does not guarantee the outer ellipsoid $\mathcal{E}_2 \subseteq \mathcal{S}$. One possible workaround to

² Given at the top of the next page.

both issues is to exploit the knowledge of the differential abstraction (2) to derive a global incremental one. This is formalized in the following lemma.

Lemma 2. *If there exist matrices R_v, S_v, Q_v with $Q_v \succ 0$ such that $\phi : \mathbb{R}^{n_v} \rightarrow \mathbb{R}^{n_v}$ satisfies*

$$\left(\frac{\partial \phi}{\partial v}(v) \right)^\top \begin{pmatrix} R_v & S_v^\top \\ S_v & Q_v \end{pmatrix} \begin{pmatrix} I_{n_v} \\ \frac{\partial \phi}{\partial v}(v) \end{pmatrix} \preceq 0, \quad (18)$$

for all $v \in \mathbb{R}^{n_v}$, then

$$\begin{pmatrix} v_1 - v_2 \\ \phi(v_1) - \phi(v_2) \end{pmatrix}^\top \begin{pmatrix} R_v & S_v^\top \\ S_v & Q_v \end{pmatrix} \begin{pmatrix} v_1 - v_2 \\ \phi(v_1) - \phi(v_2) \end{pmatrix} \preceq 0, \quad (19)$$

holds for all $v_1, v_2 \in \mathbb{R}^{n_v}$.

The proof of Lemma 2 is presented in Section 6.4.

Given the relation $v = Ex = \mathbf{E}\eta$, Lemma 2 shows that one can select $X = \gamma \mathbf{R} = \gamma \mathbf{E}^\top R_v \mathbf{E}$, $Y = \gamma \mathbf{S} = \gamma \mathbf{E} S_v$ and $Z = \gamma \mathbf{Q} = \gamma Q_v$ in (13) for any $\gamma > 0$, see for instance (Zoboli et al., 2024a, Section 2.5). Indeed, since (19) holds for all v_1, v_2 , it holds also for $v_2 = \mathbf{E}\eta^*$ and obtain $\mathcal{S} = \mathbb{R}^{n_\eta}$ in Proposition 2, ensuring $\mathcal{E}_2 \subseteq \mathcal{S}$. Then, Lemma 1 allows mapping the obtained abstraction to (14). Given (20a), the requirement of $Q_v \succ 0$ does not restrict the set of solutions to the LMI, as the central block of (13) imposes the same constraint in the form $\mathbf{Z} \succ 0$.

Unfortunately, the exploitation of Lemma 2 is very conservative and still presents drawbacks. Importantly, (19) holds for any pair v_1, v_2 . As such, the resulting abstraction represents an incremental sector condition rather than a local one as per (14). Therefore, while holding also for the ellipsoid center η^* , it is not specific to such a point. This may lead to increased conservativeness and numerical problems since the resulting ellipsoids are not anchored to a specific point, i.e., they could be interpreted as incremental ones.

Given the above discussion, we argue that estimating the matrices $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ given a desired open-loop center x^* is a more reliable solution. This approach only requires minor knowledge of local sector bounds for the nonlinearity ϕ . Moreover, it allows including constraints guaranteeing \mathcal{E}_2 is included in the known local sector. We formalize the proposed technique in the following theorem.

Theorem 1. *Let $\Theta_1, \Theta_2 \in \mathbb{R}^{n_v \times n_v}$ be given diagonal matrices such that $\Theta_1 \preceq \Theta_2$. Assume there exist vectors $\underline{v}, \bar{v}, x^*$ such that $v^* = Ex^* \in [\underline{v}, \bar{v}]$ and*

$$(\phi(v) - \phi(v^*) - \Theta_1(v - v^*))_i (\phi(v) - \phi(v^*) - \Theta_2(v - v^*))_i \leq 0 \quad (21)$$

for all $i = 1, \dots, n_v$ and for all $v \in [\underline{v}, \bar{v}]$, where $(\cdot)_i$ represents the i^{th} element of the argument vector or the i^{th} row of the argument matrix. If there exist positive scalars τ_1, τ_2 , a matrix $\Omega \in \mathbb{R}^{n_\eta \times n_v}$, two matrices $P_{\mathcal{E}_1} \succeq P_{\mathcal{E}_2} \succ 0$, matrices Υ_i with $i = 1, \dots, 8$ and matrices $X_v = X_v^\top, Y_v, Z_v = Z_v^\top, \mathbf{X} = \mathbf{X}^\top, \mathbf{Y}, \mathbf{Z} = \mathbf{Z}^\top$ such that (13), (16) and (20) hold with $\bar{\mathbf{D}}$ as in (20a), then $\mathcal{E}_1\{\eta \in \mathbb{R}^{n_\eta} : (\eta - \eta^*)^\top P_{\mathcal{E}_1}(\eta - \eta^*) \leq 1\}$ is attractive and forward invariant for (7a) with region of attraction including the non-empty set $\tilde{\mathcal{E}}_2 \setminus \mathcal{E}_1$, with $\eta^* = \text{col}(x^*, 0, 0)$ and $\mathcal{E}_2\{\eta \in \mathbb{R}^{n_\eta} : (\eta - \eta^*)^\top P_{\mathcal{E}_2}(\eta - \eta^*) \leq 1\}$.

