

# **Numerical Optimization for Large Scale Problems**

## **Report**

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### **Contents**

## 1 Introduction

## 2 Implemented methods

Both the implemented methods use a `switch/case` to handle the three options for derivative evaluation supported:

1. exact gradient and exact Hessian (Mode = exact)
2. finite-difference (FD) approximations of both gradient and Hessian (Mode = full fd)
3. exact gradient and finite-difference approximation of the Hessian using the gradient (Mode = mixed fd)

### 2.1 Modified Newton method with Backtracking

The implemented algorithm is a Modified Newton method that applies a Hessian correction to enforce positive definiteness before computing the search direction, thereby ensuring that the resulting direction is a descent direction. Once the direction is obtained, an inexact line search is carried out via backtracking until the Armijo condition is satisfied.

We now outline the algorithmic steps performed at each iteration and highlight the role of the Hessian modification and the Armijo backtracking line search.

#### 2.1.1 Hessian computation and symmetrization

The outer loop starts by computing the Hessian (or Hessian approximation) at  $x_k$ , denoted by  $H_k \approx \nabla^2 f(x_k)$ . Since FD-based evaluations may introduce numerical asymmetries, symmetry is enforced by updating  $H_k \leftarrow \frac{1}{2}(H_k + H_k^\top)$ .

#### 2.1.2 Positive definiteness enforcement via Cholesky and diagonal shift

Subsequently,  $\tau$  is initialized and updated until a Cholesky factorization succeeds. First,  $m$  is computed as the minimum diagonal entry of  $H_k$ , i.e.  $m \leftarrow \min(\text{diag}(H_k))$ . If  $m > 0$  then  $\tau \leftarrow 0$ , otherwise  $\tau \leftarrow \max(0, \beta - m)$ . This is done because positive diagonal entries are a necessary condition for positive definiteness, but since it is not a sufficient condition, positive definiteness must be explicitly verified. A failure (reported by the flag output of `chol`) indicates that the current matrix is not positive definite and must be corrected through a diagonal shift. Hence, a Cholesky factorization is attempted on  $H_k + \tau I$  and, if it fails,  $\tau$  is increased according to  $\tau \leftarrow \max(2\tau, \beta)$  and the factorization is retried. The process continues until Cholesky factorization succeeds, which means  $H_k + \tau I$  has been perturbed enough to be positive definite.

#### 2.1.3 Search direction and Armijo backtracking

Once Cholesky succeeds, the factor  $R$  is used to compute the descent direction  $p_k$ , and backtracking is performed until the Armijo condition is satisfied.

#### 2.1.4 Stopping criterion and safeguards

The outer loop repeats until the stopping criterion is satisfied or the maximum number of iterations is reached (safeguard). The stopping criterion implemented is  $\|\nabla f(x_k)\| < \text{tol}$ , where `tol` is the given tolerance.

## 2.2 Truncated Newton method

This implementation follows the Inexact Newton framework [1]. At each iteration  $k$ , the search direction  $p_k$  is computed by approximately solving the Newton system  $B_k p = -\nabla f(x_k)$  via Preconditioned Conjugate Gradient (PCG), truncated to handle non-convexity or achieve efficient convergence.

### Algorithm Outline

1. **Forcing Term ( $\eta_k$ ):** Determines the relative tolerance for the inner solver.
  - $k = 1$ :  $\eta_k = 0.5$ .
  - $k > 1$ : **Superlinear:**  $\min(0.5, \sqrt{\|\nabla f(x_{k-1})\|})$  or **Quadratic:**  $\min(0.5, \|\nabla f(x_{k-1})\|)$ .
2. **Preconditioning:** Supports  $M = \text{diag}(B_k)$  or Modified Cholesky via `ichol` with diagonal shifting to ensure  $M \succ 0$ . The system  $My_j = r_j$  is solved at each inner step.
3. **Inner Solver: Truncated PCG Updates:** The system  $B_k p = -\nabla f(x_k)$  is solved starting with  $z_0 = 0, r_0 = \nabla f(x_k)$ . At each inner iteration  $j$ :
  - **Curvature Check:** Compute  $\kappa_j = d_j^T B_k d_j$ .
    - If  $\kappa_j \leq 0$  and  $j = 1$ : Return  $p_k = -\nabla f(x_k)$  (Steepest Descent).
    - If  $\kappa_j \leq 0$  and  $j > 1$ : Truncate and return  $p_k = z_j$ .
  - **Iterative Updates:**

$$\alpha_j = \frac{r_j^T y_j}{\kappa_j}, \quad z_{j+1} = z_j + \alpha_j d_j, \quad r_{j+1} = r_j + \alpha_j B_k d_j$$
    - **Conjugate Update:** With  $y_{j+1} = M^{-1} r_{j+1}$  and  $\beta_j = \frac{r_{j+1}^T y_{j+1}}{r_j^T y_j}$ :
$$d_{j+1} = -y_{j+1} + \beta_j d_j$$
  - **Truncation:** Stop when  $\|r_j\| \leq \eta_k \|\nabla f(x_k)\|$  or  $j = \text{maxit}$ .
4. **Descent Safeguard:** If  $\nabla f(x_k)^T p_k \geq 0$  or  $p_k$  contains NaNs, set  $p_k = -\nabla f(x_k)$ .
5. **Line Search:** A backtracking approach finds  $\alpha_k$  satisfying the Armijo condition:
 
$$f(x_k + \alpha_k p_k) \leq f(x_k) + c_1 \alpha_k \nabla f(x_k)^T p_k$$
 with the usual break condition if line search fails.
6. **Update:**  $x_{k+1} = x_k + \alpha_k p_k$  until  $\|\nabla f(x_k)\| < \text{tol}$ .

### Remarks

The code utilizes pre-allocation for the `history` struct to record function values, gradient norms, and CG iteration counts. Robustness is ensured via `condest(Bk)` monitoring and a fallback mechanism to steepest descent during line search failures or negative curvature detections.

