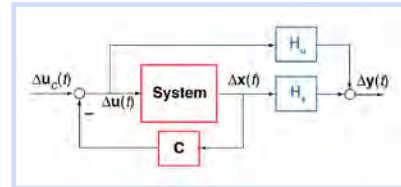


# Modal Properties of Linear-Quadratic Regulators

Robert Stengel

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- Frequency domain models of optimally regulated systems
- Determinant identities
- Transmission zeros
- Root locus analysis of optimally regulated systems
- Eigenvectors of linearly regulated systems



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<http://www.princeton.edu/~stengel/MAE546.html>  
<http://www.princeton.edu/~stengel/OptConEst.html>

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## Linear-Quadratic Control

Quadratic cost function for infinite final time

$$J = \frac{1}{2} \int_{t_o}^{\infty} \begin{bmatrix} \Delta \mathbf{x}^T(t) & \Delta \mathbf{u}^T(t) \end{bmatrix} \begin{bmatrix} \mathbf{Q} & \mathbf{0} \\ \mathbf{0} & \mathbf{R} \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(t) \\ \Delta \mathbf{u}(t) \end{bmatrix} dt = \frac{1}{2} \int_{t_o}^{\infty} [\Delta \mathbf{x}^T(t) \mathbf{Q} \Delta \mathbf{x}(t) + \Delta \mathbf{u}(t) \mathbf{R} \Delta \mathbf{u}(t)] dt$$

- Linear, time-invariant dynamic system
- Adjoint equation derives from Euler-Lagrange equations ("adjoint system")
- Optimal control is proportional to adjoint vector

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F} \Delta \mathbf{x}(t) + \mathbf{G} \Delta \mathbf{u}(t)$$

$$\Delta \dot{\boldsymbol{\lambda}}(t) = -\mathbf{Q} \Delta \mathbf{x}(t) - \mathbf{F}^T \Delta \boldsymbol{\lambda}(t)$$

$$\Delta \mathbf{u}(t) = -\mathbf{R}^{-1} \mathbf{G}^T \Delta \boldsymbol{\lambda}(t)$$

hence

$$\Delta \dot{\mathbf{x}}(t) = \mathbf{F} \Delta \mathbf{x}(t) - \mathbf{G} \mathbf{R}^{-1} \mathbf{G}^T \Delta \boldsymbol{\lambda}(t)$$

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# Coupling of State and Adjoint System Dynamics Due to Optimal Control

State and adjoint equations are coupled by optimal control

$$\begin{bmatrix} \Delta \dot{\mathbf{x}}(t) \\ \Delta \dot{\boldsymbol{\lambda}}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{F} & -\mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ -\mathbf{Q} & -\mathbf{F}^T \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(t) \\ \Delta \boldsymbol{\lambda}(t) \end{bmatrix} \quad \text{or} \quad \begin{matrix} \Delta \dot{\boldsymbol{\chi}}(t) = \mathbf{F}' \Delta \boldsymbol{\chi}(t) \\ \dim(\Delta \boldsymbol{\chi}) = 2n \times 1 \end{matrix}$$

|  |                            |
|--|----------------------------|
| State<br>Dynamics  | Adjoint Effect on<br>State |
| $\mathbf{F}' = \begin{bmatrix} \mathbf{F} & -\mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ -\mathbf{Q} & -\mathbf{F}^T \end{bmatrix}$ |                            |
| State Effect on<br>Adjoint   | Adjoint System<br>Dynamics |

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## Frequency Domain Model of State-Adjoint System

Laplace transform of state and adjoint equations, neglecting initial/final conditions

$$\begin{bmatrix} s\Delta \mathbf{x}(s) \\ s\Delta \boldsymbol{\lambda}(s) \end{bmatrix} = \begin{bmatrix} \mathbf{F} & -\mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ -\mathbf{Q} & -\mathbf{F}^T \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}(s) \\ \Delta \boldsymbol{\lambda}(s) \end{bmatrix} \triangleq \mathbf{F}' \begin{bmatrix} \Delta \mathbf{x}(s) \\ \Delta \boldsymbol{\lambda}(s) \end{bmatrix}$$

$(s\mathbf{I}_{2n} - \mathbf{F}')$  is the **characteristic matrix** of the coupled system

Characteristic polynomial of the control-coupled system

$$\begin{aligned} |(s\mathbf{I}_{2n} - \mathbf{F}')| &= \begin{vmatrix} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ \mathbf{Q} & (s\mathbf{I}_n + \mathbf{F}^T) \end{vmatrix} = 0 \\ \Delta_{\text{coupled}}(s) &= s^{2n} + a_{2n-1}s^{2n-1} + \dots + a_1s + a_0 \\ &= (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_{2n}) = 0 \end{aligned}$$

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# *Uncoupled State and Adjoint Dynamics*

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## Uncoupled System

With no coupling due to control

$$\begin{bmatrix} s\Delta\mathbf{x}(s) \\ s\Delta\lambda(s) \end{bmatrix} = \begin{bmatrix} \mathbf{F} & \mathbf{0} \\ -\mathbf{Q} & -\mathbf{F}^T \end{bmatrix} \begin{bmatrix} \Delta\mathbf{x}(s) \\ \Delta\lambda(s) \end{bmatrix}$$

**Determinants of the uncoupled system's  
characteristic matrix**

$$\begin{vmatrix} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{0} \\ \mathbf{Q} & (s\mathbf{I}_n + \mathbf{F}^T) \end{vmatrix} = |(s\mathbf{I}_n - \mathbf{F})(s\mathbf{I}_n + \mathbf{F}^T)| = |\mathbf{sI}_n - \mathbf{F}| |\mathbf{sI}_n + \mathbf{F}^T| = \mathbf{0}$$

**Eigenvalues of a block triangular matrix are eigenvalues of  
the diagonal block matrices**

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## Two Determinant Identities

1) Determinant is a scalar

$$|\mathbf{A}^T| = |\mathbf{A}|$$

2) Square matrices,  
scalar determinant

$$|\mathbf{AB}| = |\mathbf{BA}| = |\mathbf{A}| |\mathbf{B}|$$

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## Characteristic Equation of the Uncoupled System

$$|s\mathbf{I}_{2n} - \mathbf{F}'_{\text{uncoupled}}| = |s\mathbf{I}_n - \mathbf{F}| |s\mathbf{I}_n + \mathbf{F}^T| = 0$$

**Dynamic system**

$$|s\mathbf{I}_n - \mathbf{F}| = \Delta_{\text{state}}(s) \triangleq \Delta_{\text{OL}}(s) = 0$$

**Adjoint system**

$$\begin{aligned} |s\mathbf{I}_n + \mathbf{F}^T| &= \Delta_{\text{adjoint}}(s) = (-1)^n | -s\mathbf{I}_n - \mathbf{F}^T | \\ &= (-1)^n \Delta_{\text{state}}(-s) \triangleq (-1)^n \Delta_{\text{OL}}(-s) = 0 \end{aligned}$$

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# Eigenvalue Symmetry

Uncoupled system polynomials: same polynomial of  $(s)$  and  $(-s)$

$$\Delta_{\text{uncoupled}}(s) \triangleq (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s)$$

Characteristic polynomial has  $2n$  roots

With no control coupling, ...

$$\begin{aligned} \Delta_{\text{uncoupled}}(s) &= s^{2n} + a_{2n-1}s^{2n-1} + \dots + a_1s + a_0 = (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_{2n}) \\ &= \left[ (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_n) \right]_{\text{state}} \left[ (s - \lambda_{n+1})(s - \lambda_{n+2}) \dots (s - \lambda_{2n}) \right]_{\text{adjoint}} \end{aligned}$$

