The background of the slide features a dark blue grid with a light blue signal waveform. The waveform consists of a high-frequency, high-amplitude sine wave and a lower-frequency, lower-amplitude sine wave, both rendered in a glowing cyan color.

# Signalbehandling for computer-ingeniører COMTEK-5, E22 & Signalbehandling EIT-5, E22

## 7. Digital IIR Filters: Impulse Invariant Method Bilinear Transformation

Assoc. Prof. Peter Koch, AAU

# Frequency

Continuous  
Time

$x(t)$

Laplace

$$\begin{aligned} X(s) &= \int_{-\infty}^{\infty} x(t) e^{-st} dt \\ &= \int_{-\infty}^{\infty} x(t) e^{-(\sigma + j\Omega)t} dt \\ &= \int_{-\infty}^{\infty} x(t) e^{-j\Omega t} dt \text{ for } \sigma = 0 \\ &= X(j\Omega) \text{ Fourier transform} \end{aligned}$$

Sampling

$$T = \frac{1}{f_s}$$

Reconstruction

$x[n]$

z transform

$$\begin{aligned} X(z) &= \sum_{n=-\infty}^{\infty} x[n] z^{-n} \\ &= \sum_{n=-\infty}^{\infty} x[n] (r e^{j\omega}) \\ &= \sum_{n=-\infty}^{\infty} (r \cdot x[n]) e^{j\omega} \\ &= \sum_{n=-\infty}^{\infty} x[n] e^{j\omega} \text{ for } r = 1 \\ &= X(e^{j\omega}) \text{ Discrete Time FT} \end{aligned}$$

