

# Control Systems

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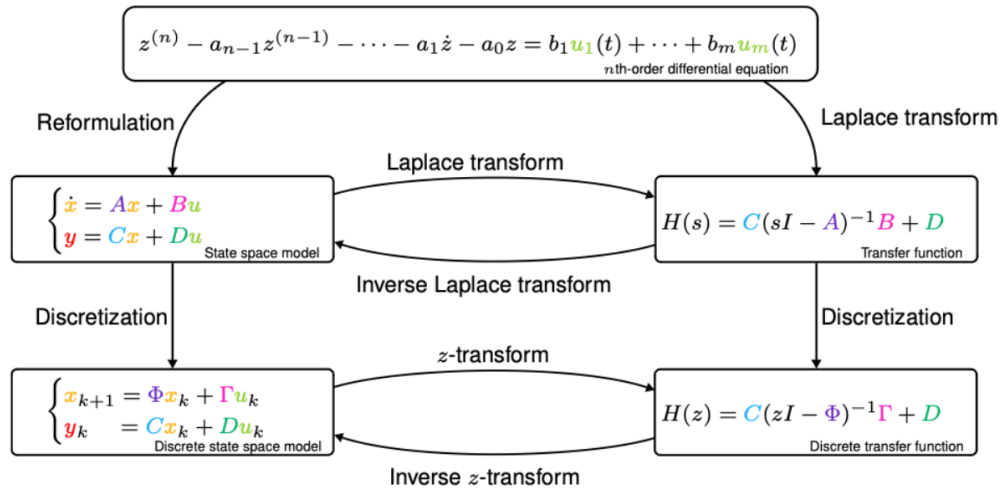
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# 1 Linear Time Invariant Systems

## Overview



## 1.1 Time-Domain models

### Linear Map

The map  $f : \mathbb{R}^n \rightarrow \mathbb{R}^m$  is said to be linear if for any  $x, y \in \mathbb{R}^n$  and  $\alpha \in \mathbb{R}$ , the following conditions hold

$$f(x + y) = f(x) + f(y) \quad \text{Super position}$$

$$f(ax) = \alpha f(x) \quad \text{Homogeneity}$$

The function has to go through (0,0) in 2D for it to be linear due to homogeneity.

### Time-Invariant System

Let  $\sigma : \mathbb{R} \times \mathbb{R}^m \rightarrow \mathbb{R}^p$  define the input-output behavior of a system model  $\Sigma$ . The system  $\Sigma$  is time-invariant if for any input signal  $u : \mathbb{R} \rightarrow \mathbb{R}^m$  and any delay  $\tau \in \mathbb{R}$  the following relation holds:

$$y(t - \tau) = \sigma(t, u(t - \tau))$$

for all times  $t \in \mathbb{R}$ , where  $y$  denotes the output signal of the system.

The importance is that the system does not change its behavior due to time. This can be seen as a canon firing at 8am it will not fire different compared to if you do the same at 5pm.

Two types of linear time-domain models.

Continuous-time state space models (based on differential equations)

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

- $x \in \mathbb{R}^n$  is state. e.g. position or velocity
- $u \in \mathbb{R}^m$  is input
- $y \in \mathbb{R}^p$  is output
- $A \in \mathbb{R}^{n \times n}$  is system matrix

- $B \in \mathbb{R}^{n \times m}$  is input matrix
- $C \in \mathbb{R}^{p \times n}$  is output matrix
- $D \in \mathbb{R}^{p \times m}$  is the direct feedthrough matrix

Discrete-time state space models (based on difference equations)

$$x_{k+1} = \Phi x_k + \Gamma u_k$$

$$y_k = Cx_k + Du_k$$

## 1.2 Frequency-Domain models

Transfer function:

$$G(s) = \frac{Q(s)}{P(s)}$$

where  $Q(s)$  and  $P(s)$  are polynomials in  $s$ .