The proof of Theorem 1 is presented in Section 6.5.

Theorem 1 considers the abstraction matrices $\mathbf{X}, \mathbf{Y}, \mathbf{Z}, X_v, Y_v, Z_v$ as problem variables. To reduce the size of the optimization problem, one could select $\mathbf{X} = \hat{X}$, $\mathbf{Y} = \hat{Y}$ and $\mathbf{Z} = \hat{Z}$, thus removing (20c). However, the inclusion of (20c) leaves more degrees of freedom to the optimization problem, which can exploit entries in the directions of the integrator and controller states. Under the selection mentioned previously, these entries would be set to 0 by the structure of \mathbf{E} . We also highlight that (20b) is typically hard to solve. However, if we constrain the diagonal elements of Z_v to be nonpositive, it is sufficient to check the condition for all matrices Λ corresponding to the finitely many vertices of the matrix interval $[\Theta_1, \Theta_2]$ (Ebihara et al., 2021). This can be easily done by, e.g., decomposing $Z_v Z_d + \tilde{Z}^\top + \tilde{Z}$ with diagonal $Z_d \preceq 0$ and lower triangular \tilde{Z} .

Remark 2. *Since the differential quadratic abstraction (2) holds for all $v \in \mathcal{V}$ and given the degree of freedom arising from letting matrices X_v, Y_v, Z_v as decision variables, one can select \underline{v}, \bar{v} and compute Θ_1, Θ_2 for Theorem 1 such that the resulting polytope is included in \mathcal{V} . This choice connects the regions where 2-contractivity holds and the invariant ellipsoid is looked for.*

4. COMPARISON WITH THE LITERATURE

We highlight that alternative solutions to the considered stabilization problem can be found on the literature. Thus, we find it necessary to discuss the main differences between these results and the proposal of this work.

The main property that characterizes a noninvasive control is that the input signal is zero at steady-state. In this paper, we achieved this property through the noninvasive condition in (4). An alternative way for obtaining zero steady-state input is to design a feedback policy that uses the derivative of the state, that is $u = \alpha(\dot{x})$ with $\alpha(0) = 0$. This approach have been explored by some authors under the name of state-derivative feedback (Zaheer et al., 2021; Arthur and Yoon, 2019) and was generalized to its derivative-output version in (Zaheer et al., 2021; Arthur and Yoon, 2020). We highlight that these results only provide design conditions for linear systems or linearized systems around a unique equilibrium point. Thus, these approaches have very limited applicability to nonlinear systems with multiple uncertain equilibrium points or with initial conditions far from an equilibrium point.

Recently, the authors in (Angeli et al., 2024) applied 2-contraction theory for designing state-derivative controllers. 2-contraction enabled the development of non-local design conditions for multistable systems. A similar framework to the one proposed in (Angeli et al., 2024) can be recovered from (1) by selecting $C = A, G = D$ and the static control policy $u = Ky$. Nonetheless, the proposal in (Angeli et al., 2024) is not free of limitations. First, it requires a direct measurement of the derivative of the state or an exact knowledge of the system vector field. Second, the design conditions are based on mathematical objects known as matrix compounds (Bar-Shalom et al., 2023), which usually explode in dimension and may destroy advantageous structural properties of the system.

$$\begin{aligned}\hat{X} &= \mathbf{E}^\top X_v \mathbf{E} - \mathbf{E}^\top Y_v^\top \bar{\mathbf{D}} \tilde{\mathbf{A}} - \tilde{\mathbf{A}}^\top \bar{\mathbf{D}}^\top Y_v \mathbf{E} - \tilde{\mathbf{A}}^\top \bar{\mathbf{D}}^\top Z_v \bar{\mathbf{D}} \tilde{\mathbf{A}}, \\ \hat{Y} &= \bar{\mathbf{D}} Y + \bar{\mathbf{D}}^\top Z \bar{\mathbf{D}} \tilde{\mathbf{A}}, \\ \hat{Z} &= \bar{\mathbf{D}}^\top Z \bar{\mathbf{D}}.\end{aligned}\tag{20a}$$

$$\begin{pmatrix} \mathbf{I}_{n_v} \\ \Lambda \end{pmatrix}^\top \begin{pmatrix} X_v & Y_v^\top \\ Y_v & Z_v \end{pmatrix} \begin{pmatrix} \mathbf{I}_{n_v} \\ \Lambda \end{pmatrix} \preceq 0, \quad \forall \Lambda : \Theta_1 \preceq \Lambda \preceq \Theta_2\tag{20b}$$

$$\begin{pmatrix} 0 & 0 & 0 \\ 0 & \mathbf{X} - \hat{\mathbf{X}} & \mathbf{Y}^\top - \hat{\mathbf{Y}}^\top \\ 0 & \mathbf{Y} - \hat{\mathbf{Y}} & \mathbf{Z} - \hat{\mathbf{Z}} \end{pmatrix} + \text{He} \left\{ \begin{pmatrix} \Upsilon_1 \\ \Upsilon_2 \\ \Upsilon_3 \end{pmatrix} (\mathbf{I}_{n_\eta} - \mathbf{A} \mathbf{I}_{n_v}) \right\} \preceq 0\tag{20c}$$

$$\begin{pmatrix} P_{\mathcal{E}_2} & \mathbf{E}_i^\top \\ \mathbf{E}_i & (\bar{v} - \underline{v})_i^2 \end{pmatrix} \succeq 0, \quad i = 1, \dots, n_v.\tag{20d}$$