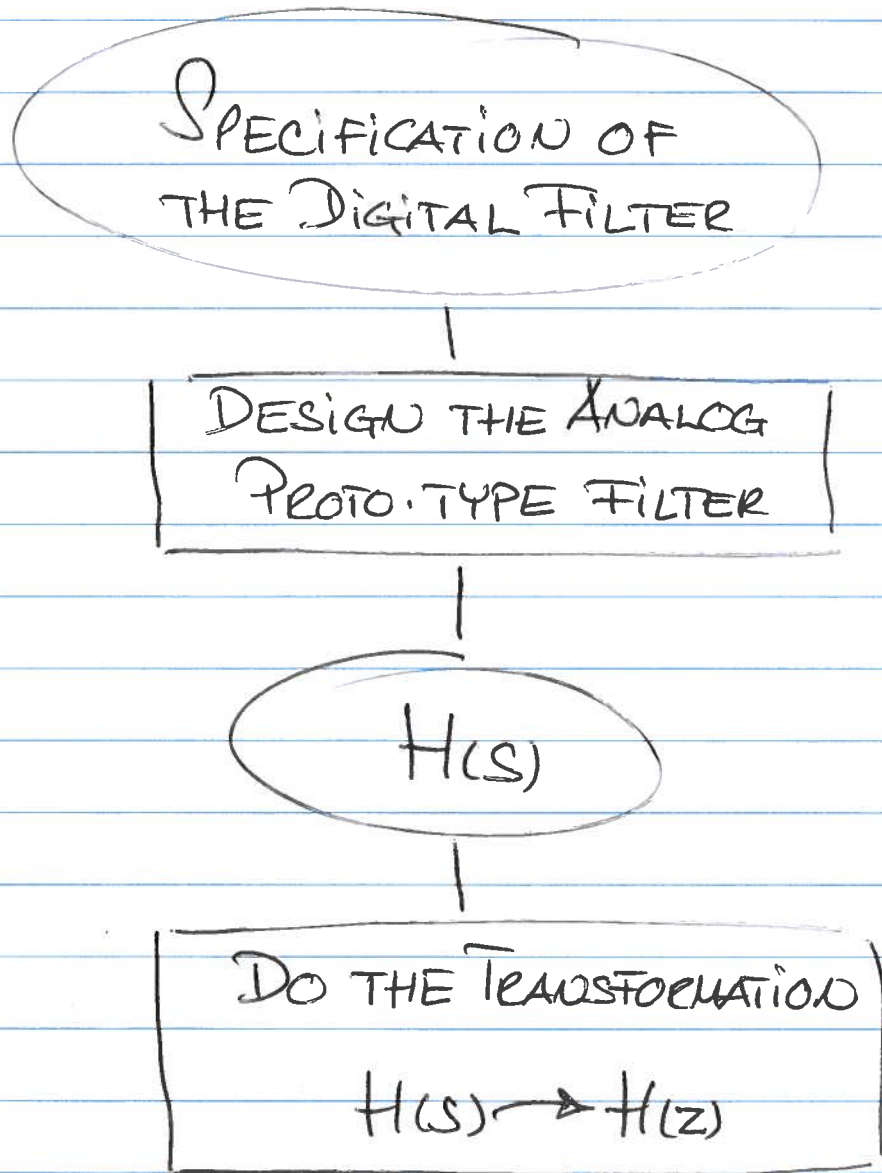
Discrete  
Time



$$\omega = \Omega T = 2\pi f \frac{1}{f_s}$$

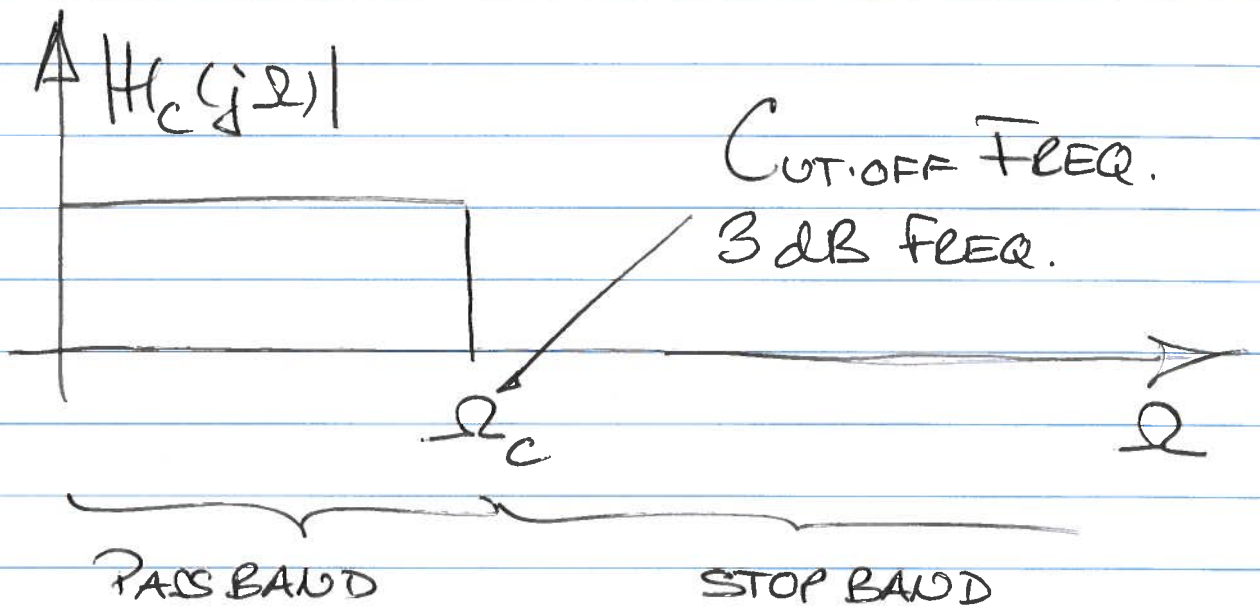
# 7<sup>TH</sup> LECTURE

## "SYNTHESIS OF IIR FILTER"



- ① A BRIEF RE-CAP ON ANALOG FILTERS (BUTTERWORTH)
- ② IMPULSE INVARIANCE METHOD
- ③ THE BILINEAR TRANSFORMATION.

## BUTTERWORTH LP FILTERS



WE CAN DESIGN THIS IDEAL FILTER ONLY MATHEMATICAL.

THUS WE NEED AN APPROXIMATION.

ONE SUCH OPTION IS THE BUTTERWORTH FUNCTION

$$|H_c(j\Omega)|^2 = \frac{1}{1 + \left(\frac{j\Omega}{j\Omega_c}\right)^{2N}}$$

(AMPLITUDE RESPONSE)<sup>2</sup>

WHERE  $N$  IS THE FILTER ORDER

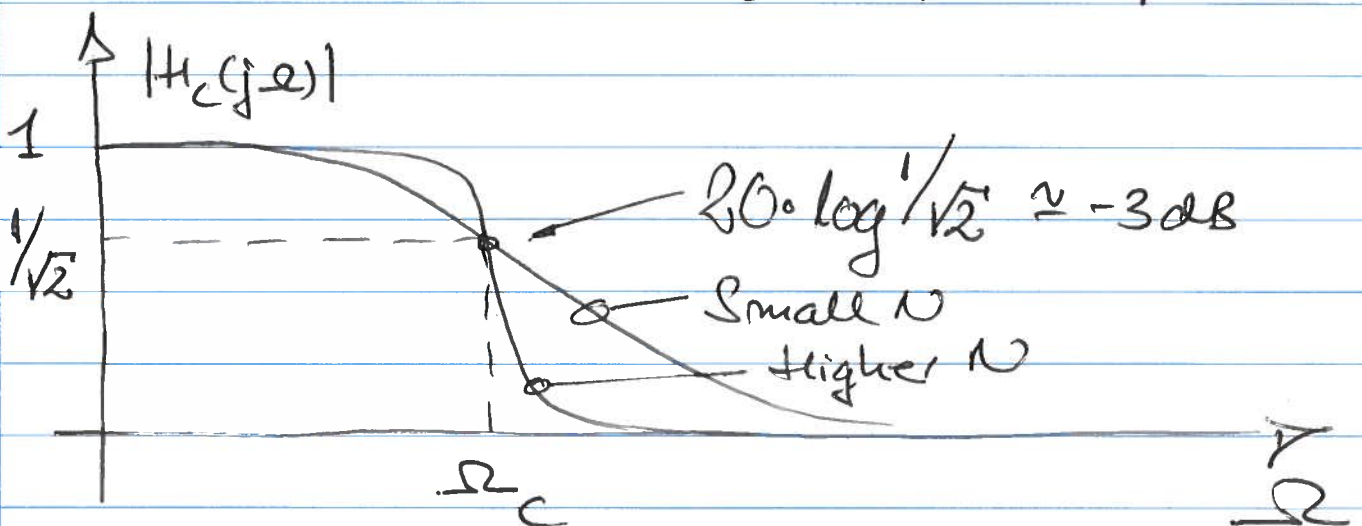
③

THIS FUNCTION HAS SOME INTERESTING CHARACTERISTICS ;

•  $|H_c(j\omega)|^2 = 1 \quad \omega = 0 \quad \forall N$

•  $|H_c(j\omega)|^2 = \frac{1}{2} \quad \omega = \omega_c \quad \forall N$

• MONOTONICALLY DECREASING IN PASS/STOP BAND.



• THE HIGHER  $N$ , THE BETTER APPROXIMATION TO THE IDEAL FILTER.

↳ THE NARROWER THE TRANSITION BAND



(4)

## POLE LOCATION

$$|H_c(s)|^2 = |H_c(j\Omega)|^2 \Big|_{s=j\Omega} = H_c(s)H_c(-s)$$

 $\Downarrow$ 

$$|H_c(s)|^2 = \frac{1}{1 + (s/j\Omega_c)^{2N}}$$

$$1 + (s/j\Omega_c)^{2N} = 0$$

The poles are the values of  $s$  where the denominator equals zero

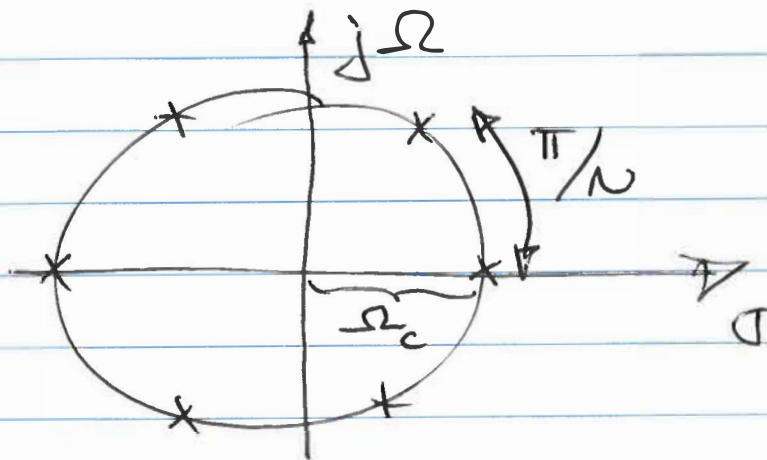
 $\Downarrow$ 

$$s/j\Omega_c = \sqrt[2N]{-1}$$

 $\Downarrow$ 

$$s_k = (-1)^{1/2N} (j\Omega_c) = \Omega_c \cdot e^{(j\pi/2N)(2k+N-1)}$$

for  $k=0, 1, \dots, 2N-1$



$H(s)$  is now derived from the poles in the left-hand side of the plane. (STABILITY)

