Principles of Classical and Modern Radar Systems "Monostatic Pulse Radar for Complex Targets"

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1 Task 1-Phase Shifters

The phase shifter vector and the associate transmitter(Tx) and receiver(Rx) manifolds are computed using the following equations:

$$\underline{\psi} = \frac{2 \cdot \pi}{\lambda} \cdot \underline{r}_x \cdot \cos(\theta) \tag{1}$$

$$\underline{Tx}_{manifold} = exp(i \cdot \psi) \tag{2}$$

$$\underline{Rx}_{manifold} = exp(-i \cdot \psi) \tag{3}$$

The phase shifter vectors for the steering angles 40°,70°, and 120° are shown below in Table 1.

| 40° | 70° | 120° |
|-----------------------|----------|----------|
| 206.4640 | 85.6002 | 180.0000 |
| 344.3520 | 147.1639 | 90.0000 |
| 122.2400 | 208.7275 | 360.0000 |
| 260.1280 | 270.2911 | 270.0000 |
| 38.0160 | 331.8547 | 180.0000 |
| $\overline{175.9040}$ | 33.4184 | 90.0000 |
| 313.7920 | 94.9820 | 360.0000 |
| 91.6800 | 156.5456 | 270.0000 |
| 229.5680 | 218.1092 | 180.0000 |
| 7.4560 | 279.6729 | 90.0000 |
| 145.3440 | 341.2365 | 360.0000 |
| 283.2320 | 42.8001 | 270.0000 |
| 61.1200 | 104.3637 | 180.0000 |
| 199.0080 | 165.9274 | 90.0000 |
| 336.8960 | 227.4910 | 360.0000 |
| 114.7840 | 289.0546 | 270.0000 |
| 252.6720 | 350.6182 | 180.0000 |
| 30.5600 | 52.1819 | 90.0000 |
| 168.4480 | 113.7455 | 360.0000 |
| 306.3360 | 175.3091 | 270.0000 |
| 84.2240 | 236.8727 | 180.0000 |
| 222.1120 | 298.4364 | 90.0000 |
| 0.0000 | 0.0000 | 0.0000 |
| 137.8880 | 61.5636 | 270.0000 |
| 275.7760 | 123.1273 | 180.0000 |
| 53.6640 | 184.6909 | 90.0000 |
| 191.5520 | 246.2545 | 0.0000 |
| 329.4400 | 307.8181 | 270.0000 |
| 107.3280 | 9.3818 | 180.0000 |
| 245.2160 | 70.9454 | 90.0000 |
| 23.1040 | 132.5090 | 0.0000 |
| 160.9920 | 194.0726 | 270.0000 |
| 298.8800 | 255.6363 | 180.0000 |
| 76.7680 | 317.1999 | 90.0000 |
| 214.6560 | 18.7635 | 0.0000 |
| 352.5440 | 80.3271 | 270.0000 |
| 130.4320 | 141.8908 | 180.0000 |
| 268.3200 | 203.4544 | 90.0000 |
| 46.2080 | 265.0180 | 0.0000 |
| 184.0960 | 326.5816 | 270.0000 |
| 321.9840 | 28.1453 | 180.0000 |
| 99.8720 | 89.7089 | 90.0000 |
| 237.7600 | 151.2725 | 0.0000 |
| 15.6480 | 212.8361 | 270.0000 |
| 153.5360 | 274.3998 | 180.0000 |
| | | |

Table 1: Phase shifter vector in degrees $\overset{2}{2}$

The array pattern for the steering angles 40°,70°, and 120° are plotted below.

