

Numerička analiza elektroenergetskog sustava

- AUDITORNE VJEŽBE -

Numerička analiza elektoenergetskih sustava

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Ovaj “radni materijal” predstavlja kratki zapis dijela gradiva i zadataka koji se obrađuju u sklopu auditornih vježbi predmeta *Numerička analiza elektroenergetskih sustava* po nastavnom programu FER I. Dio gradiva obuhvaćen je samo zadacima, a dio i malim objašnjenjem ili analizom.

Preporučena literatura:

Marija Ožegović, Karlo Ožegović: *Električne energetske mreže I-VI*, FESB Split, 1996-2006.

G. W. Stagg, A. H. El-Abiad: *Computer Methods in Power System Analysis*, McGraw-Hill, 1968.

B. Stefanini, S. Babić, M. Urbiha-Feuerbach: *Matrične metode u analizi električnih mreža*, Školska knjiga, Zagreb, 1975.

Popis oznaka i kratica

φ	kut napona [°] [rad]	P	djelatna snaga [W] [pu]
B	susceptancija ($2\pi fC$) [S]	Q	jalova snaga [var] [pu]
C	kapacitet [F]	R	otpor [Ω]
G	vodljivost [S]	S	prividna snaga [VA] [pu]
I	struja [A] [pu]	U	linijski napon, napon [V] [pu]
L	induktivitet [H]	V	fazni napon [V]
		X	reaktancija ($2\pi fL$) [Ω] [pu]
		Y	admitancija ($G+jB$) [S] [pu]
		Z	impedancija ($R+jX$) [Ω] [pu]
		z^*	konjugirano kompleksni broj

Metoda za proračun mreža

Metoda otpora	Metoda reduciranih admitancija	Metoda p.u. (per unit)
$U' = \frac{U_B}{U_n} \cdot U$	$U_r = \frac{U}{U_n}$	$U_{[p.u.]} = \frac{U}{U_n}$
$I' = \frac{\sqrt{3} \cdot U_n}{U_B} \cdot I$	$I_r = \sqrt{3} \cdot U_n \cdot I$	$I_{[p.u.]} = \frac{S}{S_B} \cdot \frac{U_n}{U} = \frac{\sqrt{3} \cdot U_n}{S_B} \cdot I$
$Z' = \left(\frac{U_B}{U_n} \right)^2 \cdot Z$	$Z_r = \frac{Z}{U_n^2}$	$Z_{[p.u.]} = \frac{S_B}{U_n^2} \cdot Z$
$Y' = \left(\frac{U_n}{U_B} \right)^2 \cdot Y$	$Y_r = U_n^2 \cdot Y$	$Y_{[p.u.]} = \frac{U_n^2}{S_B} \cdot Y$

Teorem superpozicije (za aktivne mreže)

Svaka EMS proizvodi u linearnoj mreži struje nezavisno od struja proizvedenih nekim drugim EMS-om. Konačno stanje dobiva se sumiranjem pojedinačnih struja i analogno pojedinačnih padova napona.

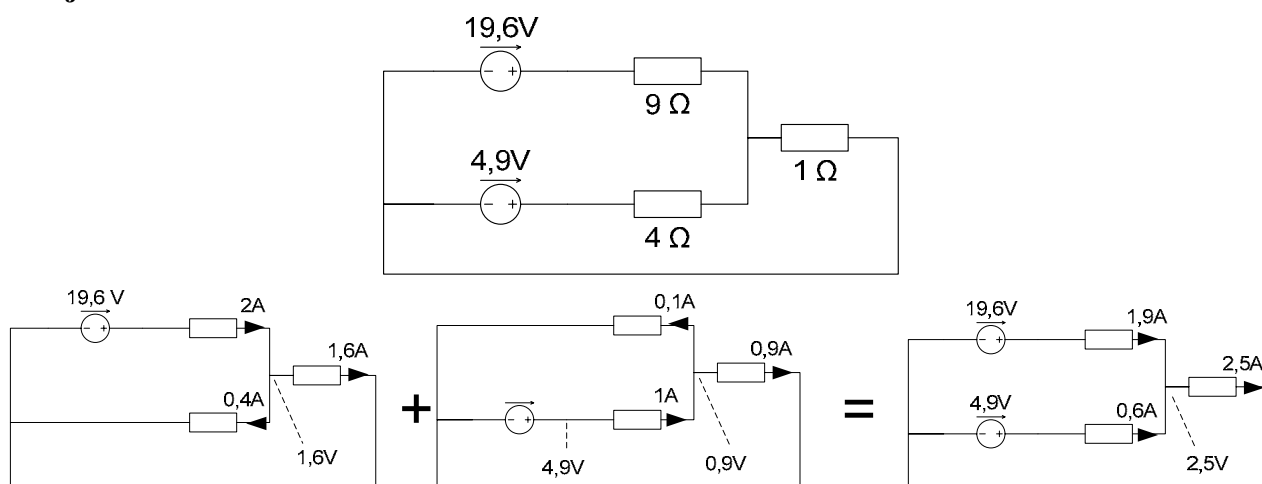
Primjena:

- samo za linearne mreže
- za heterogene struje (izmjenične i istosmjerne, simetrične i nesimetrične, različitih frekvencija)

Postupak:

- uzimamo samo jedan izvor, a druge kratko spojimo
- izračunamo struje po granama i napone u čvorištima
- prve 2 točke ponovimo za sve ostale izvore
- zbrojimo struje u granama od pojedinih izvora i napone po čvorištima

Primjer:



$$R = \frac{1 \cdot 4}{1 + 4} + 9 = \frac{49}{5}$$

$$19,6 = \frac{196}{100}$$

$$I = \frac{\frac{196}{100}}{\frac{49}{5}} = 2A$$

$$R = \frac{1 \cdot 9}{1 + 9} + 4 = \frac{49}{10}$$

$$I = \frac{\frac{49}{10}}{\frac{49}{10}} = 1A$$

Teorem kompenzacije (za aktivne mreže)

Ako se u jednoj grani mreže poveća impedancija za $\Delta \vec{Z}$, promjena struja u svim granama bit će jednaka struji, koju daje izvor $\Delta \vec{Z} \cdot \vec{I}$, spojen u seriju s promijenjenom granom kojom je prije tekla struja \vec{I} .

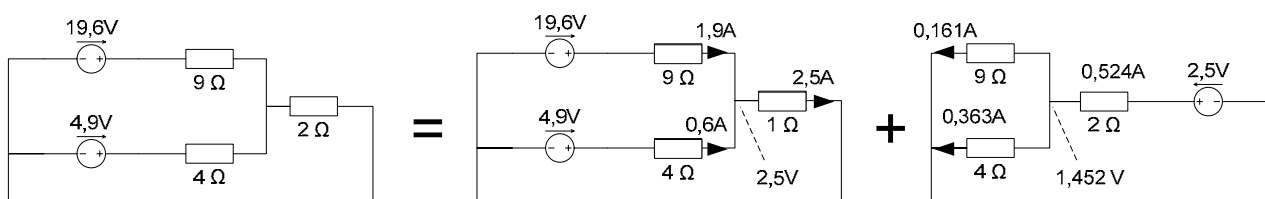
Primjena:

- za mreže koje su već analizirane, samo nam se sada jedna impedancija promijenila
- za aktivne i linearne mreže

Postupak:

- postaviti stanje koje je prije izračunato nekom od metoda
- tom stanju dodati struje u granama i napone u čvorištima izračunate samo za izvor $\Delta \vec{Z} \cdot \vec{I}$ (ostali su kratko spojeni)

Primjer:

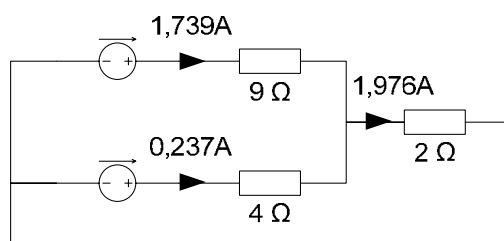


$$\text{Nova EMS} = \Delta Z \cdot I = (Z_{\text{poč}} - Z_{\text{kon}}) \cdot I = (1 - 2) \cdot 2,5 = -2,5V$$

$$R = \frac{4 \cdot 9}{4 + 9} + 2 = \frac{62}{13} = 4,769\Omega$$

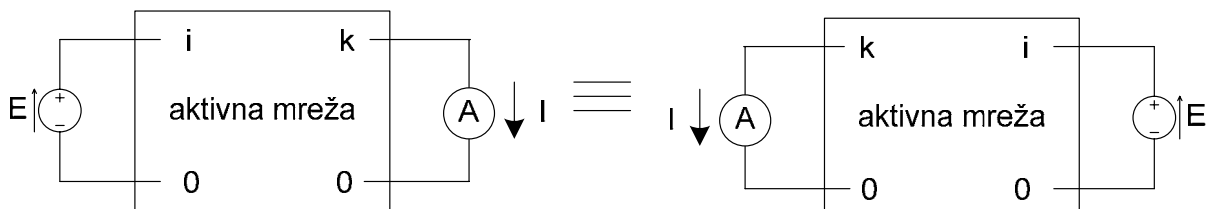
$$I = \frac{2,5}{4,796} = 0,524A \quad ; \quad 0,524 \cdot 2 = 1,048 \quad ; \quad 2,5 - 1,048 = 1,452V$$

$$I_1 = \frac{1,452}{9} = 0,161 \quad ; \quad I_2 = \frac{1,452}{4} = 0,363$$



Teorem reciprociteta

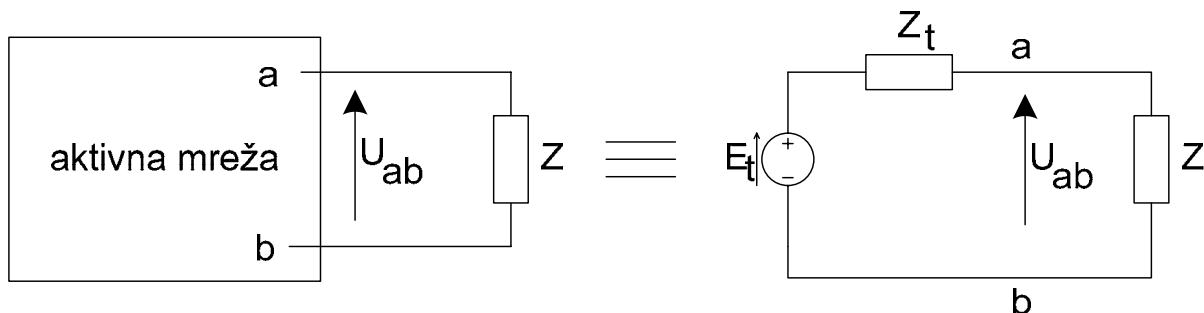
Neka u pasivnoj mreži djeluje samo jedna EMS na odabranom paru čvorova. Ampermetar priključen na neki drugi par čvorova pokazat će određeni otklon. Ako zamijenimo ampermetar i EMS otklon će biti isti.



Teorem vrijedi i ako umjesto naponskog izvora E uzmemo strujni izvor I , a na drugom kraju mjerimo napon V .

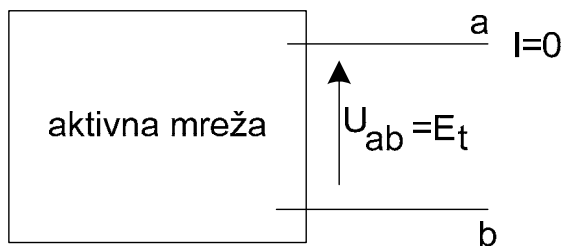
Theveninov teorem

Svaku stvarnu aktivnu mrežu promatranu iz 2 čvora možemo nadomjestiti fiktivnom mrežom, koja je serijski spoj impedancije \vec{Z}_T i EMS-e \vec{E}_T , a naziva se Theveninov ekvivalent.

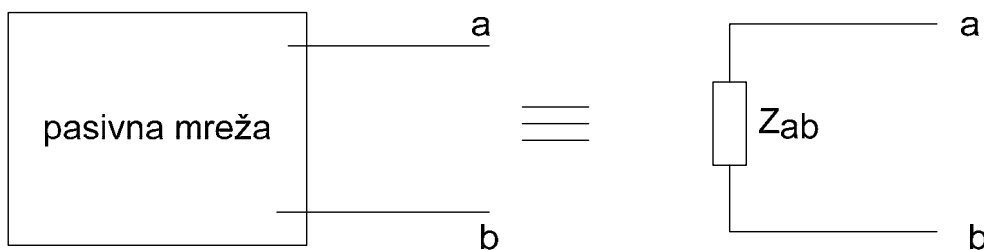


Postupak: Odrediti \vec{E}_T i \vec{Z}_T

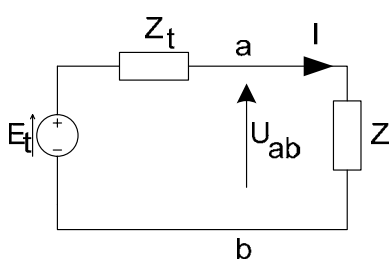
- 1) \vec{E}_T određujemo tako da otvorimo mrežu na čvorištima a i b i izmjerimo taj napon U_{ab}



- 2) \vec{Z}_T odredimo tako da aktivnoj mreži kratko spojimo sve EMS-ove i dobijemo pasivnu mrežu, a zatim izmjerimo impedanciju između čvorišta a i b



Theveninov ekvivalent:



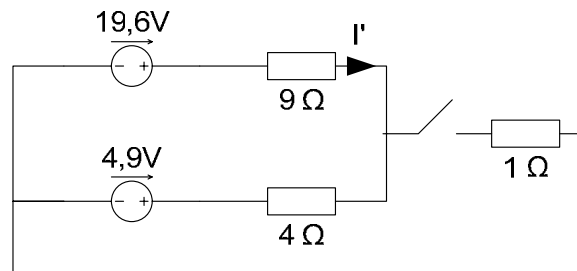
$$\vec{I} = \frac{\vec{E}_T}{\vec{Z}_T + \vec{Z}}$$

$$\vec{U}_{ab}' = \vec{E}_T - I\vec{Z}_T = \vec{E}_T - \frac{\vec{E}_T}{\vec{Z}_T + \vec{Z}} \cdot \vec{Z}_T = \vec{E}_T \left(1 - \frac{\vec{Z}_T}{\vec{Z}_T + \vec{Z}} \right)$$

$$U_{ab}' = \vec{E}_T \frac{\vec{Z}}{\vec{Z}_T + \vec{Z}}$$

Sa energetskog stajališta aktivna mreža i Theveninov ekvivalent ne smiju se poistovjetiti jer u slučaju praznog hoda tj. otvorenih stezaljki a i b u Theveninovu ekvivalentu ne teče nikakva struja, dok u aktivnoj mreži teče struja te postoje i gubici.