⑤

Thus, we can express the transfer function as ;

$$H_c(s) = \frac{G}{\prod_{k=1}^n (s - s_k)}$$

The denominator represents the

Butterworth Polynomial

Denominator coefficients for polynomials of the form  $S^n + a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \dots + a_1s + a_0$

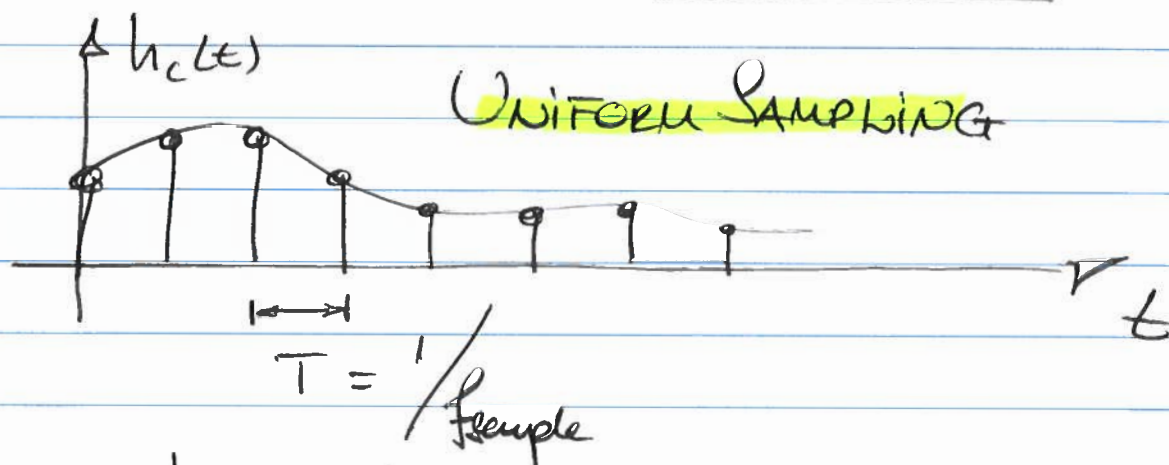
n	a <sub>0</sub>	a <sub>1</sub>	a <sub>2</sub>	a <sub>3</sub>	a <sub>4</sub>	a <sub>5</sub>	a <sub>6</sub>	a <sub>7</sub>	a <sub>8</sub>	a <sub>9</sub>
1	1									
2	1	1.414								
3	1	2.000	2.000							
4	1	2.613	3.414	2.613						
5	1	3.236	5.236	5.236	3.236					
6	1	3.864	7.464	9.142	7.464	3.864				
7	1	4.494	10.098	14.592	14.592	10.098	4.494			
8	1	5.126	13.137	21.846	25.688	21.846	13.137	5.126		
9	1	5.759	16.582	31.163	41.986	41.986	31.163	16.582	5.759	
10	1	6.392	20.432	42.802	64.882	74.233	64.882	42.802	20.432	6.392

n (order)	Normalized Denominator Polynomials in Factored Form
1	(1+s)
2	(1+1.414s+s <sup>2</sup> )
3	(1+s)(1+s+s <sup>2</sup> )
4	(1+0.765s+s <sup>2</sup> )(1+1.848s+s <sup>2</sup> )
5	(1+s)(1+0.618s+s <sup>2</sup> )(1+1.618s+s <sup>2</sup> )
6	(1+0.518s+s <sup>2</sup> )(1+1.414s+s <sup>2</sup> )(1+1.932s+s <sup>2</sup> )
7	(1+s)(1+0.445s+s <sup>2</sup> )(1+1.247s+s <sup>2</sup> )(1+1.802s+s <sup>2</sup> )
8	(1+0.390s+s <sup>2</sup> )(1+1.111s+s <sup>2</sup> )(1+1.663s+s <sup>2</sup> )(1+1.962s+s <sup>2</sup> )
9	(1+s)(1+0.347s+s <sup>2</sup> )(1+s+s <sup>2</sup> )(1+1.532s+s <sup>2</sup> )(1+1.879s+s <sup>2</sup> )
10	(1+0.313s+s <sup>2</sup> )(1+0.908s+s <sup>2</sup> )(1+1.414s+s <sup>2</sup> )(1+1.782s+s <sup>2</sup> )(1+1.975s+s <sup>2</sup> )



Now that we have  $H_c(s)$ , we also have  $h_c(t)$ .

Derive  $H(z)$  using the impulse invariance method



$$h[n] = h_c(nT) \quad \text{where } n \text{ is the sample number.}$$

Now, let's see how it looks like in the frequency domain;

$$H(e^{j\omega}) = \text{DTFT} \{ h[n] \}$$

$$= \sum_{n=-\infty}^{\infty} h[n] \cdot e^{-j\omega n} = \sum_{n=-\infty}^{\infty} h_c(nT) \cdot e^{-j\omega n}$$

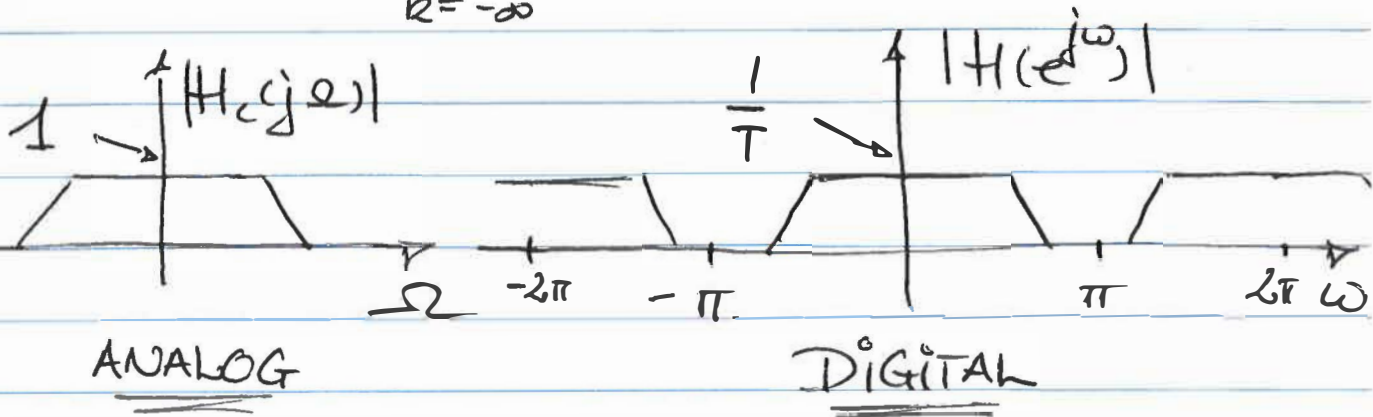
$\Downarrow$   $h[n]$  is discrete in time

$H(e^{j\omega})$  is periodic in frequency

This is a consequence of sampling

(11)

$$H(e^{j\omega}) = \frac{1}{T} \sum_{k=-\infty}^{\infty} H_c\left(j\frac{\omega}{T} + j\frac{2\pi}{T} \cdot k\right), \quad \omega = T \cdot \Omega$$



IN ORDER TO MAINTAIN THE SAME PASS-BAND AMPLIFICATION, WE MUST MULTIPLY WITH  $T$ ;

$$h[n] = T \cdot h_c(nT)$$

Now, LET'S ASSUME THAT <sup>WE</sup> HAVE  $H_c(s)$ , WHICH GENERALLY HAS THE FORM;

$$H_c(s) = \frac{\sum_{k=0}^M \beta_k s^k}{\sum_{l=0}^N \alpha_l s^l}$$

FOR BUTTERWORTH LOW-PASS,  $M=0$

FIND  $H(z)$ ?