### 3 Test problems

#### 3.1 Problem 31 Broyden Tridiagonal

The objective function for the Broyden tridiagonal function, formulated as a nonlinear least-squares problem, is given by:

$$F(x) = \frac{1}{2} \sum_{k=1}^n f_k(x)^2$$

where the residual functions  $f_k(x)$  are defined as:

$$f_k(x) = (3 - 2x_k)x_k - x_{k-1} - 2x_{k+1} + 1$$

This function is subject to the following boundary conditions:

$$x_0 = 0 \quad \text{and} \quad x_{n+1} = 0$$

The standard starting point for optimization algorithms is  $x_i = -1$  for all  $i = 1, \dots, n$ .

#### Gradient of the Objective Function

The gradient of the objective function is required for derivative-based optimization methods. The factor of  $\frac{1}{2}$  in the objective function simplifies the expression.

$$\frac{\partial F}{\partial x_j} = \sum_{k=1}^n f_k(x) \frac{\partial f_k}{\partial x_j}$$

Using the Kronecker delta,  $\delta_{ij}$ , the partial derivative of the residual function  $f_k(x)$  with respect to  $x_j$  is:

$$\frac{\partial f_k}{\partial x_j} = (3 - 4x_k)\delta_{kj} - \delta_{k,j+1} - 2\delta_{k,j-1}$$

Substituting this into the gradient expression and simplifying the sum by using the sifting property of the Kronecker delta, we arrive at a single compact formula. By defining  $f_0 = 0$  and  $f_{n+1} = 0$  to handle the boundaries, the gradient components are:

$$\frac{\partial F}{\partial x_j} = f_j(x)(3 - 4x_j) - f_{j+1}(x) - 2f_{j-1}(x)$$

This single expression is valid for all  $j = 1, \dots, n$ .

#### Hessian of the Objective Function

For second-order optimization methods, the Hessian of  $F(x) = \frac{1}{2}\mathbf{f}(x)^T\mathbf{f}(x)$  is given by:

$$\nabla^2 F(x) = J(x)^T J(x) + \sum_{k=1}^n f_k(x) \nabla^2 f_k(x)$$

where  $J(x)$  is the Jacobian matrix of the vector of residuals  $\mathbf{f}(x) = [f_1(x), \dots, f_n(x)]^T$ .

The Jacobian matrix,  $J(x)$ , has a tridiagonal structure based on the partial derivatives of the residuals:

$$J(x) = \begin{pmatrix} 3 - 4x_1 & -2 & 0 & \dots & 0 \\ -1 & 3 - 4x_2 & -2 & \dots & 0 \\ 0 & -1 & 3 - 4x_3 & \dots & 0 \\ \vdots & \vdots & \ddots & \ddots & \vdots \\ 0 & 0 & \dots & -1 & 3 - 4x_n \end{pmatrix}$$

The second term involves the Hessians of the individual residual functions,  $\nabla^2 f_k(x)$ . The only non-zero second partial derivative of  $f_k(x)$  is:

$$\frac{\partial^2 f_k}{\partial x_k^2} = -4$$

This means the summation term simplifies to a diagonal matrix:

$$\sum_{k=1}^n f_k(x) \nabla^2 f_k(x) = \text{diag}(-4f_1(x), -4f_2(x), \dots, -4f_n(x))$$

Combining the terms, the full Hessian of the objective function is:

$$\nabla^2 F(x) = J(x)^T J(x) - 4 \cdot \text{diag}(f_1(x), f_2(x), \dots, f_n(x))$$

### 3.2 Problem 83 Lukšan and Vlček

The objective function for Problem 83, formulated as a nonlinear least-squares problem, is given by:

$$F(x) = \frac{1}{2} \sum_{k=1}^n f_k(x)^2$$

where the residual functions  $f_k(x)$  are defined as:

$$f_k(x) = 2x_k + h^2(x_k + \sin(x_k)) - x_{k-1} - x_{k+1}$$

with the constant  $h = 1/(n+1)$ . The function is subject to the following boundary conditions:

$$x_0 = 0 \quad \text{and} \quad x_{n+1} = 1$$

The standard starting point for optimization algorithms is  $x_i = 1$  for all  $i = 1, \dots, n$ .

#### Gradient of the Objective Function

The gradient of the objective function is found using the chain rule, simplified by the  $\frac{1}{2}$  factor in the objective function:

$$\frac{\partial F}{\partial x_j} = \sum_{k=1}^n f_k(x) \frac{\partial f_k}{\partial x_j}$$

The partial derivative of the residual function  $f_k(x)$  with respect to  $x_j$  can be expressed compactly using the Kronecker delta,  $\delta_{ij}$ :

$$\frac{\partial f_k}{\partial x_j} = (2 + h^2 + h^2 \cos(x_k)) \delta_{kj} - \delta_{k,j+1} - \delta_{k,j-1}$$

By defining  $f_0 = 0$  and  $f_{n+1} = 0$  to handle the boundaries, substituting this into the gradient expression and simplifying the sum yields a single general formula for the gradient components:

$$\frac{\partial F}{\partial x_j} = f_j(x)(2 + h^2 + h^2 \cos(x_j)) - f_{j+1}(x) - f_{j-1}(x)$$

This single expression is valid for all  $j = 1, \dots, n$ .

### Hessian of the Objective Function

For second-order optimization methods, the Hessian of  $F(x) = \frac{1}{2}\mathbf{f}(x)^T\mathbf{f}(x)$  is given by:

$$\nabla^2 F(x) = J(x)^T J(x) + \sum_{k=1}^n f_k(x) \nabla^2 f_k(x)$$

where  $J(x)$  is the Jacobian matrix of the vector of residuals  $\mathbf{f}(x)$ .

The Jacobian matrix,  $J(x)$ , is symmetric and tridiagonal:

$$J(x) = \begin{pmatrix} \alpha_1 & -1 & 0 & \dots \\ -1 & \alpha_2 & -1 & \dots \\ 0 & -1 & \ddots & \dots \\ \vdots & \ddots & \ddots & -1 \\ 0 & \dots & -1 & \alpha_n \end{pmatrix}$$

where  $\alpha_k = 2 + h^2 + h^2 \cos(x_k)$ .