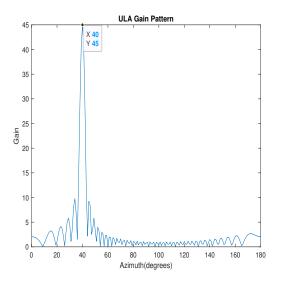


Fig. 1: Linear pattern plot for 40°

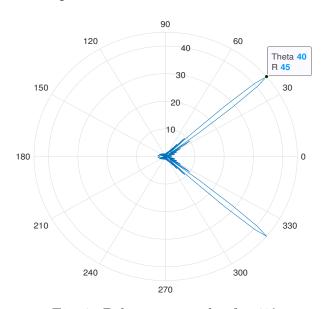


Fig. 2: Polar pattern plot for 40°

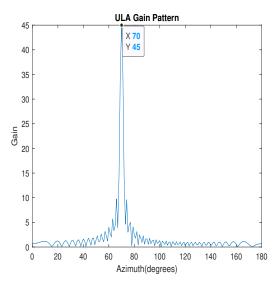


Fig. 3: Linear pattern plot for 70°

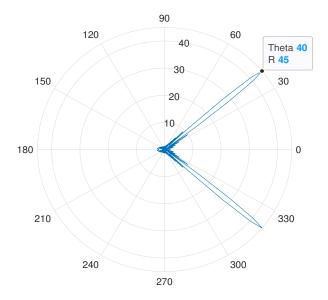
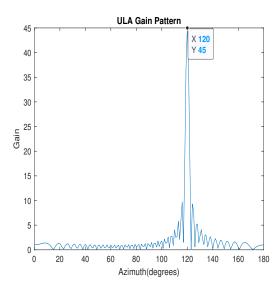


Fig. 4: Polar pattern plot for 70°



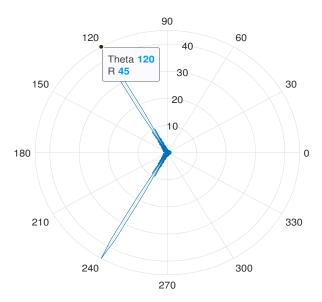


Fig. 5: Linear pattern plot for 120°

Fig. 6: Polar pattern plot for 120°

2 Task 2-Backscatter Modelling Function

The backscatter modelling function is provided in the submitted MATLAB files and follows the diagram shown in Figure 7.

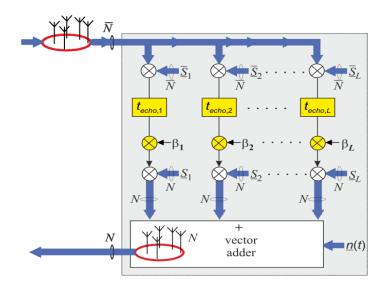


Fig. 7: Backscatter function diagram

3 Task 3-First Scan-No Targets

The noise samples at the baseband Rx ports are generated with the noise power defined in the following equation:

$$P_{noise} = k_B \cdot T_o * F_n * B \tag{4}$$

where:

- $k_B = 1.28 \cdot 10^{-3} \ m^2 \ kg \ s^{-2} \ K^{-1}$
- $T_o = 290$ °K
- $F_n = 3.1068$
- $B = \frac{1}{Tc} = 3.5714 \cdot 10^7 \text{ Hz}$

The noise power is thus equal to $P_n = 4.1187 \times 10^{-13}$.

The magnitude of the noise snapshots at point Z for one Dwell-time is plotted in Figure 8.

