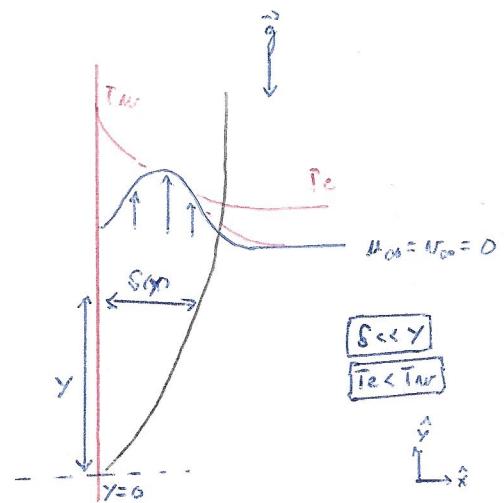


$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\rho \left[u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right] = - \frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right]$$

$$\rho \left[u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right] = - \frac{\partial p}{\partial y} + \mu \left[\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right]$$

$$\mu \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$$



simplifications:

$S \ll Y$ ✓

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\mathcal{O}\left(\frac{v}{S}\right) = O\left(\frac{v}{y}\right) \Rightarrow \boxed{U = V S \ll V}$$

méglorable

$$\boxed{\rho \left[u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right] = - \frac{1}{\rho} \frac{\partial p}{\partial x} + \left(\frac{\mu}{\rho} \right) \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right]}$$

$$\begin{aligned} \mathcal{O}(v) &\frac{v}{S} \gg \frac{v}{y^2} \\ \text{VISQUEUX} & \end{aligned}$$

$$\Rightarrow \frac{V^2}{y^2} \cdot S \gg \frac{V^2}{S^2} \Rightarrow \frac{V^2}{y^2} \cdot S = O\left(\frac{V}{y} \cdot \frac{1}{S^2}\right) \Rightarrow \frac{S^2}{y^2} = O\left(\frac{V}{y^2}\right)$$

couche lumineuse: termes d'inerties \approx termes visqueux

$$\boxed{\frac{S}{Y} = \sqrt{\frac{1}{Re_y}}} \Rightarrow \boxed{\text{Rey grand}}$$

$$\boxed{\rho \left[u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right] = - \frac{\partial p}{\partial y} + \mu \left[\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right]}$$

$$\text{Hypothèse de Prandtl: } \frac{V^2}{y} = \mu \frac{V}{S^2} \Rightarrow \frac{S^2}{y^2} = \frac{\mu}{V_p y} = \frac{1}{Re_y}$$

$$\Rightarrow \boxed{\frac{S}{Y} = \sqrt{\frac{1}{Re_y}}}$$

$$\boxed{\text{Pression dans la couche lumineuse } x \approx O(S)} \quad \checkmark \quad [P] = \left[\frac{kg}{m \cdot s^2} \right]$$

$$\begin{aligned} P(x,y) - P_0 &\approx P(S,y) - P_0 + \cancel{\frac{\partial P}{\partial x} \Big|_{x=S}^{(x,y)}} - \cancel{(x-S) \frac{\partial P}{\partial S}} + \dots \\ &= y \frac{\partial P}{\partial y} \\ &\cancel{O(y)} \cancel{O\left(\frac{V^2}{S^2}\right)} \\ &\cancel{O\left(\frac{V^2}{S^2}\right)} \cancel{O\left(\frac{V^2}{y^2}\right)} \\ &= O\left(\frac{V^2}{y^2}\right) \gg O\left(\frac{V^2 S^2}{y^2}\right) \end{aligned}$$

~~partie~~

$\Rightarrow P = \text{conste sur une trajectoire horizontale } (P(y))$

$$\Rightarrow \boxed{P(x,y) \approx O(p V^2) \approx p n^2}$$

→ on supprime l'équation car le rapport $\frac{\partial P}{\partial x}$ confluant est négligeable.

on obtient les équations de Prandtl :