Our proposal can be understood as an extension of the washout filter discussed in (Garrard and Jordan, 1977; Wang and Abed, 1995; Hassouneh et al., 2004). Indeed, we achieve a zero steady-state input by designing the controller as a linear filter with a blocking zero in the origin. Thus, we do not require any measurement of the state or output derivative, and we can operate directly with the system output. Nevertheless, we remark that our approach is not free from tradeoffs. Indeed, the addition of input integrators does not allow any of the system's outputs to be regulated. From output regulation theory, the number of regulated outputs must be smaller than or equal to the number of inputs, see e.g. (Isidori et al., 2003). By adding integrator dynamics on all input signals, such a regulation limit is reached. We also stress that the addition of input-integrator dynamics may cause the loss of controllability properties. This is shown by the following simple example. Consider the planar linear time invariant system

$$\begin{aligned}\dot{x}_1 &= x_1 + u \\ \dot{x}_2 &= x_1\end{aligned}\tag{22}$$

with $x = \text{col}(x_1, x_2) \in \mathbb{R}^2$ and $u \in \mathbb{R}$. It can be easily verified that (22) is controllable. However, by adding the input-integrator dynamics, the resulting extended system

$$\begin{aligned}\dot{x}_1 &= x_1 + u \\ \dot{x}_2 &= x_1 \\ \dot{z} &= u,\end{aligned}$$

has a simply stable uncontrollable mode. However, the 2-contraction framework proposed in this paper only requires a generalized notion of stabilizability properties (Cecilia et al., 2023). We also highlight that, different from previous results with washout filter, the combination of 2-contraction (Cecilia et al., 2023) with the design conditions provided in (Zoboli et al., 2024a) provides for the first time LMI design conditions for the proposed stabilization problem which are:

- non-local (in the sense that the state can be initialized far from any equilibrium point);
- can be implemented in nonlinear systems with multiple equilibria;
- can be implemented just with the system output.

5. NUMERICAL SIMULATION

As an illustration of the proposed we consider a second order system of the form (1) with the following matrices

$$A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad D = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad C = E = [1 \ 0], \quad G = 1$$

and the following nonlinearity:

$$\phi(v) = \cos(v + \theta),$$

where $\theta \in \mathbb{R}$ is a constant unknown by the designer. For this particular system, defining x_1 and x_2 and $x = [x_1 \ x_2]^\top$, we have the following set of equilibrium points:

$$\mathcal{F}^* = \{x \in \mathbb{R}^2 \mid \cos(x_1 + \theta) = 0, \ x_2 = 0\}.$$

In the unforced case $u = 0$, the considered system can be understood as a frictionless pendulum with x_1 being the pendulum angle shifted by θ and x_2 is the angular velocity. Therefore, the set \mathcal{F}^* is not attractive and for any initial condition outside \mathcal{F}^* the system converges to a non-trivial limit cycle. With this in mind, the objective is to make the set \mathcal{F}^* attractive and invariant.

We highlight that the proposed stabilization problem can be trivially solved using the state-derivative feedback discussed in Section 4. Indeed, any feedback term of the form $u = -\kappa x_2$, with a sufficiently large $\kappa > 0$, would solve the considered stabilization problem, since at any equilibrium we have $x_2 = 0$. Nonetheless, we highlight that we have no direct measure of the states or its derivative, only of the signal $y = x_1 + \cos(x_1 + \theta)$. Thus, the state derivative feedback methodology cannot be directly implemented. Naturally, one could try to design an observer for the system and then use the estimation of the second state, denoted \hat{x}_2 , as the state derivative feedback, that is $u = -\kappa \hat{x}_2$. Nonetheless, the design of such an observer is not trivial due to the unknown constant θ . If one tries to, somehow, design an observer robust to the unknown parameter θ , it will significantly increase the noise sensitivity of the feedback policy. Additionally, the extended system:

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= \cos(x_2 + x_3) + u \\ \dot{x}_3 &= 0 \\ y &= x_1 + \cos(x_1 + x_3)\end{aligned}$$

is not observable at any equilibrium point with $u = 0$, since we have $\dot{y} = 0$ and $y = x_1 + \cos(x_1 + x_3) = x_1 + \cos(x_1 + nx_3)$ for any positive and odd integer n . Thus, the design of an observer that jointly estimates the states x and the unknown parameter θ is not a trivial task if we impose a zero steady-state input. Considering these difficulties, the

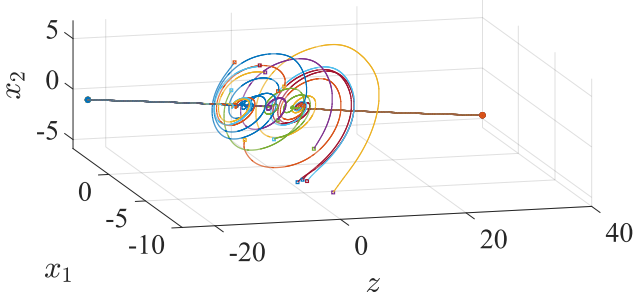


Fig. 1. Constant theta case, closed loop

purpose of this section is to show how the problem can be directly solved with the framework proposed in this work.

