1 Leitungsgleichungen

a)

$$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}$$
(1)

$$\underline{Z}_W = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}$$
 (2)

$$P_{nat} = \frac{U_n^2}{Z_W} \tag{3}$$

b)

$$R_L = \frac{U_n^2}{P_L} \tag{4}$$

c)

$$\underline{S}_1 = \underline{U}_1 \underline{I}_1^* = \underline{U}_1 \frac{\underline{U}_1^*}{\underline{Z}_W^*} = \frac{U_n^2}{\underline{Z}_W^*}$$
 (5)

d)

$$\underline{U}_{1} = \cosh\left(\gamma l\right)\underline{U}_{2} + \sinh\left(\gamma l\right)\underline{Z}_{W}\underline{I}_{2} \tag{6}$$

$$= \cosh\left(\underline{\gamma}l\right)\underline{U}_2 + \sinh\left(\underline{\gamma}l\right)\underline{Z}_W \frac{\underline{U}_2}{R_L} \tag{7}$$

$$\underline{U}_{2} = \frac{\underline{U}_{1}}{\cosh(\gamma l) + \sinh(\gamma l) \frac{\underline{Z}_{W}}{R_{L}}}$$
(8)

e)

$$\underline{U}_1 = \cosh(\gamma l) \, \underline{U}_2 + \sinh(\gamma l) \, \underline{Z}_W \underline{I}_2 \tag{9}$$

$$= \cosh\left(\underline{\gamma}l\right) 0.9 \,\underline{\mathbf{U}}_1 + \sinh\left(\underline{\gamma}l\right) \,\underline{Z}_W \frac{0.9 \,\underline{\mathbf{U}}_1}{\underline{Z}_2} \tag{10}$$

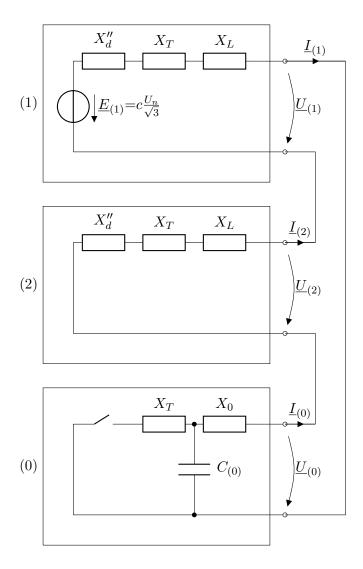
$$\sinh\left(\underline{\gamma}l\right)\underline{Z}_{W}\frac{0.9\,\underline{\mathbf{U}}_{1}}{\underline{Z}_{2}} = \underline{U}_{1} - \cosh\left(\underline{\gamma}l\right)0.9\,\underline{\mathbf{U}}_{1} \tag{11}$$

$$\underline{Z}_{2} = \frac{\sinh\left(\underline{\gamma}l\right)\underline{Z}_{W}0,9\,\underline{\mathbf{U}}_{1}}{\underline{U}_{1} - \cosh\left(\gamma l\right)0,9\,\underline{\mathbf{U}}_{1}} \tag{12}$$

f)

2 Ein- und zweipoliger Kurzschluss

a)



b)

$$X_d'' = x_d'' \frac{U_2^2}{S_N}$$

$$X_T = u_k \frac{U_2^2}{S_N}$$
(13)

$$X_T = u_k \frac{U_2^2}{S_N} \tag{14}$$

$$X_L = \omega L_B' l \tag{15}$$

$$C_{(0)} = C_E' l \tag{16}$$

$$\underline{I}_{(1)} = \frac{c\frac{U_n}{\sqrt{3}}}{2j\left(X_d'' + X_T + X_L\right) + jX_0 + \frac{1}{j\omega C_{(0)}}}$$
(17)

$$\underline{I}_{k1p}^{"} = \underline{I}_a = \underline{I}_{(0)} + \underline{I}_{(1)} + \underline{I}_{(2)} = 3\underline{I}_{(1)}$$