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad \text{P(y)}$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = -\frac{1}{\rho} \frac{dP}{dy} + \nu \frac{\partial^2 v}{\partial x^2}$$

note : si l'écoulement est uniforme : $\frac{\partial P}{\partial y} = 0$

introduction des fonctions de courant :

$$\boxed{u = \frac{\partial \psi}{\partial y}; \quad v = -\frac{\partial \psi}{\partial x}}$$

on remplace dans les équations de Prandtl :

$$\cancel{\frac{\partial^2 \psi}{\partial x \partial y} - \frac{\partial^2 \psi}{\partial y \partial y}} = 0$$

$$-\frac{\partial u}{\partial y} \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial v}{\partial x} \frac{\partial^2 \psi}{\partial y \partial x} = -\frac{1}{\rho} \frac{dP}{dy} + \nu \frac{\partial^3 \psi}{\partial x^3}$$

on obtient :

La fonction de courant peut s'écrire : $\Psi(x,y) = -\frac{1}{\rho} \frac{dP}{dy} + \nu \frac{\partial^3 \psi}{\partial x^3}$

$$\Psi(x,y) = -4 \delta'(y) \left[\frac{1}{4} (G_n(y))^{1/4} \right]^{1/4} \quad (\text{TP 8})$$

$$\frac{\delta'}{\delta} = \frac{1}{y} + \frac{3}{4y} = \frac{7}{4y}$$

$$\boxed{\frac{\partial \eta}{\partial x} = \frac{1}{y} \left(\frac{G_n(y)}{4} \right)^{1/4} = \frac{1}{S(y)}}$$

$$\frac{1}{\delta^2} = \frac{1}{2y^2} \sqrt{G_n}$$

$$G_n = y \left(\frac{u}{G_n} \right)^{1/4}$$

$$S'(\eta) = \left(\frac{u}{G_n} \right)^{1/4} + \gamma \frac{1}{4} \left(\frac{u}{G_n} \right)^{-3/4} \left(\frac{-4}{G_n^2} \right) G_n^2$$

$$\text{avec } G_n(y) = \frac{\beta \Delta T g y^3}{\nu^2}$$

$$\boxed{\frac{\partial \eta}{\partial y} = -\frac{x}{y^2} \left(\frac{G_n(y)}{4} \right)^{1/4} + \frac{x}{y} \cdot \frac{1}{4} \left(\frac{G_n(y)}{4} \right)^{-3/4} \cdot \frac{1}{4} \frac{\beta \Delta T g y^2}{\nu^2}}$$

$$= -x \frac{S'(\eta)}{S(\eta)^2} = -\eta \frac{S'(\eta)}{S(\eta)}$$

$$= V S'(\eta) \left(f'_1(y) - f'_2(y) S'(\eta) \right)$$

on trouve donc (via l'analyse) :

$$-\frac{\partial \psi}{\partial y} = V S'(\eta) f(\eta) + V S(\eta) f'(\eta) \frac{\partial \eta}{\partial y} \quad (x,y)$$

$$= V(S'(\eta) f + S(\eta) f') \left[\frac{x}{4y} \left(\frac{G_n(y)}{4} \right)^{-3/4} \cdot \frac{3}{4} \frac{\beta \Delta T y^2}{\nu^2} - \frac{x}{y^2} \left(\frac{G_n(y)}{4} \right)^{1/4} \right]$$

$$\frac{\partial \psi}{\partial x} = -V S(\eta) f'(\eta) \frac{\partial \eta}{\partial x}$$

$$= -V S(\eta) f' \cdot \frac{1}{S(\eta)} = -V f'(\eta)$$

$$\frac{\partial^2 \psi}{\partial x^2} = -V f''(\eta) \frac{\partial \eta}{\partial x}$$