Controller:

$$\begin{aligned} M &= 0.29 & -2.041.45 \\ -2.04 - 3.34 & & -0.97 \\ 1.45 - 0.97 & 1.23, N & = -13.91 - 0.17 \\ -3.45 - 1.42 & & \\ 10.52 - 4.3, & & \\ K &= -3.77 & -4.38, L & = -16.02 - 0.68 & -13.8, \end{aligned}$$

6. PROOFS

6.1 Proof of Proposition 1

Note that the extended matrices A_e, B_e, C_e, D_e, G_e in (9) describe the (x, z) -dynamics in (5). Therefore, by (Zoboli et al., 2024a, Theorem 2) adapted with the result on known quadratic abstraction of (Zoboli et al., 2024a, Corollary 2), the matrix inequalities in (9) paired with items i)-iii) of Proposition 1 guarantee $(\Sigma_1) = (1, 0, 2n_\eta - 1)$ and

$$\begin{cases} \left(\mathbf{A} + \mathbf{D} \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \right)^\top P_0 + P_0 \left(\mathbf{A} + \mathbf{D} \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \right) \prec 2\mu_0 P_0, \\ \left(\mathbf{A} + \mathbf{D} \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \right)^\top P_1 + P_1 \left(\mathbf{A} + \mathbf{D} \frac{\partial \phi}{\partial \eta}(\mathbf{E}\eta) \right) \prec 2\mu_1 P_1, \\ \mu_0 + \mu_1 < 0 \end{cases} \quad (23)$$

for all $\eta \in \mathcal{K}$ with $P_0 = \Sigma_0, P_1 = \Sigma_1, \beta_0 = \mu_0, \beta_1 = \mu_1$. Since \mathcal{K} is bounded and compact, there exist strictly positive scalars $\varepsilon_0, \varepsilon_1$ such that

$$\begin{cases} \frac{\partial f}{\partial \eta}(\eta)^\top P_0 + P_0 \frac{\partial f}{\partial \eta}(\eta) \preceq 2\mu_0 P_0 - \varepsilon_0 \mathbf{I}_{n_\eta}, \\ \frac{\partial f}{\partial \eta}(\eta)^\top P_1 + P_1 \frac{\partial f}{\partial \eta}(\eta) \preceq 2\mu_1 P_1 - \varepsilon_1 \mathbf{I}_{n_\eta}, \\ \mu_0 + \mu_1 < 0. \end{cases}$$

Note that $|\frac{\partial \delta}{\partial \eta}(\eta)| = |\frac{\partial \delta_x}{\partial \eta}(\eta)|$ for all $\eta \in \mathcal{K}$. By (Zoboli et al., 2024a, Lemma 8) and the relative proof, there exist strictly positive γ_0, γ_1 small enough and $\Delta_0^* \in (0, \varepsilon_0 \gamma_0), \Delta_1^* \in (0, \varepsilon_1 \gamma_1)$ such that

$$\begin{cases} \frac{\partial \tilde{f}}{\partial \eta}(\eta)^\top P_0 + P_0 \frac{\partial \tilde{f}}{\partial \eta}(\eta) \prec 2\bar{\mu}_0 P_0, \\ \frac{\partial \tilde{f}}{\partial \eta}(\eta)^\top P_1 + P_1 \frac{\partial \tilde{f}}{\partial \eta}(\eta) \prec 2\bar{\mu}_1 P_1, \end{cases}$$

with $\bar{\mu}_0 = \mu_0 + \frac{\gamma_0}{2}, \bar{\mu}_1 = \mu_1 + \frac{\gamma_1}{2}$. Let such upperbounds on γ_0, γ_1 be denoted by $\bar{\gamma}_0, \bar{\gamma}_1$. Since $\mu_0 + \mu_1 < 0$, by

continuity there exists $\bar{\gamma} > 0$ such that $\mu_0 + \mu_1 + \bar{\gamma} < 0$. By selecting $\gamma_0 = \gamma_1 = \min(\bar{\gamma}_0, \bar{\gamma}_1, \bar{\gamma})$ and $\Delta^* < \min(\varepsilon_0 \gamma, \varepsilon_1 \gamma)$ we obtain

$$\begin{cases} \frac{\partial \tilde{f}}{\partial \eta}(\eta)^\top P_0 + P_0 \frac{\partial \tilde{f}}{\partial \eta}(\eta) \prec 2\bar{\mu}_0 P_0, \\ \frac{\partial \tilde{f}}{\partial \eta}(\eta)^\top P_1 + P_1 \frac{\partial \tilde{f}}{\partial \eta}(\eta) \prec 2\bar{\mu}_1 P_1, \\ \bar{\mu}_0 + \bar{\mu}_1 < 0. \end{cases}$$