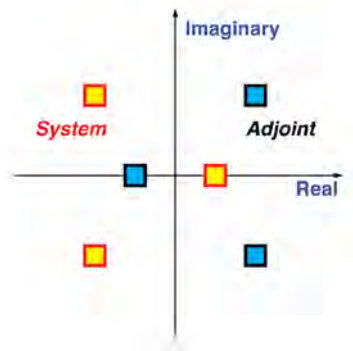
$$\begin{aligned} \Delta_{\text{uncoupled}}(s) &= |s\mathbf{I}_n - \mathbf{F}| |s\mathbf{I}_n + \mathbf{F}^T| = |s\mathbf{I}_n - \mathbf{F}| |s\mathbf{I}_n + \mathbf{F}| \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) = 0 \end{aligned}$$

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# Eigenvalue Symmetry

Eigenvalues are mirrored about the imaginary axis

$$\begin{aligned} \Delta_{\text{uncoupled}}(s) &= \left[ (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_n) \right]_{\text{state}} \left[ (-s - \lambda_1)(-s - \lambda_2) \dots (-s - \lambda_n) \right]_{\text{adjoint}} \\ &= (-1)^n \left[ (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_n) \right]_{\text{state}} \left[ (s + \lambda_1)(s + \lambda_2) \dots (s + \lambda_n) \right]_{\text{adjoint}} \\ &= 0 \end{aligned}$$



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# Coupled State and Adjoint Dynamics

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## More Determinant Identities

3) from Laplace expansion

$$\begin{vmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{0} & \mathbf{I}_m \end{vmatrix} = \begin{vmatrix} \mathbf{A} & \mathbf{0} \\ \mathbf{B}^T & \mathbf{I}_m \end{vmatrix} = |\mathbf{A}|$$

4) From (2) and (3)

$$\begin{vmatrix} \mathbf{A}_1 & \mathbf{0} \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = \begin{bmatrix} \mathbf{A}_1 & \mathbf{0} \\ \mathbf{A}_3 & \mathbf{I}_m \end{bmatrix} \begin{bmatrix} \mathbf{I}_n & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_4 \end{bmatrix} \\ = \begin{vmatrix} \mathbf{A}_1 & \mathbf{0} \\ \mathbf{A}_3 & \mathbf{I}_m \end{vmatrix} \begin{vmatrix} \mathbf{I}_n & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_4 \end{vmatrix} = |\mathbf{A}_1| |\mathbf{A}_4|$$

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# Schur' s Formula

## 5. a) Non-singular $\mathbf{A}_1$

$$\begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = \begin{vmatrix} \mathbf{I}_m & \mathbf{0} \\ -\mathbf{A}_3\mathbf{A}_1^{-1} & \mathbf{I}_n \end{vmatrix} \begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = \begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{0} & (\mathbf{A}_4 - \mathbf{A}_3\mathbf{A}_1^{-1}\mathbf{A}_2) \end{vmatrix} \\ = |\mathbf{A}_1| |\mathbf{A}_4 - \mathbf{A}_3\mathbf{A}_1^{-1}\mathbf{A}_2|$$

## 5. b) Non-singular $\mathbf{A}_4$

$$\begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = \begin{vmatrix} \mathbf{I}_m & -\mathbf{A}_2\mathbf{A}_4^{-1} \\ \mathbf{0} & \mathbf{I}_n \end{vmatrix} \begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = \begin{vmatrix} (\mathbf{A}_1 - \mathbf{A}_2\mathbf{A}_4^{-1}\mathbf{A}_3) & \mathbf{0} \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} \\ = |\mathbf{A}_4| |\mathbf{A}_1 - \mathbf{A}_2\mathbf{A}_4^{-1}\mathbf{A}_3|$$

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## Application of Schur' s Formula to System Polynomial

With coupling due to optimal control, ...

$$\begin{vmatrix} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ \mathbf{Q} & (s\mathbf{I}_n - \mathbf{F}^T) \end{vmatrix} \triangleq \begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix}$$

$$\begin{vmatrix} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ \mathbf{Q} & (s\mathbf{I}_n - \mathbf{F}^T) \end{vmatrix} \triangleq \begin{vmatrix} \mathbf{A}_1 & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{A}_4 \end{vmatrix} = |\mathbf{A}_1| |\mathbf{A}_4 - \mathbf{A}_3\mathbf{A}_1^{-1}\mathbf{A}_2| \\ = |s\mathbf{I}_n - \mathbf{F}| |(s\mathbf{I}_n - \mathbf{F}^T) - \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T|$$

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# Manipulation of Characteristic Determinant

From prior determinant identities, [5. a and 2]

$$\begin{aligned}
 & \left| \begin{array}{cc} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ \mathbf{Q} & (s\mathbf{I}_n + \mathbf{F}^T) \end{array} \right| = \\
 & = |s\mathbf{I}_n - \mathbf{F}| \left| (s\mathbf{I}_n + \mathbf{F}^T) - \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \right| \\
 & = |s\mathbf{I}_n - \mathbf{F}| |s\mathbf{I}_n + \mathbf{F}^T| \left| \mathbf{I}_n - \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T (s\mathbf{I}_n + \mathbf{F}^T)^{-1} \right|
 \end{aligned}$$

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## Application of Schur's Formula

In Schur's formula, [5. a) and 5. b)], choose

$$\mathbf{A}_1 = \mathbf{I}_m; \quad \mathbf{A}_4 = \mathbf{I}_n$$

Then

$$\begin{aligned}
 & \left| \begin{array}{cc} \mathbf{I}_m & \mathbf{A}_2 \\ \mathbf{A}_3 & \mathbf{I}_n \end{array} \right| = |\mathbf{I}_m| |\mathbf{I}_n - \mathbf{A}_3 \mathbf{I}_m^{-1} \mathbf{A}_2| = |\mathbf{I}_n - \mathbf{A}_3 \mathbf{A}_2| \\
 & = |\mathbf{I}_n| |\mathbf{I}_m - \mathbf{A}_2 \mathbf{I}_n^{-1} \mathbf{A}_3| = |\mathbf{I}_m - \mathbf{A}_2 \mathbf{A}_3|
 \end{aligned}$$

$$|\mathbf{I}_n - \mathbf{A}_3 \mathbf{A}_2| = |\mathbf{I}_m - \mathbf{A}_2 \mathbf{A}_3|$$

Application to 3<sup>rd</sup> term in determinant, ...

$$\begin{aligned}
 & \left| \mathbf{I}_n - \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T (s\mathbf{I}_n + \mathbf{F}^T)^{-1} \right| = \\
 & = \left| \mathbf{I}_m + \mathbf{R}^{-1}\mathbf{G}^T (-s\mathbf{I}_n - \mathbf{F}^T)^{-1} \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right|
 \end{aligned}$$

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## Coupled-System Characteristic Equation Retains Mirror Symmetry

... which leads to

$$\begin{aligned}
 & \left| \begin{array}{cc} (s\mathbf{I}_n - \mathbf{F}) & \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T \\ \mathbf{Q} & (s\mathbf{I}_n + \mathbf{F}^T) \end{array} \right| \triangleq \Delta_{\text{CL}}(s)\Delta_{\text{CL}}(-s) \\
 &= \left| s\mathbf{I}_n - \mathbf{F} \right| \left| s\mathbf{I}_n + \mathbf{F}^T \right| \left| \mathbf{I}_n - \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{R}^{-1}\mathbf{G}^T (s\mathbf{I}_n + \mathbf{F}^T)^{-1} \right| \\
 &= (-1)^n \Delta_{\text{OL}}(s)\Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \mathbf{R}^{-1}\mathbf{G}^T (-s\mathbf{I}_n - \mathbf{F}^T)^{-1} \mathbf{Q}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right|
 \end{aligned}$$

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## Output Matrix Derived from State Weighting Matrix