$$= -V f''(\eta)$$

$$\frac{\partial^3 \psi}{\partial x^3} = -V f'''(\eta)$$

$$\frac{\partial^2 \psi}{\partial x \partial y} = \frac{\partial}{\partial x} \left(-V \left[S'(\eta) f + S(\eta) \left[-\eta \frac{S'(\eta)}{S(\eta)} \right] \right] \right) = -V \left(S'(\eta) f'(\eta) \cdot \frac{1}{S(\eta)} - S(\eta) \cdot \frac{1}{S(\eta)} \right)$$

$$= +V S'(\eta) \left(1 - f'(\eta) \right)$$

Blocus

Si on est dans le cas de la convection naturelle, on ajoute le terme d'Archimède : (et la force d'élévation)

$$= \rho_0 (1 - \underbrace{\beta(T - T_0)}_{\ll 1})$$

$$P(y) = \rho_0 g y \Rightarrow \frac{dP}{dy} = \rho_0 g$$

On trouve les équations de Prandtl pour la convection naturelle :

$$\theta(\eta) = \frac{T - T_e}{T_w - T_e} \quad T_w - T_e = DT$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

~~$$\frac{\partial u}{\partial x} \rho_0 (1 - \underbrace{\beta(T - T_0)}_{\ll 1}) \left[u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right] = -\cancel{\rho_0 g} + \mu \frac{\partial^2 v}{\partial x^2} + \rho_0 (\cancel{\beta(T - T_0)}) g$$~~

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = \beta(T - T_0) g + \nu \frac{\partial^2 v}{\partial x^2}$$

$$\Rightarrow \frac{\partial \psi}{\partial x} \frac{\partial^2 \psi}{\partial y \partial x} - \frac{\partial \psi}{\partial y} \frac{\partial^2 \psi}{\partial x^2} = \beta(T - T_0) g - \nu \frac{\partial^3 \psi}{\partial x^3}$$

On trouve les formes de courant avec variable de similitude :

$$\Rightarrow -V f'(\eta) \cdot \frac{VS'(\eta)}{S(\eta)} (1 - f'(\eta)) * VS'(\eta) (f(\eta) - f'(\eta) \eta) \cdot \frac{V f''(\eta)}{S(\eta)} = \beta(T - T_0) g + \nu \frac{V f'''(\eta)}{S^2(\eta)}$$

On dérive :

$$\frac{\partial \psi}{\partial x} = -4\nu \left[\frac{G_n(\eta)}{4} \right]^{3/4} \cdot f'(\eta) \cdot \frac{1}{S(\eta)} ; \quad \frac{\partial^2 \psi}{\partial x^2} = -4\nu \left[\frac{G_n(\eta)}{4} \right]^{2/4} \cdot f''(\eta) \cdot \frac{1}{S^2(\eta)}$$

$$\frac{\partial^2 \psi}{\partial y \partial x} = -4\nu \cdot \frac{1}{4} \left(\frac{G_n(\eta)}{4} \right)^{-3/4} \cdot \frac{1}{4} G_n'(\eta) \cdot f'(\eta) + 4\nu \left[\frac{G_n(\eta)}{4} \right]^{-2/4} \cdot f''(\eta) \cdot \eta \frac{S'(\eta)}{S(\eta)} \cdot \frac{1}{S(\eta)} + 4\nu \left[\frac{G_n(\eta)}{4} \right]^{1/4} \cdot f'(\eta) \cdot \frac{1}{S^2(\eta)} \cdot S'(\eta)$$

$$\frac{\partial \psi}{\partial y} = +4\nu f'(\eta) \eta \frac{S'(\eta)}{S(\eta)} - 4\nu f(\eta) \frac{1}{4} \left[\frac{G_n(\eta)}{4} \right]^{-3/4} \cdot \frac{1}{4} G_n'(\eta)$$

$$\frac{\partial^3 \psi}{\partial x^3} = -4\nu \left[\frac{G_n(\eta)}{4} \right]^{2/4} \cdot f'''(\eta) \cdot \frac{1}{S^3(\eta)}$$

$$G_n(\eta) = \frac{B \Delta T g \eta^3}{\nu^2}$$

$$G_n'(\eta) = \frac{3 B \Delta T g \eta^2}{\nu^2}$$

$$\Rightarrow \frac{3}{4} G_n(\eta)$$

On trouve :