1) FIRST, FIND  $h_c(t)$

WE USE PARTIAL FRACTION EXPANSION OF  $H_c(s)$

$$H_c(s) = \frac{A_1}{s-s_1} + \frac{A_2}{s-s_2} + \dots + \frac{A_N}{s-s_N} = \sum_{k=1}^N \frac{A_k}{s-s_k}$$

NEXT WE DO INVERSE LAPLACE

$$h_c(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t} + \dots + A_N e^{s_N t} = \sum_{k=1}^N A_k e^{s_k t}$$

(EQU. 8 p. 523)

2) NEXT, WE SAMPLE  $h_c(t)$

$$\Downarrow \quad h[n] = T \cdot h_c(nT)$$

$$h[n] = T \cdot \sum_{k=1}^N A_k \cdot e^{s_k nT} \cdot u[n] \quad \text{Causal System.}$$

3) FINALLY, WE CONDUCT Z-TRANSFORM

$$H(z) = \mathcal{Z}\{h[n]\} = \sum_{n=0}^{\infty} \left\{ T \cdot \sum_{k=1}^N A_k \cdot e^{s_k nT} \right\} \cdot z^{-n}$$



(13)

$$H(z) = \sum_{n=0}^{\infty} \left\{ T \cdot \sum_{k=1}^N A_k \cdot e^{s_k n T} \right\} \cdot z^{-n}$$

⇓

$$H(z) = T \sum_{k=1}^N A_k \sum_{n=0}^{\infty} (e^{s_k T} \cdot z^{-1})^n$$

⇓

$$H(z) = \sum_{k=1}^N \frac{T A_k}{1 - e^{s_k T} z^{-1}}$$

ROC:  
 $|z| > e^{s_k T}$

THIS IS THE GENERAL TRANSFER FUNCTION  $H(z)$  FOUND BY TRANSFORMING  $H(s)$ , USING THE IMPULSE INVARIANCE METHOD

Now, since  $H(s)$  is STABLE, WE COULD HOPE FOR  $H(z)$  ALSO BEING STABLE — LET'S FIND OUT ;

POLES in  $H(s)$  ;  $s_k$

POLES in  $H(z)$  ;  $z_k = e^{s_k T}$

WE WOULD LIKE  $H(s)$  STABLE  $\rightarrow$   $H(z)$  STABLE

$$\begin{cases} s_k = \sigma_k + j\Omega_k \\ z_k = e^{s_k \cdot T} \end{cases}$$

$\Downarrow$

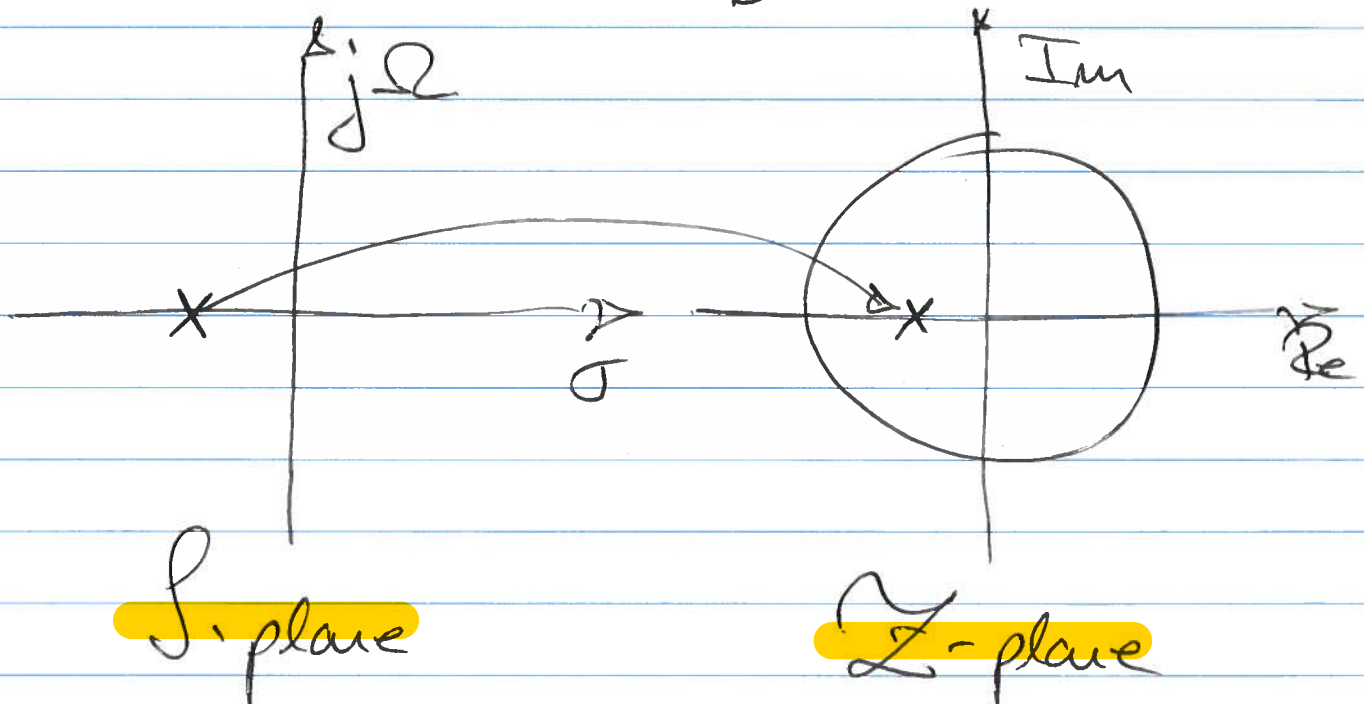
$$z_k = e^{\sigma_k \cdot T} \cdot e^{j\Omega_k \cdot T}$$

