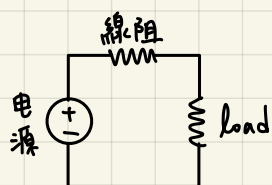
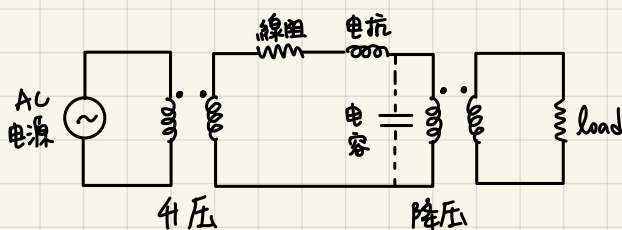


DC 電力系統



AC 電力系統



輸電線的參數 (被動元件)

R (電阻 Ω) 能量損失

L (電感 H) 有導線就有電感

C (電容 F)

$$R = \rho \left(\frac{l}{A} \right) = \frac{l}{\mu A}$$

導磁 \neq 導電

① 無限長電線的磁通鏈

$$\lambda = \lambda_2 + \lambda_1 = \frac{\mu_0 i}{2\pi}$$

② 無限長電線的磁通鏈 (多導體)

③ a 相 . b 相 c 相 互擾 (單-導體)

④ a 相 . b 相 c 相 互擾 (每相多導體)

⑤ 移位 (多導體互擾) : 先求 $r' = re^{-\frac{1}{2}}$
再求 $R_{eq} = ?$

3. 輸電線參數(Transmission-Line Parameters)

3.0 簡介(Introduction)

3.1 磁學回顧(Review of Magnetism)

3.2 無限長直電線的磁通鏈(Flux Linkages of Infinite Straight Wire)

3.3 多導體情況下的磁通鏈(Flux Linkages of Multi-Conductors)

3.4 捆束導體(Conductor Bundling)

3.5 移位(Transposition)

3.6 電場回顧(Review of Electric Fields)

3.7 線路電容(Line Capacitance)

3.8 典型參數值(Typical Parameter Values)

3.9 結論與習題(Summary)

3.0 簡介(Introduction)

A line is characterized by four distributed parameters: **series resistance, series inductance, shunt conductance, and shunt capacitance** (assuming without mutual inductance and capacitance).

Resistance: $R=\rho(l/A)$, ρ (resistivity: 電阻率 Ωm), length: l , cross-sectional area: A . (Conductor, Semiconductor, and Insulator)

Silver: $\rho = 1.64 \times 10^{-8} \Omega\text{m}$,

Copper: $\rho = 1.72 \times 10^{-8} \Omega\text{m}$, $R=1.72 \times 10^{-8} \times 1\text{km} / \pi(0.01\text{m})^2 = 0.0547\Omega$

Aluminum: $\rho = 2.8 \times 10^{-8} \Omega\text{m}$,

Gold: $\rho = 2.45 \times 10^{-8} \Omega\text{m}$,

Carbon: $\rho = 4 \times 10^{-5} \Omega\text{m}$, Germanium (鍺): $\rho = 4.7 \times 10^{-1} \Omega\text{m}$, Silicon: $\rho = 6.4 \times 10^2 \Omega\text{m}$,

Paper: $\rho = 10^{10} \Omega\text{m}$, Mica (雲母): $\rho = 5 \times 10^{11} \Omega\text{m}$, Glass: $\rho = 10^{12} \Omega\text{m}$, Teflon: $\rho = 3 \times 10^{12} \Omega\text{m}$, Air: $\rho = 1.5 \times 10^{14} \Omega\text{m}$,

集膚效應(Skin Effect)

In high frequency applications the current in a good conductor tends to shift to the surface of the conductor (due to the **skin effect**).