Consequently, (Cecilia et al., 2023, Theorem 5) proves 2-contractivity of the closed loop (11) and (Li and Muldowney, 1995, Theorem 2.5) paired with boundedness and forward-invariance of \mathcal{K} guarantees the trajectories of (7a) converge to a (possibly nonunique) equilibrium point. The result is proven by noting that all equilibria of (11) satisfy $0 = (KC \ H \ L) \eta + KG\phi(\mathbf{E}\eta) = u$.

6.2 Proof of Proposition 2

Let $\tilde{\eta} \eta - \eta^*, \tilde{\phi} \phi(\mathbf{E}\eta) - \phi(\mathbf{E}\eta^*)$ and $\tilde{\psi} \psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^*) = \mathbf{D}\tilde{\phi} + \tilde{\mathbf{A}}\tilde{\eta}$. According to the dynamics (7a) and the relation $\mathbf{A} = \mathbf{A}_s + \tilde{\mathbf{A}}$, we have

$$\dot{\tilde{\eta}} = \mathbf{A}_s \tilde{\eta} + \tilde{\psi}.$$

If (14) holds for all $\eta \in \mathcal{S}$, right and left multiplication of (13) by $\nu = \text{col}(\tilde{\eta}, \tilde{\psi})$ and its transpose implies

$$\nu^\top \begin{pmatrix} \tau_1 P_{\mathcal{E}_1} - \tau_2 P_{\mathcal{E}_2} + \text{He}\{P_{\mathcal{E}_1} \mathbf{A}\} & P_{\mathcal{E}_1} & 0 \\ & P_{\mathcal{E}_1} & 0 \\ 0 & 0 & -\tau_1 + \tau_2 \end{pmatrix} \nu \prec 0.$$

By expanding the product, we have

$$\begin{aligned} & \text{He}\{\tilde{\eta}^\top P_{\mathcal{E}_1} (\mathbf{A}_s \tilde{\eta} + \tilde{\psi})\} \\ & + \tau_1 (\tilde{\eta}^\top P_{\mathcal{E}_1} \tilde{\eta} - 1) + \tau_2 (1 - \tilde{\eta}^\top P_{\mathcal{E}_2} \tilde{\eta}) < 0. \end{aligned}$$

Therefore, by (7a) we have

$$\text{He}\{\tilde{\eta}^\top P_{\mathcal{E}_1} \tilde{\eta}\} + \tau_1 (\eta^\top P_{\mathcal{E}_1} \eta - 1) - \tau_2 (\eta^\top P_{\mathcal{E}_2} \eta - 1) \leq 0,$$

for all $\eta \in \mathcal{S}$. Since τ_1, τ_2 are positive, if $\mathcal{E}_2 \subseteq \mathcal{S}$ the above inequality implies

$$\tilde{\eta}^\top P_{\mathcal{E}_1} \tilde{\eta} + \tilde{\eta}^\top P_{\mathcal{E}_1} \dot{\tilde{\eta}} < 0, \quad (24)$$

for all $\eta \in \tilde{\mathcal{E}}$. Note that the constraint $P_{\mathcal{E}_1} \succeq P_{\mathcal{E}_2}$ ensures $\tilde{\mathcal{E}}$ is not empty. Indeed, it implies

$$\tilde{\eta}^\top P_{\mathcal{E}_1} \tilde{\eta} \geq \tilde{\eta}^\top P_{\mathcal{E}_2} \tilde{\eta}$$

and therefore $\mathcal{E}_1 \subseteq \mathcal{E}_2$. Consequently, $\tilde{\mathcal{E}}$ contains at least the boundary of \mathcal{E}_1 and thus it is not empty.

Consider now the function $V(\eta) = \tilde{\eta}^\top P_{\mathcal{E}_1} \tilde{\eta}$. Given (24), for all $\eta \in \tilde{\mathcal{E}}$ we have $\dot{V}(\eta) < 0$. Therefore, all trajectories starting in $\tilde{\mathcal{E}}$ converge to \mathcal{E}_1 , thus proving its attractiveness and forward-invariance.