Primjer:



1) Određivanje \vec{E}_T

$$\vec{I}' = \frac{19,6 - 4,9}{13} = \frac{14,7}{13} = 1,1307 \quad ; \quad \vec{I} \cdot 9 = 10,1736$$

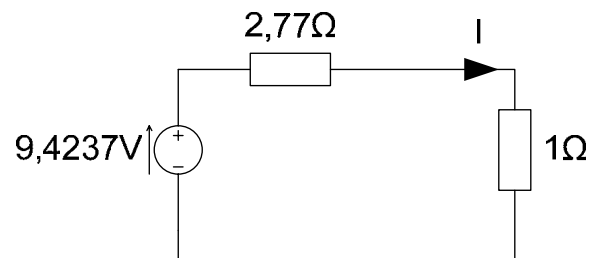
$$\vec{E}_T = 19,6 - 10,1736 = 9,4237V$$

2) Određivanje \vec{Z}_T

$$9 \parallel 4 = \vec{Z}_T = \frac{4 \cdot 9}{4 + 9} = \frac{36}{13} = 2,77\Omega$$

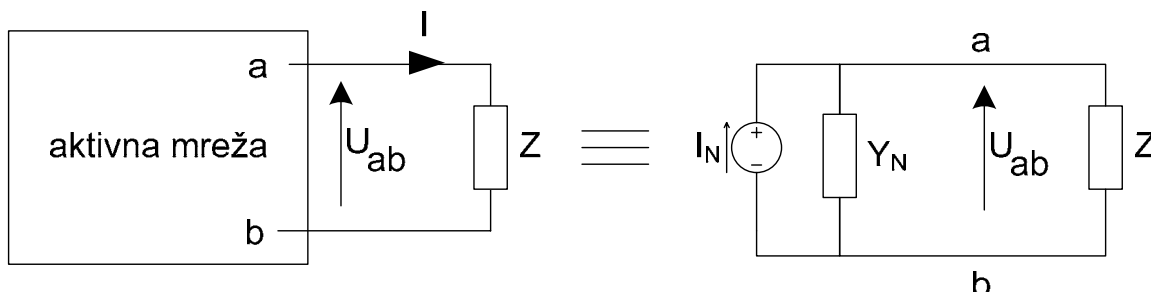
$$\vec{I} = \frac{\vec{E}_T}{\vec{Z}_T + \vec{Z}} = \frac{9,4237}{2,77 + 1} = 2,5A$$

$$\vec{U}_{ab}' = \frac{\vec{E}_T}{\vec{Z}_T + \vec{Z}} \cdot \vec{Z} = 2,5 \cdot 1 = 2,5V$$



Nortonov teorem (za aktivne mreže)

Svaku stvarnu aktivnu mrežu promatranu iz 2 čvora možemo nadomjestiti fiktivnom mrežom, koja je paralelni spoj admitancije \vec{Y}_N i strujnog izvora \vec{I}_N



Postupak:

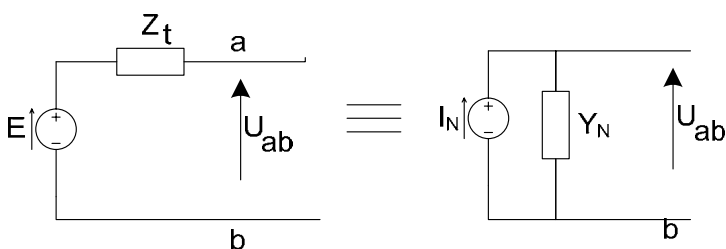
Odrediti \vec{I}_N i \vec{Y}_N :

- 1) \vec{I}_N odredimo tako da u aktivnoj mreži kratko spojimo stezaljke a i b te izmjerimo struju \vec{I}_N
- 2) \vec{Y}_N odredimo tako da sve strujne izvore otkojimo, a naponske kratko spojimo, te izmjerimo admitanciju takve pasivne mreže

2. način:

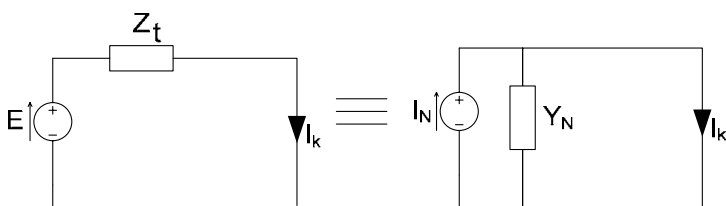
Odredimo Theveninov ekvivalent \vec{E}_T i \vec{Z}_T i zatim uz pomoć pokusa P.H. i K.S. odredimo Nortonov ekvivalent

P.H.:



$$\begin{aligned}\vec{U}_{ab} &= \vec{E}_T \\ \vec{I}_N &= \vec{U}_{ab} \cdot \vec{Y}_N = \vec{E}_T \cdot \vec{Y}_N\end{aligned}\quad (1)$$

K.S.:



$$\begin{aligned}\vec{I}_k &= \vec{I}_N \\ \vec{E}_T &= \vec{Z}_T \vec{I}_k = \vec{Z}_T \vec{I}_N \\ \vec{I}_N &= \frac{\vec{E}_T}{\vec{Z}_T}\end{aligned}\quad (2)$$

Iz izraza (1) i (2) slijedi:

$$\vec{I}_N = \vec{E}_T \cdot \vec{Y}_N$$

$$\vec{I}_N = \frac{\vec{E}_T}{\vec{Z}_T}$$

$$\vec{Z}_T = \frac{1}{\vec{Y}_N}$$

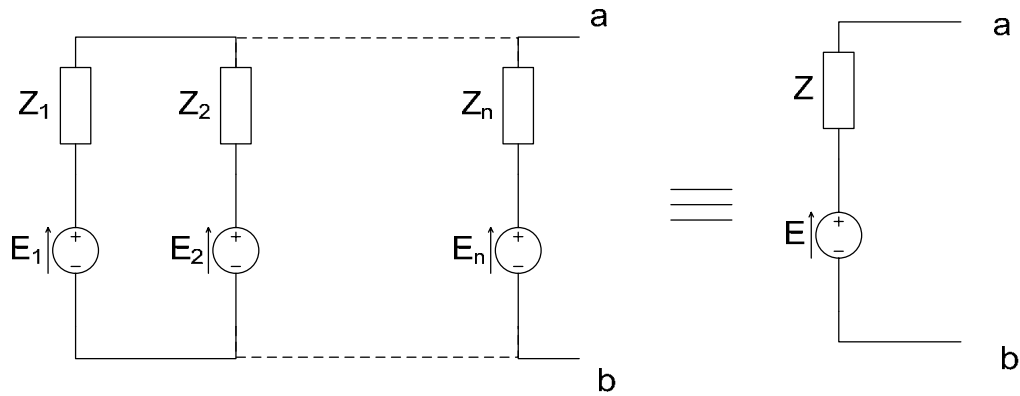
Dakle dobili smo:

$$\boxed{\vec{I}_N = \frac{\vec{E}_T}{\vec{Z}_T} \quad ; \quad \vec{Y}_N = \frac{1}{\vec{Z}_T}}$$

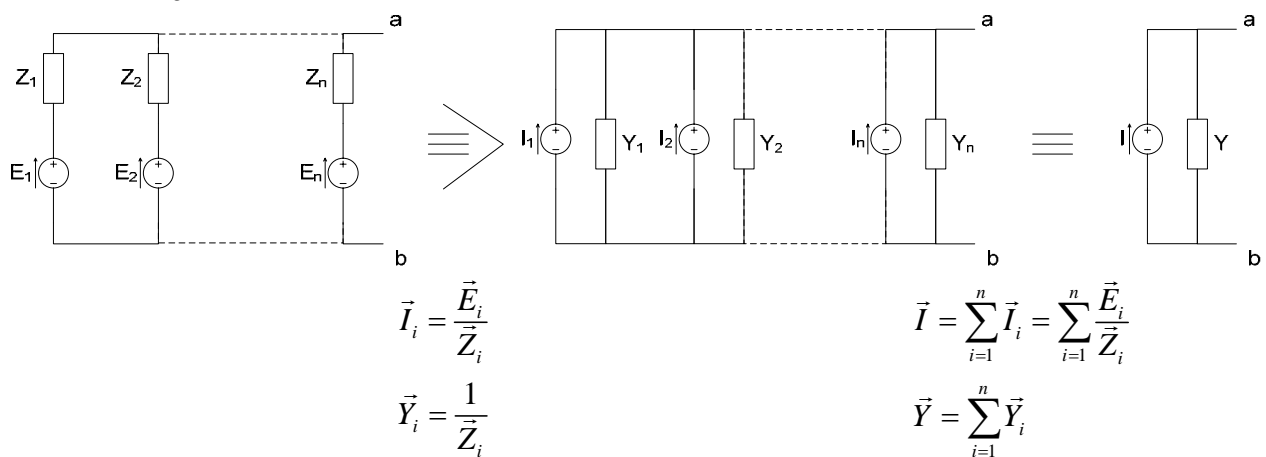
Millmanov teorem (za aktivne mreže)

Kompletnu aktivnu mrežu ekvivalentiramo uz pomoć Nortonovog i Theveninovog teorema u impedantni ili admitantni oblik.

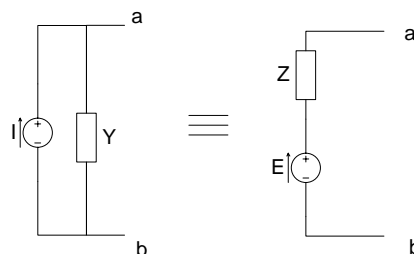
1. način:



2. način (bolji):



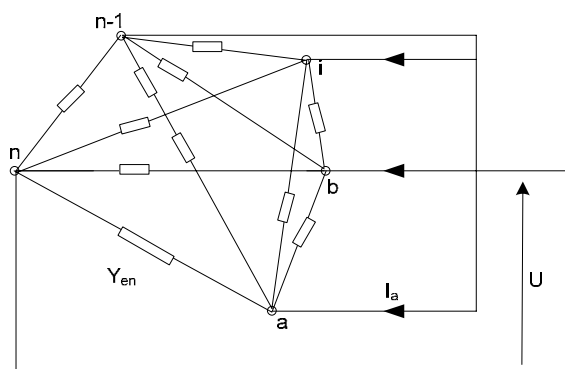
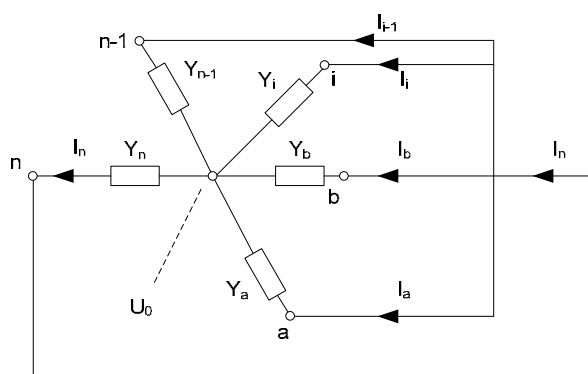
Zatim se ponovo možemo vratiti na impedantni oblik



$$\vec{E} = \frac{\vec{I}}{\vec{Y}} = \frac{\sum_{i=1}^n \frac{\vec{E}_i}{\vec{Z}_i}}{\sum_{i=1}^n \frac{1}{\vec{Z}_i}}$$

$$Z = \frac{1}{Y} = \frac{1}{\sum_{i=1}^n \frac{1}{Y_i}}$$

Izrazi za pretvorbu opće zvijezde u opći poligon



$$I_n = \frac{(Y_a + Y_b + \dots + Y_i + Y_{n-1}) \cdot Y_n}{(Y_a + Y_b + \dots + Y_i + Y_{n-1}) + Y_n} \cdot U = \frac{(Y_a + Y_b + \dots + Y_i + Y_{n-1}) \cdot Y_n}{\sum_{i=a}^n Y_i} \cdot U$$

$$I_a = (U - U_0) Y_a \quad ; \quad I_n = (U - U_0) \cdot (Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1})$$

$$\frac{I_a}{I_n} = \frac{(U - U_0) Y_a}{(U - U_0) \cdot (Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1})} = \frac{Y_a}{(Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1})}$$

$$I_a = I_n \frac{Y_a}{(Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1})} = \frac{(Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1}) Y_n \cdot Y_a}{\sum_{i=1}^n Y_a \cdot (Y_a + Y_b + \dots + Y_i + \dots + Y_{n-1})} \cdot U$$

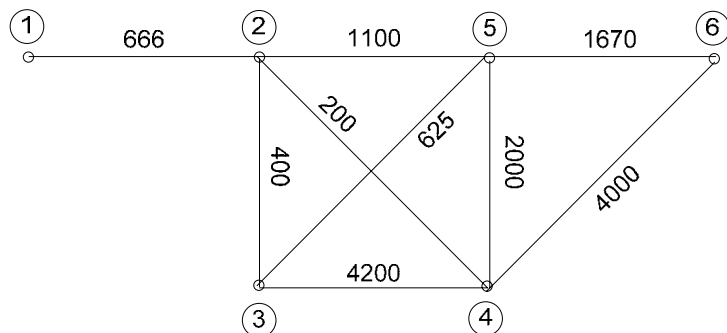
$$I_a = U \cdot \frac{Y_n \cdot Y_a}{\sum_{i=a}^n Y_i} \Rightarrow$$

$$\Rightarrow Y_{an} = \frac{Y_n \cdot Y_a}{\sum_{i=a}^n Y_i}$$

$$I_a = U \cdot Y_{en} \Rightarrow$$

$$Y_{jk} = \frac{Y_j \cdot Y_k}{\sum_{i=a}^n Y_i}$$

Primjer za transfiguraciju mreže



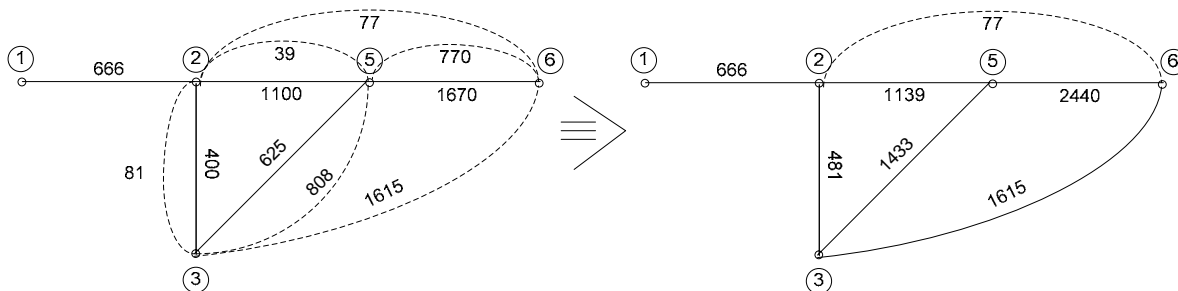
(zadržati čvorišta 1, 3 i 6)

Čvorište 4:

$$\sum Y = 4200 + 2000 + 4000 + 200 = 10400$$

$$Y_{23} = \frac{4200 \cdot 200}{10400} = 81 \quad ; \quad Y_{25} = \frac{200 \cdot 2000}{10400} = 39 \quad ; \quad Y_{26} = \frac{200 \cdot 4000}{10400} = 77$$

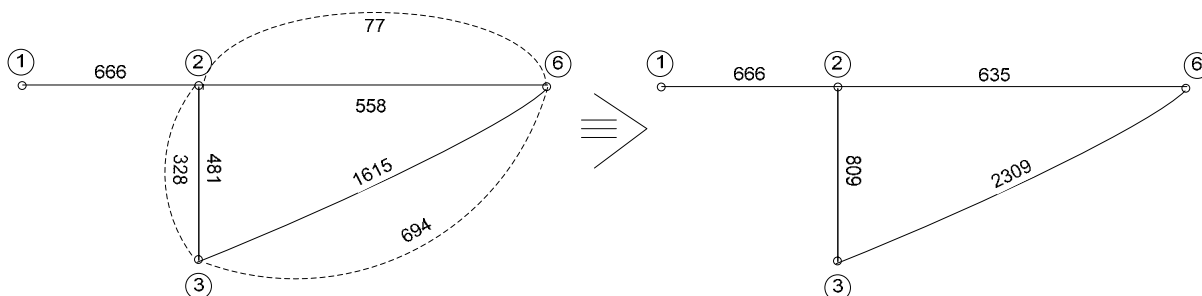
$$Y_{35} = \frac{4200 \cdot 2000}{10400} = 808 \quad ; \quad Y_{36} = \frac{4200 \cdot 4000}{10400} = 1615 \quad ; \quad Y_{56} = \frac{2000 \cdot 4000}{10400} = 770$$



Čvorište 5:

$$\sum Y = 1139 + 2440 + 1433 = 5012$$

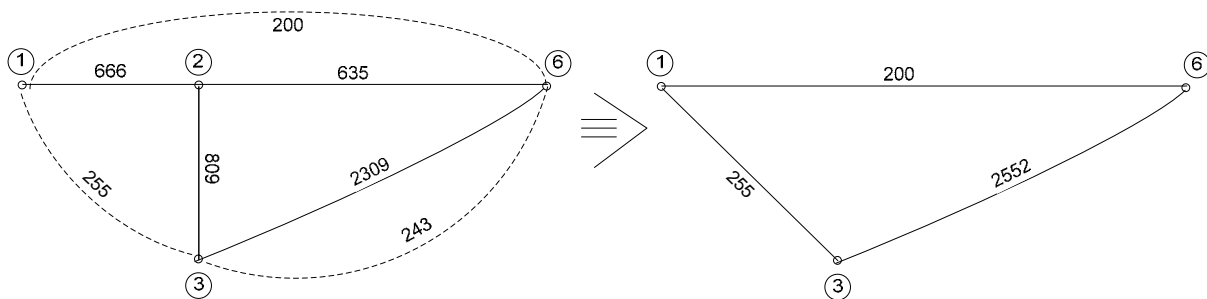
$$Y_{23} = \frac{1139 \cdot 1439}{5012} = 328 \quad ; \quad Y_{26} = \frac{1139 \cdot 2440}{5012} = 538 \quad ; \quad Y_{36} = \frac{1439 \cdot 2440}{5012} = 694$$



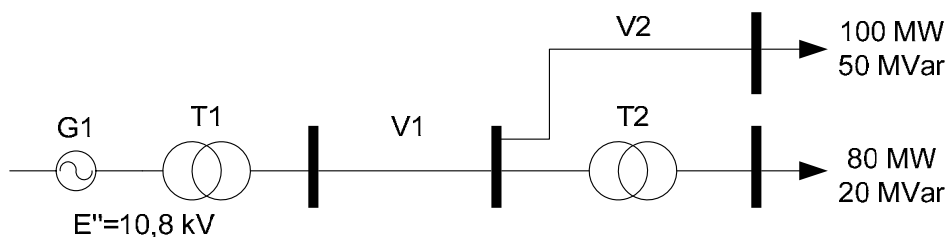
Čvorište 2:

$$\sum Y = 666 + 635 + 809 = 2100$$

$$Y_{13} = \frac{666 \cdot 809}{2100} = 255 \quad ; \quad Y_{16} = \frac{666 \cdot 635}{2100} = 200; \quad Y_{36} = \frac{809 \cdot 635}{2100} = 243$$



ZADATAK 1 Za prijenosni sustav prikazan na slici zadani su podaci za pojedine elemente.