Resistance: $R = \rho(l/A)$, ρ (resistivity: 電阻率 Ωm), $\sigma = 1/\rho$ (conductivity: 導電率 $1/\Omega\text{m} = \text{A}/(\text{V} \times \text{m})$)

Skin Depth, $\delta = 1/(\pi f \mu \sigma)^{0.5}$, $\mu_0 = 4\pi \times 10^{-7} \text{ (H/m)}$ (permeability: 導磁係數)

Silver: $\sigma = 6.17 \times 10^7$, $\delta = 8.27 \text{ mm}$ (at 60Hz), $\delta = 0.064 \text{ mm}$ (at 1MHz)

Copper: $\sigma = 5.8 \times 10^7$, $\delta = 8.53 \text{ mm}$ (at 60Hz), $\delta = 0.066 \text{ mm}$ (at 1MHz)

Aluminum: $\sigma = 3.54 \times 10^7$, $\delta = 10.92 \text{ mm}$ (at 60Hz), $\delta = 0.084 \text{ mm}$ (at 1MHz)

Gold: $\sigma = 4.1 \times 10^7$, $\delta = 10.14 \text{ mm}$ (at 60Hz), $\delta = 0.079 \text{ mm}$ (at 1MHz)

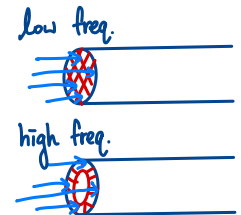
Iron ($\mu_r = 10^3$): $\sigma = 100 \times 10^7$, $\delta = 0.65 \text{ mm}$ (at 60Hz), $\delta = 0.005 \text{ mm}$ (at 1MHz)

Seawater: $\sigma = 4$, $\delta = 32 \text{ m}$ (at 60Hz), $\delta = 0.25 \text{ m}$ (at 1MHz)

$\epsilon_0 = (1/36\pi) \times 10^{-9} \text{ (F/m)}$ (permittivity: 介電係數)

Speed of light: $C = 1/(\mu_0 \epsilon_0)^{0.5} = 3 \times 10^8 \text{ m/s}$, $[(\text{H} \cdot \text{F}) = (\text{s}^2), \text{亨利} \cdot \text{法拉} = \text{s}^2]$

Wave length of 60Hz: $\lambda = C/f = 5 \times 10^6 \text{ m}$,



3.1 磁學回顧 (Review of Magnetism)

Ampere's Circuital Law: $F = \oint \mathbf{H} \cdot d\mathbf{l} = Ni$ 磁動勢

磁通密度

$\mathbf{B} = \mu \mathbf{H}$, $B = \Phi/A$, Φ : flux, B : flux density (webers/m²), H : magnetic field intensity (A · turn/m)

磁通鏈 Flux linkages: $\lambda = N\Phi = Li = \sum_{i=1}^N \Phi_i$

Ex3.1 Calculate the inductance.

$$F = Hl = Ni$$

$$B = \mu H = \mu Ni / l,$$

$$\Phi = BA = (\mu A / l) Ni,$$

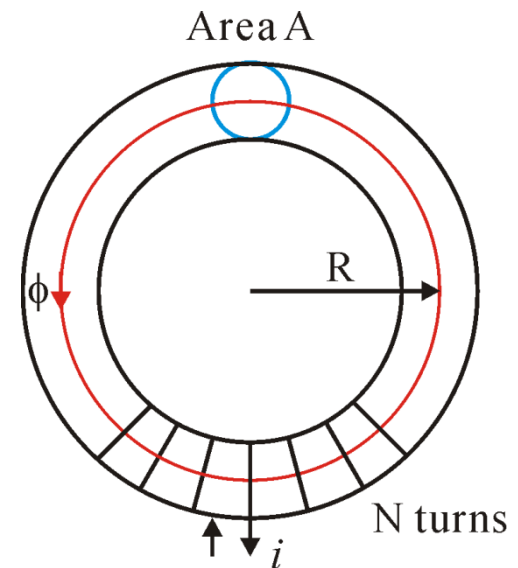
$$L = \lambda / i = N\Phi / i = (\mu AN^2 / l) = \mu AN^2 / (2\pi R)$$

inductance: relates flux linkage to current

$$\mathcal{E}_{\text{ind}} = L \frac{di}{dt} = N \frac{d\Phi}{dt} \quad \Phi = BA = \mu HA = \mu \frac{Ni}{l} A$$

$$\frac{Li}{t} = \frac{N\Phi}{t} = N\mu \frac{Ni}{l} A$$

$$L = \frac{N^2 \mu A}{l}$$



3.2 無限長直電線的磁通鏈 (Flux Linkages of Infinite Straight Wire)