6.3 Proof of Lemma 1

If (16) holds, a Schur complement on the bottom-right entry provides

$$\mathbf{D}^\top \Omega + \Omega^\top \mathbf{D} - \Omega^\top \Omega \succ 0.$$

By adding and subtracting $\mathbf{D}^\top \mathbf{D}$, we obtain

$$\mathbf{D}^\top \mathbf{D} \succ (\Omega - \mathbf{D})^\top (\Omega - \mathbf{D}).$$

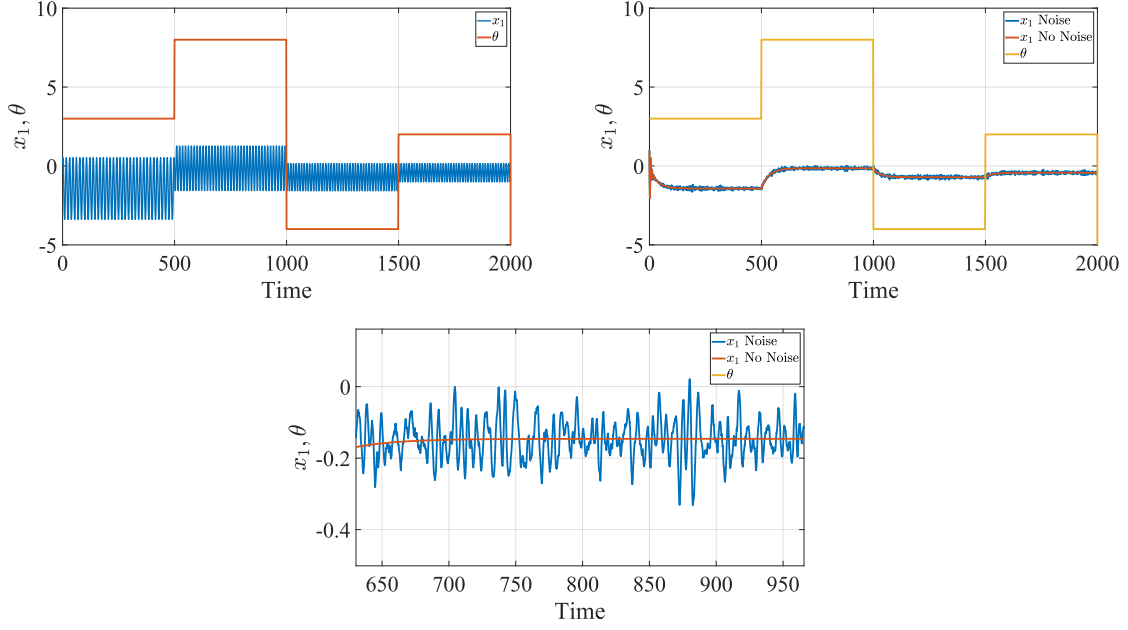


Fig. 2. Open-loop and closed-loop with no noise and noise (variance 0.05.)

Therefore, since $(\Omega - \mathbf{D})^\top (\Omega - \mathbf{D}) \succeq 0$, $\mathbf{D}^\top \mathbf{D} \succ 0$. Let $\tilde{\eta}\eta - \eta^*$, $\tilde{\phi}\phi(\mathbf{E}\eta) - \phi(\mathbf{E}\eta^*)$ and $\tilde{\psi}\psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^*) = \mathbf{D}\tilde{\phi} + \tilde{\mathbf{A}}\tilde{\eta}$. Since $\mathbf{D}^\top \mathbf{D}$ is invertible, we have

$$\begin{aligned} \mathbf{D}^\top \tilde{\psi} &= \mathbf{D}^\top \mathbf{D}\tilde{\phi} + \mathbf{D}^\top \tilde{\mathbf{A}}\tilde{\eta} \\ (\mathbf{D}^\top \mathbf{D})^{-1} \mathbf{D}^\top (\tilde{\psi} - \tilde{\mathbf{A}}\tilde{\eta}) &= \tilde{\phi} \\ \bar{\mathbf{D}}(\tilde{\psi} - \tilde{\mathbf{A}}\tilde{\eta}) &= \tilde{\phi} \end{aligned}$$

If (15) holds, the result is proven by substituting the above relation in (15) and collecting the terms in $\tilde{\eta}$ and $\tilde{\psi}$.

6.4 Proof of Lemma 2

Left and right multiplication of (18) by $\tilde{v}v_1 - v_2$ and expansion of the product yields

$$\tilde{v}^\top R_v \tilde{v} + 2\tilde{v}^\top S_v^\top \frac{\partial \phi}{\partial v}(v) \tilde{v} + \tilde{v}^\top \frac{\partial \phi}{\partial v}(v)^\top Q_v \frac{\partial \phi}{\partial v}(v) \tilde{v} \leq 0.$$

Since $Q \succ 0$, by Schur complement we obtain

$$\begin{pmatrix} \tilde{v}^\top R_v \tilde{v} + 2\tilde{v}^\top S_v^\top \frac{\partial \phi}{\partial v}(v) \tilde{v} & \tilde{v}^\top \frac{\partial \phi}{\partial v}(v)^\top \\ \frac{\partial \phi}{\partial v}(v) \tilde{v} & -Q_v^{-1} \end{pmatrix} \leq 0, \quad (25)$$

for all $v, \tilde{v} \in \mathbb{R}^{n_v}$. Consider now the function $F : [0, 1] \rightarrow \mathbb{R}^{n_v}$ defined as

$$F(s)\phi(v_2 + s(v_1 - v_2)) = \phi(v_2 + s\tilde{v}).$$

By the fundamental theorem of calculus, we have

$$F(1) - F(0) = \phi(v_1) - \phi(v_2) = \int_0^1 \frac{\partial \phi}{\partial s}(v_2 + s\tilde{v}) ds \tilde{v}.$$