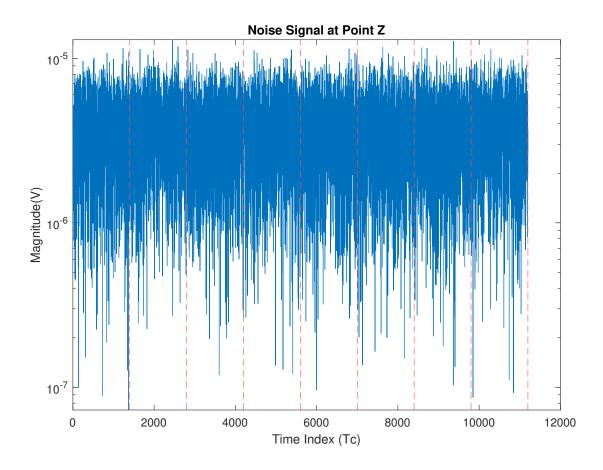


Fig. 8: Magnitude of noise samples at point Z

The power of the noise signal at point Z is estimated using the equation $P_{n,est} = \frac{1}{L} \cdot \underline{n}(t) \times \underline{n}^H(t)$ and is found equal to $P_{n,est} = 1.8842 \times 10^{-11}$. The magnitudes of the noise samples follow a Rayleigh distribution. This is confirmed by plotting the a theoretical Rayleigh Probability Density Function(PDF) with the estimated noise power as its parameter. The samples' histogram and the theoretical distribution are illustrated in Figure 9.

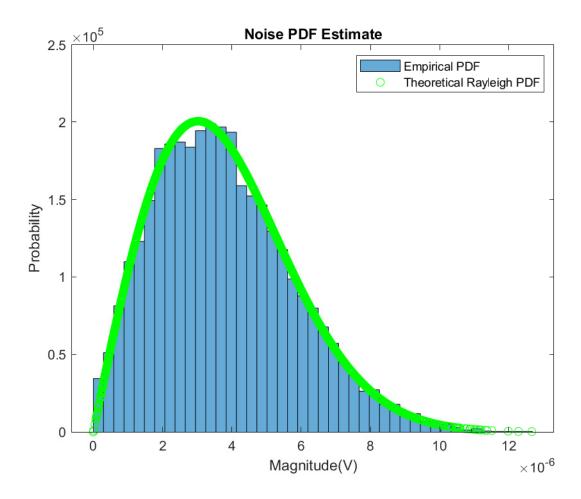


Fig. 9: Histogram of noise samples and Rayleigh PDF

The transmission of a pure noise signal allows us to determine a threshold value using the probability of false alarm, which is specified as $P_{FA} = 10^{-3}$. Because of the randomness of noise samples, the threshold varies between 2×10^{-6} V and 9×10^{-6} V.

4 Task 4-Second Scan-One Target

According to the brief, the radar searches for targets in the range between 30° and 150°. An angle sweep in this range is thus performed. For each angle, the maximum of the received signal at point Z is found. The resultant vector is plotted in Figure 10.

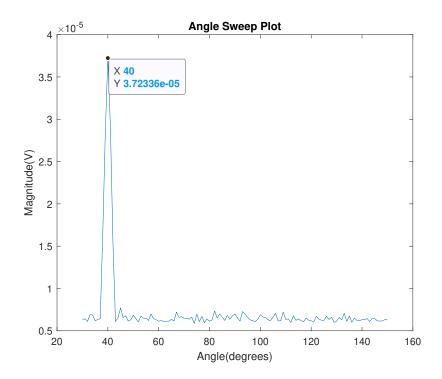


Fig. 10: Sweep for second scan

It can be concluded from this plot that there is a target present in the direction $\theta = 40^{\circ}$. The received signal for this angle is plotted in Figure 11.

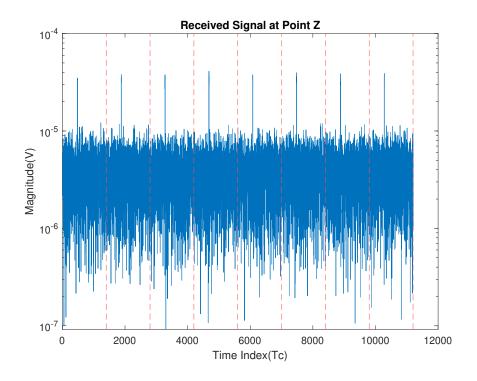


Fig. 11: Signal at point Z at angle 40°

Figure 12 shows the signal following matched filtering.