Figure 3.2: wire carrying current

Case 1 ($x > r$): $F = \oint \mathbf{H} \cdot d\mathbf{l} = \overset{N=1}{i} = \mathbf{H} \cdot 2\pi x \Rightarrow \mathbf{H} = i/(2\pi x)$

Case 2 ($x \leq r$): $\oint \mathbf{H} \cdot d\mathbf{l} = i_e = (\pi x^2 / \pi r^2) i = \mathbf{H} \cdot 2\pi x \Rightarrow \mathbf{H} = (x / 2\pi r^2) i$

$B = \mu_r \mu_0 H$, $\mu_0 = 4\pi \times 10^{-7}$,

μ_r of the air, copper, and aluminum is near 1.

線外: $\mu_0 \int_r^R \frac{1}{x} dx = \mu_0 \left[\ln x \right]_r^R = \frac{\mu_0 i}{2\pi} \ln \left(\frac{R}{r} \right)$

線內: $\mu_r \mu_0 \int_0^r \frac{x}{2\pi r^2} i dx = \frac{\mu_r \mu_0 i}{2\pi r^2} \int_0^r x^2 dx = \frac{\mu_r \mu_0 i}{2\pi r^2} \cdot \frac{r^3}{3} = \frac{\mu_r \mu_0 i}{6\pi}$

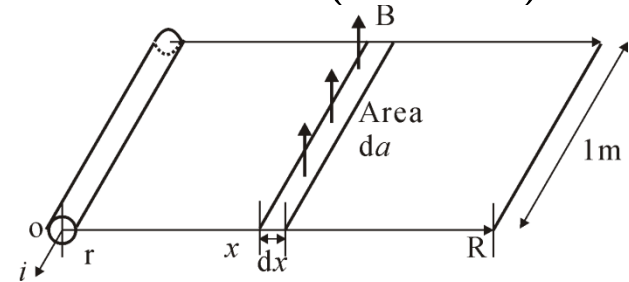
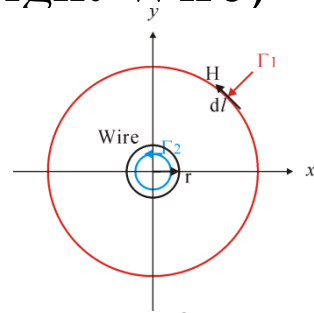
Figure 3.3: infinite wire of radius r , find flux crossing rectangle.

Case 1 ($x > r$, $N=1$): $\lambda_1 = \Phi_1 = \int_A B(x) dx = \mu_0 \int_A H(x) dx = \mu_0 \int_r^R \frac{i}{2\pi x} dx = (\mu_0 i / 2\pi) \ln(R/r)$. (Caution: $R \rightarrow \infty$)

Case 2 ($x \leq r$, $N = \pi x^2 / \pi r^2$): $\lambda_2 = \mu_r \mu_0 \int_0^r \left(\frac{x}{2\pi r^2} \right) \left(\frac{\pi x^2}{\pi r^2} \right) i dx = \mu_r \mu_0 i / (8\pi)$

Total Flux Linkages per meter of one Infinite Straight Wire :

$\lambda = \lambda_2 + \lambda_1 = (\mu_0 i / 2\pi) [\mu_r / 4 + \ln(R/r)]$



3.3 多導體情況下的磁通鏈(Flux Linkages of Multi-Conductors)

Total Flux Linkages per meter of one Infinite Straight Wire :

$$\lambda = \lambda_2 + \lambda_1 = (\mu_0 i / 2\pi) [\mu_r / 4 + \ln(R/r)]$$

$$\lambda_1 = \phi_1 = B_1 A_1 = \mu_0 H_1 A_1$$

$$\lambda_2 = \phi_2 = B_2 A_2 = \mu_r \mu_0 H_2 A_2$$

$$H_1 A_1 = \int_A H(x) dx = \int_A \frac{i}{2\pi x} dx$$

$$H_2 A_2 = \int_A H(x) dx = \int_A \frac{x}{2\pi r^2} (\frac{\pi x^2}{\pi r^2}) i dx$$