Define

$$\mathbf{Q} = \mathbf{H}^T \mathbf{H}$$

and

$$\Delta \mathbf{y}(t) = \mathbf{H} \Delta \mathbf{x}(t)$$

$$\Delta \mathbf{y}(s) = \mathbf{H} \Delta \mathbf{x}(s)$$

$$\begin{aligned}
 J &= \frac{1}{2} \int_{t_o}^{\infty} [\Delta \mathbf{x}^T(t) \mathbf{Q} \Delta \mathbf{x}(t) + \Delta \mathbf{u}(t) \mathbf{R} \Delta \mathbf{u}^T(t)] dt \\
 &= \frac{1}{2} \int_{t_o}^{\infty} [\Delta \mathbf{x}^T(t) \mathbf{H}^T \mathbf{H} \Delta \mathbf{x}(t) + \Delta \mathbf{u}(t) \mathbf{R} \Delta \mathbf{u}^T(t)] dt \\
 &= \frac{1}{2} \int_{t_o}^{\infty} [\Delta \mathbf{y}^T(t) \Delta \mathbf{y}(t) + \Delta \mathbf{u}(t) \mathbf{R} \Delta \mathbf{u}^T(t)] dt
 \end{aligned}$$

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## Cost Function Transfer Matrix

$$\mathbf{Y}_1(s) = \mathbf{H}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} = \frac{\mathbf{V}_1(s)}{\Delta_{\text{OL}}(s)} \quad \begin{matrix} (r \times m) \\ (1 \times 1) \end{matrix}$$

- **Analogous to regular transfer function matrix**
  - “Output” is “square root” of state integrand term in cost function
  - Numerator reflects relative weighting of state elements
  - Denominator is the uncoupled characteristic polynomial

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## Expression of Characteristic Polynomial Using Cost Function Transfer Matrix

$$\mathbf{Y}_1(s) = \mathbf{H}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} = \frac{\mathbf{V}_1(s)}{\Delta_{\text{OL}}(s)} \quad \begin{matrix} (r \times m) \\ (1 \times 1) \end{matrix}$$

Cost function transfer matrix affects state and adjoint characteristic polynomials

$$\begin{aligned} \Delta_{\text{CL}}(s) \Delta_{\text{CL}}(-s) &= \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \mathbf{R}^{-1} \mathbf{G}^T (-s\mathbf{I}_n - \mathbf{F}^T)^{-1} \mathbf{H}^T \mathbf{H} (s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right| \\ &\triangleq (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \mathbf{R}^{-1} \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \right| \end{aligned}$$

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## Determinant of $\mathbf{Y}_1(s)$

**H** need not be square, but cost observability/detectability criterion must be satisfied to guarantee closed-loop stability

$$\dim(\mathbf{H}) = r \times n \quad (\mathbf{F}, \mathbf{H}) \text{ observable}$$

$$\text{Rank}(\mathbf{H}) = \text{Rank}(\mathbf{Q}) \leq \min(r, n)$$

$$\text{If } \dim(\Delta \mathbf{u}) = m \times 1, \text{ and } r = m$$

$$\text{Then } \mathbf{Y}_1(s) \text{ is square } [r \times m]$$

If  $\mathbf{Y}_1(s)$  is square, it possesses a determinant

$$\begin{aligned} |\mathbf{Y}_1(s)| &= \left| \mathbf{H}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right| = \left| \frac{\mathbf{V}_1(s)}{\Delta_{\text{OL}}(s)} \right| \\ &= \frac{|\mathbf{V}_1(s)|}{|s\mathbf{I}_n - \mathbf{F}|} = \frac{|\mathbf{V}_1(s)|}{|s\mathbf{I}_n - \mathbf{F}|} \\ &\triangleq \frac{\psi_1(s)}{\Delta_{\text{OL}}(s)} \text{ (scalar)} \end{aligned}$$

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## *Transmission Zeros of Cost Function Transfer Matrix*

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## Transmission Zeros of $|Y_1(s)|$

$$|Y_1(s)| = \left| H(sI_n - F)^{-1} G \right| = \frac{|V_1(s)|}{|sI_n - F|}$$

$$\triangleq \frac{\psi_1(s)}{\Delta_{OL}(s)}$$

Roots of the numerator are the **transmission zeros** of  $|Y_1(s)|$

$$\psi_1(s) = a_q s^q + a_{q-1} s^{q-1} + \dots + a_1 s + a_0$$

$$= a_q (s - z_1)(s - z_2) \dots (s - z_q)$$

$$\text{Number of zeros} = q = (n - m - d)$$

$$d = \text{Rank deficiency of } HG$$

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## 2<sup>nd</sup>-Order System Examples of Cost Transfer Function

### • Example 6.4-1 a)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a & 0 \\ 0 & d \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$Y_1(s) = H(sI_n - F)^{-1} G$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} (s-a) & 0 \\ 0 & (s-d) \end{bmatrix}^{-1} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} (s-d) & 0 \\ 0 & (s-a) \end{bmatrix} \begin{bmatrix} \frac{1}{(s-a)} & 0 \\ 0 & \frac{1}{(s-d)} \end{bmatrix}$$

$$|Y_1(s)| = \begin{vmatrix} \frac{1}{(s-a)} & 0 \\ 0 & \frac{1}{(s-d)} \end{vmatrix} = \frac{1}{(s-a)(s-d)} = \frac{\psi_1(s)}{\Delta_{OL}(s)}$$

$\therefore$  **No transmission zeros in system**

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## 2<sup>nd</sup>-Order System Examples of Cost Transfer Function

### Example 6.4-1 (d)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} e \\ f \end{bmatrix} u; \quad y = \begin{bmatrix} g & h \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\begin{aligned} \mathbf{Y}_1(s) &= \frac{(eg + fh)s + [e(hc - gd) + f(gb - ha)]}{\Delta_{OL}(s)} \\ &= \frac{(eg + fh) \left\{ s + \frac{e(hc - gd) + f(gb - ha)}{(eg + fh)} \right\}}{\Delta_{OL}(s)} \\ \text{Zero at } s &= -\frac{[e(hc - gd) + f(gb - ha)]}{(eg + fh)} \end{aligned}$$

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## Scalar Cost Function Multiplier

Use  $|\mathbf{Y}_1(s)|$  in the characteristic polynomial

$$\begin{aligned} \Delta_{CL}(s)\Delta_{CL}(-s) &= (-1)^n \Delta_{OL}(s)\Delta_{OL}(-s) \left| \mathbf{I}_m + \mathbf{R}^{-1} \mathbf{G}^T (-s\mathbf{I}_n - \mathbf{F}^T)^{-1} \mathbf{H}^T \mathbf{H} (s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right| \\ &= (-1)^n \Delta_{OL}(s)\Delta_{OL}(-s) \left| \mathbf{I}_m + \mathbf{R}^{-1} \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \right| \end{aligned}$$

Scalar multiplier for control weighting matrix

$$\text{Define } \mathbf{R} = \rho^2 \mathbf{R}_o$$

Closed-loop characteristic polynomial

$$\begin{aligned} \Delta_{CL}(s)\Delta_{CL}(-s) &= \\ &= (-1)^n \Delta_{OL}(s)\Delta_{OL}(-s) \left| \mathbf{I}_m + (\rho^2 \mathbf{R}_o)^{-1} \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \right| \\ &= (-1)^n \Delta_{OL}(s)\Delta_{OL}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{R}_o^{-1} \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \right| \end{aligned}$$

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## Weighted Cost Function Transfer Matrix, $\mathbf{Y}_2(s)$