$$16\nu^2 \cdot \frac{2}{4} \left[\frac{G_n(\eta)}{4} \right]^{-2/4} \cdot G_n'(\eta) \left[\frac{f'(\eta)}{S(\eta)} \right]^2 = -16\nu^2 \left[\frac{G_n(\eta)}{4} \right]^{2/4} \frac{f'(\eta) f''(\eta)}{S(\eta) S(\eta)} \eta \frac{S'(\eta)}{S(\eta)} - 16\nu^2 \left[\frac{G_n(\eta)}{4} \right]^{2/4} \left[\frac{f'(\eta)}{S(\eta)} \right]^2 \cdot \frac{S'(\eta)}{S(\eta)}$$

$$+ 16\nu^2 \left[\frac{G_n(\eta)}{4} \right]^{2/4} \left[\frac{f'(\eta)}{S(\eta)} \right] \cdot \eta f''(\eta) \frac{S'(\eta)}{S^2(\eta)} - 16\nu^2 \cdot \frac{2}{4} \left[\frac{G_n(\eta)}{4} \right]^{-2/4} \cdot G_n'(\eta) f(\eta) f'(\eta) \cdot \frac{1}{S^2(\eta)}$$

$$- \underbrace{\beta(T - T_e) g}_{= B \theta(\eta) \Delta T g} - 4\nu^2 \left[\frac{G_n(\eta)}{4} \right]^{1/4} \cdot f'''(\eta) \frac{1}{S^3(\eta)} = 0$$

$$= B \theta(\eta) \Delta T g = \theta(\eta) G_n(\eta) \frac{\nu^2}{\eta^3}$$

problème thermique:

$$u \frac{\partial T}{\partial x} + N \frac{\partial T}{\partial y} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$$

simplification:

toujours : $S \ll Y$

toujours : $U = \frac{V\delta}{Y} \ll V$

condition d'interface

$$Pr = \frac{V}{\alpha}$$

$$Nu = \frac{q_m}{k \Delta T / 2 R}$$

Flux de chaleur
dans l'écoulement

$$Pe = \frac{UL}{\alpha}$$

$$\begin{array}{l} \text{transport} \quad \text{diffusion} \\ \boxed{u \frac{\partial T}{\partial x} + N \frac{\partial T}{\partial y}} = \alpha \left(\underbrace{\frac{\partial^2 T}{\partial x^2}}_{\frac{U \cdot \Delta T}{S}} + \underbrace{\frac{\partial^2 T}{\partial y^2}}_{\frac{\Delta T}{S^2}} \right) \\ u \frac{\partial T}{\partial x} = \frac{U \cdot \Delta T}{S} \quad \frac{\Delta T}{S^2} \gg \frac{\Delta T}{Y^2} \\ \frac{VAT}{Y} \quad \frac{U \cdot \Delta T}{S} \\ \Rightarrow \left(\frac{VAT}{Y} \right) \end{array}$$

On a donc :

$$u \frac{\partial T}{\partial x} + N \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial x^2}$$

$$\begin{aligned} 1 &= \frac{V}{\alpha} = \frac{VAT}{Y} \frac{S^2}{\alpha \Delta T} \Rightarrow \frac{VY}{\alpha} \cdot \frac{\delta^2}{Y^2} \\ &\Rightarrow \frac{\delta^2}{Y^2} = \frac{\alpha}{VY} \\ &\Rightarrow \frac{\delta}{Y} = \sqrt{\frac{\alpha}{VY}} = \sqrt{\frac{1}{Pe}} \end{aligned}$$

transfert de
chaleur d'un
écoulement

$$\Theta(y) = \frac{T - T_e}{\Delta T} \Rightarrow T = \Delta T \cdot \Theta(y) + T_e$$

→ calculer les dérivées ... pour retrouver l'équation de similitude.