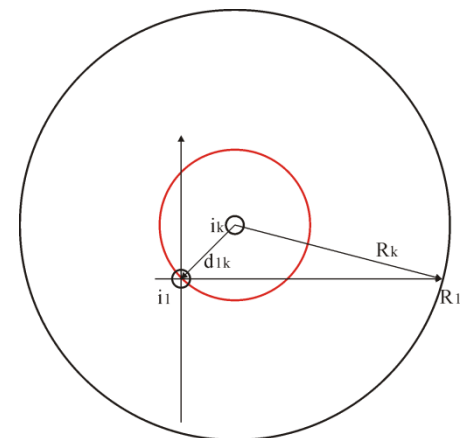
Total Flux Linkages per meter of multi-Conductors for wire 1:

$$\begin{aligned} \lambda_1 &= (\mu_0 / 2\pi) \{ i_1 [\mu_r / 4 + \ln(R_1/r_1)] + i_2 \ln(R_2/d_{12}) + \dots + i_n \ln(R_n/d_{1n}) \} \\ &= (\mu_0 / 2\pi) \{ i_1 [\mu_r / 4 + \ln(1/r_1)] + i_2 \ln(1/d_{12}) + \dots + i_n \ln(1/d_{1n}) \} \\ &\quad + (\mu_0 / 2\pi) [i_1 (\ln(R_1) + i_2 \ln(R_2) + \dots + i_n \ln(R_n))] \end{aligned}$$

Assuming $i_1 + i_2 + \dots + i_n = 0$ and $R_1 = R_2 = \dots = R_n = R$

$$\begin{aligned} \lambda_1 &= (\mu_0 / 2\pi) \{ i_1 [\mu_r / 4 + \ln(1/r_1)] + i_2 \ln(1/d_{12}) + \dots + i_n \ln(1/d_{1n}) \} \\ &= l_{11} i_1 + l_{12} i_2 + \dots + l_{1n} i_n \end{aligned}$$

$$\begin{aligned} \lambda_k &= (\mu_0 / 2\pi) \{ i_1 (\ln(1/d_{k1}) + i_2 \ln(1/d_{k2}) + \dots + i_k [\mu_r / 4 + (\ln(1/r_k)] + \dots + i_n \ln(1/d_{kn}) \} \\ &= l_{k1} i_1 + l_{k2} i_2 + \dots + l_{kk} i_k + \dots + l_{kn} i_n \end{aligned}$$

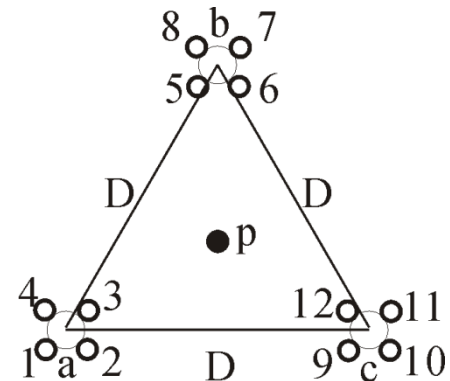
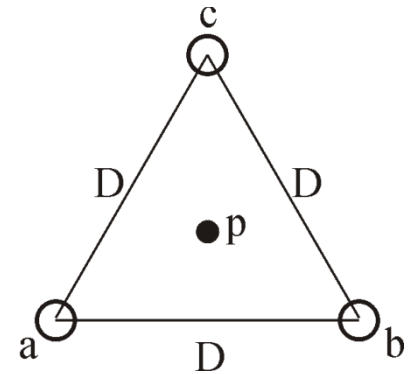


Ex3.2 Calculate the inductance per meter of each phase of a three-phase transmission line.

Assume that 1. Conductors equally spaced D and have equal radii r .