G1	$S_n = 300 \text{ MVA}$ $X_d'' = 10\%$ $U_n = 10,5 \text{ kV}$ $E'' = 10,8 \text{ kV}$	T1	$S_n = 300 \text{ MVA}$ $U_{n1}/U_{n2} = 220 \text{ kV} / 10,5 \text{ kV}$ $P_{Cu} = 1 \text{ MW}$ $u_k = 12\%$	T2	$S_n = 100 \text{ MVA}$ $U_{n1}/U_{n2} = 220 \text{ kV} / 110 \text{ kV}$ $P_{Cu} = 1,5 \text{ MW}$ $u_k = 10\%$
V1	$l = 100 \text{ km}$ $X_1 = 0,4 \Omega / \text{km}$ $R_1 = 0,1 \Omega / \text{km}$	V2	$l = 80 \text{ km}$ $X_1 = 0,35 \Omega / \text{km}$ $R_1 = 0,05 \Omega / \text{km}$		

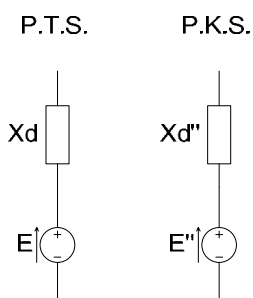
- Metodom otpora preračunaj sve elemente zadanog prijenosnog sustava na bazni napon 100 kV
- Uz pomoć metode p.u. preračunaj na baznu snagu $S_B = 100 \text{ MVA}$ elemente zadanog prijenosnog sustava

Rješenje:

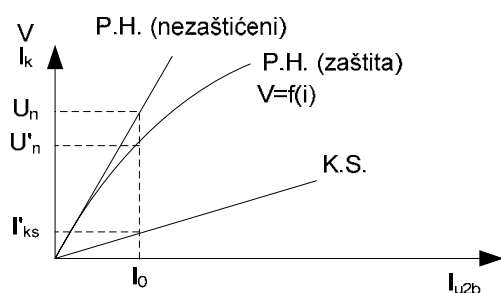
Zanemarenja:

1. G1 – turbogenerator

- za potrebe proračuna mreža:



- R generatora je zanemaren
- definicija sinhronne reaktacije:



$$X_n = \frac{U_n}{I_n}, \quad X_d [\%] = \frac{X_d [\Omega]}{X_n} \cdot 100 = \frac{\frac{U_n}{I_{ks}}}{\frac{U_n}{I_n}} \cdot 100 = \frac{I_n}{I_{ks}} \cdot 100$$

$$X_d [\%] = \frac{I_n}{I_{ks}} \cdot 100 \cdot \frac{3U_n}{3U_n} = \frac{V_n}{I_{ks}} \cdot \frac{3I_n}{3U_n} \cdot 100 = X_d [\%] \cdot \frac{3I_n}{3U_n} \cdot 100$$

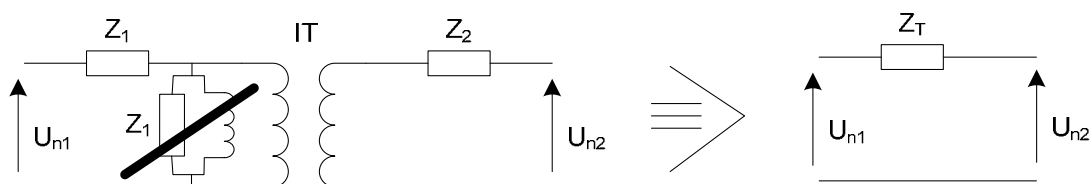
$$X_d [\%] = X_d [\Omega] \cdot \frac{3U_n V_n}{3U_n^2} \cdot 100$$

$$X_d [\%] = X_d [\Omega] \cdot \frac{S_n}{U_n^2} \cdot 100$$

$$X_d [\Omega] = \frac{X_d [\%]}{100} \cdot \frac{U_n^2}{S_n}$$

2. T1, T2

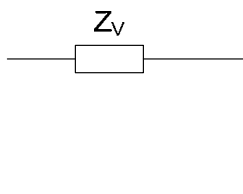
- transformator nazivnog prijenosnog omjera
- zanemareni su gubici praznog hoda (struja magnetiziranja i gubici u Fe)
- nema poprečnih grana u modelu transformatora



$$Z_T = \frac{U_{n1}^2}{S_n} \left[\frac{P_{Cu}}{S_n} + j \sqrt{u_k^2 - \left(\frac{P_{Cu}}{S_n} \right)^2} \right]$$

3. V1, V2

- zanemarene su poprečne grane (admitancije)
- model voda:



$$Z_V = Z_{V1} \cdot l$$

$$X_g [\Omega] = \frac{X_d'' [\%]}{100} \cdot \frac{U_n^2}{S_n} = \frac{10}{100} \cdot \frac{10,5^2}{300} \left[\frac{(kV)^2}{MVA} = \frac{MV^2}{MVA} = \Omega \right]$$

$$X_g [\Omega] = 0,03675 \Omega$$

$$Z_{T1} [\Omega] = \frac{U_{n2}^2}{S_n} \left[\frac{P_{Cu}}{S_n} + j \sqrt{u_k^2 + \left(\frac{P_{Cu}}{S_n} \right)^2} \right] = \frac{220^2}{300} \left[\frac{1}{300} + j \sqrt{0,12^2 - \left(\frac{1}{300} \right)^2} \right]$$

$$Z_{T1} [\Omega] = 0,537 + j19,352 [\Omega]$$

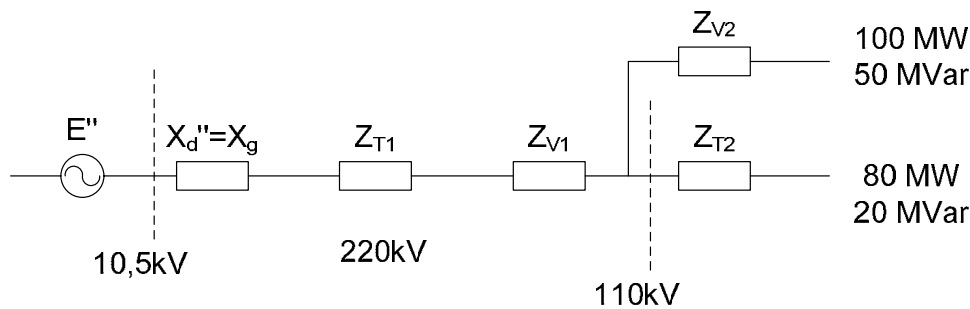
$$Z_{V1} = Z_1 \cdot l_1 = (0,1 + j0,4) \cdot 100 = 10 + j40 [\Omega]$$

$$Z_{V2} = Z_2 \cdot l_2 = (0,05 + j0,35) \cdot 180 = 4 + j28 [\Omega]$$

$$Z_{T2} = \frac{U_{n2}^2}{S_n} \left[\frac{P_{Cu}}{S_n} + j \sqrt{u_k^2 + \left(\frac{P_{Cu}}{S_n} \right)^2} \right] = \frac{110^2}{100} \left[\frac{1,5}{100} + j \sqrt{0,1^2 - \left(\frac{1,5}{100} \right)^2} \right]$$

$$Z_{T2} = 1,815 + j11,963$$

Model:



a)

$$U_B = 100 kV$$

$$U_g' = \frac{U_B}{U_n} \cdot E'' = \frac{100}{10,5} \cdot 10,8 = 102,857 kV$$

$$X_g' = \left(\frac{U_B}{U_n} \right)^2 \cdot X_g = \left(\frac{100}{10,5} \right)^2 \cdot 0,03675 = j3,333 \Omega$$

$$Z_{T1}' = \left(\frac{U_B}{U_n} \right)^2 \cdot Z_{T1} = \left(\frac{100}{220} \right)^2 \cdot (0,537 + j19,352) = 0,1109 + j3,998 \Omega$$

$$Z_{V1}' = \left(\frac{U_B}{U_n} \right)^2 \cdot Z_{V1} = \left(\frac{100}{220} \right)^2 \cdot (10 + j40) = 2,066 + j8,2645 \Omega$$

$$Z_{V2}' = \left(\frac{U_B}{U_n} \right)^2 \cdot Z_{V2} = \left(\frac{100}{220} \right)^2 \cdot (4 + j28) = 0,8264 + j5,785 \Omega$$

$$Z_{T2}' = \left(\frac{U_B}{U_n} \right)^2 \cdot Z_{T2} = \left(\frac{100}{110} \right)^2 \cdot (1,815 + j11,963) = 1,5 + j9,8868 \Omega$$

b)

$$S_B = 100 \text{ MVA}$$

$$U_g [p.u.] = \frac{E''}{U_B} = \frac{E''}{U_n} = \frac{10,8}{10,5} = 1,02857 \text{ p.u.}$$

$$X_g [p.u.] = X_g [\Omega] \cdot \frac{S_B}{U_n^2} = 0,03675 \cdot \frac{100}{10,5^2} = j0,0333 \text{ p.u.}$$

$$Z_{T1} [p.u.] = Z_{T1} [\Omega] \cdot \frac{S_B}{U_{n2}^2} = (0,537 + j19,352) \cdot \frac{100}{220^2} = 0,001109 + j0,03998 \text{ p.u.}$$

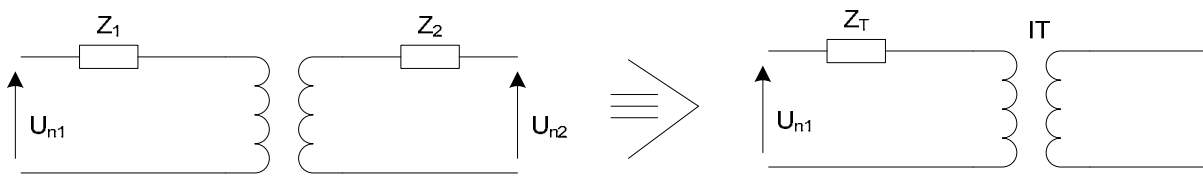
$$Z_{V1} [p.u.] = Z_{V1} [\Omega] \cdot \frac{S_B}{U_n^2} = (10 + j40) \cdot \frac{100}{220^2} = 0,02066 + j0,082645 \text{ p.u.}$$

$$Z_{V2} [p.u.] = Z_{V2} [\Omega] \cdot \frac{S_B}{U_n^2} = (4 + j28) \cdot \frac{100}{220^2} = 0,008264 + j0,05785 \text{ p.u.}$$

$$Z_{T2} [p.u.] = Z_{T2} [\Omega] \cdot \frac{S_B}{U_n^2} = (1,815 + j11,963) \cdot \frac{100}{110^2} = 0,015 + j0,09887 \text{ p.u.}$$

DODATAK:

Transformator



$$Z_T = Z_1 + Z_2' \quad Z_2' = \left(\frac{U_1}{U_2}\right)^2 Z_2 \quad \rightarrow \text{vrijedi za nominalni prijenosni omjer}$$

Definicija: (iz pokusa k.s.)

$$u_k [\%] = \frac{I_n \cdot Z_T}{\frac{U_n}{\sqrt{3}}} \cdot 100$$

U_n – napon ove strane transformatora na kraju svoditi obje impedancije (u našem slučaju U_{n1})

U_k – napon na primaru da u slučaju kad je sekundar kratko spojen poteče kroz trafo I_n (U_k – fazni napon)

$$u_k [\%] = \frac{I_n \cdot Z_T}{\frac{U_n}{\sqrt{3}}} \cdot 100$$

$$Z_T = \frac{u_k [\%] \cdot U_n}{\sqrt{3} \cdot I_n \cdot 100} = \frac{u_k [\%] \cdot U_n^2}{S_n \cdot 100} = \frac{u_k [\%]}{100} \cdot \frac{U_n^2}{S_n} \quad [\Omega]$$

Koliki je kut impedancije? Odredit ćemo ga pomoću mjerenja djelatne snage pri pokusu k.s.

$$P_k = 3I_n^2 \cdot R = 3 \left[\frac{S_n}{\sqrt{3} \cdot U_n} \right] \cdot R = \frac{S_n^2}{U_n^2} \cdot R$$

$$R = \frac{P_k}{S_n^2} \cdot U_n^2 \quad [\Omega] \quad X = \sqrt{Z^2 - R^2} = \frac{U_n^2}{S_n} \sqrt{(u_k)^2 - \left(\frac{P_k}{S_n}\right)^2}$$

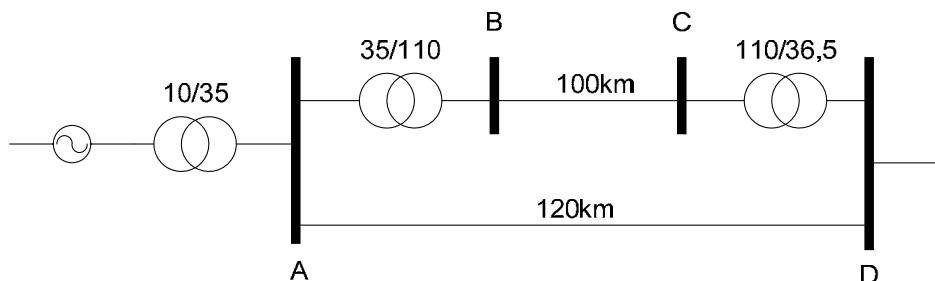
$$Z_T = \frac{P_k}{S_n^2} \cdot U_n^2 + j \cdot \frac{U_n^2}{S_n} \sqrt{(u_k)^2 - \left(\frac{P_k}{S_n}\right)^2}$$

$$Z_T = \frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} + j \sqrt{(u_k)^2 - \left(\frac{P_k}{S_n}\right)^2} \right] \quad [\Omega]$$

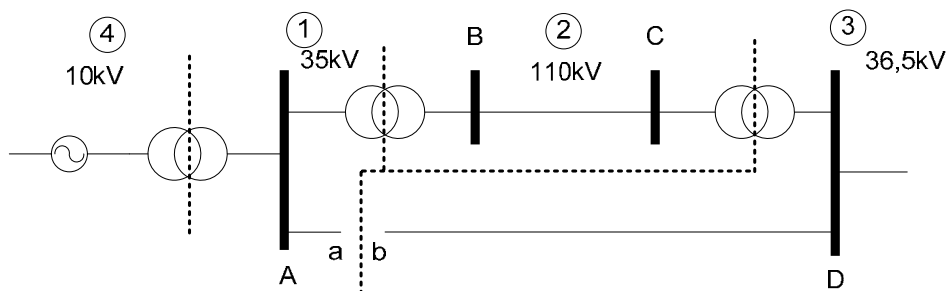
ZADATAK 2 U mreži na slici odredi prilike u praznom hodu za $U_A = 34kV$. Za sve transformatore $u_k = 10\%$, a nazivna snaga je 20 MVA. (Stvarni prijenosni omjer transformatora jednak je nazivnom.)

Podaci generatora: $U_n = 10,5kV$; $S_n = 20MVA$; $X_d = 115\%$.

Reaktancija voda je $X_V = 0,4\Omega/km$.