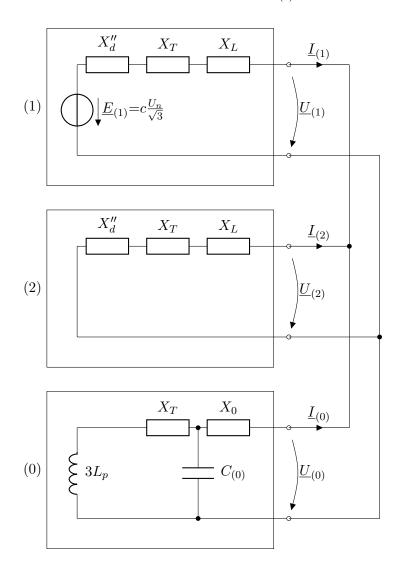
$$\tag{18}$$

c)

$$j\omega 3L_p + jX_T + \frac{1}{j\omega C_{(0)}} = 0$$

$$L_p = \frac{1}{3\omega^2 C_{(0)}} - \frac{X_T}{3\omega}$$
(20)

$$L_p = \frac{1}{3\omega^2 C_{(0)}} - \frac{X_T}{3\omega} \tag{20}$$



d)

e)

$$\underline{I}_{(0)} = 0 \,\mathrm{A} \tag{21}$$

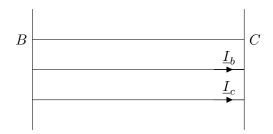
$$\underline{I}_{(1)} = -\underline{I}_{(2)} = \frac{c\frac{U_n}{\sqrt{3}}}{2j\left(X_d'' + X_T + X_L\right)}$$
(22)

$$\underline{I}_b = \underline{I}_{(0)} + \underline{a}^2 \underline{I}_{(1)} + \underline{a}\underline{I}_{(2)} = \left(\underline{a}^2 - \underline{a}\right)\underline{I}_{(1)} = -j\sqrt{3}\underline{I}_{(1)}$$
(23)

$$\underline{I}_c = \underline{I}_{(0)} + \underline{a}\underline{I}_{(1)} + \underline{a}^2\underline{I}_{(2)} = \left(\underline{a} - \underline{a}^2\right)\underline{I}_{(1)} = \mathrm{j}\sqrt{3}\underline{I}_{(1)}$$
(24)

(26)

f) In der Skizze sind die wahren Flussrichtungen und nicht die Orientierungen eingezeichnet.



3 A Transformator

a) $R_k = P_k \frac{U_2^2}{S_N^2}$ (25)

b)
$$P_L = G_L U_L^2 \tag{26}$$

$$G_L = \frac{P_L}{U_r^2} = \frac{P_L}{U_2^2} \tag{27}$$

$$Q_L = -B_L U_L^2 \tag{28}$$

$$S_L = U_L I_L = U_N I_N \cdot 0.25 \% = S_N \cdot 0.25 \%$$
(29)

$$Q_L = \sqrt{S_L^2 - P_L^2} (30)$$

$$B_L = -\frac{Q_L}{U_L^2} \tag{31}$$

$$Z_k = u_k \frac{U_2^2}{S_N} \tag{32}$$

3 B Parallelschaltung von zwei Transformatoren

a)

c)

$$\Delta \underline{U}_{US} = \underline{U}_{US1} - \underline{U}_{US2} = \underline{U}_{OS} \left(\frac{1}{\underline{\dot{u}}_1} - \frac{1}{\underline{\dot{u}}_2} \right)$$

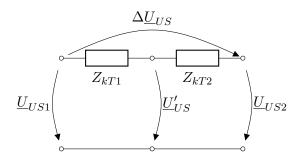
$$\underline{U}'_{US} = \underline{U}_{US1} - \frac{Z_{kT1}}{Z_{kT1} + Z_{kT2}} \Delta \underline{U}_{US}$$

$$(33)$$

$$\underline{U}'_{US} = \underline{U}_{US1} - \frac{Z_{kT1}}{Z_{kT1} + Z_{kT2}} \Delta \underline{U}_{US}$$
(34)

b)
$$\underline{I}_k = \frac{\Delta \underline{U}_{US}}{Z_{kT1} + Z_{kT2}} \tag{35}$$

c)