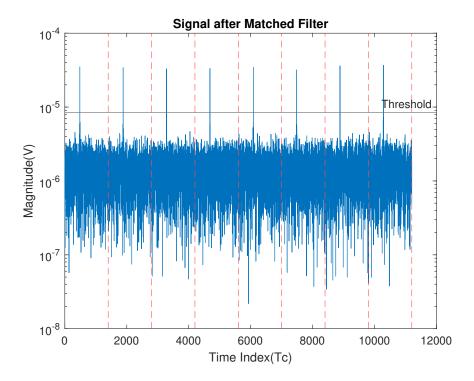


Fig. 12: Target 1 signal after matched filtering

The matched filter boosts the output signal's Signal-to-Noise Ratio (SNR) by reducing the effect of noise. Assuming only knowledge of the received signal at point Z, the parameters of target 1 are estimated. Given that $Tc = 28 \times 10^{-9}$, the range resolution is computed as $\Delta_R = \frac{cT_c}{2} = 4.2$ m. After matched filtering, a threshold in the range discussed in Section 3 is applied and the average of the signal across the 8 PRIs is found and plotted in Figure 13.

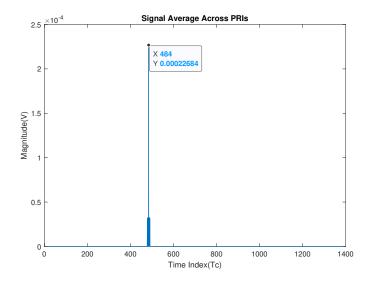


Fig. 13: Signal at 40° angle after matched filtering and thresholding

Matched filtering is implemented through discrete convolution, which introduces a delay of 7 (equal to the length of the modulation pulse). Therefore, t_{echo} is found equal to 1.3356×10^{-5} s. The estimated values for the round trip time, direction, range, and RCS are listed in Table 2.

| Parameters | Target 1 |
|-----------------------|-----------------------------------|
| $\overline{t_{echo}}$ | $1.3356 \times 10^{-5} \text{ s}$ |
| Direction | 40° |
| Range | 2,003.4 m |
| RCS | 1.03 |

Table 2: Task 4 Estimated Parameters

5 Task 5-Third Scan-Two Targets

The result of the angle sweep in the range [30°,150°] is depicted in Figure 14. It indicates that there are two targets present at angles $\theta_1 = 40^\circ$ and $\theta_2 = 70^\circ$.

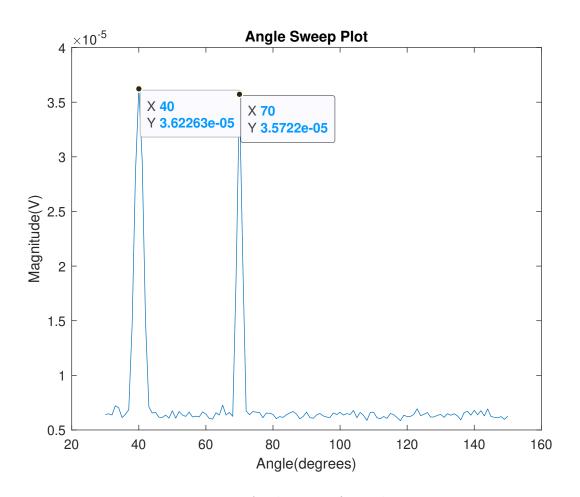


Fig. 14: Angle sweep for task 5

The signal at point Z for both directions is plotted in Figure 15.