Square root of control weight inverse

$$\text{Define } \mathbf{U}^T \mathbf{U} = \mathbf{R}_o^{-1}$$

Incorporate  $\mathbf{U}$  in definition of  $|\mathbf{Y}_2(s)|$

$$\begin{aligned} \mathbf{Y}_2(s) &\triangleq \mathbf{Y}_1(s) \mathbf{U} \\ &= \mathbf{H}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \mathbf{U} = \frac{\mathbf{V}_2(s)}{\Delta_{\text{OL}}(s)} \quad (r \times m) \end{aligned}$$

Closed-loop characteristic polynomial

$$\begin{aligned} \Delta_{\text{coupled}}(s) &= \Delta_{\text{CL}}(s) \Delta_{\text{CL}}(-s) = \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{U}^T \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \mathbf{U} \right| \\ &\triangleq (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{Y}_2^T(-s) \mathbf{Y}_2(s) \right| \end{aligned}$$

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*Effects of Cost  
Function Weights on  
Root Locations*

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# Variations in Cost Function Transfer Matrix

- Open-loop poles are independent of **Q** and **R**
- Q** and **R<sub>o</sub>** specify locations of transmission zeros

$$\mathbf{Q} = \mathbf{H}^T \mathbf{H}; \quad \mathbf{R}_o^{-1} = \mathbf{U}^T \mathbf{U}$$

$$\mathbf{Y}_2(s) = \mathbf{H}(s\mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \mathbf{U} = \frac{\mathbf{V}_2(s)}{\Delta_{OL}(s)}$$

$$|\mathbf{Y}_2(s)| = \frac{|\mathbf{V}_2(s)|}{|s\mathbf{I}_n - \mathbf{F}|} \triangleq \frac{\psi_2(s)}{\Delta_{OL}(s)} \text{ (scalar)}$$

- Roots of characteristic equation vary with  $1/\rho^2$

$$\begin{aligned} \Delta_{\text{coupled}}(s) &= \Delta_{\text{CL}}(s) \Delta_{\text{CL}}(-s) \\ &= (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{U}^T \mathbf{Y}_1^T(-s) \mathbf{Y}_1(s) \mathbf{U} \right| \\ &\triangleq (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{Y}_2^T(-s) \mathbf{Y}_2(s) \right| \end{aligned}$$

## Coupled-System Eigenvalues

Roots of characteristic equation vary with  $1/\rho^2$

$$\begin{aligned} (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{Y}_2^T(-s) \mathbf{Y}_2(s) \right| &\xrightarrow{\rho^2 \rightarrow \infty} (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) |\mathbf{I}_m| \\ &= (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) \end{aligned}$$

Open-loop system roots may be stable or unstable

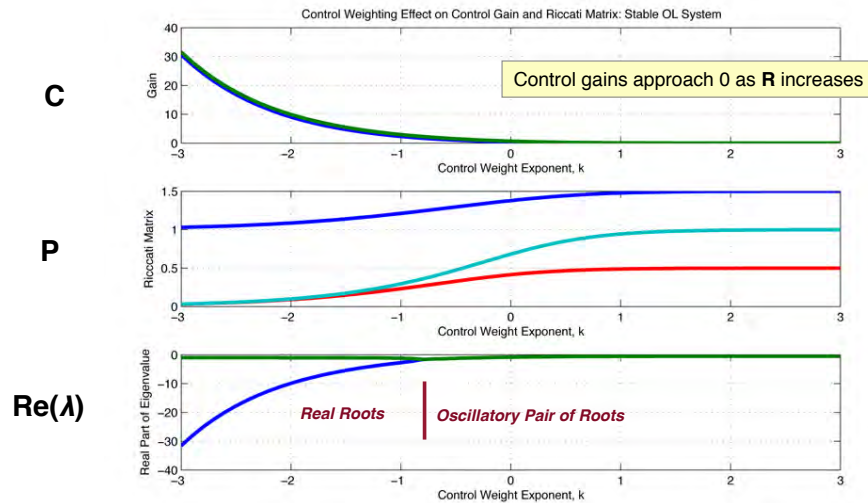
$$\begin{aligned} \Delta_{\text{coupled}}(s) &= s^{2n} + a_{2n-1}s^{2n-1} + \dots + a_1s + a_o \\ &= (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_{2n}) \\ &= (-1)^n [(s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_n)]_{OL} [(s + \lambda_1)(s + \lambda_2) \dots (s + \lambda_n)]_{OL} = 0 \end{aligned}$$

But we know that the all closed-loop system roots must be stable

## Control Weighting Effect for Stable 2<sup>nd</sup>-Order System

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$\mathbf{Q} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}; \quad \mathbf{R} = r \text{ in } (10^{-3}, 10^3)$$

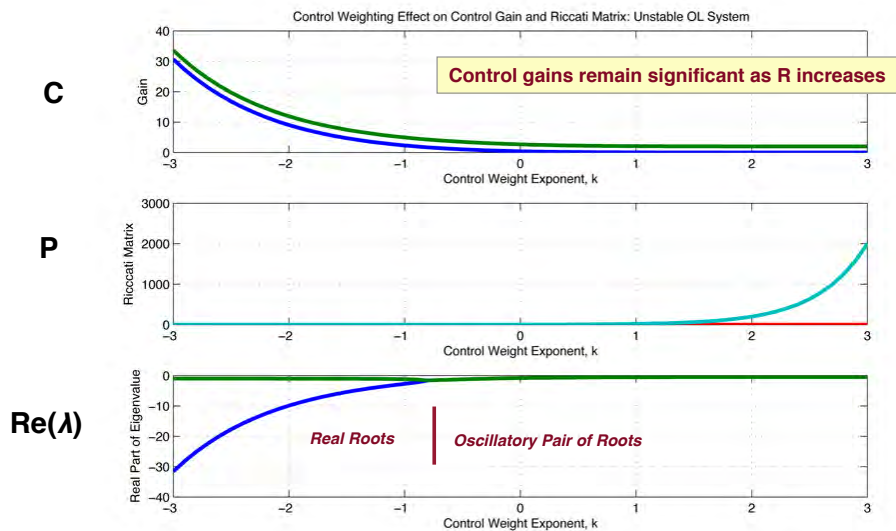


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## Control Weighting Effect for Unstable 2<sup>nd</sup>-Order System

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

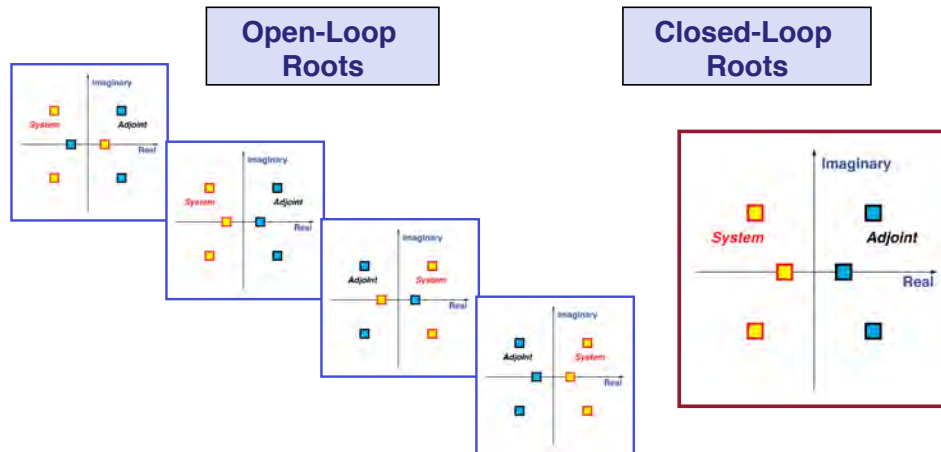
$$\mathbf{Q} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}; \quad \mathbf{R} = r \text{ in } (10^{-3}, 10^3)$$



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# All Closed-Loop System State Roots Go To Stable Images as $\rho^2 \rightarrow \infty$



All closed-loop **adjoint-system roots** are in right half plane

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## What Happens to the Roots when $\rho^2 \rightarrow \infty$ ?