Flux de chaleur: (à la paroi)

$$\alpha = \frac{k}{\rho c} \Rightarrow \rho c \alpha = k$$

$$q_m = -k \frac{\partial T}{\partial x} \Big|_{x=0}$$

$$= -k \frac{\partial}{\partial x} (\Delta T \cdot \Theta(y) + T_e) \Big|_{y=0}$$

comme : (pour $Pr > 0,02$)
 $\Theta'(y) \Big|_{y=0} = 0,332 \sqrt{2} (Pr)^{1/2}$

$$= -k \Delta T \Theta'(y) \Big|_{y=0} \cdot \frac{\partial y}{\partial x}$$

$$= -k \Delta T \Theta'(y) \Big|_{y=0} \cdot \frac{1}{S(y)} \sim \frac{1}{Y} \left(\frac{Gn}{q} \right)^{1/4}$$

$$= -k \Delta T \Theta'(y) \Big|_{y=0} \cdot \frac{1}{Y} \left(\frac{Gn}{q} \right)^{1/4}$$

$$i \frac{\partial N}{\partial x} + N \frac{\partial N}{\partial y} = \beta(T-T_e)g + v \frac{\partial^2 N}{\partial x^2}$$

où $\theta(y) = \frac{T-T_e}{T_w-T_e} = \frac{T-T_e}{\Delta T}$

Fonction de courant :

$$u = \frac{\partial \Psi}{\partial y}; \quad N = -\frac{\partial \Psi}{\partial x}$$

avec $\Psi(x, y) = -4v f(y) \left[\frac{G_n(y)}{4} \right]^{1/4}$

$$\beta(T-T_e)g = \theta G_n \frac{v^2}{y^3}$$

Variable de similitude :

$$M(x, y) = \frac{x}{S(y)} = \frac{x}{y} \left[\frac{G_n(y)}{4} \right]^{1/4}$$

avec $\begin{cases} G_n(y) = \frac{\beta \Delta T g y^3}{v^2} \\ G_n'(y) = \frac{3 \beta \Delta T y^2}{v^2} = \frac{3}{y} G_n(y) \end{cases}$

Quelques calculs préliminaires :

$$\rightarrow S(y) = y \left[\frac{4}{G_n(y)} \right]^{1/4}$$

$$\begin{aligned} \rightarrow S'(y) &= \left[\frac{4}{G_n(y)} \right]^{1/4} - y^4 \left[\frac{4}{G_n(y)} \right]^{-3/4} \cdot \frac{1}{G_n^2(y)} \cdot G_n'(y) \\ &= \left[\frac{4}{G_n(y)} \right]^{1/4} - \frac{3}{G_n(y)} \left[\frac{4}{G_n(y)} \right]^{-3/4} \end{aligned}$$

$$\rightarrow \frac{1}{S^2(y)} = \frac{1}{2y^2} \left[\frac{G_n(y)}{4} \right]^2$$

$$\rightarrow \frac{S'(y)}{S(y)} = \frac{1}{y} - \frac{3}{G_n(y)} \underbrace{\left[\frac{4}{G_n(y)} \right]^{-3/4}}_{y} \underbrace{\left[\frac{4}{G_n(y)} \right]^{-3/4}}_{= \frac{1}{y}} = \frac{1}{y} - \frac{3}{4y} = \frac{4-3}{4y} = \boxed{\frac{1}{4y}}$$

$$\rightarrow \frac{\partial M}{\partial x} = \frac{1}{S(y)} = \frac{1}{y} \left[\frac{G_n(y)}{4} \right]^{1/4}$$

$$\rightarrow \frac{\partial M}{\partial y} = -M \frac{S'(y)}{S(y)} = -\frac{M}{4y} = -\frac{x}{4y^2} \left[\frac{G_n(y)}{4} \right]^{1/4}$$