The second term in the Hessian expression involves the Hessians of the individual residual functions,  $\nabla^2 f_k(x)$ . The only non-zero second partial derivative of  $f_k(x)$  is:

$$\frac{\partial^2 f_k}{\partial x_k^2} = -h^2 \sin(x_k)$$

This simplifies the summation term to a diagonal matrix:

$$\sum_{k=1}^n f_k(x) \nabla^2 f_k(x) = \text{diag}(-h^2 f_1(x) \sin(x_1), \dots, -h^2 f_n(x) \sin(x_n))$$

Combining the terms, the full Hessian of the objective function is:

$$\nabla^2 F(x) = J(x)^T J(x) - h^2 \cdot \text{diag}(f_1(x) \sin(x_1), \dots, f_n(x) \sin(x_n))$$

## 4 Finite Differences implementation

First and second order finite difference approximations were implemented by exploiting the problem structure and sparsity pattern, in order to reduce computational cost and improve performance. When perturbing a single component, only the locally affected terms are updated.

### 4.1 FD Problem 31

#### 4.1.1 FD Gradient Problem 31

For this specific problem, each residual  $f_k$  depends only on  $(x_{k-1}, x_k, x_{k+1})$ . This is directly exploited in the computation of the centered finite differences (preferred over forwards/backward because error is  $O(h^2)$  instead of  $O(h)$ ):

$$[\nabla F(x)]_i \approx \frac{F(x + he_i) - F(x - he_i)}{2h} \quad (1)$$

Since perturbing a single component  $x_i$  can only affect the residuals  $f_{i-1}, f_i, f_{i+1}$ , all other terms in the sum defining  $F$  remain unchanged and cancel out in the difference  $F(x + he_i) - F(x - he_i)$ . Therefore, defining:

$$S(i) := \{i - 1, i, i + 1\} \cap \{1, \dots, n\}, \quad E_{\text{loc}}(x; i) := \frac{1}{2} \sum_{k \in S(i)} f_k(x)^2,$$

we can compute the same centered FD quotient via the local contribution only:

$$[\nabla F(x)]_i \approx \frac{E_{\text{loc}}(x + he_i; i) - E_{\text{loc}}(x - he_i; i)}{2h}.$$

This drastically reduces the cost to compute FD approximation of the gradient. For example, naive FD implementation for  $n = 10^3$  requires  $2 \cdot 10^6$  residual evaluations, while our efficient implementation requires only 5996 residual evaluations, without sacrificing accuracy.

#### 4.1.2 FD Hessian Problem 31

The same locality property can be exploited to approximate the Hessian entries by centered finite differences. For the diagonal terms, we use the standard second-order centered formula:

$$H_{ii}(x) = \frac{\partial^2 F(x)}{\partial x_i^2} \approx \frac{F(x + h_i e_i) - 2F(x) + F(x - h_i e_i)}{h_i^2}. \quad (2)$$

Since perturbing  $x_i$  affects only the residuals  $f_{i-1}, f_i, f_{i+1}$ , we can replace full evaluations of  $F$  with the local energy  $E_{\text{loc}}(\cdot; i)$  defined on  $S(i) = \{i - 1, i, i + 1\} \cap \{1, \dots, n\}$ , obtaining:

$$H_{ii}(x) \approx \frac{E_{\text{loc}}(x + h_i e_i; i) - 2E_{\text{loc}}(x; i) + E_{\text{loc}}(x - h_i e_i; i)}{h_i^2}. \quad (3)$$

For off-diagonal entries ( $i \neq j$ ), we approximate mixed second derivatives with the centered cross difference formula:

$$H_{ij}(x) \approx \frac{F(x + h_i e_i + h_j e_j) - F(x + h_i e_i - h_j e_j) - F(x - h_i e_i + h_j e_j) + F(x - h_i e_i - h_j e_j)}{4h_i h_j}. \quad (4)$$

Due to the problem structure,  $H_{ij}$  is nonzero only for  $|i - j| \leq 2$ , hence the Hessian is pentadiagonal. When perturbing  $(x_i, x_{i+1})$  only the residuals with indices  $S(i, i + 1) = \{i - 1, i, i + 1, i + 2\} \cap \{1, \dots, n\}$  can change, and when perturbing  $(x_i, x_{i+2})$  only  $S(i, i + 2) =$

$\{i-1, i, i+1, i+2, i+3\} \cap \{1, \dots, n\}$  can change. Therefore, each  $F(\cdot)$  appearing in the mixed difference formula can be replaced by the corresponding local energy evaluation, leading to an efficient construction of the five relevant diagonals  $(0, \pm 1, \pm 2)$  and assembly of the sparse pentadiagonal Hessian in  $i$  and  $j$  of the second order finite difference  $H_{i,j}$ .

In terms of residual evaluations, for  $n = 10^3$  a naive Hessian FD implementation requires  $\approx 10^7$  residual evaluations, whereas our implementation requires only  $\approx 4.5 \cdot 10^4$  residual evaluations, without sacrificing accuracy.

## 4.2 FD Problem 83

### 4.2.1 FD Gradient Problem 83

As in (??), we approximate each component of the gradient via centered finite differences. Similarly as in problem 31 each residual  $f_k$  depends only on  $(x_{k-1}, x_k, x_{k+1})$ , so perturbing  $x_i$  affects only  $f_{i-1}, f_i$  and  $f_{i+1}$ . Therefore, in the difference  $F(x + h_i e_i) - F(x - h_i e_i)$  all the terms  $f_k(x)^2$  with  $k \notin \{i-1, i, i+1\}$  remain unchanged and cancel out. Defining

$$S(i) := \{i-1, i, i+1\} \cap \{1, \dots, n\}, \quad E_{\text{loc}}(x; i) := \frac{1}{2} \sum_{k \in S(i)} f_k(x)^2,$$

we can compute the same centered FD quotient via the local contribution only:

$$[\nabla F(x)]_i \approx \frac{E_{\text{loc}}(x + h_i e_i; i) - E_{\text{loc}}(x - h_i e_i; i)}{2h_i}.$$

Here the residuals  $f_k$  are evaluated consistently with the boundary conditions  $x_0 = 0$  and  $x_{n+1} = 1$  (in particular, the last residual includes the constant term  $-1$ ).