Closed-loop characteristic polynomial

$$\Delta_{\text{coupled}}(s) = (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| \mathbf{I}_m + \frac{1}{\rho^2} \mathbf{Y}_2^T(-s) \mathbf{Y}_2(s) \right|$$

$$\dim[\mathbf{Y}_2(s)] = r \times m$$

Consider case in which  $r = m$ , i.e.,  $\mathbf{Y}_2(s)$  is square

$|\mathbf{Y}_2(s)|$  possesses a determinant

$$|\mathbf{Y}_2(s)| = \frac{\psi_2(s)}{\Delta_{\text{OL}}(s)}$$

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## Characteristic Polynomial of Scalar Coupled System

Let  $r = m = 1$

$$\left| \mathbf{Y}_2(s) \right| = \frac{\left| \mathbf{V}_2(s) \right|}{\Delta_{\text{OL}}(s)} = Y_2(s) = \frac{\psi_2(s)}{\Delta_{\text{OL}}(s)}$$

Closed-loop characteristic polynomial

$$\begin{aligned} \Delta_{\text{coupled}}(s) &= \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left| 1 + \frac{1}{\rho^2} Y_2(-s) Y_2(s) \right| \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left[ 1 + \frac{1}{\rho^2} Y_2(-s) Y_2(s) \right] \end{aligned}$$

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## Characteristic Polynomial of Scalar Coupled System

Closed-loop characteristic polynomial

$$\begin{aligned} \Delta_{\text{coupled}}(s) &= \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) \left[ 1 + \left( \frac{1}{\rho^2} \right) \frac{\psi_2(-s) \psi_2(s)}{(-1)^n \Delta_{\text{OL}}(-s) \Delta_{\text{OL}}(s)} \right] \\ &= (-1)^n \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) + \left( \frac{1}{\rho^2} \right) \psi_2(-s) \psi_2(s) \end{aligned}$$

Numerator polynomial multiplied by  $(-1)^q$

$$\begin{aligned} \psi_2(s) &= a_q (s - z_1)(s - z_2) \cdots (s - z_q) \\ \psi_2(-s) &= (-1)^q a_q (s + z_1)(s + z_2) \cdots (s + z_q) \end{aligned}$$

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## Significance of Powers of $(-1)$

Denominator polynomial multiplied by  $(-1)^n$

$$\begin{aligned} & (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) = \\ & = (-1)^n [(s - \lambda_1)(s - \lambda_2) \cdots (s - \lambda_n)] [(s + \lambda_1)(s + \lambda_2) \cdots (s + \lambda_n)] \end{aligned}$$

Closed-loop characteristic polynomial

$$\begin{aligned} \Delta_{\text{coupled}}(s) &= (-1)^n \Delta_{OL}(s) \Delta_{OL}(-s) \\ &+ (-1)^q \left( \frac{a_q^2}{\rho^2} \right) [(s + z_1)(s + z_2) \cdots (s + z_q)] [(s - z_1)(s - z_2) \cdots (s - z_q)] \end{aligned}$$

Mirror-image poles and zeros

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## Characteristic Polynomial of the Coupled System Can Be Put In Root-Locus Form

Because characteristic polynomial equals zero,  $(-1)^n$  multiplier can be discarded in the solution for roots

$$\begin{aligned} & (-1)^{-n} \Delta_{\text{coupled}}(s) = 0 = \Delta_{\text{coupled}}(s) \\ & = \Delta_{OL}(s) \Delta_{OL}(-s) + (-1)^{(q-n)} \left( \frac{a_q^2}{\rho^2} \right) [(s + z_1)(s + z_2) \cdots (s + z_q)] [(s - z_1)(s - z_2) \cdots (s - z_q)] \\ & \triangleq D(s) + KN(s) \quad \text{[Root locus form]} \end{aligned}$$

Poles and zeros of the coupled system's root locus are symmetric about the imaginary axis

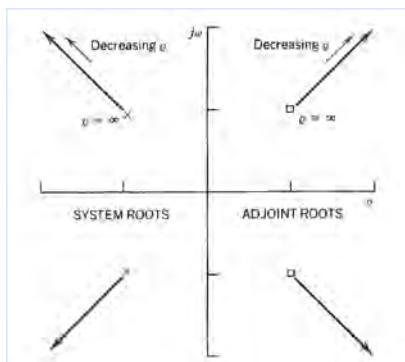
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# Root Locus Analysis of the Coupled State/Adjoint System

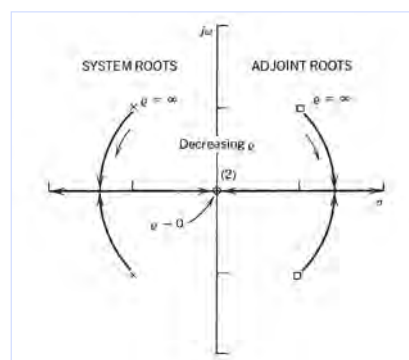
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## Optimal Closed-Loop Root Loci of Two 2<sup>nd</sup>-Order Systems

Complex Roots, No Transmission Zero



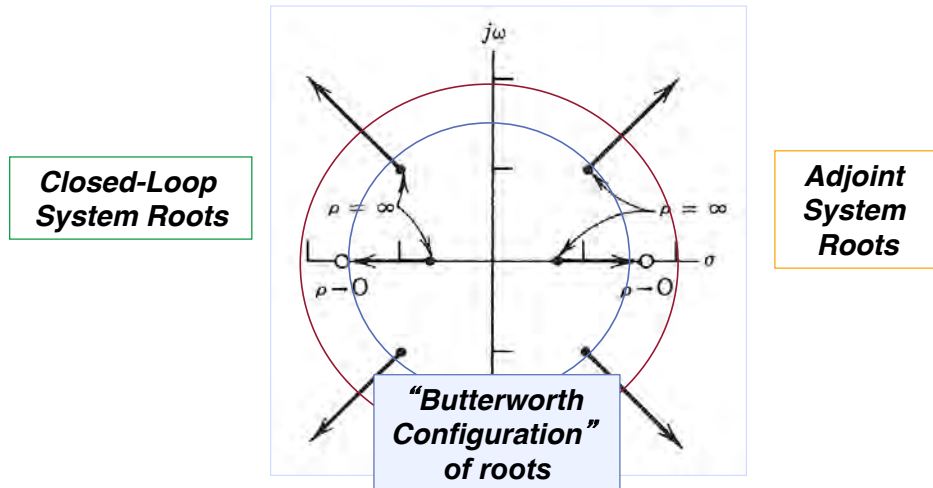
Complex Roots, One Transmission Zero



“Center of gravity” is **always** at the **origin** for state/adjoint root locus  
 Roots originating in the left/right half plane **remain** in the left/right half plane  
**ROOT LOCUS IS SYMMETRIC ABOUT THE IMAGINARY AXIS**  
 Closed-loop system is **stable** for all values of  $\rho$

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# Optimal Closed-Loop Root Locus of 3<sup>rd</sup>-Order System with One Transmission Zero



Closed-loop system is stable for all values of  $\rho$

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## *Eigenvectors*

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# Eigenvectors

## Eigenvalues of square matrix, **F**

$$\begin{aligned} |s\mathbf{I} - \mathbf{F}| &= \Delta(s) = \\ &= (s - \lambda_1)(s - \lambda_2) \cdots (s - \lambda_n) = 0 \end{aligned}$$

## Eigenvectors of **F**

Defined within an arbitrary constant

Constant may be real or complex

$$\begin{aligned} (\lambda_i \mathbf{I} - \mathbf{F}) \mathbf{e}_i &= 0, \quad i = 1, n \\ (\lambda_i \mathbf{I} - \mathbf{F}) \alpha \mathbf{e}_i &= 0 \end{aligned}$$

$$\dim(\mathbf{e}_i) = n \times 1$$

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## Computation of Eigenvectors and the Modal Matrix