$\Downarrow$

$$|z_k| = e^{\sigma_k \cdot T}$$

$\Downarrow$

$$|z_k| < 1 \quad | \quad \sigma_k < 0$$





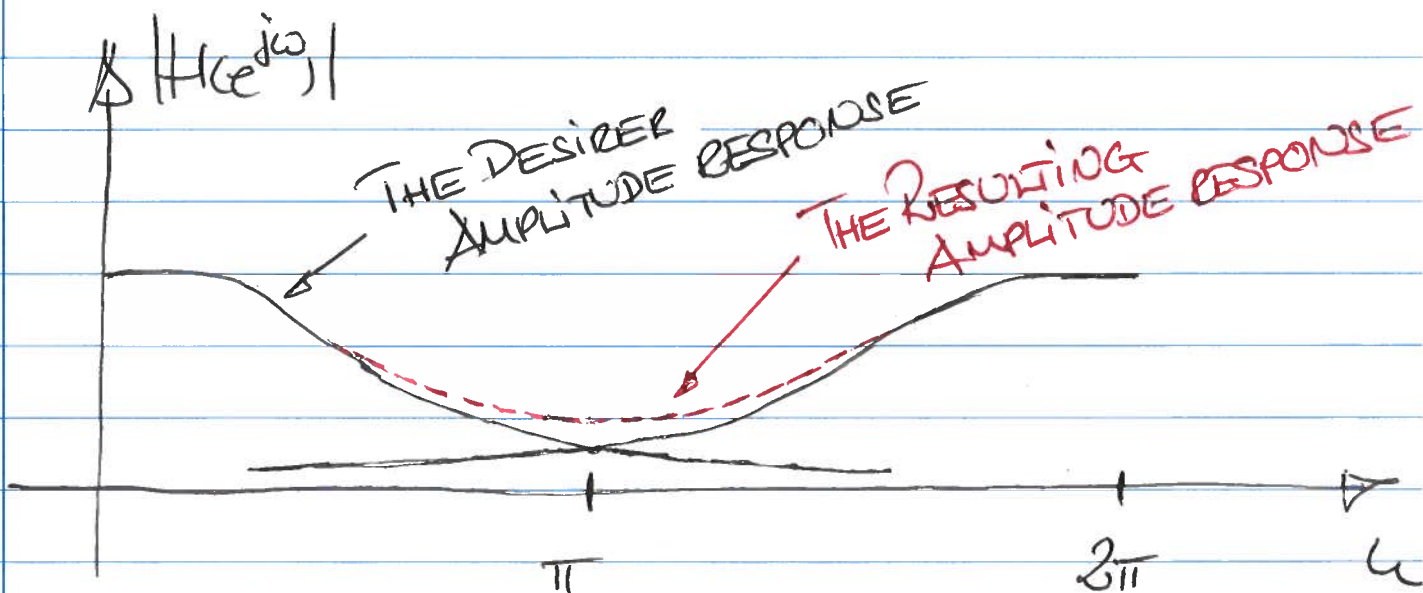
③ THERE IS NO SIMPLE MATHEMATICAL DESCRIPTION OF THE  $s$ -plane TO  $z$ -plane mapping.

④ THE ZEROS IN  $H(z)$  ARE FUNCTIONS OF THE POLES AND  $T \cdot A_k$ , AND THUS THE ZEROS ARE BEING MAPPED DIFFERENTLY THAN THE POLES.

THERE IS A PROBLEM THOUGH....

⑤  $H(e^{j\omega})$  IS A PERIODIC FUNCTION.

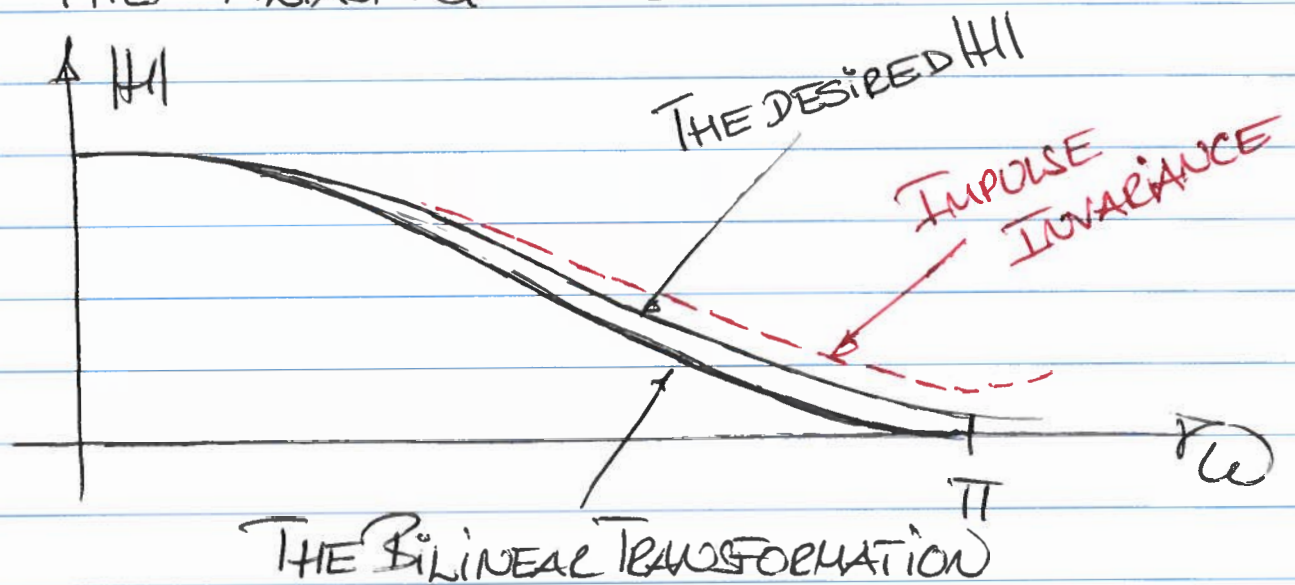
⑥ NO ANALOG FILTER IS BAND-LIMITED.



SO, THERE IS AN OVERLAP AMONG CONSECUTIVE VERSIONS OF THE DESIRED AMPLITUDE RESPONSE

ALIASING

How CAN WE POSSIBLY ELIMINATE THE ALIASING PROBLEM?



o

IDEA :

$$-\infty < \Omega < \infty \rightarrow -\pi \leq \omega \leq \pi$$

THIS NON-LINEAR TRANSFORMATION MAPS THE ENTIRE FREQUENCY AXIS  $\Omega$  ONTO ONE ITERATION ON THE UNIT CIRCLE.