In terms of residual evaluations the same computational advantages already discussed at the end of ?? are obtained.

### 4.2.2 FD Hessian Problem 83

The same locality property can be exploited to approximate the Hessian entries by centered finite differences. For the diagonal terms, we use the standard second-order centered formula (??). Since perturbing  $x_i$  affects only the residuals  $f_{i-1}, f_i, f_{i+1}$ , we can replace full evaluations of  $F$  with the local energy  $E_{\text{loc}}(\cdot; i)$  defined on  $S(i) = \{i-1, i, i+1\} \cap \{1, \dots, n\}$ , obtaining (??).

For first off-diagonal entries ( $j = i+1$ ), we approximate mixed second derivatives with the centered cross difference formula (??). Here, perturbing  $(x_i, x_{i+1})$  affects only the residuals with indices  $S(i, i+1) = \{i-1, i, i+1, i+2\} \cap \{1, \dots, n\}$ , hence each  $F(\cdot)$  term in the formula above is replaced by the corresponding local energy evaluation on  $S(i, i+1)$ .

Due to the problem structure,  $H_{ij}$  is nonzero only for  $|i - j| \leq 2$ , hence the Hessian is pentadiagonal. It's important to note that for Problem 83 the second off-diagonal entries ( $j = i+2$ ) are known analytically and are equal to 1, so they are inserted directly without finite differences. The resulting sparse pentadiagonal Hessian is then assembled by constructing the five relevant diagonals  $(0, \pm 1, \pm 2)$  and exploiting symmetry of the formula defining  $H_{i,j}$ . Boundary conditions  $x_0 = 0$  and  $x_{n+1} = 1$  are handled consistently in the residual evaluations.

## 5 Experimental setup

We use a common protocol for both test problems and for both solvers (Modified Newton and Truncated Newton).

**Dimensions.**

$$n \in \{2, 10^3, 10^4, 10^5\}.$$

**Seed.** All randomized runs are reproducible with

$$\text{seed} = \min\{360426, 361794\}.$$

**Initialization.** For each dimension  $n$ , we use as baseline initial guess the point suggested in the reference PDF, denoted by  $\bar{x} \in R^n$ . In addition, we generate 5 perturbed starting points by sampling uniformly in the hypercube centered at  $\bar{x}$ , i.e.

$$x_0 \sim \mathcal{U}([\bar{x}_1 - 1, \bar{x}_1 + 1] \times \cdots \times [\bar{x}_n - 1, \bar{x}_n + 1]),$$

so that each component  $(x_0)_i$  is drawn independently from  $\mathcal{U}([\bar{x}_i - 1, \bar{x}_i + 1])$ .

**Derivative regimes and finite differences.** We run three derivative settings:

- **Exact:** exact gradient and exact Hessian;
- **Mixed:** exact gradient and FD Hessian
- **Full FD:** FD gradient and FD Hessian.

In the FD-based experiments we test the increments  $h = 10^{-k}$  with

$$k \in \{4, 8, 12\},$$

and we consider both a *constant* step  $h$  and a *component-wise* step  $h_i$  proportional to the current evaluation point.

**Success/failure criteria.** A run is successful if the stopping test is met within  $k_{\max}$ ; otherwise it is a failure. For all experiments the stopping criteria is  $\|\nabla f(x^k)\|_2 < tol$

**Logged metrics.** For each run we store the final outputs

$$(x_k, \|\nabla f(x_k)\|_2, \text{iters} = k, \text{btflag}, p_{\text{exp}}, t_{\text{run}}),$$

together with the diagnostic sequences

$$(\{x_j\}_{j=0}^k, \{\text{bt}_j\}_{j=0}^{k-1}, \{\text{mod}_j\}_{j=0}^{k-1}, \{\tau_j\}_{j=0}^{k-1}),$$

where  $\text{bt}_j$  is the number of backtracking reductions,  $\text{mod}_j$  the number of Hessian modifications, and  $\tau_j$  the final damping parameter at iteration  $j$ .

## 6 Results - Exact derivatives

### 6.1 Problem 31

#### 6.1.1 Modified Newton

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
31	2	exact	$\bar{x}$	$2.61 \times 10^{-15}$	6/1000	yes		1.98	0.0056s
			1	$1.92 \times 10^{-15}$	7/1000	yes		2.01	0.0012s
			2	$2.16 \times 10^{-9}$	6/1000	yes		1.99	0.0012s
			3	$8.94 \times 10^{-10}$	6/1000	yes		1.99	0.0009s
			4	$2.67 \times 10^{-10}$	5/1000	yes		1.99	0.0008s
			5	$1.04 \times 10^{-12}$	8/1000	yes		2.00	0.0013s
			<i>Avg (successes)</i>		$5.55 \times 10^{-10}$	6.3/1000	6/6	1.99	0.0018s