2. $i_a + i_b + i_c = 0$.

$$\begin{aligned}
 \lambda_a &= (\mu_o/2\pi) \{ i_a [\mu_r/4 + \ln(1/r)] + i_b \ln(1/D) + i_c \ln(1/D) \} \\
 &= (\mu_o/2\pi) \{ i_a [\mu_r/4 + \ln(1/r)] - i_a \ln(1/D) \} \\
 &= (\mu_o/2\pi) [\mu_r/4 + \ln(1/r) - \ln(1/D)] \times i_a \\
 &= (\mu_o/2\pi) [\ln e^{(\mu_r/4)} + \ln(1/r) - \ln(1/D)] \times i_a \\
 &= (\mu_o/2\pi) [\ln(1/r e^{-(\mu_r/4)}) - \ln(1/D)] \times i_a \\
 &= (\mu_o/2\pi) [\ln(1/r') - \ln(1/D)] \times i_a \\
 &= (\mu_o/2\pi) [\ln(D/r')] \times i_a \\
 &= l_a \times i_a
 \end{aligned}$$



Assume that 1. $D = 1\text{m}$, $r = 0.01\text{m}$.

$\mu_r = 1$, $\mu_o = 4\pi \times 10^{-7}$,

$l_a = ?$

3.4 捆束導體 (Conductor Bundling)

$$\lambda_1 = (\mu_o/2\pi) \left\{ (i_a/4) [\mu_r/4 + \ln(1/r) + \ln(1/d_{12}) + \ln(1/d_{13}) + \ln(1/d_{14})] \right. \\ \left. + (i_b/4) [\ln(1/d_{15}) + \ln(1/d_{16}) + \ln(1/d_{17}) + \ln(1/d_{18})] \right. \\ \left. + (i_c/4) [\ln(1/d_{19}) + \ln(1/d_{1,10}) + \ln(1/d_{1,11}) + \ln(1/d_{1,12})] \right\} \\ = (\mu_o/2\pi) (i_a \ln 1/R_{\text{GMR}} + i_b \ln 1/D_{1b} + i_c \ln 1/D_{1c})$$

$$r' = r e^{-(\mu_r/4)}, R_{\text{GMR}} = (r' d_{12} d_{13} d_{14})^{1/4} \text{ (geometric mean radius)}$$

$$D_{1b} = (d_{15} d_{16} d_{17} d_{18})^{1/4}, D_{1c} = (d_{19} d_{1,10} d_{1,11} d_{1,12})^{1/4}$$

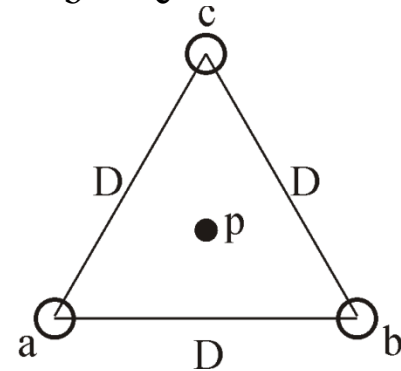
Assuming $D_{1b} = D_{1c} = D$ (geometric mean distance), $i_a + i_b + i_c = 0$,

$$\lambda_1 = (\mu_o/2\pi) i_a \ln D / R_{\text{GMR}}$$

$$\text{Inductance } l_1 = \lambda_1 / (i_a/4) = 4 (\mu_o/2\pi) \ln D / R_{\text{GMR}}$$

For phase a: $l_1 = l_2 = l_3 = l_4$, and four parallel lines,

$$l_a = l_1 / 4 = (\mu_o/2\pi) \ln D / R_{\text{GMR}}, \text{ and } l_a = l_b = l_c$$



Ex3.3 Find the geometric mean radius (**GMR**) of three symmetrically spaced conductors. Assume that $r = 2\text{cm}$ and $r' = r e^{-(\mu_r/4)} = 2e^{-1/4} = 1.56 \text{ cm}$,

$$d_{12} = d_{13} = d_{23} = 50\text{cm}, R_{\text{GMR}} = (r' d_{12} d_{13})^{1/3} = ? ,$$

3.5 移位 (Transposition)

It is usually more convenient to arrange the phases in a **horizontal or vertical** configuration, therefore the **symmetry is lost**. One way to regain the symmetry and restore balanced conditions is to use the method of **transposition of lines**.