THE IDEA IS THAT  $s$  IS SUBSTITUTED BY A FUNCTION ;

$$H(z) = H(s) \Big|_{s=f(z)}$$

$$\left\{ \begin{array}{ll} \bullet & z = e^{j\omega} \quad (\text{ON THE UNIT CIRCLE}) \\ \bullet & \omega = T \cdot \Omega \quad (\text{RELATION BETWEEN ANALOG AND DIGITAL FREQUENCY}) \\ \bullet & s = j\Omega \quad (\text{THE ANALOG FREQ.-AXIS}) \end{array} \right.$$

$$\Downarrow \quad z = e^{jT \cdot \frac{s}{j}} = e^{sT}$$

Taylor Series for  $\ln(z)$

$$\Downarrow \quad \ln(z) = sT$$

$$\Downarrow \quad s = \frac{1}{T} \cdot \ln(z) = \frac{1}{T} \cdot 2 \left\{ \frac{z-1}{z+1} + \frac{1}{3} \left( \frac{z-1}{z+1} \right)^2 + \dots \right\}$$

$$\Downarrow \quad s \approx \frac{1}{T} \cdot 2 \cdot \frac{z-1}{z+1}$$

$$\Downarrow \quad \boxed{s = \frac{2}{T} \cdot \frac{z-1}{z+1}}$$

Equ. 18 p. 528

THIS IS THE BILINEAR TRANSFORMATION

Now, A MAJOR QUESTION is; How is ??  
THE  $s$ -plane MAPPED TO THE  $z$ -plane .



$$S = \frac{2}{T} \cdot \frac{Z-1}{Z+1}$$



$$Z = \frac{1 + \frac{T}{2}S}{1 - \frac{T}{2}S} = \frac{1 + \frac{T}{2}(\sigma + j\Omega)}{1 - \frac{T}{2}(\sigma + j\Omega)}$$

Using this equation, we can now investigate three important things ;

1) Origin in the  $s$ -plane

$$S=0 \rightarrow Z=1 \text{ i.e.; } DC \rightarrow DC$$

2) Left-hand side of the  $s$ -plane

$$\operatorname{Re}\{s\} = \sigma < 0$$

$$|Z| = \frac{\sqrt{(1 + \frac{T}{2}\sigma)^2 + (\frac{T}{2}\Omega)^2}}{\sqrt{(1 - \frac{T}{2}\sigma)^2 + (\frac{T}{2}\Omega)^2}} < 1 \quad \left| \sigma < 0 \right.$$



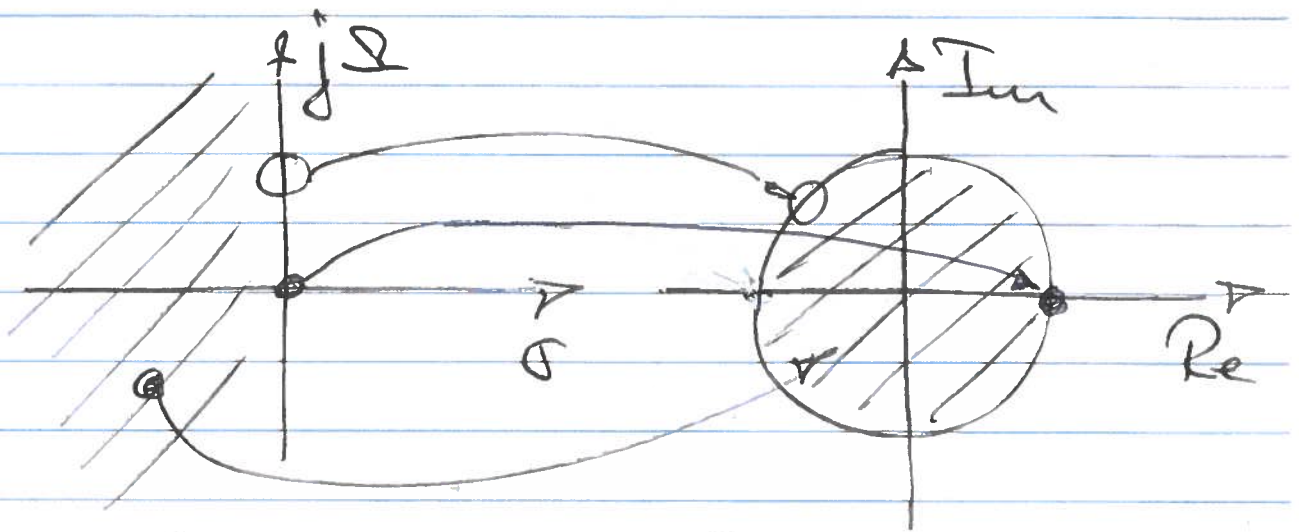
Left-hand side of the  $s$ -plane is mapped to the  $Z$ -plane inside the unit-circle

3)  $j\Omega$ -axis in the  $s$ -plane

$$\sigma=0 \Rightarrow |z|=1 \quad \forall \Omega$$



AND THUS WE CAN CONCLUDE THAT THE  $j\Omega$ -axis MAPS TO THE UNIT-CIRCLE.



$$\text{STABLE } H(s) \Rightarrow \text{STABLE } H(z)$$



(20)

Now, WHAT IS THE RELATION BETWEEN  $\Omega$  AND  $\omega$  USING THE BILINEAR TRANSF. ??

$$\left\{ s = \sigma + j\Omega = \frac{2}{T} \frac{e^{j\omega} - 1}{e^{j\omega} + 1} \right\} \quad z = e^{j\omega}$$

IF WE UTILIZE THAT  $e^{j\omega} = e^{j\frac{\omega}{2}} \cdot e^{j\frac{\omega}{2}}$  AND EULER'S IDENTITY FOR COS AND SIN