- The roots of  $P(s)$  are called the **poles** of  $G(s)$
- The roots of  $Q(s)$  are called the **zeros** of  $G(s)$

### 1.2.1 State space to transfer function

Taking Laplace transforms of the system and assuming  $x_0 = 0$ :

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

yields:

$$sX(s) = AX(s) + BU(s)$$

$$Y(s) = CX(s) + DU(s)$$

Which can be rewritten as ( $I$  is the identity matrix):

$$X(s) = (sI - A)^{-1} BU(s)$$

$$Y(s) = \left( C (sI - A)^{-1} B + D \right) U(s)$$

where

$$Y(s) = G(s)U(s)$$

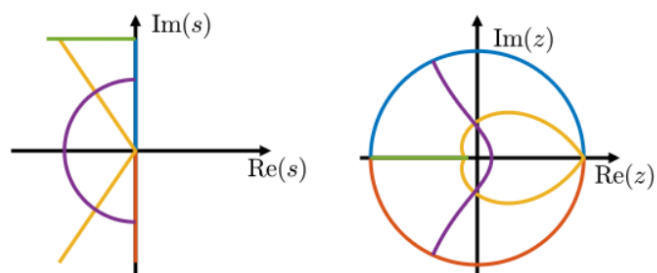
$$G(s) = C (sI - A)^{-1} B + D$$

### 1.2.2 Transfer function to state space

### 1.2.3 Discrete-time transfer function

Discretization from  $s$ -domain to  $z$ -domain can be done using:

- Matched  $z$ -transform
- Bilinear  $z$ -transform
- Impulse invariance  $z$ -transform



### 1.3 Examples

## 2 Stability and Performance Analysis

### 2.1 Basic System Classes

#### 2.1.1 First Order Systems

State-space representation of first order system:

$$\begin{aligned}\dot{x} &= -\frac{1}{\tau}x + \frac{k}{\tau}u \\ y &= x\end{aligned}$$

A first-order system has one pole and is described by:

$$H(s) = \frac{k}{\tau s + 1}$$

Where  $k$  is the DC-gain and  $\tau$  is the time-constant. The system has a pole in  $s = -\frac{1}{\tau}$  i.e., the smaller time-constant, the faster system response.

#### 2.1.2 Second Order Systems

The transfer function of a second-order system is given by:

$$H(s) = \frac{k\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

Where  $\omega_n > 0$  is the natural frequency and  $\zeta > 0$  is the damping ratio and  $k$  is the gain.

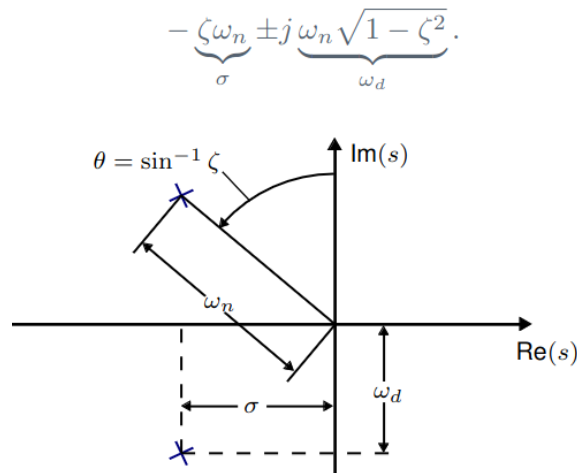
The system has two poles, which are  $s \in \mathbb{C}$  where:

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

The values of  $s$  is given by:

$$s = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$

When  $\zeta = 1$  the system is critically damped and  $H(s)$  has a double pole in  $s = -\zeta\omega_n$ , when  $0 < \zeta < 1$  the system is underdamped and has complex poles. When  $\zeta > 1$  the system is overdamped and has real and distinct poles.



Impulse response of a underdamped second-order system:

$$h(t) = k \frac{\omega_n}{\sqrt{1 - \zeta^2}} e^{-\sigma t} \sin(\omega_d t) 1(t)$$

The step response of a underdamped second-order system:

$$y(t) = k(1 - e^{-\sigma t}(\cos(\omega_d t) + \frac{\sigma}{\omega_d} \sin(\omega_d t)))$$

Impulse response of a critically damped second order system:

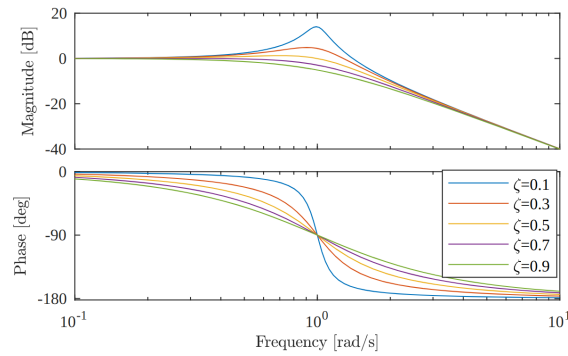
$$h(t) = k\omega_n^2 t e^{-\omega_n t}$$

Having a overdamped system with a damping ration that is greater than one leads to a slower impulse response.