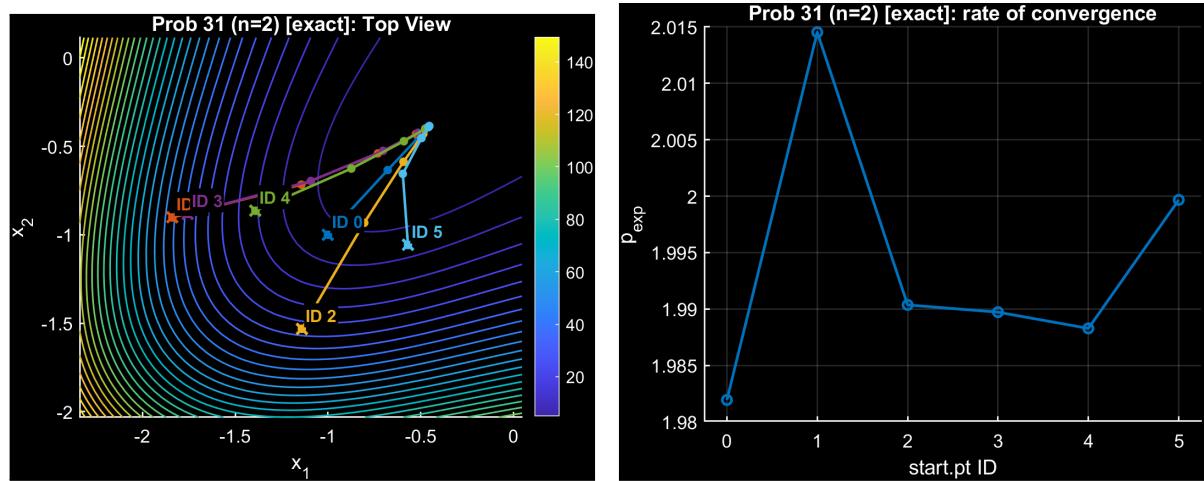


Figure 1: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

Case  $n > 2$

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
31	1000	exact	$\bar{x}$	$1.94 \times 10^{-14}$	6/1000	yes		1.37	0.0052s
			1	$4.69 \times 10^{-13}$	10/1000	yes		1.98	0.0075s
			2	$2.91 \times 10^{-14}$	10/1000	yes		1.83	0.0068s
			3	$1.07 \times 10^{-13}$	9/1000	yes		1.98	0.0071s
			4	$6.62 \times 10^{-14}$	9/1000	yes		1.96	0.0073s
			5	$1.43 \times 10^{-12}$	9/1000	yes		1.99	0.0073s
			<i>Avg (successes)</i>		$3.53 \times 10^{-13}$	8.8/1000	6/6	1.85	0.0069s

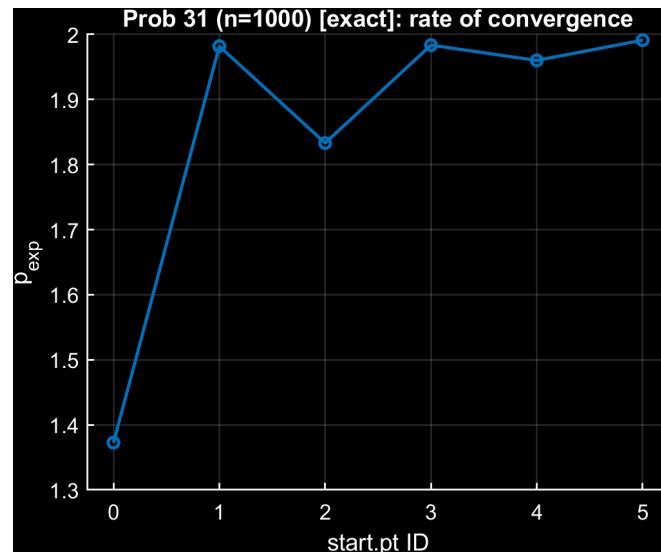


Figure 2: Problem 31, Modified Newton, exact derivatives ( $n = 1000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
31	10000	exact	$\bar{x}$	$1.94 \times 10^{-14}$	6/1000	yes		1.35	0.0285s
			1	$9.46 \times 10^{-12}$	10/1000	yes		2.00	0.0583s
			2	$3.12 \times 10^{-9}$	9/1000	yes		1.95	0.0552s
			3	$2.38 \times 10^{-14}$	11/1000	yes		1.79	0.0727s
			4	$7.10 \times 10^{-14}$	9/1000	yes		1.81	0.0637s
			5	$3.85 \times 10^{-14}$	11/1000	yes		1.97	0.0604s
				Avg (successes)	$5.22 \times 10^{-10}$	9.3/1000	6/6	1.81	0.0565s

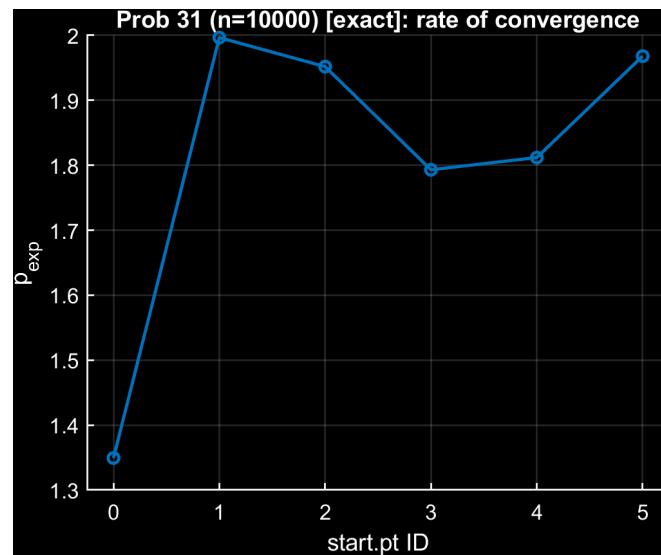


Figure 3: Problem 31, Modified Newton, exact derivatives ( $n = 10000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
31	100000	exact	$\bar{x}$	$1.94 \times 10^{-14}$	6/1000	yes		1.26	0.4384s
			1	$1.70 \times 10^{-13}$	9/1000	yes		1.53	0.9005s
			2	$2.44 \times 10^{-14}$	13/1000	yes		1.46	1.32s
			3	$3.45 \times 10^{-11}$	10/1000	yes		2.00	1.18s
			4	$1.09 \times 10^{-13}$	11/1000	yes		1.94	1.47s
			5	$1.23 \times 10^{-9}$	10/1000	yes		2.00	1.60s
			Avg (successes)	$2.10 \times 10^{-10}$	9.8/1000	6/6		1.70	1.15s