Calculation of each eigenvector typically produces ***n*** linearly dependent columns related by multiplicative constants

$$Adj(\lambda_i \mathbf{I} - \mathbf{F}) = \begin{bmatrix} \beta_1 \mathbf{e}_i & \beta_2 \mathbf{e}_i & \cdots & \beta_n \mathbf{e}_i \end{bmatrix}, \quad i = 1, n$$

## **E**: Modal Matrix of **F**

One eigenvector for each eigenvalue forms a column of **E**

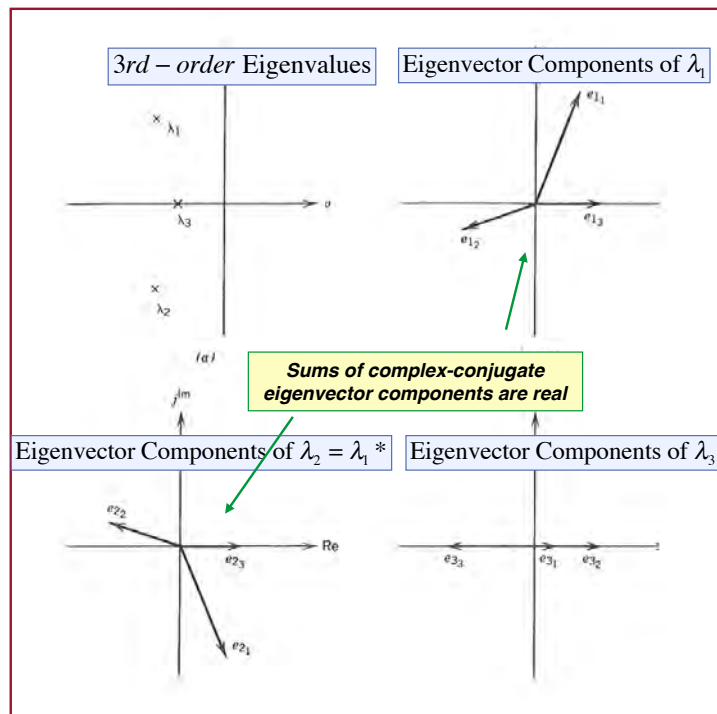
**E** is normalized appropriately, e.g.,  $|\mathbf{e}_i| = 1$  or  $|\mathbf{E}| = 1$

$$\mathbf{E} = \begin{bmatrix} \mathbf{e}_1 & \mathbf{e}_2 & \cdots & \mathbf{e}_n \end{bmatrix}; \quad \dim(\mathbf{E}) = n \times n$$

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# Complex Eigenvectors

- If eigenvalues are complex, then corresponding eigenvectors are complex
- If eigenvalues are complex conjugates, then corresponding eigenvectors are complex conjugates



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## Property of the Modal Matrix, **E**

Each eigenvector satisfies the following

$$\begin{bmatrix} \mathbf{F}\mathbf{e}_1 = \lambda_1\mathbf{e}_1 \\ \mathbf{F}\mathbf{e}_2 = \lambda_2\mathbf{e}_2 \\ \dots \\ \mathbf{F}\mathbf{e}_n = \lambda_n\mathbf{e}_n \end{bmatrix} \Rightarrow \mathbf{F}\mathbf{E} = \mathbf{E}\mathbf{\Lambda}$$

Diagonal matrix of eigenvalues

$$\mathbf{\Lambda} = \begin{bmatrix} \lambda_1 & 0 & \dots & 0 \\ 0 & \lambda_2 & \dots & 0 \\ \dots & \dots & \dots & \dots \\ 0 & 0 & \dots & \lambda_n \end{bmatrix}$$

# Modal Matrix, **E**, Can Be Used as a Similarity Transformation to “Diagonalize” **F**

If **F** is real and symmetric

Eigenvectors are real

**E** is an orthonormal transformation

Transpose = Inverse

$$\Lambda = \mathbf{E}^T \mathbf{F} \mathbf{E}$$

$$\mathbf{F} = \mathbf{E} \Lambda \mathbf{E}^T$$

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## 2<sup>nd</sup>-Order Example

$$\mathbf{F} = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\zeta\omega_n \end{bmatrix}; \quad [s\mathbf{I} - \mathbf{F}] = \begin{bmatrix} s & -1 \\ \omega_n^2 & (s + 2\zeta\omega_n) \end{bmatrix}$$

$$\Delta(s) = |s\mathbf{I} - \mathbf{F}| = s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

$$\lambda_{1,2} = -\zeta\omega_n \pm \sqrt{(\zeta\omega_n)^2 - \omega_n^2}$$

For  $\zeta > 1$ , roots are real

$$\begin{aligned} \lambda_{1,2} &= -\zeta\omega_n \pm \sqrt{(\zeta\omega_n)^2 - \omega_n^2} \\ &= -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1} \end{aligned}$$

For  $\zeta < 1$ , roots are complex

$$\begin{aligned} \lambda_{1,2} &= -\zeta\omega_n \pm \sqrt{(\zeta\omega_n)^2 - \omega_n^2} \\ &= -\zeta\omega_n \pm j\omega_n \sqrt{1 - \zeta^2}, \quad j = \sqrt{-1} \\ &= \text{Complex conjugates, } \lambda_1, \lambda_1^* \end{aligned}$$

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## Eigenvectors for 2<sup>nd</sup>-Order Example

$$\begin{aligned}
 Adj[\lambda_i \mathbf{I} - \mathbf{F}] &= Adj \begin{bmatrix} \lambda_i & -1 \\ \omega_n^2 & (\lambda_i + 2\zeta\omega_n) \end{bmatrix} \\
 &= \begin{bmatrix} (\lambda_i + 2\zeta\omega_n) & 1 \\ -\omega_n^2 & \lambda_i \end{bmatrix} \\
 &\triangleq \begin{bmatrix} \beta_1 \mathbf{e}_i & \beta_2 \mathbf{e}_i \end{bmatrix}, \quad i = 1, 2
 \end{aligned}$$

Each column is a representation of the eigenvector

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## 2<sup>nd</sup>-Order Example with Real Roots

$$Adj[\lambda_i \mathbf{I} - \mathbf{F}] = \begin{bmatrix} \left( -\zeta\omega_n \left( 1 \mp \sqrt{1 - \frac{1}{\zeta^2}} \right) + 2\zeta\omega_n \right) & 1 \\ -\omega_n^2 & -\zeta\omega_n \left( 1 \mp \sqrt{1 - \frac{1}{\zeta^2}} \right) \end{bmatrix}$$

$$\mathbf{E} = \begin{bmatrix} 1 & 1 \\ -\zeta\omega_n \left( 1 - \sqrt{1 - \frac{1}{\zeta^2}} \right) & -\zeta\omega_n \left( 1 + \sqrt{1 - \frac{1}{\zeta^2}} \right) \end{bmatrix}$$

**Modal Matrix**

$$\mathbf{\Lambda} = \begin{bmatrix} -\zeta\omega_n \left( 1 - \sqrt{1 - \frac{1}{\zeta^2}} \right) & 0 \\ 0 & -\zeta\omega_n \left( 1 + \sqrt{1 - \frac{1}{\zeta^2}} \right) \end{bmatrix}$$

**Eigenvalues**

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# *Eigenvectors of Regulated Systems*

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## Example with Single Control Variable

$$\begin{aligned} |s\mathbf{I}_n - (\mathbf{F} - \mathbf{G}\mathbf{C})| &= 0 \\ n \text{ eigenvalues} \\ 1 \times n \text{ elements of } \mathbf{C} \end{aligned}$$