On calcule ensuite que : (piloteur A)

$$\begin{aligned} \rightarrow u &= \frac{\partial \Psi}{\partial y} = 4v f' y \frac{S'(y)}{S(y)} \left[\frac{G_n}{4} \right]^{1/4} - 4v f \cdot \frac{1}{16} \left[\frac{G_n}{4} \right]^{-3/4} \cdot 6n' = -4v f' \frac{\partial M}{\partial y} \left[\frac{G_n}{4} \right]^{1/4} - \frac{v}{4} f \left[\frac{G_n}{4} \right]^{3/4} G_n' \\ &= -4v f' \frac{(-x)}{4y^2} \left[\frac{G_n(y)}{4} \right]^{1/4} \left[\frac{G_n}{4} \right]^{1/4} - \frac{3v}{4y} f \left[\frac{G_n}{4} \right]^{-3/4} \cdot 6n \\ &= \frac{v \times f' \sqrt{G_n}}{2y^2} - \frac{3v}{4y} f \left[\frac{G_n}{4} \right]^{-3/4} \cdot 6n \end{aligned}$$

vol en bord
diagonal $\rightarrow \boxed{\phi_0}$
vol en bord
au bord $\rightarrow \boxed{\phi_1}$

$$\rightarrow \frac{\partial N}{\partial x} = -\frac{\partial \Psi}{\partial x} = 4v f' \frac{\partial \eta}{\partial x} \left[\frac{Gn}{4} \right]^{1/4}$$

$$= 4v f' \cdot \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4} \cdot \left[\frac{Gn}{4} \right]^{1/4}$$

$$= \frac{2v f' \sqrt{Gn}}{y}$$

$$\rightarrow \frac{\partial N}{\partial x} = \left(\frac{\partial^2 \Psi}{\partial x^2} \right) = \frac{2v}{y} f'' \frac{\partial \eta}{\partial x} \sqrt{Gn}$$

$$= \frac{2v}{y} f'' \cdot \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn}$$

$$= \frac{2v}{y^2} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn} f''$$

$$\rightarrow \frac{\partial N}{\partial y} = \frac{(2v f'' \frac{\partial \eta}{\partial y} \sqrt{Gn} + 2v f' \cdot \frac{1}{2} (Gn)^{-3/2} Gn' \eta)}{y^2} y - (2v f' \sqrt{Gn}, 1)$$

$$= \frac{(-2v f'' \frac{x}{4y^2} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn} + v f' (Gn)^{-3/2} \cdot \frac{3}{y} Gn) y - 2v f' \sqrt{Gn}}{y^2}$$

$$= -\frac{1}{2} v \frac{x}{y^3} \left[\frac{Gn}{4} \right]^{1/4} p'' + \frac{v}{y^2} 3f' \sqrt{Gn} - \frac{2v}{y^2} f' \sqrt{Gn}$$

$$= -\frac{1}{2} v \cdot \frac{x}{y^3} \left[\frac{Gn}{4} \right]^{1/4} p'' + \frac{v}{y^2} f' \sqrt{Gn}$$

$$\rightarrow \frac{\partial^2 N}{\partial x^2} = \frac{\partial}{\partial x} \left(\frac{\partial N}{\partial x} \right) = \frac{2v}{y^2} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn} f''' \frac{\partial \eta}{\partial x}$$

$$= \frac{2v}{y^2} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn} f''' \cdot \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4}$$

$$= \frac{v}{y^3} Gn f'''$$

There we go, on remplace dans l'équation:

$$\left(\frac{v \cdot f' \sqrt{Gn}}{2y^2} - \frac{3v}{4y} f \left[\frac{Gn}{4} \right]^{-3/4} \cdot \frac{2v}{y^2} \left[\frac{Gn}{4} \right]^{1/4} \sqrt{Gn} f'' + \frac{2v}{y} f' \sqrt{Gn} \left(-\frac{v}{2} \frac{x}{y^3} \left[\frac{Gn}{4} \right]^{1/4} p'' + \frac{v}{y^2} f' \sqrt{Gn} \right) \right)$$

$$= O(Gn \frac{v^2}{y^3}) + v \cdot \frac{v}{y^3} Gn f'''$$

continue:

$$\frac{2D^2}{2y^4} \sqrt{Gn} \sqrt{Gn} \left[\frac{Gn}{4} \right]^{1/4} f''' - \frac{6D^2}{4y^3} \cdot \frac{2}{\sqrt{Gn}} f f'' + -\frac{2D^2}{2y^4} \cdot \sqrt{Gn} \left[\frac{Gn}{4} \right]^{1/4} f' p''$$