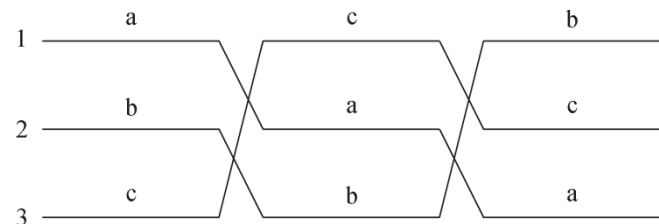
$$\lambda_a = (\lambda_{a1} + \lambda_{a2} + \lambda_{a3})/3, \quad D_m = (d_{12} d_{23} d_{13})^{1/3},$$

$$\lambda_a = (1/3)(\mu_0/2\pi) \{ i_a \ln(1/r') + i_b \ln(1/d_{12}) + i_c \ln(1/d_{13}) \\ + i_a \ln(1/r') + i_b \ln(1/d_{23}) + i_c \ln(1/d_{12}) \\ + i_a \ln(1/r') + i_b \ln(1/d_{13}) + i_c \ln(1/d_{23}) \}$$

$$\lambda_a = (\mu_0/2\pi) \{ i_a \ln(1/r') + i_b \ln(1/D_m) + i_c \ln(1/D_m) \} \\ = (\mu_0/2\pi) \{ i_a \ln(1/r') - i_a \ln(1/D_m) \} = (\mu_0/2\pi) i_a \ln(D_m/r')$$

$$l_a = l_b = l_c = (\mu_0/2\pi) \ln(D_m/r') \text{ for one line transposition}$$

$$l_a = l_b = l_c = (\mu_0/2\pi) \ln(D_m/R_{GMR}) \text{ for conductor bundling transposition}$$



Ex 3.5 Find the inductance per meter of the 3-phase line shown in figure E3.5. The conductors are aluminum ($\mu_r = 1$), with radius $r = 0.5$ inch, $d_{12} = d_{23} = 20$ ft, $d_{13} = 40$ ft, each phase has two conductors and distance is 18 inch.

(a) $r' = r e^{-(\mu_r/4)} = 0.5 \times 0.78$, $R_{GMR} = (r' \times 18)^{1/2} = 2.65$ inch = 0.22 ft

(b) $D_m = (20 \text{ ft} \times 20 \text{ ft} \times 40 \text{ ft})^{1/3} = 25.2$ ft

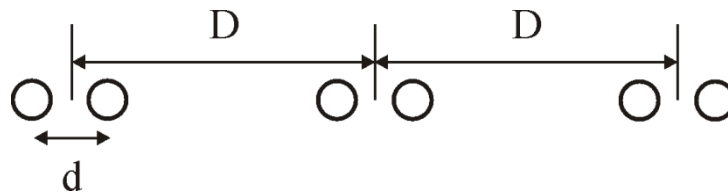
(c) $l_a' = l_b' = l_c' = (\mu_0/2\pi) \ln(D_m/R_{GMR}) = 2 \times 10^{-7} \ln(25.2/0.22)$
 $= 9.47 \times 10^{-7} \text{ H/m}$

$\approx 10^{-6} \text{ H/m} = 1 \mu\text{H/m} = 1 \text{ mH/km}$ 很大

$\chi = \omega L$

$= 377 \times 1 \text{ mH/km}$

$= 0.377 \text{ H/km}$



3.8典型參數值(Typical Parameter Values)