- State equation and control law

$$\begin{aligned} \begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \end{bmatrix} &= \begin{bmatrix} f_1 & 0 \\ 0 & f_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} + \begin{bmatrix} g_1 \\ g_2 \end{bmatrix} \Delta u_1 \\ \Delta u_1 &= - \begin{bmatrix} c_1 & c_2 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} \end{aligned}$$

- Closed-loop system dynamics

$$\begin{aligned} \begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \end{bmatrix} &= \begin{bmatrix} f_1 & 0 \\ 0 & f_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} - \begin{bmatrix} g_1 \\ g_2 \end{bmatrix} \begin{bmatrix} c_1 & c_2 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} \\ &= \begin{bmatrix} (f_1 - g_1 c_1) & -g_1 c_2 \\ -g_2 c_1 & (f_4 - g_2 c_2) \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} \end{aligned}$$

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# Eigenvalues and Eigenvectors

Relationship between **eigenvalues** and elements of **C** is unique  
2 parameters, 2 unknowns

$$\left\{ s \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} - \begin{bmatrix} f_1 - g_1 c_1 & -g_1 c_2 \\ -g_2 c_1 & f_4 - g_2 c_2 \end{bmatrix} \right\} = \begin{bmatrix} s - (f_1 - g_1 c_1) & g_1 c_2 \\ g_2 c_1 & s - (f_4 - g_2 c_2) \end{bmatrix}$$

$$= [s - (f_1 - g_1 c_1)][s - (f_4 - g_2 c_2)] + g_1 c_2 g_2 c_1$$

$$= s^2 - [(f_1 - g_1 c_1) + (f_4 - g_2 c_2)]s + [g_1 c_2 g_2 c_1 + (f_1 - g_1 c_1)(f_4 - g_2 c_2)]$$

$$= (s - \lambda_1)(s - \lambda_2) = s^2 - (\lambda_1 + \lambda_2)s + \lambda_1 \lambda_2 = 0$$

Relationship between **eigenvector components** and elements of **C** is unique

$$Adj[\lambda_i \mathbf{I} - (\mathbf{F} - \mathbf{G}\mathbf{C})] = Adj \begin{bmatrix} [\lambda_i - (f_1 - g_1 c_1)] & g_1 c_2 \\ g_2 c_1 & \lambda_i - (f_4 - g_2 c_2) \end{bmatrix}$$

$$\triangleq \begin{bmatrix} \beta_1 \mathbf{e}_i & \beta_2 \mathbf{e}_i \end{bmatrix}$$

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$$|s\mathbf{I}_n - (\mathbf{F} - \mathbf{G}\mathbf{C})| = 0$$

$n$  eigenvalues  
 $2 \times n$  elements of **C**

## Example with Two Control Variables

- State equation and control law

$$\begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \end{bmatrix} = \begin{bmatrix} f_1 & 0 \\ 0 & f_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \Delta u_1 \\ \Delta u_2 \end{bmatrix}$$

$$\begin{bmatrix} \Delta u_1 \\ \Delta u_2 \end{bmatrix} = - \begin{bmatrix} c_1 & c_2 \\ c_3 & c_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

- Closed-loop system dynamics

$$\begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \end{bmatrix} = \begin{bmatrix} f_1 & 0 \\ 0 & f_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} - \begin{bmatrix} c_1 & c_2 \\ c_3 & c_4 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

$$= \begin{bmatrix} (f_1 - c_1) & c_2 \\ c_3 & (f_4 - c_4) \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix}$$

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# Eigenvalues and Eigenvectors

Relationship between **eigenvalues** and elements of **C** is not unique

2 parameters, 4 unknowns

$$\left\{ s \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} - \begin{bmatrix} (f_1 - c_1) & c_2 \\ c_3 & (f_4 - c_4) \end{bmatrix} \right\} = \begin{bmatrix} s - (f_1 - c_1) & -c_2 \\ -c_3 & s - (f_4 - c_4) \end{bmatrix}$$

$$= [s - (f_1 - c_1)][s - (f_4 - c_4)] + c_2 c_3 = 0 = s^2 - [(f_1 - c_1) + (f_4 - c_4)]s + [c_2 c_3 + (f_1 - c_1)(f_4 - c_4)]$$

$$= (s - \lambda_1)(s - \lambda_2) = s^2 - (\lambda_1 + \lambda_2)s + \lambda_1 \lambda_2 = 0$$

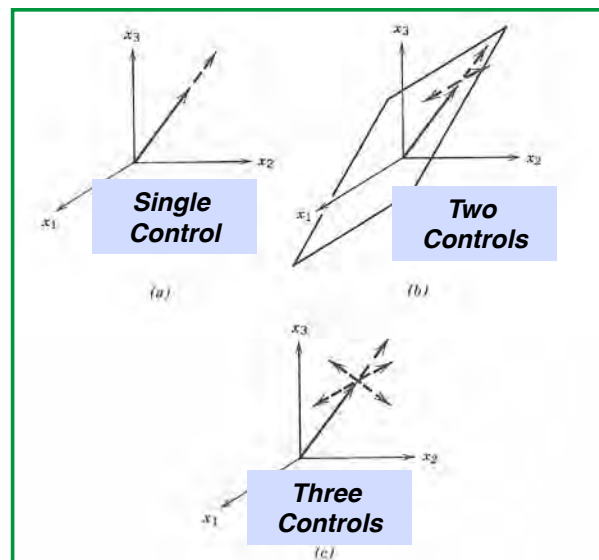
Relationship between **eigenvectors** and elements of **C** is not unique

$$Adj[\lambda_i \mathbf{I} - (\mathbf{F} - \mathbf{G}\mathbf{C})] = Adj \begin{bmatrix} \lambda_i - (f_1 - c_1) & -c_2 \\ -c_3 & \lambda_i - (f_4 - c_4) \end{bmatrix}$$

$$\triangleq \begin{bmatrix} \beta_1 \mathbf{e}_i & \beta_2 \mathbf{e}_i \end{bmatrix}$$

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## Eigenvectors Can Be Placed within an $m$ -Space, $m \leq n$



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# Modal Control Vector

$$\Delta \mathbf{u}_i = -\mathbf{C}\Delta \mathbf{x}_i, \quad i = 1, n$$

State eigenvector

$$\left[ s_i \mathbf{I}_n - (\mathbf{F} - \mathbf{G}\mathbf{C}) \right] \Delta \mathbf{x}_i = \mathbf{0}, \quad i = 1, n$$

Modal control vector of an eigenvalue's state eigenvector

$$(s_i \mathbf{I}_n - \mathbf{F}) \Delta \mathbf{x}_i = \mathbf{G} \Delta \mathbf{u}_i = -\mathbf{G}\mathbf{C} \Delta \mathbf{x}_i = \mathbf{0}, \quad i = 1, n$$

Eigenvector satisfies the following equation

$$\begin{aligned} \Delta \mathbf{x}_i &= -(s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{C} \Delta \mathbf{x}_i \\ \left[ \mathbf{I}_n + (s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{C} \right] \Delta \mathbf{x}_i &= \mathbf{0} \end{aligned}$$

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# Modal Control Vector

Modal control vector satisfies a similar equation

$$\begin{aligned} \Delta \mathbf{u}_i &= -\mathbf{C}\Delta \mathbf{x}_i = -\mathbf{C}(s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \Delta \mathbf{u}_i \\ \left[ \mathbf{I}_m + \mathbf{C}(s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right] \Delta \mathbf{u}_i &= \mathbf{0} \end{aligned}$$