Since (25) holds for all $v \in \mathbb{R}^{n_v}$, selecting $v = v_2 - s\tilde{v}$ and integrating over s yields

$$\begin{pmatrix} \tilde{v}^\top R_v \tilde{v} + 2\tilde{v}^\top S_v^\top (\phi(v_1) - \phi(v_2)) & (\phi(v_1) - \phi(v_2))^\top \\ (\phi(v_1) - \phi(v_2)) & -Q_v^{-1} \end{pmatrix} \leq 0.$$

The proof is concluded with by Schur complement on the bottom-right entry of the above matrix and by collecting the vectors $\text{col}(\tilde{v}, \phi(v_1) - \phi(v_2))$ and its transpose.

6.5 Proof of Theorem 1

By Proposition 2, the result is proven if (21), (16) and (20) imply the local abstraction (14) for $\eta^* = \text{col}(x^*, 0, 0)$ and $\mathcal{E}_2 \subseteq \mathcal{S}$ with $\mathcal{S}\{\eta \in \mathbb{R}^{n_\eta} : \mathbf{E}\eta \in [\underline{v}, \bar{v}]\}$. Consider (21) first and define $\tilde{v} = v - v^* = E(x - x^*) = E\tilde{x}$ and $\tilde{\phi} = \phi(v) - \phi(v^*)$. By (de Souza et al., 2023, Lemma 2), inequality (21) implies

$$\begin{pmatrix} \tilde{v} \\ \tilde{\phi} \end{pmatrix}^\top \begin{pmatrix} X_v & Y_v^\top \\ Y_v & Z_v \end{pmatrix} \begin{pmatrix} \tilde{v} \\ \tilde{\phi} \end{pmatrix} \leq 0 \quad (26)$$

for all $v \in [\underline{v}, \bar{v}]$ and all X_v, Y_v, Z_v such that (20b) holds. Since $\tilde{v} = \mathbf{E}\tilde{\eta}$ and $\tilde{\phi} = \phi(\mathbf{E}\eta) - \phi(\mathbf{E}\eta^*)$, (26) implies

$$\begin{pmatrix} \tilde{\eta} \\ \tilde{\phi} \end{pmatrix}^\top \begin{pmatrix} \mathbf{E}^\top X_v \mathbf{E} & \mathbf{E}^\top Y_v^\top \\ Y_v \mathbf{E} & Z_v \end{pmatrix} \begin{pmatrix} \tilde{\eta} \\ \tilde{\phi} \end{pmatrix} \leq 0 \quad (27)$$

for all $\eta \in \mathcal{S}$ and all X_v, Y_v, Z_v such that (20b) holds. Therefore, by Lemma 1 with $X = \mathbf{E}^\top X_v \mathbf{E}$, $Y = Y_v \mathbf{E}$ and $Z = Z_v$ we have

$$\begin{pmatrix} \eta - \eta^* \\ \psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^*) \end{pmatrix}^\top \begin{pmatrix} \hat{X} & \hat{Y}^\top \\ \hat{Y} & \hat{Z} \end{pmatrix} \begin{pmatrix} \eta - \eta^* \\ \psi(\mathbf{E}\eta) - \psi(\mathbf{E}\eta^*) \end{pmatrix} \leq 0, \quad (28)$$

for all $\eta \in \mathcal{S}$. Consider now (20c). Right and left multiplication of by $\nu = \text{col}(\tilde{\eta}, \tilde{\eta}, \tilde{\psi})$ and its transpose yields

$$\begin{pmatrix} \tilde{\eta} \\ \tilde{\psi} \end{pmatrix}^\top \begin{pmatrix} \mathbf{X} & \mathbf{Y}^\top \\ \mathbf{Y} & \mathbf{Z} \end{pmatrix} \begin{pmatrix} \tilde{\eta} \\ \tilde{\psi} \end{pmatrix} \leq \begin{pmatrix} \tilde{\eta} \\ \tilde{\psi} \end{pmatrix}^\top \begin{pmatrix} \hat{X} & \hat{Y}^\top \\ \hat{Y} & \hat{Z} \end{pmatrix} \begin{pmatrix} \tilde{\eta} \\ \tilde{\psi} \end{pmatrix} \leq 0,$$

for all $\eta \in \mathcal{S}$. Therefore, (26) implies the local abstraction (14) holds for all $\eta \in \mathcal{S}$.

Consider now (20d). Note that $\eta \in \mathcal{S}$ if $|\mathbf{E}\eta - \mathbf{E}\eta^*|_i \leq |\bar{v} - \underline{v}|_i$ for all vector entries $i = 1, \dots, n_v$. A Schur complement on the bottom-right block of (20d) yields

$$P_{\mathcal{E}_2} \succeq \frac{1}{(\bar{v} - \underline{v})_i^\top (\bar{v} - \underline{v})_i} \mathbf{E}_i^\top \mathbf{E}_i$$

and in turn

$$\tilde{\eta}^\top P_{\mathcal{E}_2} \tilde{\eta}^\top \geq \frac{1}{(\bar{v} - \underline{v})^\top (\bar{v} - \underline{v})} \tilde{\eta}^\top \mathbf{E}_i^\top \mathbf{E}_i \tilde{\eta}^\top.$$

Consequently, if $\eta \in \mathcal{E}_2$,

$$(\bar{v} - \underline{v})_i^\top (\bar{v} - \underline{v})_i \geq \tilde{\eta}^\top \mathbf{E}_i^\top \mathbf{E}_i \tilde{\eta}^\top$$

and thus $\eta \in \mathcal{S}$. Therefore $\mathcal{E}_2 \subseteq \mathcal{S}$ and this concludes the proof.