$$s = \frac{2}{T} \cdot j \cdot \tan \frac{\omega}{2}$$

THE RIGHT-HAND SIDE IS IMAGINARY

$$\Omega = \frac{2}{T} \cdot \tan \frac{\omega}{2}$$

Equ. 26

AND

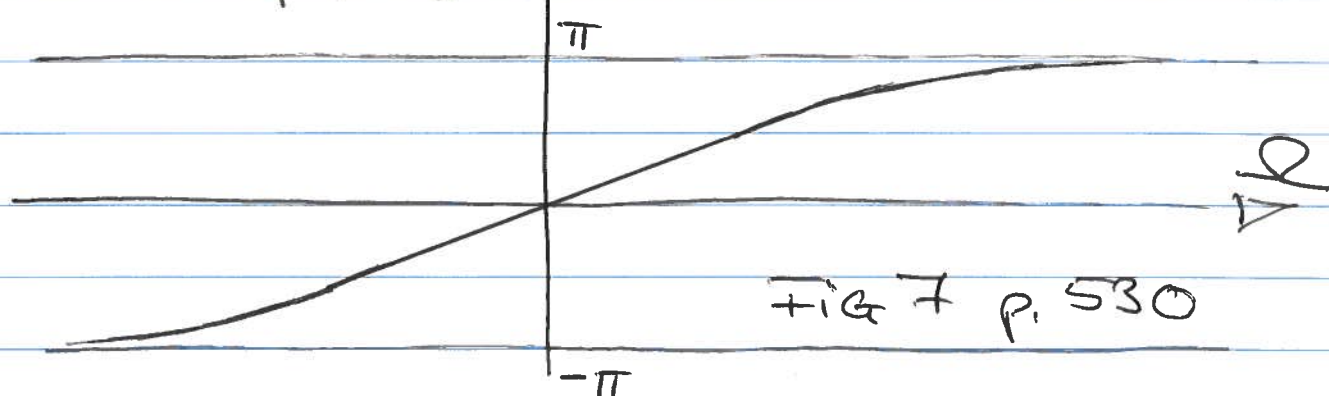
$$\omega = 2 \cdot \arctan \left( \frac{\Omega \cdot T}{2} \right)$$

Equ. 27

p. 529.

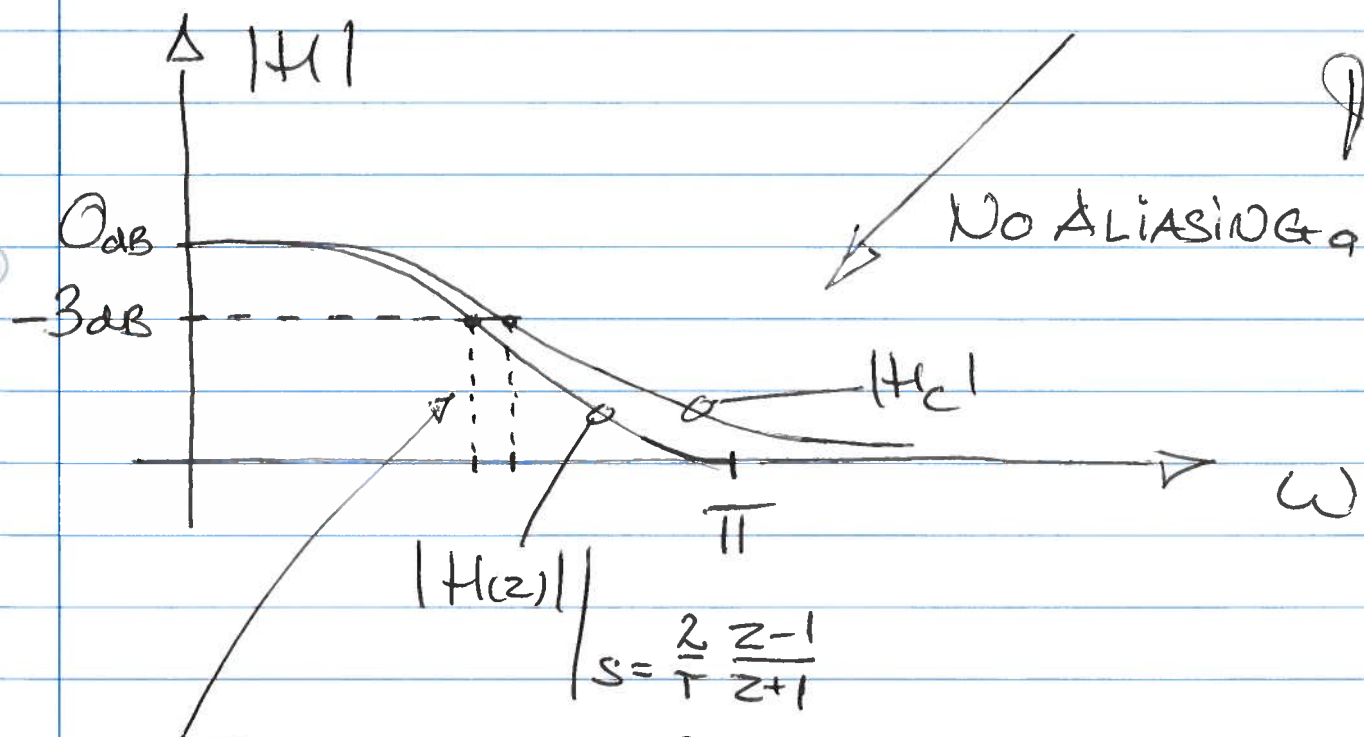
So, MAPPING FROM THE  $s$ -plane TO THE  $z$ -plane, IS AN ARCTAN-FUNCTION.

$$\omega = f(\Omega) \quad \& \quad \omega$$



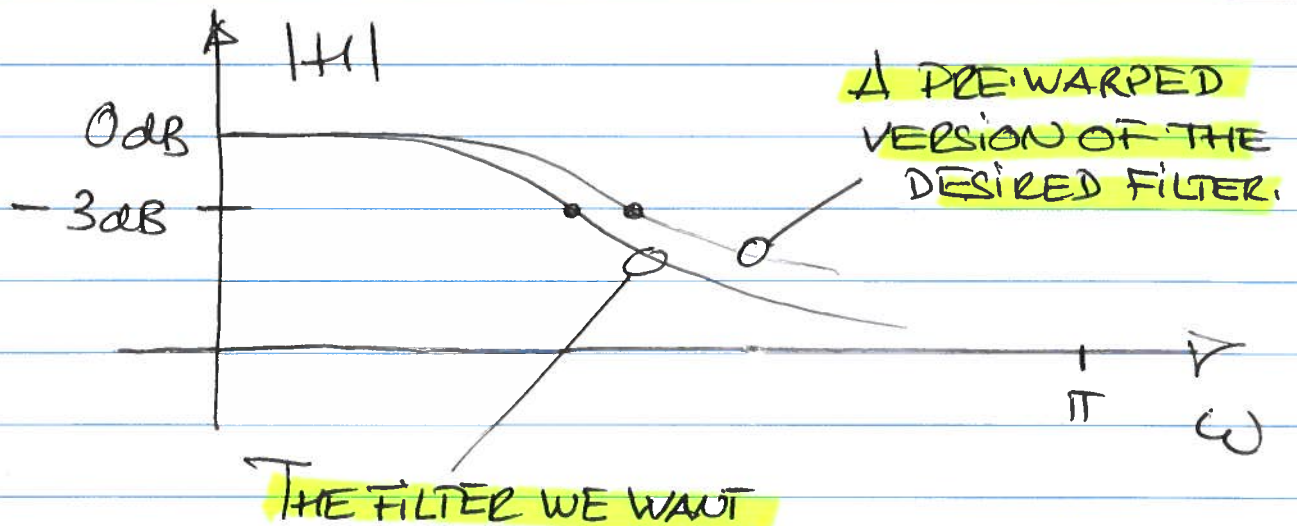
⑥ ARCTAN IS "ALMOST" LINEAR FOR VALUES OF  $\Omega$  CLOSE TO 0, BUT BECOMES MORE NON-LINEAR AS  $\Omega$  INCREASES. BAD NEWS

⑥  $\omega = 2 \cdot \text{ARCTAN} \left( \frac{\Omega \cdot T}{2} \right)$  IS DEFINED IN  $]-\pi; \pi[$  GOOD NEWS



BUT NOW THE 3dB FREQ MOVES DOWNWARDS !