Rješenje:



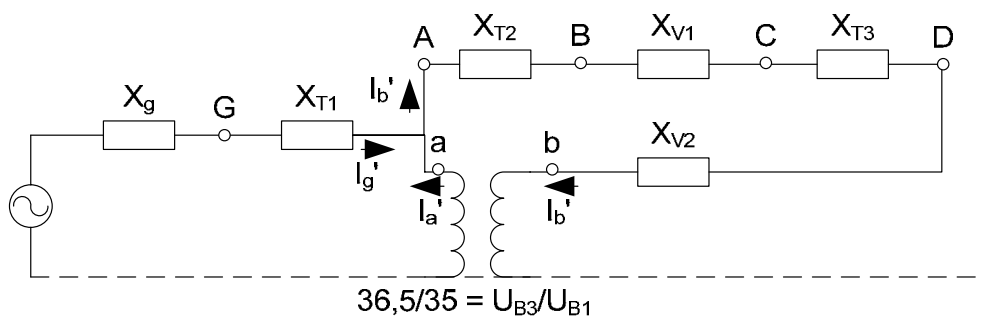
- prije otvaranja zamke vrijedi $\vec{U}_a = \vec{U}_b$
- nakon otvaranja zamke:

$$\vec{U}_a = \vec{U}_a \cdot \frac{U_{B1}}{U_{B1}} ; \vec{U}_b' = \vec{U}_b \cdot \frac{U_{B1}}{U_{B3}} \quad (\text{po metodi otpora, mrežu svodimo na } U_{B1})$$

- kad je zamka zatvorena

$$U_a = U_b \Rightarrow U_a' = U_b' \cdot \frac{U_{B3}}{U_{B1}} \Rightarrow \frac{U_a'}{U_b'} = \frac{U_{B3}}{U_{B1}} \neq 1$$

- dakle, u reduciranoj mreži ($U_a' \neq U_b'$) moramo dodati na tom mjestu EMS, tj. idealni transformator sa prijenosnim omjerom U_{B3}/U_{B1}



Omjeri baznih napona:

$$\frac{U_{B1}}{U_{B2}} = \frac{35}{110} = 0,318 \quad \frac{U_{B1}}{U_{B3}} = \frac{35}{36,5} = 0,959 \quad \frac{U_{B1}}{U_{B4}} = \frac{35}{10} = 3,5$$

Stvarne reaktancije:

$$x_g = \frac{x_{d\%}}{100} \cdot \frac{U_n^2}{S_n} = \frac{115}{100} \cdot \frac{10,5^2}{20} = 6,339\Omega$$

$$x_{T1} = x_{T2} = \frac{u_{k\%}}{100} \cdot \frac{U_n^2}{S_n} = \frac{10}{100} \cdot \frac{35^2}{20} = 6,125\Omega$$

$$x_{V1} = 0,4 \cdot 100 = 40\Omega$$

$$x_{T3} = \frac{10}{100} \cdot \frac{110^2}{20} = 60,5\Omega$$

$$x_{V2} = 0,4 \cdot 120 = 48\Omega$$

Reducirane reaktancije

$$x_g' = x_g \cdot \left(\frac{U_{B1}}{U_{B4}} \right)^2 = 6,339 \cdot 3,5^2 = 77,653\Omega$$

$$x_{T1}' = x_{T2}' = 6,125 \cdot \left(\frac{U_{B1}}{U_{B1}} \right)^2 = 6,125\Omega$$

$$x_{V1}' = 40 \cdot \left(\frac{U_{B1}}{U_{B2}} \right)^2 = 40 \cdot 0,318^2 = 4,045\Omega$$

$$x_{T3}' = 60,5 \cdot 0,318^2 = 6,118\Omega$$

$$x_{V2}' = 48 \cdot 0,959^2 = 44,145\Omega$$

Proračun u reduciranoj mreži

$$U_A = U_A' = 34kV$$

$$U_B = 34 \cdot \frac{35}{36,5} = 32,6kV$$

$$U_A' - U_B' = 34 - 32,6 = 1,4kV$$

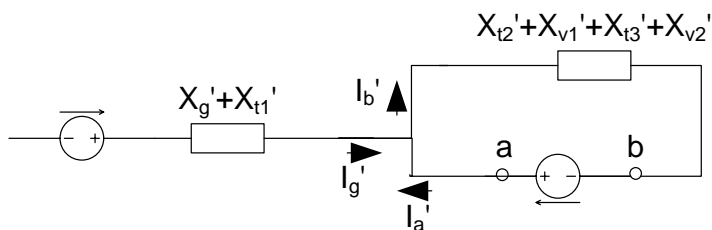
$$\sum X' = j60,433\Omega$$

$$I_b' = \frac{1,4}{j60,433} = -j23,2A$$

$$I_a' = I_b' \cdot \frac{35}{36,5} = -j22,25A$$

$$I_g' = I_b' - I_a'$$

$$I_g' = j23,2 + j22,25 = -j0,95A$$



$$U_a' = 34 + j0kV$$

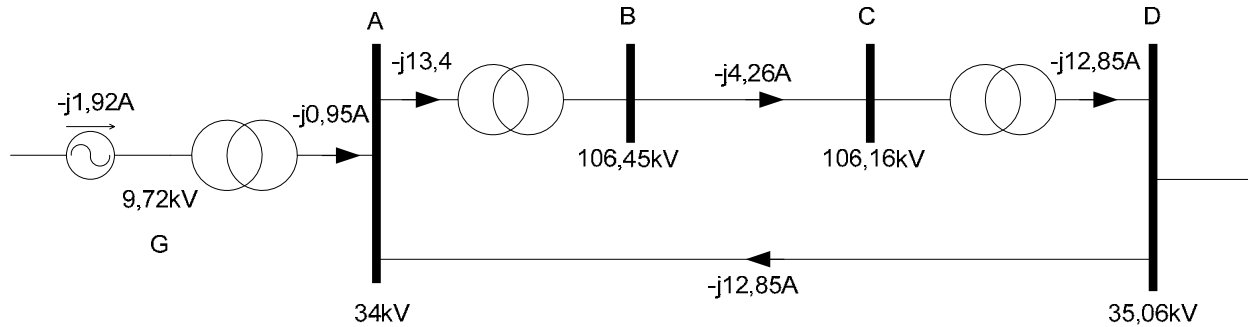
$$U_D' = 32,6 + (-j23,2) \cdot j44,145 \cdot 10^{-3} = 33,62kV$$

$$U_C' = 33,62 + (-j23,2) \cdot j6,118 \cdot 10^{-3} = 33,76kV$$

$$U_B' = 33,76 + (-j23,2) \cdot j4,045 \cdot 10^{-3} = 33,85kV$$

$$U_A' = 33,85 + (-j23,2) \cdot j6,125 \cdot 10^{-3} = 34kV$$

$$U_G' = 34 + (-j0,95) \cdot j6,125 \cdot 10^{-3} = 34,006kV$$



Stvarne vrijednosti:

$$U_A = 34kV \quad I_a = \frac{I_a'}{\sqrt{3}} \cdot \left(\frac{U_{B1}}{U_{B1}} \right) = -j12,85A$$

$$I_b = \frac{I_b'}{\sqrt{3}} \cdot \left(\frac{U_{B1}}{U_{B3}} \right) = \frac{-j23,2}{\sqrt{3}} \cdot 0,959 = -j12,85A$$

$$I_g = \frac{-j0,95}{\sqrt{3}} \cdot \left(\frac{U_{B1}}{U_{B4}} \right) = -j1,92A \quad I_{v1} = -j4,26A$$

$$U_B = U_B' \cdot \frac{1}{0,318} = 106,45kV \quad U_C = U_C' \cdot \frac{1}{0,318} = 106,16kV$$

$$U_D = U_D' \cdot \frac{1}{0,959} = 35,06kV \quad U_G = U_G' \cdot \frac{1}{3,5} = 9,72kV$$

Napomena:

Kod ove metode otpora koju koriste neki autori (npr. Ožegović) imamo jedan bazni napon na koji preračunavamo cijelu mrežu (to je u ovom zadatku $U_{b1}=35$ kV) i ostale bazne napone koji su određeni stvarnim prijenosnim omjerima transformatora (u ovom zadatku $U_{b2}=110$ kV, $U_{b3}=36,5$ kV, $U_{b4}=10$ kV).

Za razliku od metode otpora koju smo mi radili ovdje se reducirane reaktancije dobivaju od stvarnih po formuli:

$$X_i' = X_i \cdot \left(\frac{U_{B1}}{U_{Bi}} \right)^2$$

pri čemu je X_i (stvarna reaktancija u području napona „i“) računata na naponski nivo U_{Bi} koji ne mora biti jednak nazivnom naponu.

Jedino kod generatora se U_{Bi} ne uzima od transformatora već je određen podacima o generatoru.

ZADATAK 3 Zadan je transformator sa podacima prema listi.

- a) Odredi parametre π -sheme tog transformatora koristeći model s idealnim transformatorom
 b) Odredi parametre π -sheme tog transformatora koristeći model bez idealnog transformatora.

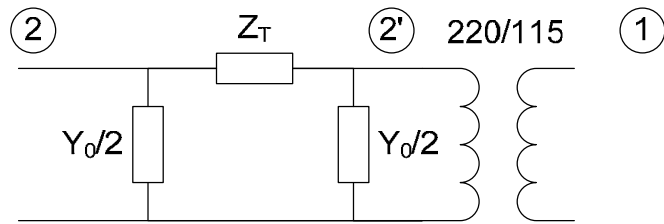
$$S_n = 100 \text{ MVA}$$

$$u_k = 12\%$$

$$i_0 = 1\%$$

$$P_k = 1\% \quad S_n = 0,01 S_n$$

$$P_0 = 25\% \quad P_k = 0,0025 S_n$$

**Rješenje:**

a)

Preračunava se na onu stranu na kojoj nije regulaciona sklopka tj. gdje je nazivni napon – obično je to VN strana (ovdje nije).

$$Z_T = \frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} + j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right] = \frac{220}{100} \left[\frac{0,01 S_n}{S_n} + j \sqrt{0,12^2 - (0,01)^2} \right]$$

$$Z_T = 4,84 + j57,88 [\Omega]$$

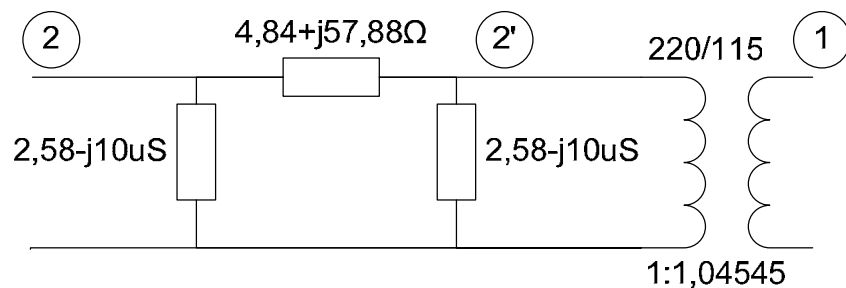
$$Y_T = \frac{1}{Z_T} = \frac{1}{58,082 \angle 85,22^\circ} = 0,0172 \angle -85,22^\circ [S]$$

$$Y_0 = \frac{S_n}{U_n^2} \left[\frac{P_0}{S_n} - j \sqrt{i_0^2 - \left(\frac{P_0}{S_n} \right)^2} \right] = \frac{110}{220^2} \left[\frac{0,0025 S_n}{S_n} - j \sqrt{(0,01)^2 - 0,0025} \right]$$

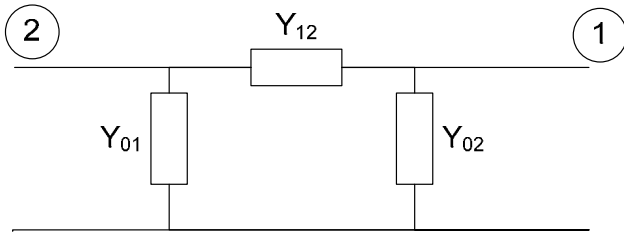
$$Y_0 = (5,16 - j20) \cdot 10^{-6} [S] = 5,16 - j20 [\mu S]$$

$$\frac{Y_0}{2} = 2,58 - j10 [\mu S]$$

$$a = \frac{\frac{115}{220}}{\frac{110}{220}} = \frac{115}{110} = 1,04545$$



b)



$$Y_{12} = \frac{Y_T}{a}$$

$$Y_{01} = \frac{Y_T}{a} \left(\frac{1}{a} - 1 \right) + \frac{1}{a^2} \frac{Y_0}{2}$$

$$Y_{02} = Y_T \left(\frac{1}{a} - 1 \right) + \frac{1}{a^2} \frac{Y_0}{2}$$

$$Y_{12} = \frac{0,0172 \angle -85,22^\circ}{1,04545} = 0,01645 \angle -85,22^\circ [S] = 0,00137 - j0,01639 [S]$$

$$Y_{01} = 0,01645 \angle -85,22^\circ \left(\frac{1}{1,04545} - 1 \right) + \frac{1}{1,04545^2} \cdot 10,327 \angle -75,53^\circ \cdot 10^{-6} =$$

$$= 7,1515 \cdot 10^{-4} \angle 94,78^\circ + 9,445 \cdot 10^{-6} \angle -75,53^\circ =$$

$$= (-5,96 + j71,27) \cdot 10^{-5} + (2,36 - j9,145) \cdot 10^{-6} =$$

$$= (-59,6 + j712,7 + 2,36 - j9,145) \cdot 10^{-6} =$$

$$= -57,25 + j703,555 \mu S$$

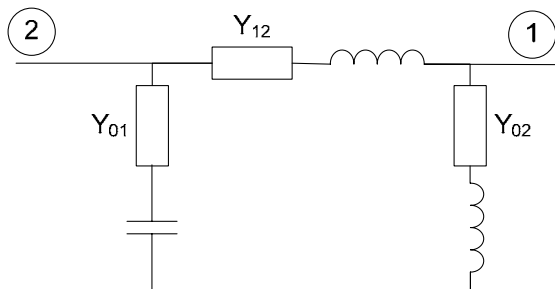
$$Y_{02} = 0,0172 \angle -85,22^\circ \left(1 - \frac{1}{1,04545} \right) + (2,58 - j10) \cdot 10^{-6} =$$

$$= (6,23 - j74,515) \cdot 10^{-5} + (2,36 - j9,145) \cdot 10^{-6} =$$

$$= (62,3 - j74,515 + 2,58 - j10) \cdot 10^{-6} =$$

$$= (64,88 - j84,515) \cdot 10^{-6} =$$

$$= 64,88 - j84,515 \mu S$$



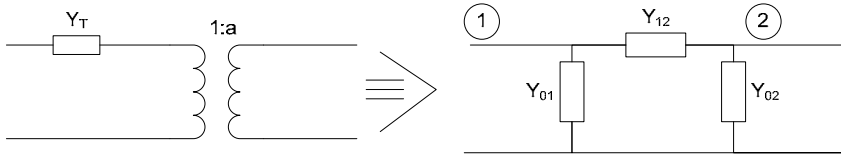
$$Y_{12} = 0,00137 - j0,01639 [S]$$

$$Y_{01} = -57,24 + j703,555 [\mu S]$$

$$Y_{02} = 64,88 - j84,515 [\mu S]$$

Zanemarenja:

1) $\frac{Y_0}{2}$ tj. i_0 i P_0

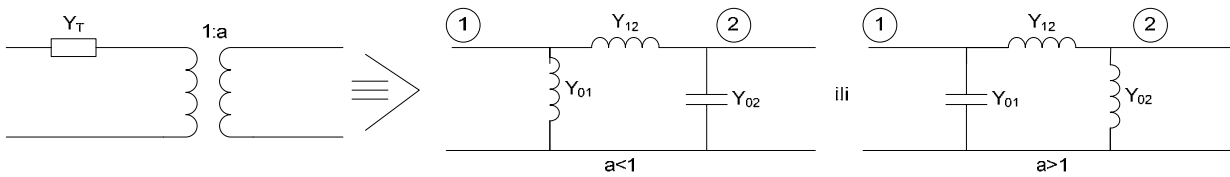


$$Y_{12} = \frac{Y_T}{a}$$

$$Y_{01} = \frac{Y_T}{a} \left(\frac{1}{a} - 1 \right) + \frac{1}{a^2} \frac{Y_0}{2}$$

$$Y_{01} = Y_T \left(1 - \frac{1}{a} \right) + \frac{Y_0}{2}$$

2) Često zanemarimo i P_k



$$Z_T = j \frac{U_n^2}{S_n} u_k = jX_T$$

$$Y_T = -j \frac{1}{X_T} = -jB_T$$

$$y_{01} = -j...$$

$$y_{02} = +j...$$

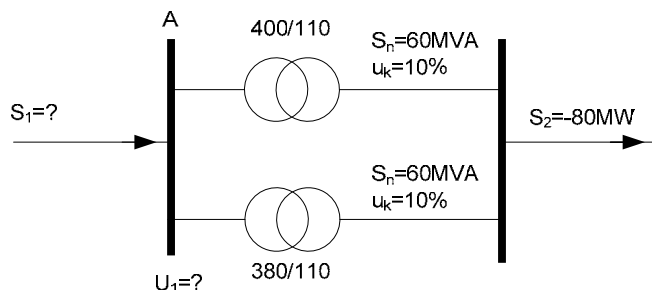
$$y_{01} = +j...$$

$$y_{02} = -j...$$

ZADATAK 4 U transformatorskoj stanici paralelno su spojena 2 transformatora nazivne snage 60 MVA i napona kratkog spoja $u_k=10\%$. Preklopka regulacione sklopke jednog od njih nalazi se na prijenosnom odnosu 400/110, a drugog 380/110. Odredi snagu i napon na primaru ako je napon na sekundaru jednak $U_2=115\text{kV}$ i ako je transformatorska stanica opterećena sa $S_2 = -80\text{MW}$.