7. CONCLUSIONS

Future work will also explore discrete-time extensions, building on the recent studies (Zoboli and Cecilia, 2024).

REFERENCES

- Angeli, D., Martini, D., Innocenti, G., and Tesi, A. (2024). Removing chaos while preserving equilibria by means of 2-contraction. *IFAC-PapersOnLine*, 58(5), 152–157. 7th IFAC Conference on Analysis and Control of Nonlinear Dynamics and Chaos ACNDC 2024.
- Arthur, K.M. and Yoon, S.Y. (2019). Robust derivative feedback control for systems with uncertain equilibrium states. In *2019 IEEE 58th Conference on Decision and Control (CDC)*, 5793–5798.
- Arthur, K.M. and Yoon, S.Y. (2020). Robust stabilization at uncertain equilibrium by output derivative feedback control. *ISA Transactions*, 107, 40–51.
- Astolfi, D. and Praly, L. (2017). Integral action in output feedback for multi-input multi-output nonlinear systems. *IEEE Transactions on Automatic Control*, 62(4), 1559–1574.
- Bar-Shalom, E., Dalin, O., and Margaliot, M. (2023). Compound matrices in systems and control theory: a tutorial. *Mathematics of Control, Signals, and Systems*, 1–55.
- Cecilia, A., Zoboli, S., Astolfi, D., Serres, U., and Andrieu, V. (2023). Generalized lyapunov conditions for k-contraction: analysis and feedback design. *Submitted to IEEE Transaction on Automatic Control*, HAL preprint hal-04300588.
- de Souza, C., Girard, A., and Tarbouriech, S. (2023). Event-triggered neural network control using quadratic constraints for perturbed systems. *Automatica*, 157, 111237.
- Ebihara, Y., Waki, H., Magron, V., Mai, N.H.A., Peaucelle, D., and Tarbouriech, S. (2021). Stability analysis of recurrent neural networks by iqc with copositive multipliers. In *2021 60th IEEE Conference on Decision and Control (CDC)*, 5098–5103. IEEE.
- Garrard, W.L. and Jordan, J.M. (1977). Design of nonlinear automatic flight control systems. *Automatica*, 13(5), 497–505.
- Giacagli, M., Andrieu, V., Tarbouriech, S., and Astolfi, D. (2023). LMI conditions for contraction, integral action, and output feedback stabilization for a class of nonlinear systems. *Automatica*, 154, 111106.
- Hassouneh, M., Lee, H.C., and Abed, E. (2004). Washout filters in feedback control: benefits, limitations and extensions. In *Proceedings of the 2004 American Control Conference*, volume 5, 3950–3955 vol.5.
- Isidori, A. (2017). Stabilization of nonlinear systems via state feedback. *Lectures in Feedback Design for Multivariable Systems*, 167–199.
- Isidori, A., Marconi, L., and Serrani, A. (2003). *Robust autonomous guidance: an internal model approach*. Springer Science & Business Media.
- Li, M.Y. and Muldowney, J.S. (1995). On R.A. Smith’s Autonomous Convergence Theorem. *Rocky Mountain Journal of Mathematics*, 25(1), 365 – 378.
- Muldowney, J. (1990). Compound matrices and ordinary differential equations. *Rocky Mountain Journal of Mathematics*, 20(4), 857–872.
- Shiriaev, A.S. and Fradkov, A.L. (2000). Stabilization of invariant sets for nonlinear non-affine systems. *Automatica*, 36(11), 1709–1715.
- Wang, H.O. and Abed, E.H. (1995). Bifurcation control of a chaotic system. *Automatica*, 31(9), 1213–1226.
- Zaheer, M.H., Arthur, K.M., and Yoon, S.Y.P. (2021). Derivative feedback control of nonlinear systems with uncertain equilibrium states and actuator constraints. *Automatica*, 127, 109495.
- Zoboli, S. and Cecilia, A. (2024). k-contraction analysis for discrete-time systems. In *4th IFAC Conference of Modelling, Identification and Control of Nonlinear Systems*.
- Zoboli, S., Cecilia, A., and Tarbouriech, S. (2024a). Dynamic output-feedback design for generalized lyapunov inequalities. *Submitted to Automatica*, HAL preprint: hal-04738534.
- Zoboli, S., Cecilia, A., and Tarbouriech, S. (2024b). Quadratic abstractions for k-contraction. In *To appear in 63rd Conference on Decision and Control*. HAL preprint hal-04619425.