WE MAY ELIMINATE THIS DISTORTION BY INTRODUCING A PRE-DISTORTION, CALLED A PRE-WARPING.



SO, THE IDEA HERE IS, THAT WE MOVE UPWARDS ONE CRITICAL FREQUENCY WHICH AFTER BILINEAR TRANSFORMATION THEN IS LOCATED EXACTLY WHERE WE WANT

$$\Omega_{c, \text{new}} = \frac{2}{T} \cdot \tan \frac{\omega_c}{2}$$

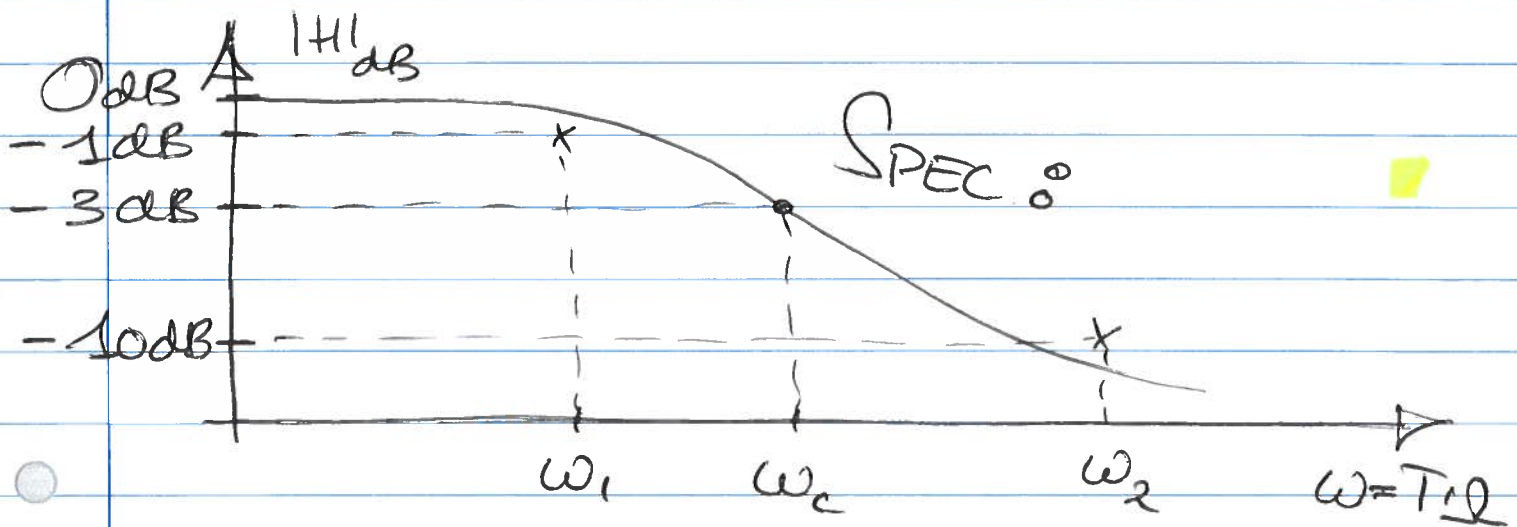
PREWARPING

THIS IS DONE ON  $H(s)$  PRIOR TO TRANSFORMATION TO  $H(z)$ .

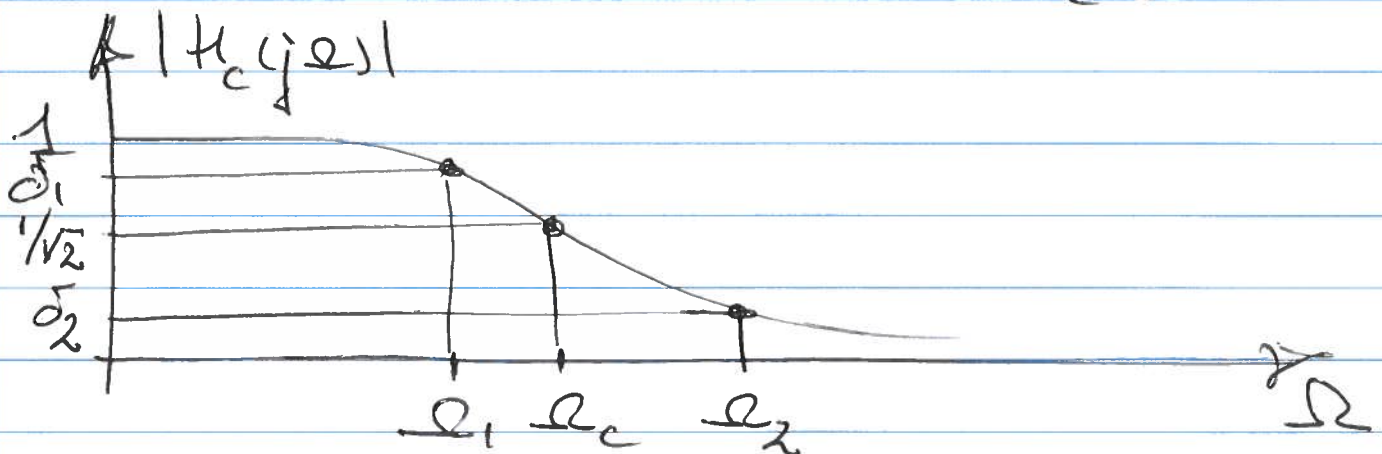


# HINT FOR TODAY'S EXERCISE

MAX FLATNESS  $\Rightarrow$  BUTTERWORTH.



FIRST — FIND THE NECESSARY ORDER OF THE ANALOG FILTER  $H_c(s)$



- 1) Find  $\delta_1$  AND  $\delta_2$
- 2) TWO EQUATIONS ;  $\delta_1^2 \leq |H_c(j\Omega)|$
- 3) PREWARP ALL CRITICAL FREQUENCIES
- 4) FIND  $N \Rightarrow H_c(s) = ??$
- 5) FIND  $H(z) = H_c(s) \Big|_{s = \frac{2}{T} \cdot \frac{z-1}{z+1}}$