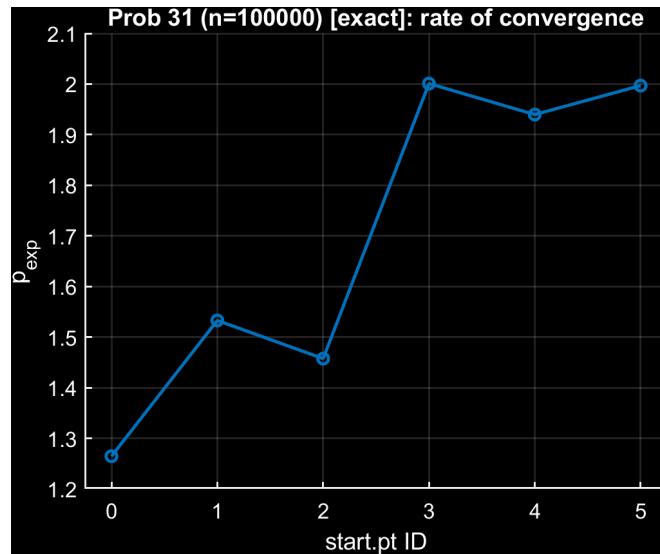


Figure 4: Problem 31, Modified Newton, exact derivatives ( $n = 100000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

### 6.1.2 Truncated Newton

## 6.2 Problem 83

### 6.2.1 Modified Newton

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
83	2	exact	$\bar{x}$	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0136s
			1	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0027s
			2	$4.39 \times 10^{-15}$	4/1000	yes		1.98	0.0014s
			3	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0018s
			4	$2.70 \times 10^{-16}$	4/1000	yes		1.95	0.0032s
			5	$9.34 \times 10^{-15}$	4/1000	yes		1.90	0.0009s
			<i>Avg (successes)</i>		$7.78 \times 10^{-10}$	3.5/1000	6/6	1.93	0.0040s

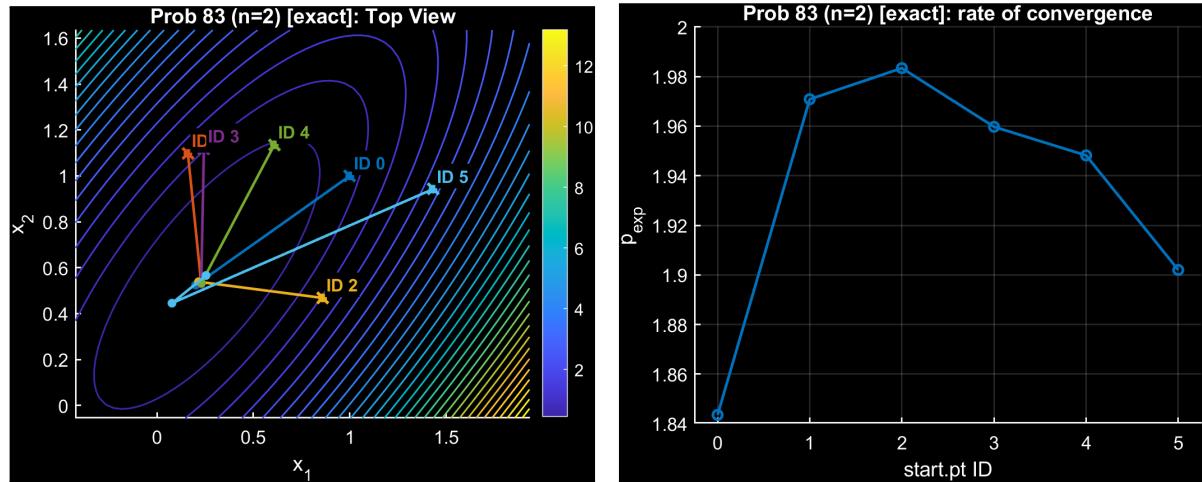


Figure 5: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

Case  $n > 2$

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
83	1000	exact	$\bar{x}$	$5.24 \times 10^{-13}$	2/1000	yes		NaN	0.0058s
			1	$3.91 \times 10^{-10}$	3/1000	yes		0.48	0.0041s
			2	$4.18 \times 10^{-11}$	3/1000	yes		0.72	0.0037s
			3	$9.06 \times 10^{-10}$	3/1000	yes		0.40	0.0038s
			4	$7.95 \times 10^{-10}$	3/1000	yes		0.42	0.0037s
			5	$1.32 \times 10^{-9}$	3/1000	yes		0.33	0.0033s
			<i>Avg (successes)</i>		$5.76 \times 10^{-10}$	2.8/1000	6/6	0.47	0.0041s

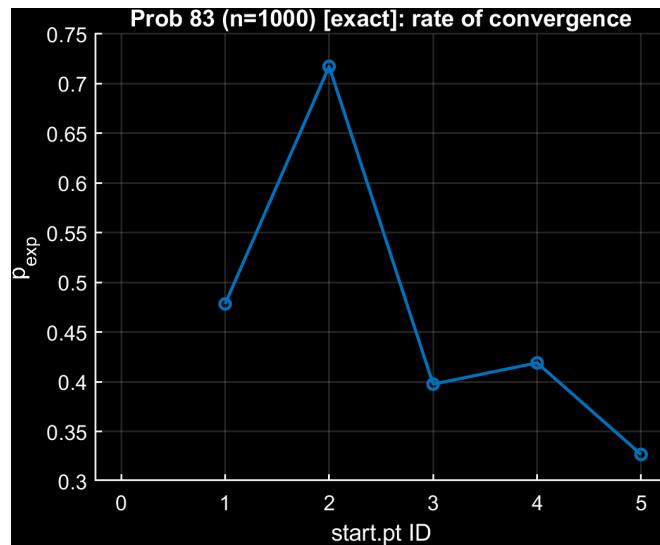


Figure 6: Problem 83, Modified Newton, exact derivatives ( $n = 1000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time
83	10000	exact	$\bar{x}$	$2.48 \times 10^{-14}$	2/1000	yes		NaN	0.0125s
			1	$2.32 \times 10^{-10}$	3/1000	yes		0.94	0.0208s
			2	$7.81 \times 10^{-10}$	4/1000	yes		5.08	0.0279s
			3	$5.63 \times 10^{-11}$	3/1000	yes		1.02	0.0205s
			4	$4.56 \times 10^{-10}$	2/1000	yes		NaN	0.0147s
			5	$2.77 \times 10^{-10}$	2/1000	yes		NaN	0.0145s
			Avg (successes)	$3.00 \times 10^{-10}$	2.7/1000	6/6		2.35	0.0185s