The step response of a critically damped second order system:

$$y(t) = k(1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t})$$

Looking at the bode plot of a second-order system depends on the damping ratio. For every pole the magnitude of the bode plot decreases by 20dB/decade. And the phase of the bode plot decreases by 90 degrees for every pole.

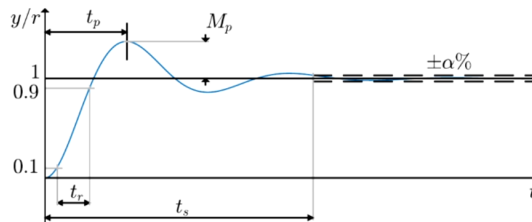


## 2.2 Performance specifications

Three different performance measurements of dynamical systems are:

1. The rise time  $t_r$  (stigtid)
2. The settling time  $t_s$  (indsvingningstid)
3. The overshoot  $M_p$  (oversving)

The rise time is the time it takes for the system to go from 10% to 90% of the final value. The settling time is the time it takes for the system to reach and stay within a certain % of the final value. The overshoot is the maximum percentage that the system goes over the final value.



The peak time is denoted  $t_p$  which is the time where the signal reaches its maximum value.

For a second-order system the rise time can be approximated as:

$$t_r = \frac{1.8}{\omega_n}$$

For a second-order system the settling time can be approximated as:

$$t_s = \frac{-\log(\alpha/100)}{\zeta\omega_n}$$

Log is ln in the equation.

The peak time can be found using:

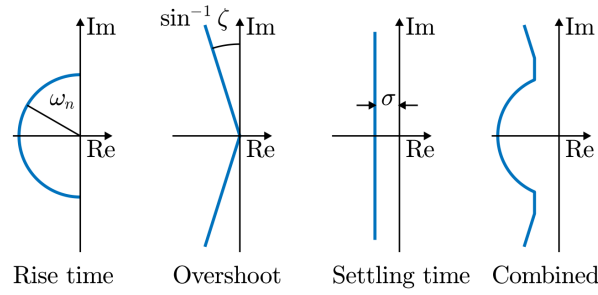
$$t_p = \frac{\pi}{\omega_d}$$

The overshoot is computed from the step response at the peak time. This gives an expression for the overshoot:

$$M_p = e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}}$$

for  $0 < \zeta < 1$ . The overshoot is given in percentage.

### Overview for determining performance variables



To obtain a rise time shorter than  $t_r$

$$\omega_n \geq \frac{1.8}{t_r}$$

To obtain an overshoot that is smaller than  $M_p$

$$\zeta \geq \sqrt{\frac{(\frac{\log(M_p)}{-\pi})^2}{1 + (\frac{\log(M_p)}{\pi})^2}}$$

To obtain an  $\alpha\%$ -settling time shorter than  $t_s$

$$\sigma \geq \frac{-\log(\alpha/100)}{t_s}$$

## 2.3 Poles and Zeros of Space-State Models

Using the state-space matrices:

$$G(s) = C(sI - A)^{-1}B + D$$

**Poles** can be found using the following equation:

When  $G(s) \rightarrow \infty$  the system has a pole at  $s \rightarrow p$ .

$$\det(pI - A) = 0$$

Here  $p$  is the eigenvalue of  $A$ .

**Zeros** can be found using the following equation:

When  $G(s) = 0$  the system has a zero at  $s = z$ .

$$\begin{vmatrix} A - zI & B \\ C & D \end{vmatrix} = 0$$

## 2.4 Stability

The stability of the dynamical system can be determined from the eigenvalues of  $A$  in the time domain. This is the equivalent of poles in the frequency domain.

$$\dot{x} = Ax + Bu$$

When the eigenvalues of  $A$  have a negative real part, the system is stable.

**Definition** A linear discrete-time system

$$x_{k+1} = \Phi x_k$$

The state of the next time step is given by  $\phi$  multiplied by  $x_k$ .

Where  $x_k \in \mathbb{R}^{n \times n}$  is asymptotically (asymptotisk) stable if

$$\lim_{k \rightarrow \infty} x_k = 0$$

for any  $x_0 \in \mathbb{R}^n$ .

A linear discrete-time system is stable if all the eigenvalues are inside the unit circle.

The closer the poles are to origin the more dominating the pole is in the system.

## 2.5 Examples