Bla bla: Non que un bon ok

$$+ \frac{2D^2}{y^3} \sqrt{Gn} \sqrt{Gn} (f')^2 = \alpha \frac{Gn D^2}{y^3} + \frac{D^2 Gn}{y^3} f'''$$

Non que ok

On trouve finalement:

$$f''' + 3ff'' - 2(f')^2 + \theta = 0$$

Temperature

$$M \frac{\partial T}{\partial x} + N \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial x^2} \quad \text{ou} \quad T = \Delta T \cdot \Theta(y) + T_0$$

On calcule que:

$$\rightarrow \frac{\partial T}{\partial x} = \frac{\partial}{\partial x} (\Delta T \cdot \Theta(y) + T_0)$$

$$= \Delta T \Theta'(y) \frac{\partial \Theta}{\partial x}$$

$$= \Delta T \Theta'(y) \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4}$$

$$\rightarrow \frac{\partial T}{\partial y} = \frac{\partial}{\partial y} (\Delta T \cdot \Theta(y) + T_0)$$

$$= \Delta T \Theta'(y) \frac{\partial \Theta}{\partial y}$$

$$= -\Delta T \Theta'(y) \frac{x}{4y^2} \left[\frac{Gn}{4} \right]^{1/4}$$

$$\rightarrow \frac{\partial^2 T}{\partial x^2} = \frac{\partial}{\partial x} (\Delta T \Theta'(y) \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4})$$

$$= \Delta T \Theta''(y) \frac{\partial \Theta}{\partial x} \cdot \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4}$$

$$= \Delta T \Theta''(y) \frac{1}{y^2} \left[\frac{Gn}{4} \right]^{1/2} = \Delta T \Theta''(y) \cdot \frac{1}{2y^2} \sqrt{Gn}$$

on remplace donc l'équation:

$$\left(\frac{D \times f' \sqrt{Gn}}{2y^2} - \frac{3D}{4y} f \left[\frac{Gn}{4} \right]^{-3/4} \cdot Gn \right) \cdot \Delta T \Theta'(y) \cdot \frac{1}{y} \left[\frac{Gn}{4} \right]^{1/4} + \frac{2D f' \sqrt{Gn}}{y} \cdot \left(-\Delta T \Theta'(y) \frac{x}{4y^2} \left[\frac{Gn}{4} \right]^{1/4} \right)$$

$$= \alpha \Delta T \Theta''(y) \cdot \frac{1}{2y^2} \sqrt{Gn}$$

$$\Rightarrow \frac{\cancel{V} \times \cancel{P'} \sqrt{G_n}}{2y^3} \left[\frac{G_n}{4} \right]^{1/4} - \frac{3\cancel{V} \cancel{P} \overbrace{\left[\frac{G_n}{4} \right]^{-3/4} \left[\frac{G_n}{4} \right]^{1/4} \cdot G_n}^{2\sqrt{G_n}}}{4y^2} - \frac{8\cancel{V} \times \cancel{P} \Delta T O'(y)}{28y^3} \left[\frac{G_n}{4} \right]^{1/4} \sqrt{G_n}$$

$$P_n = \frac{0}{\alpha}$$

$$\Rightarrow \alpha = \frac{V}{P_n}$$

$$\Rightarrow -\frac{V \Delta T \sqrt{G_n}}{2y^2} \cdot 3 P O'(y) = \frac{1}{P_n} \cdot \boxed{\frac{V \Delta T \sqrt{G_n}}{2y^2} O''(y)}$$

On trouve finalement:

$$\boxed{3 P_n O' + O'' = 0}$$