Rješenje:

Zadano:



Metoda *per unit*: $S_B = 60\text{MVA}$

Tr1:

$$a_1 = \frac{400}{\frac{110}{400}} = 1$$

$$y_{12}' = y_T = \frac{S_n}{S_B \cdot ju_k} = -j \frac{1}{u_k} = -j10 \text{ p.u.}$$

$$y_{01}' = 0$$

$$y_{02}' = 0$$

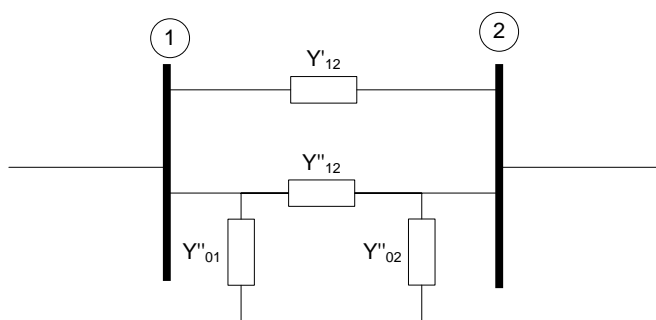
Tr2:

$$a_2 = \frac{380}{\frac{110}{400}} = \frac{380}{400} = 0,95$$

$$y_{12}'' = \frac{y_T''}{a_2} = \frac{S_n}{a_2 \cdot S_B \cdot ju_k} = -j10,526 \text{ p.u.}$$

$$y_{01}'' = \frac{y_T''}{a_2} \left(\frac{1}{a_2} - 1 \right) = -j0,554 \text{ p.u.}$$

$$y_{02}'' = y_T'' \left(1 - \frac{1}{a_2} \right) = j0,5264 \text{ p.u.}$$



$$Y = \begin{vmatrix} Y_{12}' + Y_{12}'' + Y_{01}'' & -j(Y_{12}' + Y_{12}'') \\ -(Y_{12}' + Y_{12}'') & Y_{12}' + Y_{12}'' + Y_{02}'' \end{vmatrix} = \begin{vmatrix} -j21,0803 & j20,5263 \\ j20,5263 & -j20 \end{vmatrix}$$

$$\begin{vmatrix} I_1 \\ I_2 \end{vmatrix} = |Y| \cdot \begin{vmatrix} U_1 \\ U_2 \end{vmatrix}$$

$$U_2 [p.u.] = \frac{U_2 [kV]}{U_{2n}} = \frac{115}{110} = 1,04545 p.u.$$

$$S_2 [p.u.] = \frac{S_2 [MVA]}{S_B} = -\frac{80}{60} = -1,333 p.u.$$

$$I_2 = \left(\frac{S_2}{U_2} \right)^* = \frac{S_2}{U_2} = \frac{-1,333}{1,04545} = -1,2754 p.u.$$

$$I_2 = Y_{21} \cdot U_1 + Y_{22} \cdot U_2 \Rightarrow U_1 = \frac{I_2 - Y_{22} \cdot U_2}{Y_{21}} = \frac{-1,2754 + j20 \cdot 1,04545}{j20,5263}$$

$$U_1 = 1,01865 + j0,0621 p.u.$$

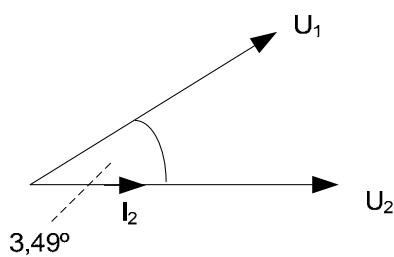
$$I_1 = Y_{11} \cdot U_1 + Y_{12} \cdot U_2 = -j21,0803(1,01865 + j0,0621) + j20,5263 \cdot 1,04545 = 1,3091 - j0,014135 p.u.$$

$$S_1 = U_1 \cdot I_1^* = 1,02054 \angle 3,49^\circ \cdot 1,30918 \angle 0,62^\circ = 1,336 \angle 4,11^\circ = 1,3326 + j0,0958 p.u.$$

$$S_1 = 79,956 + j5,75 MVA = 80 + j5,75 MVA$$

$$U_1 = 407,5 + j24,84 kV$$

ANALIZA:



$$U_1 = 408,256 \angle 3,49^\circ$$

U_1 prethodi U_2

Tok snage: od (1) prema (2)

$$S_2 = -80 MW$$

$$S_1 = 80 + j5,75 MVA$$

$$\Delta S = S_2 + S_1 = j5,75 MVar$$

ZADATAK 5 Odredi napon na sekundaru i snagu na primaru dvaju paralelnih transformatora koji su u praznom hodu, ako je na primaru narinut nazivni napon 220kV. Ostali podaci:

$$\begin{aligned} \text{T1} \quad u_k &= 10\% \\ S_n &= 100 \text{ MVA} \\ a_p &= 220/110 \end{aligned}$$

$$\begin{aligned} \text{T2} \quad u_k &= 12\% \\ S_n &= 100 \text{ MVA} \\ a_p &= 209/110 \end{aligned}$$

Rješenje:

$$S_B = S_n = 100 \text{ MVA}$$

$$Z_T [p.u.] = ju_k \quad \rightarrow \quad Y_T [p.u.] = -j \frac{1}{u_k}$$

$$\begin{aligned} \text{T1:} \quad a_1 &= \frac{\frac{220}{110}}{\frac{110}{220}} = 1 \\ Y_{T1} [p.u.] &= -j \frac{1}{0,1} = -j10 p.u. \\ Y_{12}' &= -j10 p.u. \\ Y_{01}' &= 0 \quad Y_{02}' = 0 \end{aligned}$$

$$\begin{aligned} \text{T2:} \quad a_2 &= \frac{\frac{209}{110}}{\frac{110}{220}} = 0,95 \\ Y_{T1} [p.u.] &= -j \frac{1}{0,12} = -j8,333 p.u. \\ Y_{12}' &= \frac{-j8,333}{a_2} = -j8,772 p.u. \\ Y_{01}' &= \frac{Y_{T2}}{a_2} \left(\frac{1}{a_2} - 1 \right) = \frac{-j8,33}{0,95} \left(\frac{1}{0,95} - 1 \right) = -j0,462 p.u. \\ Y_{02}' &= Y_{T2} \left(1 - \frac{1}{a_2} \right) = -j8,33 \left(1 - \frac{1}{0,95} \right) = j0,439 p.u. \end{aligned}$$

$$\vec{Y} = \begin{vmatrix} -j19,234 & j18,772 \\ j18,772 & -j18,333 \end{vmatrix}$$

$$\begin{vmatrix} \vec{I}_1 \\ \vec{I}_2 \end{vmatrix} = |\vec{Y}| \cdot \begin{vmatrix} \vec{U}_1 \\ \vec{U}_2 \end{vmatrix}$$

$$\vec{U}_1 [p.u.] = \frac{\vec{U}_1}{\vec{U}_n} = \frac{220}{220} = 1 p.u.$$

$$\vec{I}_2 [p.u.] = 0$$

$$\vec{I}_1 [p.u.] = -j19,234 \vec{U}_1 + j18,772 \vec{U}_2$$

$$0 = j18,772 \vec{U}_1 - j18,333 \vec{U}_1 \quad \{ \vec{U}_1 = 1 \}$$

$$\vec{U}_2 = \frac{j18,772}{j18,333} = 1,0239 \text{ p.u.}$$

$$\vec{U}_2 [p.u.] = \frac{\vec{U}_2}{\vec{U}_{2n}} \Rightarrow U_2 = 110 \cdot 1,0239 = 112,63 \text{ kV}$$

$$\vec{I}_1 = -j19,234 + j18,772 \cdot 1,0239 = -j0,01335 \text{ p.u.}$$

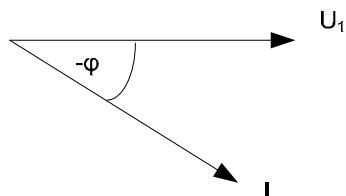
$$\vec{I}_1^* [p.u.] = j0,01335 \text{ p.u.}$$

$$\vec{S}_1 [p.u.] = \vec{U}_1 \cdot \vec{I}_1^* = 1 \cdot j0,01335 = j0,01335 \text{ p.u.}$$

$$\vec{S}_1 = \vec{S}_1 [p.u.] \cdot S_B = j1,335 \text{ Mvar}$$

NAPOMENA:

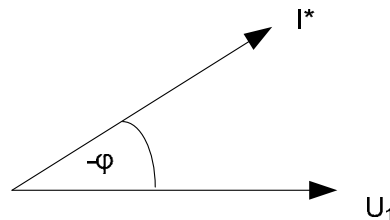
$\vec{S} = \vec{U} \cdot \vec{I}^* [p.u.]$ zbog dogovora da je U u referentnoj osi i da $P+jQ$ označava induktivni karakter snage (pri čemu su P i Q veći od 0)



-> ovo je karakteristika induktivnog potrošača (da bi snaga bila pozitivna treba uzeti struju konjugirano kompleksnu)

$$\vec{S} = \vec{U} \vec{I} = S \angle -\varphi$$

(ovo nije naš dogovor)



$$\vec{S} = S \angle +\varphi$$

$$\vec{S} = \vec{U} \vec{I}^*$$

(ovo je naš dogovor)

$$Z_T = \frac{U_n^2}{S_n} \left[\frac{P_n}{S_n} + j \sqrt{\left(\frac{u_k^2}{100} \right) - \left(\frac{P_n}{S_n} \right)^2} \right] [\Omega]$$

$$Z_T [p.u.] = Z_T [\Omega] \cdot \frac{S_B}{U_n^2} = \frac{U_n^2}{S_n} \cdot j \frac{u_k}{100} \cdot \frac{S_B}{U_n^2} \quad (\text{za } S_B = S_n)$$

$$Z_T [p.u.] = j \frac{u_k}{100}$$

$$Y_T [p.u.] = -j \frac{1}{u_k}$$

ZADATAK 6 U transformatorskoj stanici nalaze se dva transformatora sa slijedećim podacima:

T1 $S_n = 150 \text{ MVA}$

$u_k = 10\%$

$a = \frac{220}{110}$

T2 $S_n = 150 \text{ MVA}$

$u_k = 10\%$

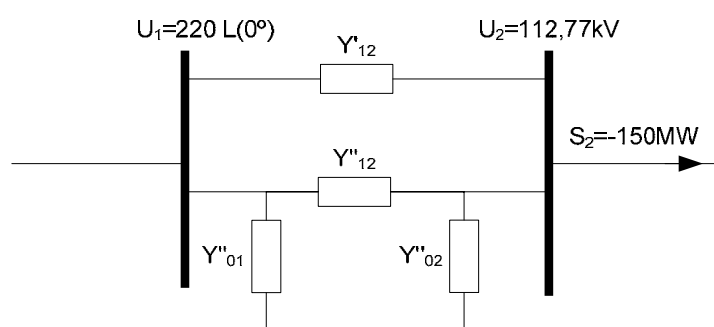
Koliki prijenosni odnos mora imati 2. transformator da bi napon na sekundaru bio 112,77 kV, uz zadanu snagu $S_2 = -150 \text{ MW}$ i nazivni napon na primaru?

Rješenje:

$U_1 = 220 \text{ kV}$

$S_2 = -150 \text{ MW}$

$a = ?$



$S_B = 150 \text{ MVA}$

$Y_T = -j10 \text{ p.u.}$

$Y_{12}' = -j10 \text{ p.u.} \quad Y_{12}'' = -\frac{j10}{a_2} \quad Y_{01}'' = \frac{Y_T}{a_2} \left(\frac{1}{a_2} - 1 \right)$

$Y_{02}'' = Y_T \left(1 - \frac{1}{a_2} \right)$

$\begin{vmatrix} I_1 \\ I_2 \end{vmatrix} = |\vec{Y}| \begin{vmatrix} U_1 \\ U_2 \end{vmatrix}$

$|\vec{Y}| = \begin{vmatrix} Y_T + \frac{Y_T}{a_2} + \frac{Y_T}{a_2} \left(\frac{1}{a_2} - 1 \right) & -Y_T \left(1 + \frac{1}{a_2} \right) \\ -Y_T \left(1 + \frac{1}{a_2} \right) & Y_T + \frac{Y_T}{a_2} + Y_T \left(1 - \frac{1}{a_2} \right) \end{vmatrix} = \begin{vmatrix} Y_T \left(1 + \frac{1}{a_2^2} \right) & -Y_T \left(1 + \frac{1}{a_2} \right) \\ -Y_T \left(1 + \frac{1}{a_2} \right) & 2Y_T \end{vmatrix}$

$\vec{I}_1 = Y_T \left(1 + \frac{1}{a_2^2} \right) \vec{U}_1 - Y_T \left(1 + \frac{1}{a_2} \right) \vec{U}_2$

$\vec{I}_2 = -Y_T \left(1 + \frac{1}{a_2} \right) \vec{U}_1 + 2Y_T \vec{U}_2$

$\vec{I}_2 = \frac{\vec{S}_2^*}{\vec{U}_2^*}$

$$\frac{\vec{S}_2^*}{\vec{U}_2^*} = -Y_T \left(1 + \frac{1}{a_2} \right) \vec{U}_1 + 2Y_T \vec{U}_2 \quad / \cdot U_2^*$$

$$\vec{S}_2^* = -Y_T \left(1 + \frac{1}{a_2} \right) \vec{U}_1 \vec{U}_2^* + 2Y_T |\vec{U}_2|^2$$

$$\vec{U}_2^* \left(1 + \frac{1}{a_2} \right) = \frac{2Y_T |\vec{U}_2|^2}{Y_T \vec{U}_1} - \frac{\vec{S}_2^*}{Y_T \vec{U}_1} = \frac{2|\vec{U}_2|^2}{\vec{U}_1} - \frac{\vec{S}_2^*}{Y_T \vec{U}_1}$$

$$\vec{S}_2[p.u.] = -1 p.u. \quad \vec{U}_1[p.u.] = 1 + j0 \quad Y_T[p.u.] = -j10 p.u.$$

$$|\vec{U}_2|[p.u.] = \frac{112,77}{110} = 1,02518 p.u.$$

$$\frac{2 \cdot 1,02518^2}{1} - \frac{-1}{-j10 \cdot 1} = 2,102 + j0,1 p.u. = 2,104 \underline{2,724^\circ}$$

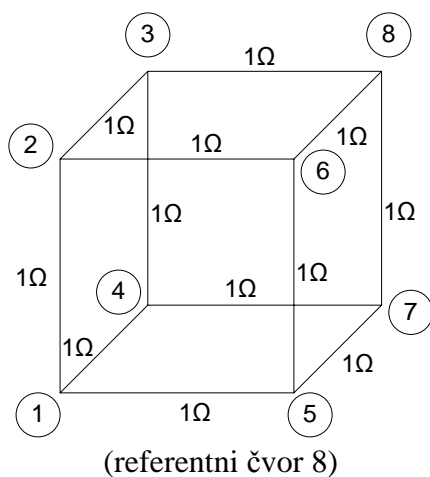
$$\vec{U}_2^* \left(1 + \frac{1}{a_2} \right) = |\vec{U}_2| \left(1 + \frac{1}{a_2} \right) \underline{-\varphi} = 2,104 \underline{2,724^\circ}$$

$$\varphi = -2,724^\circ$$

$$1 + \frac{1}{a_2} = \frac{2,104}{1,02518} = 2,0523$$

$$a_2 = \frac{1}{1,0523} = 0,95$$

ZADATAK 7 Zadana je "konfiguracija otpora" prema slici. Odredi nadomjesni otpor između točaka 1 i 8.