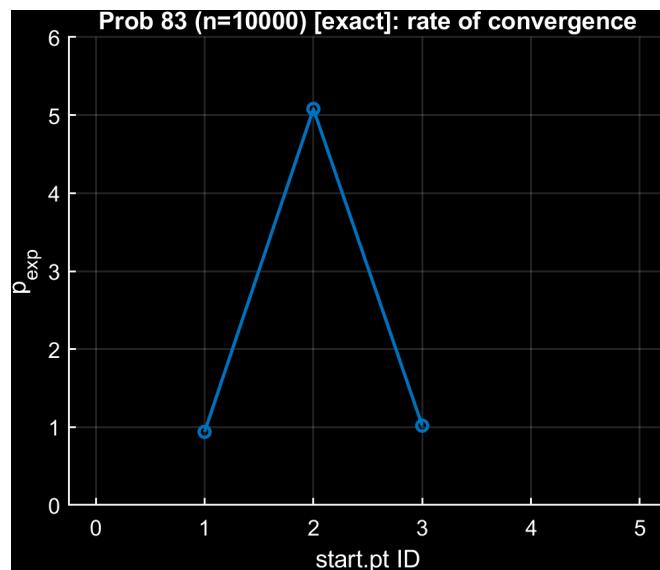


Figure 7: Problem 83, Modified Newton, exact derivatives ( $n = 10000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

Prob.	Dim.	Mode	start.pt ID	grad.norm	iters/max	succ.	flag	rate	time	
83	100000	exact	$\bar{x}$	$1.14 \times 10^{-10}$	1/1000	yes		NaN	0.0854s	
			1	$1.69 \times 10^{-13}$	2/1000	yes		NaN	0.1599s	
			2	$1.86 \times 10^{-13}$	2/1000	yes		NaN	0.1494s	
			3	$1.94 \times 10^{-13}$	2/1000	yes		NaN	0.1597s	
			4	$2.04 \times 10^{-13}$	2/1000	yes		NaN	0.1490s	
			5	$2.74 \times 10^{-9}$	2/1000	yes		NaN	0.1882s	
			<i>Avg (successes)</i>		$4.76 \times 10^{-10}$	1.8/1000	6/6		NaN	0.1486s

### 6.2.2 Truncated Newton

Case  $n = 2$

Table 1: Results for Problem 83.0 - Exact

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	Exact	0.0	N/A	N/A	$3.24e - 10$	4/1000	yes	-0.63	0.01
83.0	2.0	Exact	1.0	N/A	N/A	$5.94e - 10$	3/1000	yes	2.22	0.01
83.0	2.0	Exact	2.0	N/A	N/A	$3.61e - 07$	3/1000	yes	3.54	0.01
83.0	2.0	Exact	3.0	N/A	N/A	$3.21e - 08$	4/1000	yes	-0.54	0.01
83.0	2.0	Exact	4.0	N/A	N/A	$3.86e - 09$	3/1000	yes	2.27	0.01
83.0	2.0	Exact	5.0	N/A	N/A	$5.25e - 07$	3/1000	yes	2.64	0.01
83.0	1000.0	Exact	0.0	N/A	N/A	$4.69e - 06$	100/1000	no	N/A	0.88
83.0	1000.0	Exact	1.0	N/A	N/A	$3.97e - 06$	100/1000	no	N/A	0.63
83.0	1000.0	Exact	2.0	N/A	N/A	$3.87e - 06$	100/1000	no	N/A	0.57
83.0	1000.0	Exact	3.0	N/A	N/A	$3.42e - 06$	100/1000	no	N/A	0.91
83.0	1000.0	Exact	4.0	N/A	N/A	$8.87e - 06$	100/1000	no	N/A	0.88
83.0	1000.0	Exact	5.0	N/A	N/A	$4.03e - 06$	100/1000	no	N/A	0.57
83.0	10000.0	Exact	0.0	N/A	N/A	$6.40e - 06$	100/1000	no	N/A	7.69
83.0	10000.0	Exact	1.0	N/A	N/A	$6.80e - 06$	100/1000	no	N/A	5.79
83.0	10000.0	Exact	2.0	N/A	N/A	$7.41e - 06$	100/1000	no	N/A	5.84
83.0	10000.0	Exact	3.0	N/A	N/A	$6.96e - 06$	100/1000	no	N/A	6.99
83.0	10000.0	Exact	4.0	N/A	N/A	$7.86e - 06$	100/1000	no	N/A	6.54
83.0	10000.0	Exact	5.0	N/A	N/A	$7.78e - 06$	100/1000	no	N/A	7.36
83.0	$1.00e + 05$	Exact	0.0	N/A	N/A	$6.41e - 06$	100/1000	no	N/A	84.88
83.0	$1.00e + 05$	Exact	1.0	N/A	N/A	$1.43e - 05$	100/1000	no	N/A	79.39
83.0	$1.00e + 05$	Exact	2.0	N/A	N/A	$1.37e - 05$	100/1000	no	N/A	79.93
83.0	$1.00e + 05$	Exact	3.0	N/A	N/A	$1.50e - 05$	100/1000	no	N/A	79.56
83.0	$1.00e + 05$	Exact	4.0	N/A	N/A	$1.51e - 05$	100/1000	no	N/A	80.28
83.0	$1.00e + 05$	Exact	5.0	N/A	N/A	$1.35e - 05$	100/1000	no	N/A	80.26