4 Fünf Sicherheitsregeln

Siehe Skriptum S.IX

5 Wirtschaftlichkeitsrechnung

a)

$$\alpha = \frac{(q-1)q^n}{q^n - 1} = \frac{(1,05-1)1,05^{25}}{1,05^{25} - 1} = 0,07095\frac{1}{a}$$
(36)

$$T_m = \frac{E}{P} = \frac{2100 \frac{\text{GW h}}{\text{a}}}{300 \,\text{MW}_{\text{el}}} = 7000 \,\frac{\text{h}}{\text{a}}$$
 (37)

$$k = \frac{\alpha a + c}{T_m} + b + d \tag{38}$$

$$= \frac{0,07095\frac{1}{a} \cdot 590\frac{\mathfrak{S}}{kW_{el}} + 87\frac{\mathfrak{S}}{kW_{el}a}}{7000\frac{h}{a}} + \frac{0,37\frac{\mathfrak{S}}{m^{3}} \cdot 3,6\frac{MJ}{kWh}}{0,59 \cdot 30\frac{MJ}{m^{3}}} + 0,001\frac{\mathfrak{S}}{kWh_{el}}$$
(39)

$$= 0.09466 \frac{\epsilon}{\text{kW h}_{\text{el}}}$$
 (40)

b)

$$\alpha = \frac{(q-1)q^n}{q^n - 1} = \frac{(1,04-1)1,04^{40}}{1,04^{40} - 1} = 0,05052\frac{1}{a}$$
(41)

$$T_m = \frac{E}{P} = \frac{1560 \frac{\text{GW h}}{\text{a}}}{300 \,\text{MW}_{\text{el}}} = 5200 \,\frac{\text{h}}{\text{a}}$$
 (42)

$$k = \frac{\alpha a + c}{T_m} + b + d \tag{43}$$

$$= \frac{0,05052\frac{1}{a} \cdot 3100\frac{\epsilon}{kW_{el}} + 78\frac{\epsilon}{kW_{el}a}}{5200\frac{h}{a}}$$

$$= 0,04512\frac{\epsilon}{kW h_{el}}$$
(44)

$$= 0.045 \, 12 \, \frac{\mathbf{E}}{\text{kW h}_{\text{el}}} \tag{45}$$

c)

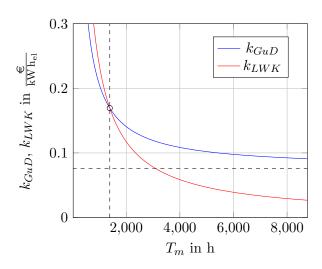
$$k_{GuD} = \frac{\alpha_{LWK} a_{LWK} + c_{LWK}}{T_{m,LWK}} \tag{46}$$

$$T_{m,LWK} = \frac{\alpha_{LWK} a_{LWK} + c_{LWK}}{k_{GuD}} = \frac{0.05052\frac{1}{a} \cdot 3100\frac{\epsilon}{kW_{el}} + 78\frac{\epsilon}{kW_{el}}}{0.09466\frac{\epsilon}{kW_{hel}}} = 2478\frac{h}{a}$$
(47)

d)

$$k_{GuD} = \frac{128.9 \frac{\text{€}}{\text{kW}_{\text{el}} \,\text{a}}}{T_m} + 0.076 \, 25 \frac{\text{€}}{\text{kW h}_{\text{el}}}$$
 (48)

$$k_{LWK} = \frac{234.6 \frac{\epsilon}{\text{kW}_{\text{el}} \, \text{a}}}{T_m} \tag{49}$$



e)