Rješenje:

$$\vec{Y} = \begin{vmatrix} 3 & -1 & 0 & -1 & -1 & 0 & 0 \\ -1 & 3 & -1 & 0 & 0 & -1 & 0 \\ 0 & -1 & 3 & -1 & 0 & 0 & 0 \\ -1 & 0 & -1 & 3 & 0 & 0 & -1 \\ -1 & 0 & 0 & 0 & 3 & -1 & -1 \\ 0 & -1 & 0 & 0 & -1 & 3 & 0 \\ 0 & 0 & 0 & -1 & -1 & 0 & 3 \end{vmatrix}$$

Precrtani stupac:

$$Y_{i,j}^{(n)} = -\frac{Y_{i,j}^{(n-1)}}{Y_{j,j}^{(n-1)}} ; i = 1, \dots, N ; i \neq j$$

Precrtani redak

$$Y_{j,i}^{(n)} = -\frac{Y_{j,i}^{(n-1)}}{Y_{j,j}^{(n-1)}} ; i = 1, \dots, N ; i \neq j$$

$$\vec{Y}^{(1)} = \begin{vmatrix} 3 & -1 & 0 & -1 & -1 & 0 & 0 \\ -1 & 8/3 & 1/3 & -1/3 & 0 & -1 & 0 \\ 0 & -1/3 & 1/3 & -1/3 & 0 & 0 & 0 \\ -1 & -1/3 & 1/3 & 8/3 & 0 & 0 & -1 \\ -1 & 0 & 0 & 0 & 3 & -1 & -1 \\ 0 & -1 & 0 & 0 & -1 & 3 & 0 \\ 0 & 0 & 0 & -1 & -1 & 0 & 3 \end{vmatrix}$$

Vanjski elementi

$$Y_{k,l}^{(n)} = Y_{k,l}^{(n-1)} - \frac{Y_{k,j}^{(n-1)} \cdot Y_{j,l}^{(n-1)}}{Y_{j,j}^{(n-1)}}$$

$$; k = 1, \dots, N ; k \neq j$$

$$; l = 1, \dots, N ; l \neq j$$

Pivot

$$Y_{j,j}^{(n)} = \frac{1}{Y_{j,j}^{(n-1)}}$$

$$\vec{Y}^{(2)} = \begin{vmatrix} 3 & -1 & 0 & -1 & -1 & 0 & 0 \\ -1 & 7/3 & 1/3 & -1/3 & -1/3 & 1/3 & 0 \\ 0 & -1/3 & 1/3 & -1/3 & 0 & 0 & 0 \\ -1 & -1/3 & 1/3 & 8/3 & 0 & 0 & -1 \\ -1 & -1/3 & 0 & 0 & 8/3 & 1/3 & -1 \\ 0 & -1/3 & 0 & 0 & -1/3 & 1/3 & 0 \\ 0 & 0 & 0 & -1 & -1 & 0 & 3 \end{vmatrix}$$

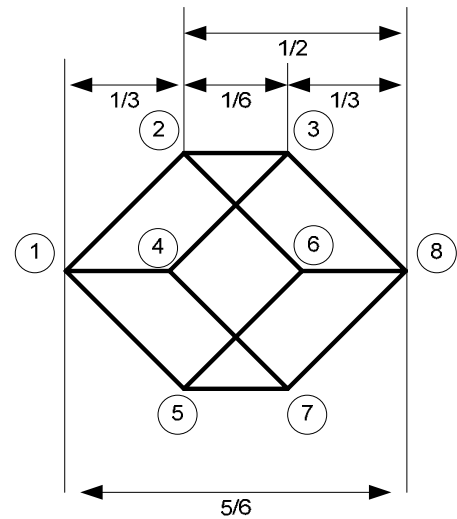
$$\vec{Y}^{(3)} = \begin{bmatrix} 3 & 1 & 0 & 1 & 1 & 0 & 0 \\ -1 & 7/3 & 1/3 & -1/3 & -1/3 & 1/3 & 0 \\ 0 & -1/3 & 1/3 & -1/3 & 0 & 0 & 0 \\ -1 & -1/3 & 1/3 & 7/3 & -1/3 & 0 & 1/3 \\ -1 & -1/3 & 0 & -1/3 & 7/3 & 1/3 & 1/3 \\ 0 & -1/3 & 0 & 0 & -1/3 & 1/3 & 0 \\ 0 & 0 & 0 & -1/3 & -1/3 & 0 & 1/3 \end{bmatrix}$$

$$\vec{Y}^{(6)} = \begin{bmatrix} 1/2 & 3/12 & 1/6 & 1/4 & -2/3 & 1/12 & 1/12 \\ 1/4 & 9/16 & 1/4 & 3/16 & -1/2 & 3/16 & 1/16 \\ 1/6 & 1/4 & 1/2 & 1/4 & -1/3 & 1/12 & 1/18 \\ 1/4 & 3/6 & 1/4 & 9/16 & -1/2 & 1/16 & 3/16 \\ 2/3 & 1/2 & 1/3 & 1/2 & 4/3 & 1/2 & 1/2 \\ 1/12 & 3/16 & 1/12 & 1/16 & -1/2 & 57/141 & 1/48 \\ 1/12 & 1/16 & 1/12 & 3/16 & -1/2 & 1/18 & 19/48 \end{bmatrix}$$

$$\vec{Y}^{(4)} = \begin{bmatrix} 1/3 & -1/3 & 0 & -1/3 & -1/3 & 0 & 0 \\ 1/3 & 6/3 & 1/3 & 2/3 & -2/3 & 1/3 & 0 \\ 0 & -1/3 & 1/3 & -1/3 & 0 & 0 & 0 \\ 1/3 & -1/3 & 1/3 & 4/3 & -2/3 & 0 & 1/3 \\ 1/3 & -1/3 & 0 & -2/3 & 6/3 & 1/3 & 1/3 \\ 0 & -1/3 & 0 & 0 & -1/3 & 1/3 & 0 \\ 0 & 0 & 0 & -1/3 & -1/3 & 0 & 1/3 \end{bmatrix}$$

$$\vec{Y}^{(7)} = \begin{bmatrix} 5/6 & 1/2 & 1/3 & 1/2 & 1/2 & 1/3 & 1/3 \\ 1/2 & 3/4 & 3/8 & 6/16 & 3/8 & 3/8 & 1/4 \\ 1/3 & 3/8 & 7/12 & 3/8 & 1/4 & 5/24 & 5/24 \\ 1/2 & 3/8 & 3/8 & 3/4 & 3/8 & 1/4 & 3/8 \\ 1/2 & 3/8 & 1/4 & 3/8 & 3/4 & 3/8 & 3/8 \\ 1/3 & 3/8 & 5/24 & 1/4 & 3/8 & 7/12 & 5/24 \\ 1/3 & 1/4 & 5/24 & 3/8 & 3/8 & 5/24 & 7/12 \end{bmatrix}$$

$$\vec{Y}^{(5)} = \begin{bmatrix} 7/18 & 1/6 & 1/18 & -4/9 & -4/9 & 1/18 & 0 \\ 1/6 & 3/6 & 1/6 & -2/6 & -2/6 & 1/6 & 0 \\ 1/18 & 1/6 & 7/18 & -4/9 & -1/9 & 1/18 & 0 \\ 4/9 & 2/6 & 4/9 & 16/9 & -8/9 & 1/9 & 1/3 \\ 4/9 & 2/6 & 1/9 & -8/9 & 16/9 & 4/9 & 1/3 \\ 1/18 & 1/6 & 1/18 & -1/9 & -4/9 & 7/18 & 0 \\ 0 & 0 & 0 & -1/3 & -1/3 & 0 & 1/3 \end{bmatrix}$$



$$I_1 = 1A$$

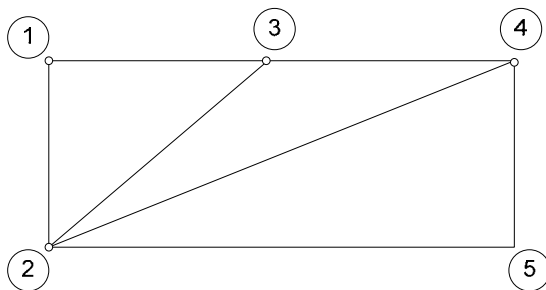
$$U_2 = 0$$

$$I_{1,n} = I_{1,2} = I_{1,5} = \frac{1}{3}A \Rightarrow U_2 = U_4 = U_5 = \frac{5}{6} - \frac{1}{3} = \frac{1}{2}V$$

$$\Rightarrow U_3 = U_6 = U_7 = \frac{1}{2} - \frac{1}{6} = \frac{1}{3}V$$

$Z_{i,j}$ - napon u čvorištu „j“ ako u „i-to“ čvorište narinemo 1A

ZADATAK 8 Za mrežu na slici, reduciraj mrežu na čvorišta 1, 2 i 3 (redukcija pasivne mreže). Y matricu formiraj kao za proračun tokova snaga pomoću Gauss-Seidel metode sa Z matricom (pri čemu poprečne grane ne ulaze u Y matricu).



Rješenje:

	$Z_{i-j} [p.u.]$	$\frac{Y_{i-j}'}{2} [p.u.]$	$Y_{i-j} [p.u.]$
1-2	0,02+j0,06	j0,003	5-j15
1-3	0,03+j0,24	j0,025	1,25-j3,75
2-3	0,06+j0,18	j0,02	1,66-j5
2-4	0,06+j0,18	j0,02	1,66-j5
2-5	0,04+j0,12	j0,015	2-j7,5
3-4	0,01+j0,03	j0,01	10-j30
4-5	0,08+j0,24	j0,025	1,25-j3,75

$$\vec{Y} = \begin{vmatrix} 6,25 - j18,75 & -5 + j15 & -1,25 + j3,75 & 0 & 0 \\ -5 + j15 & 10,833 - j32,5 & -1,66 + j5 & -1,66 + j5 & -2,5 + j7,5 \\ -1,25 + j3,75 & -1,66 + j5 & 12,916 - j38,75 & -10 + j30 & 0 \\ 0 & -1,66 + j5 & -10 + j30 & 12,916 - j38,75 & -1,25 + j3,75 \\ 0 & -2,5 + j7,5 & 0 & -1,25 + j3,75 & 3,75 - j11,25 \end{vmatrix}$$

$$\vec{Y} = \begin{vmatrix} 19,76 \angle -71,6^\circ & 15,81 \angle 108,4^\circ & 3,95 \angle 108,4^\circ & 0 & 0 \\ 15,81 \angle 108,4^\circ & 34,26 \angle -71,6^\circ & 5,27 \angle 108,4^\circ & 5,27 \angle 108,4^\circ & 7,91 \angle 108,4^\circ \\ 3,95 \angle 108,4^\circ & 5,27 \angle 108,4^\circ & 40,85 \angle -71,6^\circ & 31,62 \angle 108,4^\circ & 0 \\ 0 & 5,27 \angle 108,4^\circ & 31,62 \angle 108,4^\circ & 40,85 \angle -71,6^\circ & 3,95 \angle 108,4^\circ \\ 0 & 7,91 \angle 108,4^\circ & 0 & 3,95 \angle 108,4^\circ & 11,86 \angle -71,6^\circ \end{vmatrix}$$

$$\vec{Y} = \begin{vmatrix} 19,76 & -15,81 & -3,95 & 0 & 0 \\ -15,81 & 34,26 & -5,27 & -5,27 & -7,91 \\ -3,95 & -5,27 & 40,85 & -31,62 & 0 \\ 0 & -5,27 & -31,62 & 40,85 & -3,95 \\ 0 & -7,91 & 0 & -3,95 & 11,86 \end{vmatrix}$$

$$\vec{Y}^{1234} = \begin{vmatrix} 19,76 & -15,81 & -3,95 & 0 \\ -15,81 & 28,98 & -5,27 & -7,90 \\ -3,95 & -5,27 & 40,85 & -31,62 \\ 0 & -7,90 & -31,62 & 39,53 \end{vmatrix} \rightarrow \begin{vmatrix} 19,76 & -15,81 & -3,95 \\ -15,81 & 27,40 & -11,59 \\ -3,95 & -11,59 & 15,56 \end{vmatrix}$$

$$\begin{aligned} \vec{Y}_{23}^{-1} &= \begin{vmatrix} 27,40 & -11,59 \\ -11,59 & 15,56 \end{vmatrix} = \begin{vmatrix} 18,77 & 0,745 \\ -0,745 & 0,0643 \end{vmatrix} = \begin{vmatrix} 0,0533 \underline{71,6^\circ} & 0,0397 \underline{71,6^\circ} \\ 0,0397 \underline{71,6^\circ} & 0,0939 \underline{71,6^\circ} \end{vmatrix} = \\ &= \begin{vmatrix} 0,0168 + j0,0506 & 0,0125 + j0,0377 \\ 0,0125 + j0,0377 & 0,0296 + j0,0891 \end{vmatrix} = |Z_{23}| \end{aligned}$$

ZADATAK 9 U transformatorskoj stanici nalaze se 2 transformatora sa slijedećim podacima:

$$\begin{aligned} \text{T1} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= 216/110 \end{aligned}$$

$$\begin{aligned} \text{T2} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= 222/110 \end{aligned}$$

Napon na primaru iznosi 215 kV, a snaga na sekundaru je 100+j30 MVA. Odredi napon na sekundaru, te tokove i gubitke snage na svakom transformatoru koristeći Gauss-Seidel metodu za Z matricom.

$$U_1 = 215 \text{ kV}$$

$$S_2 = -100 - j30 \text{ MVA}$$

$$\varepsilon = 10^{-4}$$

→

$$U_2, \Delta S', \Delta S'', S_1$$

Rješenje:

$$S_B = 100 \text{ MVA}$$

$$a_1 = \frac{216}{220} = 0,982$$

$$a_2 = \frac{222}{220} = 1,009$$

$$\begin{aligned} Y_T &= \frac{1}{Z_T} = \frac{1}{\frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} + j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right]} \cdot \frac{\frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right]}{\frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} + j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right]} = \frac{\frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right]}{\left(\frac{U_n^2 P_k^2}{S_n^4} \right) + \left[u_k^2 - \left(\frac{P_k}{S_n} \right)^2 \right] \frac{U_n^4}{S_n^2}} = \\ &= \frac{\frac{U_n^2}{S_n} \left[\frac{P_k}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right]}{u_k^2 \frac{U_n^2}{S_n}} = \frac{S_n}{U_n^2} \cdot \frac{1}{u_k^2} \left[\frac{P_k}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right] \end{aligned}$$

$$Y_T [p.u.] = Y_T \cdot \frac{U_n^2}{S_B} = \frac{S_n}{S_B \cdot u_k^2} \left[\frac{P_k}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_k}{S_n} \right)^2} \right] [p.u.]$$

$$Y_{1,2}' = \frac{Y_T [p.u.]}{a_1} = 1,6835 - j7,21356$$

$$Y_{10}' = Y_{12}' \left(\frac{1}{a_1} - 1 \right) = 0,03118 - j0,13358$$

$$Y_{20}' = Y_{12}' a_1' \left(1 - \frac{1}{a_1} \right) = -0,03061 + j0,13116$$

$$Y_{12}'' = 1,638 - j7,0186$$

$$Y_{10}'' = -0,01476 + j0,06323$$

$$Y_{20}'' = 0,01489 - j0,06381$$

Z_{22} – element Z -matrice, tj. invertirane Y -matrice (u ovom slučaju dimenzije 1x1)

$$Z_{22} = \frac{1}{Y_{12}' + Y_{12}''} = 0,01555 + j0,06663$$

$$Y_{20} = Y_{20}' + Y_{20}'' = -0,01572 + j0,06735$$

$$S_2^* = \frac{-100 + j30}{100} = -1 + j0,3$$

pretpostavljamo $U_2^{(0)} = 1 + j0$

$$I_2^{(0)} = \frac{S_2^*}{U_2^{(0)*}} - U_2^{(0)} Y_{20} = -0,98428 + j0,23265$$

$$U_2^{(1)} = U_1 + Z_{22} I_2^{(0)} = 0,94646 - j0,06197$$

$$I_2^{(1)} = -1,02069 + j0,31978$$

$$U_2^{(2)} = 0,94009 - j0,06304$$

$$I_2^{(2)} = -1,02713 + j0,92439$$

$$U_2^{(3)} = 0,93968 - j0,06340$$

$$I_2^{(3)} = -1,02742 + j0,325$$

$$U_2^{(4)} = 0,93964 - j0,06341 = 103,6 \angle -3,86^\circ \text{ kV}$$

$$S_{1-2}' = U_1 [(U_1 - U_2) Y_{12}' + U_1 Y_{10}']^* = U_1 (U_1^* - U_2^*) Y_{12}^* + |U_1|^2 \cdot Y_{10}^*$$

$$S_{2-1}' = U_2 (U_1^* - U_2^*) Y_{12}^* + |U_2|^2 \cdot Y_{20}^*$$

$$S_{1-2}' = 0,539 + j0,289 \quad S_{2-1}' = -0,527 - j0,238$$

$$\Delta S' = S_{1-2}' + S_{2-1}' = 0,012 + j0,051 = 1,2 + j5,1 \text{ MVA}$$

$$S_{1-2}'' = 0,481 + j0,096 \quad S_{2-1}'' = -0,473 - j0,062$$

$$\Delta S'' = 0,008 + j0,034 = 0,8 + j3,4 \text{ MVA}$$

$$\Delta S = \Delta S' + \Delta S'' = 2 + j8,5 \text{ MVA}$$

ZADATAK 10 U transformatorskoj stanici nalaze se 2 transformatora sa slijedećim podacima:

$$\begin{aligned} \text{T1} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= 216/110 \end{aligned}$$

$$\begin{aligned} \text{T2} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= 222/110 \end{aligned}$$

Napon na primaru iznosi 215 kV, a snaga na sekundaru je 100+j30 MVA. Odredi napon na sekundaru, te tokove i gubitke snage na svakom transformatoru koristeći Gauss-Seidel metodu za Y matricom.

$$U_1 = 215 \text{ kV}$$

$$S_2 = -100 - j30 \text{ MVA}$$

→

$$U_2, \Delta S', \Delta S'', S_1$$

$$\varepsilon = 10^{-4}$$

Rješenje:

$$\begin{aligned} S_B &= 100 \text{ MVA} & a_1 &= \frac{216}{220} = 0,982 & a_2 &= \frac{222}{220} = 1,009 & U_1 &= \frac{215}{220} = 0,97727 \\ Y_{12}' &= 1,6835 - j7,21356 & Y_{10}' &= 0,03118 - j0,13358 & Y_{20}' &= -0,03061 + j0,13116 \\ Y_{12}'' &= 1,638 - j7,0186 & Y_{10}'' &= -0,01476 + j0,06323 & Y_{20}'' &= 0,01489 - j0,06381 \end{aligned}$$

$$Y = \begin{bmatrix} Y_{12}' + Y_{12}'' + Y_{10}' + Y_{10}'' & -Y_{12}' - Y_{12}'' \\ -Y_{12}' - Y_{12}'' & Y_{12}' + Y_{12}'' + Y_{20}' + Y_{20}'' \end{bmatrix}$$

$$Y = \begin{bmatrix} 3,33792 - j14,30251 & -3,3215 + j14,23216 \\ -3,3215 + j14,23216 & 3,30578 - j14,16481 \end{bmatrix}$$

Opći član:

$$U_i^{(k+1)} = \frac{KL_i}{(U_i^{(k)})^*} - \sum_{j=1}^{i-1} YL_{i,j} \cdot U_j^{(k+1)} - \sum_{j=i+1}^n YL_{i,j} \cdot U_j^{(k)}$$

$$i = 1, \dots, n$$

$$i \neq ref$$

KL_i članova ima $(n-1)$ – u našem slučaju $2-1=1$.