Conductors per phase (18-in. spacing) :	1(138kV),	^{TW max} 2(345kV),	^{next 69kV} 4(765kV)
Number of strands aluminum/steel :	54/7,	45/7,	54/19
Diameter (in.) :	0.977,	1.165,	1.424
Conductor GMR (ft) :	0.0329,	0.0386,	0.0479
Current-carrying capacity per conductor(A):	770,	1010,	1250
Bundle GMR- R_{GMR} (ft) :	0.0329,	0.2406,	0.6916
Flat phase spacing (ft) :	17.5,	26.0,	45.0
GMD phase spacing (ft) :	22.05,	32.76,	56.70
Inductance ($H/m \times 10^{-7}$) :	13.02,	9.83,	8.81
X_L (Ω /mile) :	0.789,	0.596,	0.535
Capacitance ($F/m \times 10^{-12}$) :	8.84,	11.59,	12.78
$ X_C $ ($M\Omega$ -mile to neutral) :	0.186,	0.142,	0.129
Resistance (Ω /mile), dc, 50 ° C :	0.1618,	0.0539,	0.0190
Resistance (Ω /mile), 60Hz, 50 ° C :	0.1688,	0.0564,	0.0201
Surge impedance loading (MVA) :	50,	415,	2268

Three phase line-to-line 138 kVrms / 60Hz

Conductors per phase (18-in. spacing) : 1 (138kV)

Number of strands aluminum/steel : 54/7,

Diameter (in.) : ⁱⁿ0.977 ^{半徑} $\div 2 \div 12 = 0.0407$ ft,

Conductor GMR (ft): ^{根據 Fe & Al 的含量估算} 0.0329 = $0.0407 \times 0.8 = 0.0317 = 0.0407 \times e^{-\mu r/4} = 0.0407 \times 0.7788$

Current-carrying capacity per conductor(A): 770, $1 \text{ mm}^2 \approx 7 \text{ A}$

Bundle GMR- R_{GMR} (ft) : $r' = 0.0329$, $r = 0.0407 = 0.977 \div 2 \div 12$

Flat phase spacing (ft) : 17.5,

GMD phase spacing (ft): 22.05 = $(17.5 \times 17.5 \times 2 \times 17.5)^{1/3} = 17.5 \times 1.26$

Inductance (H/m $\times 10^{-7}$) : 13.02 = $2 \times 10^{-7} \times \ln (22.05 / 0.0329)$

X_L (Ω /mile) : 0.789 = $2\pi \times 60 \times 13.02 \times 10^{-7} \times 1609.34$

Capacitance (F/m $\times 10^{-12}$) : 8.84 = $2\pi \times 8.854 \times 10^{-12} / \ln (22.05 / 0.407)$

$|X_C|$ (M Ω -mile to neutral) : 0.186 = $1 / (2\pi \times 60 \times 8.84 \times 10^{-12} \times 1609.34)$

Resistance (Ω /mile), dc, 50 °C: 0.1618 = $\rho \times 1609.34 / [\pi(0.977 \times 2.54 \times 10^{-2} / 2)^2]$, $\rho = 4.863 \times 10^{-8}$

Resistance (Ω /mile), 60Hz, 50 °C : 0.1688 = 0.1618×1.0433

Surge impedance loading (MVA): 50 ? = 61.4 = $1 \times \sqrt{3} \times 138 \times 0.77 / 3$ (MVA)
_{一個相}

Three phase line-to-line 345 kVrms / 60Hz

Conductors per phase (18-in. spacing) : 2(345kV)

Number of strands aluminum/steel : 45/7,

Diameter (in.) : $1.165 \div 2 \div 12 = 0.0485$ ft,

Conductor GMR (ft): $0.0386 = 0.0485 \times 0.8^{1/4} = 0.0378 = 0.0485 \times e^{-\mu_r/4} = 0.0485 \times 0.7788$

Current-carrying capacity per conductor(A): 1010,

Bundle GMR- R_{GMR} (ft) : $0.2406 = [0.0386 \times (18/12)]^{1/2}$,
 $0.2697 = [0.0485 \times (18/12)]^{1/2}$

Flat phase spacing (ft) : 26.0,

GMD phase spacing (ft): $32.76 = (26.0 \times 26.0 \times 2 \times 26.0)^{1/3} = 26.0 \times 1.26$

Inductance (H/m $\times 10^{-7}$) : $9.83 = 2 \times 10^{-7} \times \ln (32.76 / 0.2406)$

X_L (Ω /mile) : $0.596 = 2\pi \times 60 \times 9.83 \times 10^{-7} \times 1609.34$