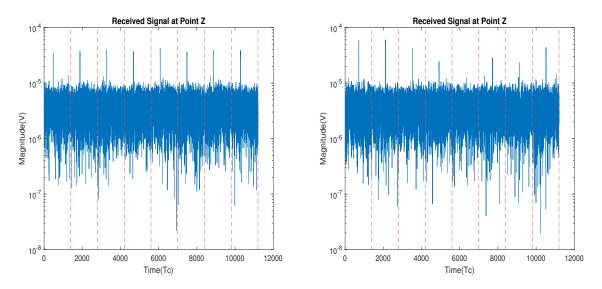


Fig. 15: (a)Point Z-40°angle (b)Point Z-70°angle

The round trip time is found in the same way as Task 4 for both targets. The second target features scatterers of similar amplitudes, which leads to a RCS value that varies across PRIs. Therefore, the estimated RCS value for the second target varies in every trial. The RCS values obtained at the time of writing are shown in Figure 16. Table 3 lists the estimated parameter values for targets 1 and 2.

| Parameters | Target 1 | Target 2 |
|-----------------------|-----------------------------------|----------------------------------|
| $\overline{t_{echo}}$ | $1.3356 \times 10^{-5} \text{ s}$ | $2.002 \times 10^{-5} \text{ s}$ |
| Direction | 40° | 70° |
| Range | 2,003.4 m | 3,003 m |
| RCS | 1.03 | 5.1541 |

Table 3: Task 5 Estimated Parameters

```
Estimated RCS are:
1.0030
5.1541
```

Fig. 16: Task 5 RCS estimates

6 Task 6-Fourth Scan-Three Targets

The result of the angle sweep in the range [30°,150°] is depicted in Figure 17. It is evident that there are three targets present at angles $\theta_1 = 40^\circ$, $\theta_2 = 70^\circ$, and $\theta_3 = 120^\circ$.

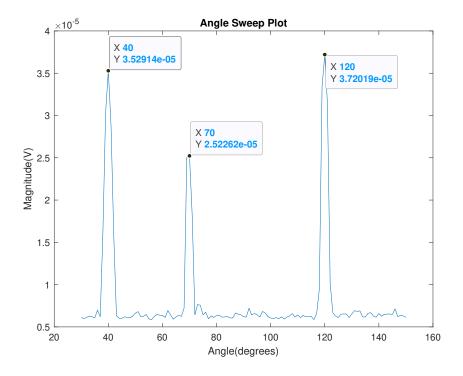


Fig. 17: Angle sweep for task 6

The signal for each target direction is plotted in Figure 18, 19 and 20.

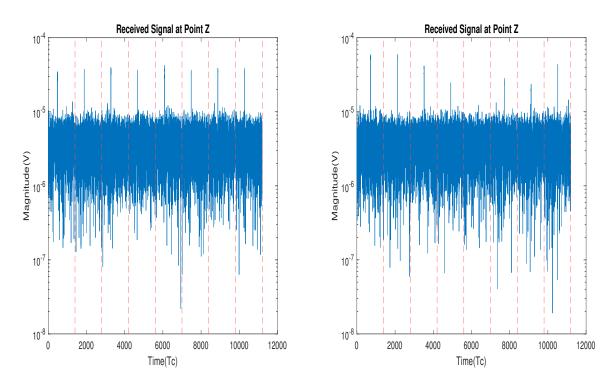


Fig. 18: Point Z-40°angle

Fig. 19: Point Z-70°angle

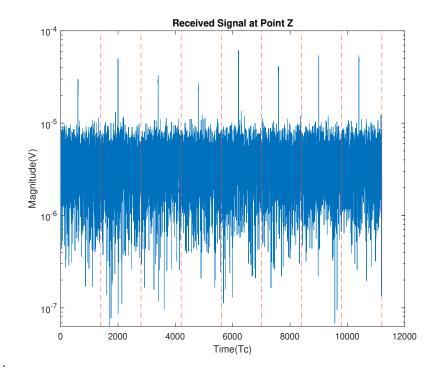


Fig. 20: Point Z-120°angle

Target 3 has a scatterer of much larger size than the rest, which means that RCS varies across PRIs. Hence, the estimated RCS value for target 3 is not constant across trials. A close estimate of the third target's RCS is shown in Figure 21. Table 4 shows the estimated parameter values for the three targets.