$YL_{i,j}$ članova ima koliko ima van dijagonalnih elemenata – elementi u referentnom retku.

$$KL_2 = \frac{S_2^*}{Y_{2,2}} = \frac{-1 + j0,3}{3,30578 - j14,16481} = 0,0717771 \angle 240,16^\circ = -0,03571 - j0,06226$$

$$YL_{2,1} = \frac{Y_{2,1}}{Y_{2,2}} = \frac{-3,3215 + j14,23216}{3,30578 - j14,16481} = 1,004755 \angle 180^\circ = -1,004755$$

$$U_2^{(0)} = 1 + j0$$

$$U_2^{(1)} = \frac{KL_2}{(U_2^{(0)})^*} - Y_{L_{2,1}} \cdot U_1$$

$$Y_{L_{2,1}} \cdot U_1 = -1,004755 \cdot 0,97727 = -0,98192$$

$$U_2^{(1)} = \frac{0,07177 \angle 240,16^\circ}{1} + 0,98192 = -0,03571 - j0,06226 + 0,98192$$

$$U_2^{(1)} = 0,94621 - j0,06226$$

Izaberemo $\alpha = 1,2$ (faktor ubrzanja)

$$\Delta U_2^{(1)} = U_2^{(1)} - U_{2ub}^{(0)} = 0,94621 - j0,06226 - 1 = -0,05379 - j0,06226$$

$$U_{2ub}^{(1)} = U_{2ub}^{(0)} + \alpha \Delta U_2^{(1)} = 1 + j0 + 1,2(-0,05379 - j0,06226) = 0,93545 - j0,07471 = 0,93843 \angle -4,566^\circ$$

$$U_2^{(2)} = \frac{KL_2}{(U_{2ub}^{(1)})^*} - Y_{L_{2,1}} \cdot U_1 = \frac{0,07177 \angle 240,16^\circ}{0,93843 \angle -4,566^\circ} + 0,98192 = 0,93871 - j0,06310$$

$$\Delta U_2^{(2)} = U_2^{(2)} - U_{2ub}^{(1)} = 0,93871 - j0,06310 - 0,93545 + j0,07471 = 0,00326 + j0,01161$$

$$U_{2ub}^{(2)} = U_{2ub}^{(1)} + \alpha \Delta U_2^{(2)} = 0,93545 - j0,07471 + 1,2(0,00326 + j0,01161) = 0,93936 - j0,06078 = 0,94132 \angle -3,70^\circ$$

$$U_2^{(3)} = \frac{0,07177 \angle 240,16^\circ}{0,94132 \angle -3,70^\circ} + 0,98192 = 0,93979 - j0,06355$$

$$\Delta U_2^{(3)} = U_2^{(3)} - U_{2ub}^{(2)} = 0,93979 - j0,06355 - 0,93936 + j0,06078 = 0,00043 - j0,00277$$

$$U_{2ub}^{(3)} = U_{2ub}^{(2)} + \alpha \Delta U_2^{(3)} = 0,93988 - j0,06410 = 0,94206 \angle -3,90^\circ$$

$$U_2^{(4)} = \frac{0,07177 \angle 240,16^\circ}{0,94206 \angle -3,90^\circ} + 0,98192 = 0,93960 - j0,06335 = 0,94173 \angle -3,86^\circ$$

$$\Delta U_2^{(4)} = U_2^{(4)} - U_{2ub}^{(3)} = -0,00027 + j0,00075$$

$$U_{2ub}^{(4)} = U_{2ub}^{(3)} + \alpha \Delta U_2^{(4)} = 0,93955 - j0,06320 = 0,94167 \angle -3,85^\circ$$

$$U_2^{(5)} = \frac{0,07177 \angle 240,16^\circ}{0,94167 \angle -3,85^\circ} + 0,98192 = 0,93965 - j0,06342$$

$$\Delta U_2^{(5)} = U_2^{(5)} - U_{2ub}^{(4)} = 0,0001 - j0,00022$$

$$U_{2ub}^{(5)} = U_{2ub}^{(4)} + \alpha \Delta U_2^{(5)} = 0,93966 - j0,06346 = 0,94180 \angle -3,86^\circ$$

$$U_2^{(6)} = \frac{0,07177 \angle 240,16^\circ}{0,94180 \angle -3,86^\circ} + 0,98192 = 0,93963 - j0,06340$$

$$\Delta U_2^{(6)} = U_2^{(6)} - U_{2ub}^{(5)} = -0,00003 + j0,00006$$

$U_2 = 0,93963 - j0,06340 = 0,94177 \angle -3,86^\circ$ $U_2 = 103,6 \angle -3,86^\circ \text{ kV}$
--

ZADATAK 11 Zadani su podaci za transformatore u stanici.

$$\begin{aligned} \text{T1} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= \frac{216}{110} \end{aligned}$$

$$\begin{aligned} \text{T2} \quad S_n &= 80 \text{ MVA} \\ P_k &= 2 \text{ MW} \\ u_k &= 11\% \\ a_1 &= \frac{222}{110} \end{aligned}$$

Napon na primaru iznosi $U_1 = 215 \text{ kV}$, a snaga sekundara je $S_2 = -100 - j30 \text{ MVA}$. Odrediti napon na sekundaru i tokove snage kroz transformatore koristeći Newton-Rapshon metodu. $\varepsilon = 10^{-2}$.

Rješenje:

$$S_B = 100 \text{ MVA}$$

$$a_1 = \frac{\frac{216}{110}}{\frac{220}{110}} = 0,98182 \quad a_2 = \frac{\frac{222}{110}}{\frac{220}{110}} = 1,009$$

$$Y_{1,2}' = \frac{1}{a_1} \left[\frac{S_n}{S_B u_k^2} \cdot \left(\frac{P_n}{S_n} - j \sqrt{u_k^2 - \left(\frac{P_n}{S_n} \right)^2} \right) \right] = 1,6835 - j7,21356 \text{ p.u.}$$

$$Y_{1,0}' = Y_{12}' \left(\frac{1}{a_1} - 1 \right) = 0,03118 - j0,13358 \text{ p.u.}$$

$$Y_{2,0}' = Y_{1,2}' \cdot a_1 \left(1 - \frac{1}{a_1} \right) = -0,03061 + j0,13116 \text{ p.u.}$$

$$Y_{1,2}'' = 1,638 - j7,0186 \text{ p.u.}$$

$$Y_{1,0}'' = -0,01476 + j0,06323 \text{ p.u.}$$

$$Y_{2,0}'' = 0,01489 - j0,06381 \text{ p.u.}$$

$$[Y] = \begin{bmatrix} 3,33792 - j14,30231 & -3,3215 + j14,23216 \\ -3,3215 + j14,23216 & 3,30578 - j14,16481 \end{bmatrix} = \begin{bmatrix} 14,68685 \angle -76.863^\circ & 14,61461 \angle 103.137^\circ \\ 14,61461 \angle 103.137^\circ & 14,54545 \angle -76.863^\circ \end{bmatrix}$$

$$U_1 = \frac{215}{220} = 0,977273 + j0 \quad (\text{ref. čvorište})$$

$$U_2^{(0)} = 1 + j0 \quad (\text{pretpostavljeni napon})$$

Za sva nezavisna čvorišta vrijedi:

$$P_{i,izr}^{(k)} = U_i^{(k)} \sum_{j=1}^n Y_{i,j} \cdot U_j^{(k)} \cos(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)}) ; i = 1, \dots, n ; i \neq j$$

$$Q_{i,izr}^{(k)} = U_i^{(k)} \sum_{j=1}^n Y_{i,j} \cdot U_j^{(k)} \sin(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)}) ; i = 1, \dots, n ; i \neq j ; i \neq \text{gen.}$$

Referentno čvorište 1:

$$i = 2$$

$$\begin{aligned} P_2^{(0)} &= U_2^{(0)} \left[Y_{2,1} \cdot U_1 \cos(-\Theta_{2,1} + \delta_2^{(0)} - \delta_1) + Y_{2,2} \cdot U_2^{(2)} \cos(-\Theta_{2,2}) \right] = \\ &= 1 \cdot 14,61461 \cdot 0,977273 \cdot \cos(-103,137) + 1 \cdot 14,54545 \cdot \cos(76,863) = \\ &= -3,24612 + 3,3058 = 0,0598 \end{aligned}$$

$$\begin{aligned} Q_2^{(0)} &= U_2^{(0)} \left[Y_{2,1} \cdot U_1 \sin(-\Theta_{2,1} + \delta_2^{(0)} - \delta_1) + Y_{2,2} \cdot U_2^{(2)} \sin(-\Theta_{2,2}) \right] = \\ &= 1 \cdot 14,61461 \cdot 0,977273 \cdot \sin(-103,137) + 1 \cdot 1 \cdot 14,54545 \cdot \sin(76,863) = \\ &= 13,9087 + 14,16481 = 0,25611 \end{aligned}$$

$$\Delta P_2^{(0)} = P_2^{ZAD} - P_2^{(0)} = -1 - 0,0598 = -1,0598$$

$$\Delta Q_2^{(0)} = Q_2^{ZAD} - Q_2^{(0)} = -0,3 - 0,25611 = -0,55611$$

I₁ za $i, j \neq ref$.:

$$\left(\frac{\partial P_i}{\partial \delta_j} \right)^{(k)} = U_i^{(k)} \cdot U_j^{(k)} \cdot Y_{i,j} \cdot \sin(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)}) \quad i \neq j$$

$$\left(\frac{\partial P_i}{\partial \delta_i} \right)^{(k)} = - \sum_{\substack{j=1 \\ j \neq i}}^n U_i^{(k)} \cdot U_j^{(k)} \cdot Y_{i,j} \cdot \sin(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)})$$

I_n za $i, j \neq ref$.:

$$\left(\frac{\partial Q_i}{\partial U_j} \cdot U_j \right)^{(k)} = U_i^{(k)} \cdot U_j^{(k)} \cdot Y_{i,j} \cdot \sin(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)}) \quad i \neq j$$

$$\left(\frac{\partial Q_i}{\partial U_i} \cdot U_i \right)^{(k)} = 2U_i^{(k)} \cdot U_i^{(k)} \cdot Y_{i,i} \cdot \sin(\Theta_{ii}) + \sum_{\substack{j=1 \\ j \neq i}}^n U_i^{(k)} \cdot U_j^{(k)} \cdot Y_{i,j} \cdot \sin(-\Theta_{i,j} + \delta_i^{(k)} - \delta_j^{(k)})$$

$$\begin{aligned} \left(\frac{\partial P_2}{\partial \delta_2} \right)^{(0)} &= -U_2^{(0)} \cdot U_1^{(0)} \cdot Y_{2,1} \cdot \sin(-\Theta_{2,1} + \delta_2^{(0)} - \delta_1^{(0)}) = \\ &= -1 \cdot 0,977273 \cdot 14,61461 \cdot \sin(-103,137) = 13,9087 \end{aligned}$$

$$\begin{aligned} \left(\frac{\partial Q_2}{\partial U_2} \cdot U_2 \right)^{(0)} &= 2U_2^{(0)} \cdot U_2^{(0)} \cdot Y_{2,2} \cdot \sin(-\Theta_{2,2}) + U_2^{(0)} \cdot U_1 \cdot Y_{2,2} \cdot \sin(-\Theta_{2,2} + \delta_2^{(0)} - \delta_1^{(0)}) = \\ &= 2 \cdot 1 \cdot 1 \cdot 14,54545 \cdot \sin(76,863) + 1 \cdot 0,977273 \cdot 14,61461 \cdot \sin(-103,137) = 14,4209 \end{aligned}$$

$$\Delta P_2^{(0)} = \left(\frac{\partial P_2}{\partial \delta_2} \right)^{(0)} \Delta \delta_2^{(0)} \quad \Rightarrow \quad -1,0598 = 13,9087 \cdot \Delta \delta_2^{(0)}$$

$$\Delta Q_2^{(0)} = \left(\frac{\partial Q_2}{\partial U_2} \cdot U_2 \right)^{(0)} \left(\frac{\Delta U_2}{U_2} \right)^{(0)} \quad \Rightarrow \quad -0,55611 = 14,4209 \cdot \left(\frac{\Delta U_2}{U_2} \right)^{(0)}$$

$$\Delta\delta_2^{(0)} = -\frac{1,0598}{13,9087} = -0,076197$$

$$\left(\frac{\Delta U_2}{U_2}\right)^{(0)} = -\frac{0,55611}{14,4209} = -0,038563 \quad \longrightarrow \quad \text{kraj 0. iteracijskog koraka}$$

$$U_2^{(1)} = U_2^{(0)} + \left(\frac{\Delta U_2}{U_2}\right)^{(0)} \cdot U_2^{(0)} = 1 - 0,038569 = 0,961437$$

$$\delta_2^{(1)} = \delta_2^{(0)} + \Delta\delta_2^{(0)} = -0,076197 \text{ rad} = -4,366^\circ$$

$$\begin{aligned} P_2^{(1)} &= 0,961437 \cdot 14,61461 \cdot 0,977273 \cdot \cos(-103,137 - 4,366) + \\ &\quad + 0,961437 \cdot 14,54545 \cdot 0,961437 \cdot \cos(76,863) = \\ &= -4,12988 + 3,05984 = -1,074 \end{aligned}$$

$$\begin{aligned} Q_2^{(1)} &= 0,961437 \cdot 14,61461 \cdot 0,977273 \cdot \sin(-103,137 - 4,366) + \\ &\quad + 0,961437 \cdot 14,54545 \cdot 0,961437 \cdot \sin(76,863) = \\ &= -13,09599 + 13,09338 = -0,00255 \end{aligned}$$

$$\Delta P_2^{(1)} = P_2^{\text{ZAD}} - P_2^{(1)} = -1 + 1,074 = 0,074$$

$$\Delta Q_2^{(1)} = Q_2^{\text{ZAD}} - Q_2^{(1)} = -0,3 + 0,00255 = -0,29745$$

$$\left(\frac{\partial P_2}{\partial \delta_2}\right)^{(1)} = -0,961437 \cdot 0,977279 \cdot 14,61461 \cdot \sin(-103,137 - 4,366) = 13,09983$$

$$\begin{aligned} \left(\frac{\partial Q_2}{\partial U_2} \cdot U_2\right)^{(1)} &= 2 \cdot 0,961437^2 \cdot 14,54545 \cdot \sin(76,869) + \\ &\quad + 0,961437 \cdot 0,977273 \cdot 14,61451 \cdot \sin(-107,303) = \\ &= 26,186736 - 13,09393 = 13,090826 \end{aligned}$$

$$\Delta P_2^{(1)} = \left(\frac{\partial P_2}{\partial \delta_2}\right)^{(1)} \cdot \Delta\delta_2^{(1)} \quad \Rightarrow \quad 0,075 = 13,09393 \cdot \Delta\delta_2^{(1)}$$

$$\Delta Q_2^{(1)} = \left(\frac{\partial Q_2}{\partial U_2} \cdot U_2\right)^{(1)} \cdot \left(\frac{\Delta U_2}{U_2}\right)^{(1)} \quad \Rightarrow \quad -0,29745 = 13,090825 \cdot \left(\frac{\Delta U_2}{U_2}\right)^{(1)}$$

$$\Delta\delta_2^{(1)} = \frac{0,074}{13,09593} = 0,00363 = 0,3237^\circ$$

$$\left(\frac{\Delta U_2}{U_2}\right)^{(1)} = -\frac{0,29745}{13,09393} = -0,02272$$

$$U_2^{(2)} = U_2^{(1)} + \left(\frac{\Delta U_2}{U_2}\right)^{(1)} \cdot U_2^{(1)} = 0,961437 - 0,02272 \cdot 0,961437 = 0,93959$$

$$\Delta\delta_2^{(2)} = \delta_2^{(1)} + \Delta\delta_2^{(1)} = -4,366 + 0,3237 = -4,0423$$

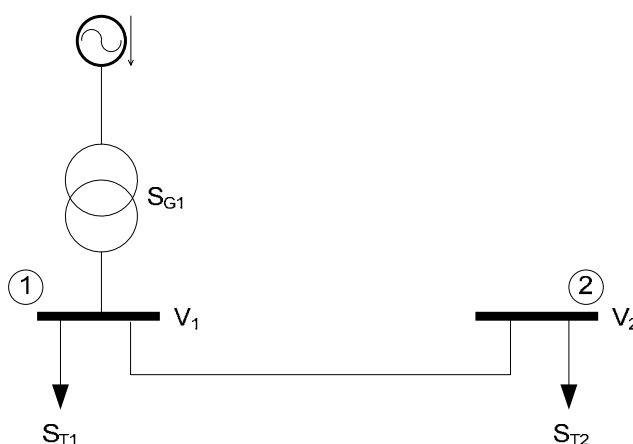
$$\begin{aligned} P_2^{(2)} &= 0,93939 \cdot 14,61461 \cdot 0,977273 \cdot \cos(-103,137 - 4,0423) + \\ &\quad + 0,93939 \cdot 14,54545 \cdot \cos(76,863) = -3,96367 + 2,91863 = -1,045 \end{aligned}$$

$$Q_2^{(2)} = \dots$$

$$\Delta P_2^{(2)} = 0,045$$

$$\Delta Q_2^{(2)} = \dots$$

ZADATAK 12 Za mali sustav na slici, napravi proračun tokova snaga Gauss-Seidelovom metodom pomoću Y-matrice.