Capacitance (F/m $\times 10^{-12}$) : $11.59 = 2\pi \times 8.854 \times 10^{-12} / \ln (32.76 / 0.2697)$


$|X_C|$ ($M\Omega$ -mile to neutral) : $0.142 = 1/(2\pi \times 60 \times 11.59 \times 10^{-12} \times 1609.34)$

Resistance (Ω /mile), dc, 50 ° C: $0.0539 = \rho \times 1609.34 / [2 \times \pi (1.165 \times 2.54 \times 10^{-2} / 2)^2]$, $\rho = 4.6066 \times 10^{-8}$

Resistance (Ω /mile), 60Hz, 50 ° C : $0.0564 = 0.0539 \times 1.0464$

Surge impedance loading (MVA): $415 = 402.3 = 2 \times \sqrt{3} \times 345 \times 1.010 / 3$ (MVA)

Three phase line-to-line 765 kVrms / 60Hz

Conductors per phase (18-in. = 1.5-ft spacing) : 4(765kV) 

Number of strands aluminum/steel : 54/19,

Diameter (in.) : $1.424 \div 2 \div 12 = 0.0593$ ft,

Conductor GMR (ft): 0.0479 = $0.0593 \times 0.8^{1/4} = 0.0462 = 0.0593 \times e^{-\mu_r/4} = 0.0593 \times 0.7788$

Current-carrying capacity per conductor(A): 1250,

Bundle GMR- R_{GMR} (ft) : 0.6916 = $[0.0479 \times 1.5 \times 1.5 \times 1.5 \times \sqrt[4]{2}]^{1/4}$,
0.7294 = $[0.0593 \times 1.5 \times 1.5 \times 1.5 \times \sqrt[4]{2}]^{1/4}$,

Flat phase spacing (ft) : 45.0,

GMD phase spacing (ft): 56.7 = $(45.0 \times 45.0 \times 2 \times 45.0)^{1/3} = 45.0 \times 1.26$

Inductance (H/m $\times 10^{-7}$) : 8.81 = $2 \times 10^{-7} \times \ln (56.7 / 0.6916)$

X_L (Ω /mile) : 0.535 = $2\pi \times 60 \times 8.81 \times 10^{-7} \times 1609.34$

Capacitance (F/m $\times 10^{-12}$) : 12.78 = $2\pi \times 8.854 \times 10^{-12} / \ln (56.7 / 0.7294)$

$|X_C|$ (M Ω -mile to neutral) : 0.129 = $1 / (2\pi \times 60 \times 12.78 \times 10^{-12} \times 1609.34)$

Resistance (Ω /mile), dc, 50 ° C: 0.0190 = $\rho \times 1609.34 / [4 \times \pi (1.424 \times 2.54 \times 10^{-2} / 2)^2]$, $\rho = 4.854 \times 10^{-8}$

Resistance (Ω /mile), 60Hz, 50 ° C : 0.0201 = 0.0190×1.0579

Surge impedance loading (MVA) : 2268 ? = $2208.3 = 4 \times \sqrt{3} \times 765 \times 1.250 / 3$ (MVA)

3.9 結論與習題(Summary)

For a three-phase line with transposition and bundling, the average per phase **inductance** (H/m) is given by

$L = (\mu_0 / 2\pi) \ln(D_m / R_{GMR})$ for conductor bundling transposition

$$D_m = (D_{12} D_{23} D_{13})^{1/3}$$

$$r' = r e^{-(\mu r / 4)}, R_b = R_{GMR} = (r' d_{12} d_{13} \cdot d_{1b})^{1/b}, b > 1; R_b = R_{GMR} = r', \text{ when } b = 1$$

The formula for average **capacitance** (F/m) to neutral is

$C = (2\pi\epsilon) \ln(D_m / R_{GMR})$ for conductor bundling transposition

$$D_m = (D_{12} D_{23} D_{13})^{1/3}$$

$$R_b^c = R_{GMR} = (r d_{12} d_{13} \cdot d_{1b})^{1/b}, b > 1; R_b^c = R_{GMR} = r, \text{ when } b = 1$$