| Parameters | Target 1 | Target 2 | Target 3 |
|------------|-----------------------------------|----------------------------------|---------------------------|
| t_{echo} | $1.3356 \times 10^{-5} \text{ s}$ | $2.002 \times 10^{-5} \text{ s}$ | 1.6685×10^{-5} s |
| Direction | 40° | 70° | 120° |
| Range | 2,003.4 m | 3,003 m | 2,500.3 m |
| RCS | 1.03 | 5.1541 | 4.4730 |

Table 4: Task 6 Estimated Parameters

Estimated RCS are:

1.0067

3.1070

4.4730

Fig. 21: Task 6 RCS estimates

7 Task 7-Radar Data- Multi-target Detection and Parameter Estimation

Using the provided backscatter data, a full angle sweep is first performed to identify targets' directions. From the plot in Figure 22, it can be seen that there are targets present in the direction $\theta = 137^{\circ}$.

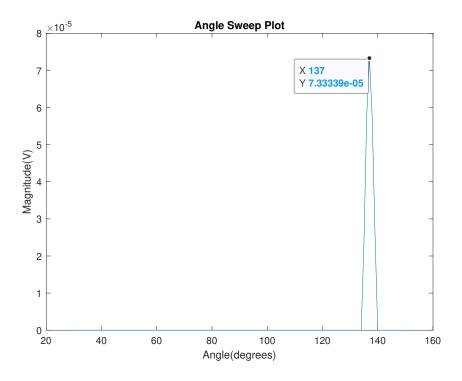


Fig. 22: Task 7 angle sweep

The received signal at point Z and the signal obtained after applying the matched filter and the threshold, and averaging across PRIs is shown in Figure 23 and 24.

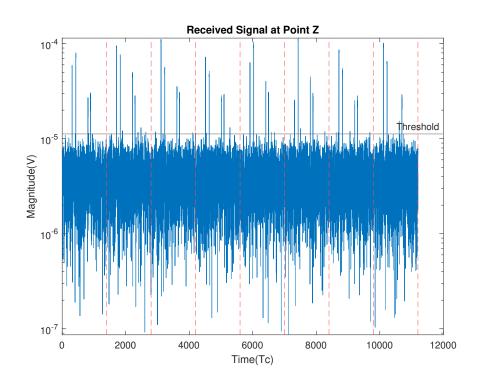


Fig. 23: Received signal at point Z-137° angle

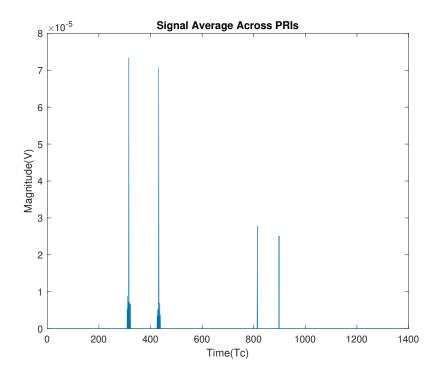


Fig. 24: Received signal averaged across PRIs

From Figure 24, it can be concluded that there are 4 targets present. Table num lists the estimated parameter values for each target.

| | Target 1 | Target 2 | Target 3 | Target 4 |
|-----------------------|----------------------------------|---------------------------------|-----------------------------------|-----------------------------------|
| $\overline{t_{echo}}$ | $8.652 \times 10^{-6} \text{ s}$ | $1.19 \times 10^{-5} \text{ s}$ | $2.2596 \times 10^{-5} \text{ s}$ | $2.4948 \times 10^{-5} \text{ s}$ |
| Direction | 137° | 137° | 137° | 137° |
| Range | 1,297.8 m | 1,785 m | 3,389.4 m | 3,742.2 m |
| RCS | 0.8203 | 2.7305 | 5.4763 | 6.6429 |