Zadano:

$$V_1 = 1,05 \angle 0^\circ [p.u.]$$

$$Y_V = 0,3044 - j1,87996 [p.u.]$$

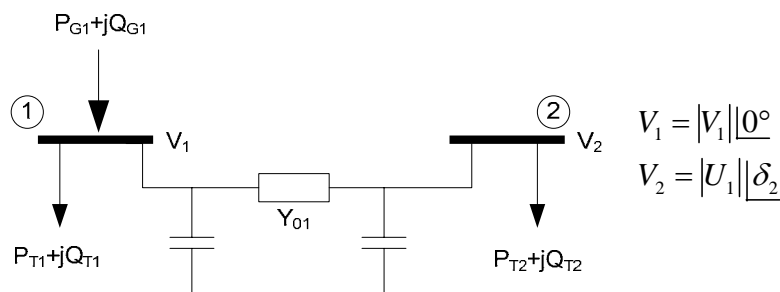
$$S_{T1} = 1,15 + j0,31 [p.u.]$$

$$\frac{Y_P}{2} = j0,06366 [p.u.]$$

$$S_{T2} = 0,45 + j0,20 [p.u.]$$

$$|V_2^{(0)}| = 0,95 \quad ; \quad \delta_2^{(0)} = -13,5^\circ \quad ; \quad \varepsilon = 10^{-4}$$

Rješenje:



$$|Y| = \begin{bmatrix} 0,3044 - j1,8163 & -0,3044 + j1,87996 \\ -0,3044 + j1,87996 & 0,3044 - j1,8163 \end{bmatrix} = \begin{bmatrix} 1,8416 \angle -80,48561^\circ & 1,904443 \angle 99,197819^\circ \\ 1,904443 \angle 99,197819^\circ & 1,8416 \angle -80,48561^\circ \end{bmatrix}$$

$$|V_2^{(0)}| = 0,95 \angle \delta_2^{(0)} \quad \delta_2^{(0)} = ?$$

$$P_2 = \frac{|V_1| \cdot |V_2|}{K} \sin \delta_2 \Rightarrow 0,45 = 1,05 \cdot 0,95 (-1,87996) \cdot \sin \delta_2 \Rightarrow \delta_2 \approx -13,5^\circ$$

$$V_2^{(0)} = 0,95 \angle -13,5^\circ$$

TERET = „ - ”

$$V_i^{(k+1)} = \frac{P_i - jQ_i}{Y_{i,i}} \cdot \frac{1}{(V_i^{(k)})^*} - \sum_{j=1}^{i-1} \frac{Y_{i,j}}{Y_{i,i}} \cdot V_j^{(k+1)} - \sum_{j=i+1}^n \frac{Y_{i,j}}{Y_{i,i}} \cdot V_j^{(k)} \quad , i \neq reg.$$

$$= KL_i \cdot \frac{1}{(V_i^{(k)})^*} - \sum_{j=1}^{i-1} YL_{i,j} \cdot V_j^{(k+1)} - \sum_{j=i+1}^n YL_{i,j} \cdot V_j^{(k)}$$

$$reg = 1 \quad i \neq 1 \quad j = 1, 2$$

$$i = 2$$

$$KL_2 = \frac{-P_2 + jQ_2}{Y_{2,2}} = \frac{0,492443 \angle 156,0375^\circ}{1,841631 \angle -80,48561^\circ} = 0,267395 \angle 236,52311^\circ$$

$$YL_{2,1} = \frac{Y_{2,1}}{Y_{2,2}} = \frac{1,90443 \angle 99,197819^\circ}{1,841631 \angle -80,48561^\circ} = 1,0340997 \angle 179,68343^\circ$$

$$V_2^{(1)} = \frac{KL_2}{(V_2^{(0)})^*} - YL_{2,1} \cdot V_1 = \frac{0,267395 \angle 236,52311^\circ}{0,95 \angle 19,5^\circ} - 1,0340997 \angle 179,68343^\circ \cdot 1,05 \angle 0^\circ =$$

$$= 0,2814684 \angle 223,02311^\circ - 1,0838047 \angle 179,68343^\circ =$$

$$= -0,2057755 - j0,192044 + 1,085788 - j0,0060182 =$$

$$= 0,8800125 - j0,198622 = 0,9020258 \angle -12,684^\circ p.u.$$

$$V_2^{(2)} = \frac{KL_2}{(V_2^{(1)})^*} - YL_{2,1} \cdot V_1 =$$

$$\varepsilon = 10^{-4} \quad V_2^{(7)} = 0,89103 \angle -13,6448^\circ \quad [p.u.]$$

$$S_{1-2} = V_1 (V_1^* - V_2^*) Y_{1,2}^* + |V_1|^2 \cdot \frac{Y_p^*}{2}$$

$$S_{1-2} = 1,05 \angle 0^\circ \cdot (1,05 - 0,89103 \angle 13,6448^\circ) \cdot (0,3044 + j1,87996) + 1,05^2 \cdot (-j0,06366) =$$

$$= 0,47377 + j0,22067 \quad [p.u.]$$

$$S_{2-1} = V_2 (V_1^* - V_2^*) Y_{1,2}^* + |V_2|^2 \cdot \frac{Y_p^*}{2} =$$

$$= 0,89103 \angle -13,6448^\circ \cdot (0,89103 \angle 13,6448^\circ - 1,05) \cdot (0,3044 + j1,87996) + 0,89103^2 \cdot (-j0,06336)$$

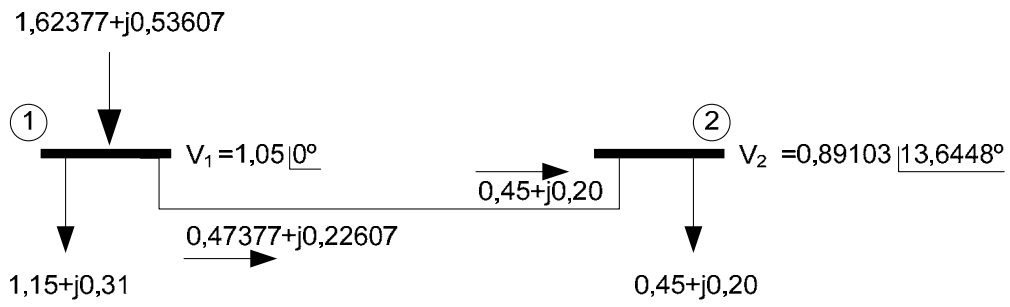
$$= -0,45000 - j0,20000 \quad [p.u.]$$

$$P_{1-2} = 0,47377 \text{ p.u.}$$

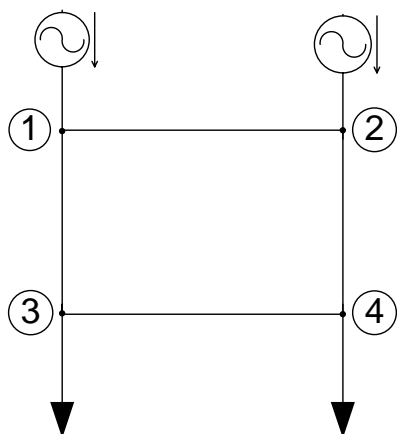
$$Q_{1-2} = 0,22067 \text{ p.u.}$$

$$P_{G1} = P_{1-2} + P_{T1} = 0,47377 + 1,15 = 1,62972 \text{ [p.u.]}$$

$$Q_{G1} = Q_{1-2} + Q_{T1} = 0,22607 + 0,31 = 0,53607 \text{ [p.u.]}$$



ZADATAK 13 Zadana je mreža na slici. Prema istosmjernom modelu, odredi tokove snaga u granama. ($S_B=100\text{MVA}$).



$$X_{2-4} = j0,1 [p.u.]$$

$$X_{3-4} = j0,15 [p.u.]$$

$$X_{1-2} = j0,2 [p.u.]$$

$$X_{1-3} = j0,1 [p.u.]$$

$$P_3 = -50\text{MW} \rightarrow -0,5 [p.u.]$$

$$P_1 = -40\text{MW} \rightarrow -0,4 [p.u.]$$

$$P_2 = 30\text{MW} \rightarrow 0,3 [p.u.]$$

$$P_{1-2} = ?; \quad P_{1-3} = ?; \quad P_{4-3} = ?; \quad P_{2-4} = ?$$

4 – ref.

Rješenje:

$$Y_{2-4} = -j10 [p.u.]$$

$$Y_{3-4} = -j6,667 [p.u.]$$

$$Y_{1-2} = -j5 [p.u.]$$

$$Y_{1-3} = -j10 [p.u.]$$

$$Z = j \begin{vmatrix} 0,13636 & 0,04545 & 0,08181 \\ 0,04545 & 0,08181 & 0,02727 \\ 0,08181 & 0,02727 & 0,10909 \end{vmatrix}$$

$$\begin{bmatrix} \delta_1 \\ \delta_2 \\ \delta_3 \end{bmatrix} = [Z] \begin{bmatrix} P_1 \\ P_2 \\ P_3 \end{bmatrix}$$

$$\delta_1 = j0,13636 \cdot (-0,4) + j0,04545 \cdot 0,3 + j0,08181 \cdot (-0,5) = -j0,08181$$

$$\delta_2 = j0,04545 \cdot (-0,4) + j0,08181 \cdot 0,3 + j0,02727 \cdot (-0,5) = -j0,007272$$

$$\delta_3 = j0,08181 \cdot (-0,4) + j0,02727 \cdot 0,3 + j0,10909 \cdot (-0,5) = -j0,079088$$

$$P_{1-2} = \frac{\delta_1 - \delta_2}{X_{1-2}} = \frac{-j0,08181 + j0,007272}{j0,1} = -0,3727 [p.u.]$$

$$P_{1-3} = \frac{\delta_1 - \delta_3}{X_{1-3}} = \frac{-j0,08181 + 0,079088}{j0,1} = -0,02722 [p.u.]$$

$$P_{2-4} = \frac{\delta_2 - \delta_4}{X_{2-4}} = \frac{-j0,007272 + 0}{j0,1} = -0,07272 [p.u.]$$

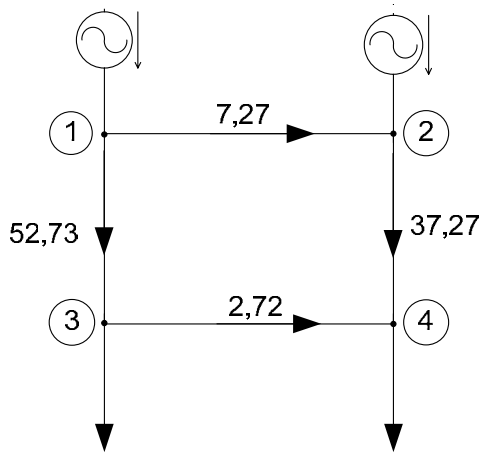
$$P_{3-4} = \frac{\delta_3 - \delta_4}{X_{3-4}} = \frac{-j0,079088 + 0}{j0,15} = -0,52725 [p.u.]$$

$$P_{1-2} = -37,26 MW$$

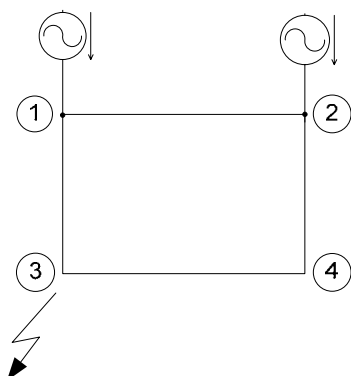
$$P_{1-3} = -2,72 MW$$

$$P_{2-4} = -7,27 MW$$

$$P_{3-4} = -52,73 MW$$



ZADATAK 14 Odredi struju kratkog spoja u vodu 1-3 u mreži na slici ako su zadane reaktancije generatora $X_{d4}'' = X_{d2}'' = j0,1$. Napon mreže je 110kV (radi određivanja struje u A). Simetrični kratki spoj je nastao u čvorištu 3 u trenutku kada je mreža bila neopterećena.



$$X_{2-4} = j0,1 [p.u.]$$

$$Y_{2-4} = -j10 [p.u.]$$

$$X_{3-4} = j0,15 [p.u.]$$

$$Y_{3-4} = -j6,667 [p.u.]$$

$$X_{1-2} = j0,2 [p.u.]$$

$$Y_{1-2} = -j5 [p.u.]$$

$$X_{1-3} = j0,1 [p.u.]$$

$$Y_{1-3} = -j10 [p.u.]$$

$$I_{1-3} = ?$$

Rješenje:

$$Y = -j \begin{vmatrix} 15 & -5 & -10 & 0 \\ -5 & 25 & 0 & -10 \\ -10 & 0 & 16,667 & -6,667 \\ 0 & -10 & -6,667 & 26,667 \end{vmatrix}$$

$$Z = Y^{-1} = j \begin{vmatrix} 0,1613 & 0,0516 & 0,1161 & 0,0484 \\ 0,0516 & 0,0643 & 0,0452 & 0,0355 \\ 0,1161 & 0,0452 & 0,1516 & 0,0548 \\ 0,0484 & 0,0355 & 0,0548 & 0,0645 \end{vmatrix}$$

$$\begin{bmatrix} U_1^k \\ U_2^k \\ 0 \\ U_4^k \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \\ 1 \\ 1 \end{bmatrix} + j[Z] \begin{bmatrix} 0 \\ 0 \\ I_m \\ 0 \end{bmatrix}$$

$$0 = 1 + j0,1516 \cdot I_m \Rightarrow I_m = j \frac{1}{0,1516} = j6,596 p.u.$$

$$U_1^k = 1 + j0,1161 \cdot I_m = 1 - 0,7658 = 0,2342 p.u.$$

$$I_{1-3} = \frac{U_1^k - U_3^k}{X_{1-3}} = \frac{0,2342}{j0,1} = -j2,342 p.u.$$

$$I_{1-3} = -j2,342 \cdot \frac{100}{\sqrt{3} \cdot 110} = -j1,229 kA$$

$$U_2^k = 1 + j0,0452 \cdot I_m = 1 - 0,2981 = 0,7019 p.u.$$

$$I_{2-1} = \frac{U_2^k - U_1^k}{X_{2-1}} = \frac{0,7019 - 0,2342}{j0,2} = -j2,339 p.u.$$

$$U_4^k = 1 + j0,0548 \cdot I_m = 1 - 0,3615 = 0,6385 p.u.$$

$$I_{2-4} = \frac{U_2^k - U_4^k}{X_{2-4}} = \frac{0,7019 - 0,6385}{j0,1} = -j0,634 p.u.$$

$$I_{4-3} = \frac{U_4^k - U_3^k}{X_{4-3}} = \frac{0,6385 - 0}{j0,15} = -j4,256 p.u.$$