Eigenvector and modal control vector equations have the same eigenvalues

$$\begin{aligned} \text{Because } |\mathbf{I}_n - \mathbf{A}_3 \mathbf{A}_2| &= |\mathbf{I}_m - \mathbf{A}_2 \mathbf{A}_3| \\ \left| \mathbf{I}_n + (s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G}\mathbf{C} \right| &= \left| \mathbf{I}_m + \mathbf{C}(s_i \mathbf{I}_n - \mathbf{F})^{-1} \mathbf{G} \right| \end{aligned}$$

State eigenvector can be adjusted in a space with a dimension of Rank (**C**)

$$\text{Rank}(\mathbf{C}) \leq \min(m, n)$$

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***Next Time:***  
***Spectral Analysis of Linear-  
Quadratic Regulators***

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***Supplemental  
Material***

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## 2<sup>nd</sup>-Order System Examples of Cost Transfer Function

- Example 6.4-1 b)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}; \quad \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\mathbf{Y}_1(s) = \frac{\begin{bmatrix} (s-d) & b \\ c & (s-a) \end{bmatrix}}{[s^2 - (a+d)s + (ad-bc)]}$$

$$\|\mathbf{Y}_1(s)\| = \frac{[s^2 - (a+d)s + (ad-bc)]}{[s^2 - (a+d)s + (ad-bc)]^2} = \frac{1}{[s^2 - (a+d)s + (ad-bc)]}$$

$\therefore$  No transmission zeros in system

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## 2<sup>nd</sup>-Order System Examples of Cost Transfer Function

- Example 6.4-1 c)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a & 0 \\ c & d \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}; \quad \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

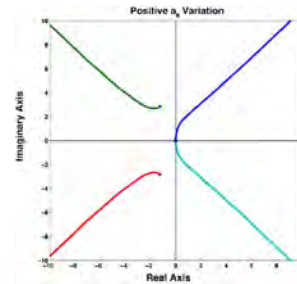
$$\mathbf{Y}_1(s) = \frac{\begin{bmatrix} (s-d)+c & (s-a) \\ c & (s-a) \end{bmatrix}}{(s-a)(s-d)}$$

$$\|\mathbf{Y}_1(s)\| = \frac{[s^2 - (a+d)s + ad]}{[(s-a)(s-d)]^2} = \frac{1}{[s^2 - (a+d)s + (ad)]}$$

$\therefore$  No transmission zeros in system

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# Root Locus Construction Rules



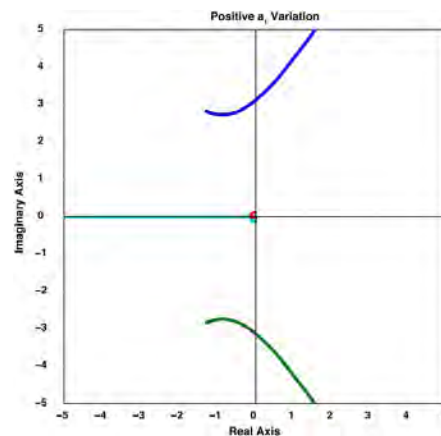
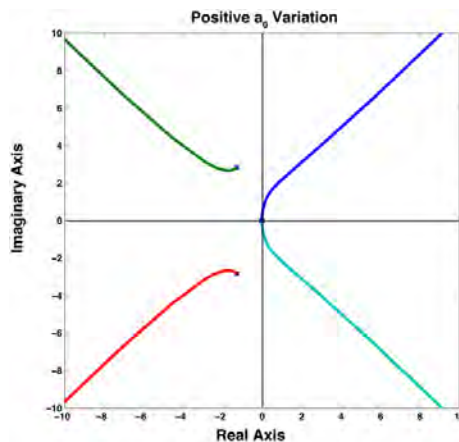
- All points on the locus of roots must satisfy the equation  $K[N(s)/D(s)] = -1$ 
  - Phase angle of transfer function =  $-180$  deg
- Number of roots (or *poles*) of the denominator =  $n$
- Number of zeros of the numerator =  $q$

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## Origins of Roots (for $K = 0$ )

- Origins of the roots are the Poles of  $D(s)$

$$\Delta(s) = D(s) + KN(s) \xrightarrow{K \rightarrow 0} D(s)$$



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## Destinations of Roots (for $K \rightarrow \pm\infty$ )

$q$  roots go to the zeros of  $N(s)$

$$\frac{D(s) + KN(s)}{K} = \frac{D(s)}{K} + N(s) \xrightarrow{K \rightarrow \infty} N(s)$$

$(n - q)$  roots go to infinite radius from the origin

$$\frac{D(s) + KN(s)}{N(s)} = \frac{D(s)}{N(s)} + K \xrightarrow{K \rightarrow \infty} s^{(n-q)} \pm R \rightarrow \pm\infty$$

$$s^{(n-q)} = (R)e^{-j180^\circ} \rightarrow \infty \quad \text{or} \quad (R)e^{-j360^\circ} \rightarrow -\infty$$

which leads to

$$s = (R)e^{-j180^\circ/(n-q)} \rightarrow \infty \quad \text{or} \quad (R)e^{-j360^\circ/(n-q)} \rightarrow -\infty$$

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## Three More Root Locus Construction Rules

Angles of asymptotes for the  $(n - q)$  roots going to  $\infty$

$$\begin{aligned} K \rightarrow +\infty: \quad \theta(\text{rad}) &= \frac{\pi + 2k\pi}{n - q}, \quad k = 0, 1, \dots, (n - q) - 1 \\ K \rightarrow -\infty: \quad \theta(\text{rad}) &= \frac{2k\pi}{n - q}, \quad k = 0, 1, \dots, (n - q) - 1 \end{aligned}$$

Origin of asymptotes = "center of gravity"

$$\text{"c.g."} = \frac{\sum_{i=1}^n \sigma_{\lambda_i} - \sum_{j=1}^q \sigma_{z_j}}{n - q}$$

Locus on real axis

$K > 0$ : Any segment with odd number of poles and zeros to the right

$K < 0$ : Any segment with even number of poles and zeros to the right

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# Characteristic Polynomial of the Coupled System, Root-Locus Form

When entire characteristic polynomial is multiplied by  $(-1)^n$ ,  
Numerator multiplier is  $(-1)^{(n-q)}$

$$\Delta_{\text{coupled}}(s) = (-1)^n \left\{ \Delta_{\text{OL}}(s) \Delta_{\text{OL}}(-s) + (-1)^{(q-n)} \left( \frac{a_q^2}{\rho^2} \right) \left[ (s+z_1)(s+z_2) \cdots (s+z_q) \right] \left[ (s-z_1)(s-z_2) \cdots (s-z_q) \right] \right\} = 0$$

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## $K$ , $D(s)$ , and $N(s)$ of the Root Locus Equation

Sign of root locus gain depends on  $(-1)^{(q-n)}$

$$\begin{aligned} & (-1)^{-n} \Delta_{\text{coupled}}(s) = 0 \\ & = \left[ (s-\lambda_1)(s-\lambda_2) \cdots (s-\lambda_n) \right] \left[ (s+\lambda_1)(s+\lambda_2) \cdots (s+\lambda_n) \right] \\ & + (-1)^{(q-n)} \left( \frac{a_q^2}{\rho^2} \right) \left[ (s+z_1)(s+z_2) \cdots (s+z_q) \right] \left[ (s-z_1)(s-z_2) \cdots (s-z_q) \right] \\ & \triangleq D(s) + KN(s) \end{aligned}$$

where

$$K = (-1)^{(q-n)} \left( \frac{a_q^2}{\rho^2} \right)$$

$$D(s) = \left[ (s-\lambda_1)(s-\lambda_2) \cdots (s-\lambda_n) \right] \left[ (s+\lambda_1)(s+\lambda_2) \cdots (s+\lambda_n) \right]$$

$$N(s) = \left[ (s+z_1)(s+z_2) \cdots (s+z_q) \right] \left[ (s-z_1)(s-z_2) \cdots (s-z_q) \right]$$

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