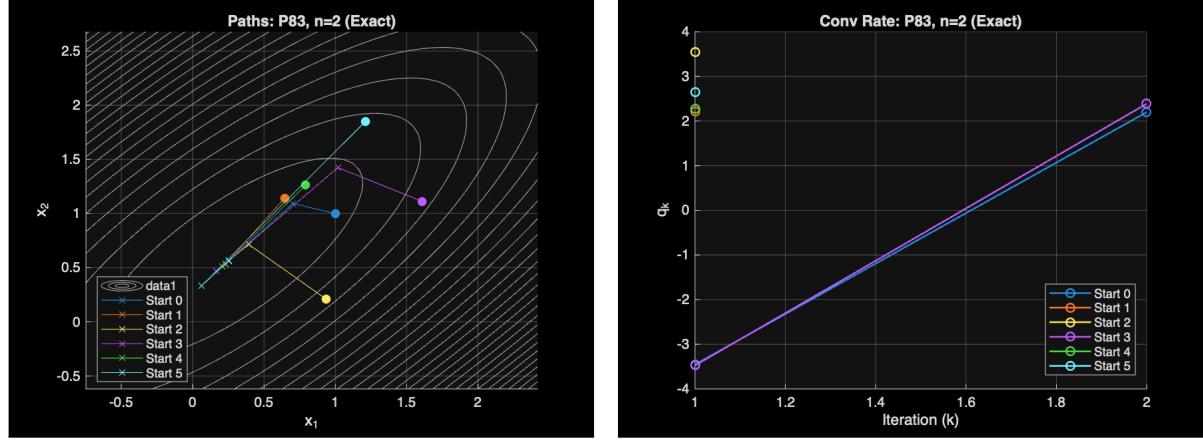


Figure 8: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $n > 2$

Table 2: Results for Problem 83.0 - Exact

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	Exact	0.0	N/A	N/A	$3.24e-10$	4/1000	yes	-0.63	0.01
83.0	2.0	Exact	1.0	N/A	N/A	$5.94e-10$	3/1000	yes	2.22	0.01
83.0	2.0	Exact	2.0	N/A	N/A	$3.61e-07$	3/1000	yes	3.54	0.01
83.0	2.0	Exact	3.0	N/A	N/A	$3.21e-08$	4/1000	yes	-0.54	0.01
83.0	2.0	Exact	4.0	N/A	N/A	$3.86e-09$	3/1000	yes	2.27	0.01
83.0	2.0	Exact	5.0	N/A	N/A	$5.25e-07$	3/1000	yes	2.64	0.01
83.0	1000.0	Exact	0.0	N/A	N/A	$4.69e-06$	100/1000	no	N/A	0.88
83.0	1000.0	Exact	1.0	N/A	N/A	$3.97e-06$	100/1000	no	N/A	0.63
83.0	1000.0	Exact	2.0	N/A	N/A	$3.87e-06$	100/1000	no	N/A	0.57
83.0	1000.0	Exact	3.0	N/A	N/A	$3.42e-06$	100/1000	no	N/A	0.91
83.0	1000.0	Exact	4.0	N/A	N/A	$8.87e-06$	100/1000	no	N/A	0.88
83.0	1000.0	Exact	5.0	N/A	N/A	$4.03e-06$	100/1000	no	N/A	0.57
83.0	10000.0	Exact	0.0	N/A	N/A	$6.40e-06$	100/1000	no	N/A	7.69
83.0	10000.0	Exact	1.0	N/A	N/A	$6.80e-06$	100/1000	no	N/A	5.79
83.0	10000.0	Exact	2.0	N/A	N/A	$7.41e-06$	100/1000	no	N/A	5.84
83.0	10000.0	Exact	3.0	N/A	N/A	$6.96e-06$	100/1000	no	N/A	6.99
83.0	10000.0	Exact	4.0	N/A	N/A	$7.86e-06$	100/1000	no	N/A	6.54
83.0	10000.0	Exact	5.0	N/A	N/A	$7.78e-06$	100/1000	no	N/A	7.36
83.0	$1.00e+05$	Exact	0.0	N/A	N/A	$6.41e-06$	100/1000	no	N/A	84.88
83.0	$1.00e+05$	Exact	1.0	N/A	N/A	$1.43e-05$	100/1000	no	N/A	79.39
83.0	$1.00e+05$	Exact	2.0	N/A	N/A	$1.37e-05$	100/1000	no	N/A	79.93
83.0	$1.00e+05$	Exact	3.0	N/A	N/A	$1.50e-05$	100/1000	no	N/A	79.56
83.0	$1.00e+05$	Exact	4.0	N/A	N/A	$1.51e-05$	100/1000	no	N/A	80.28
83.0	$1.00e+05$	Exact	5.0	N/A	N/A	$1.35e-05$	100/1000	no	N/A	80.26

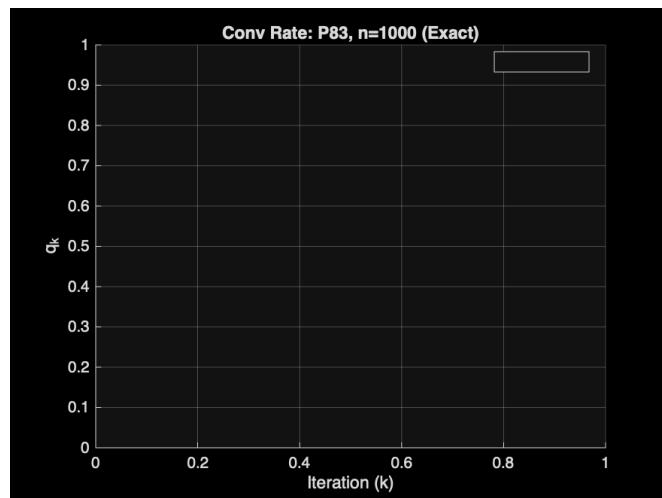


Figure 9: Problem 83, Truncated Newton, exact derivatives ( $n = 1000$ ): experimental convergence rate  $p_{exp}$  for converged runs.

## 7 Results - Mixed (constant $h$ )

### 7.1 Problem 31

#### 7.1.1 Modified Newton

Mixed FD (constant  $h$ ),  $k = 4$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd	$\bar{x}$	4	$2.14 \times 10^{-7}$	5/1000	yes		1.89	0.0013s
			1	4	$2.17 \times 10^{-7}$	6/1000	yes		1.89	0.0008s
			2	4	$1.22 \times 10^{-8}$	6/1000	yes		1.69	0.0008s
			3	4	$7.20 \times 10^{-9}$	6/1000	yes		1.64	0.0008s
			4	4	$3.70 \times 10^{-9}$	5/1000	yes		1.57	0.0008s
			5	4	$2.55 \times 10^{-10}$	8/1000	yes		1.30	0.0014s
			Avg (successes)	4	$7.56 \times 10^{-8}$	6.0/1000	6/6		1.66	0.0010s

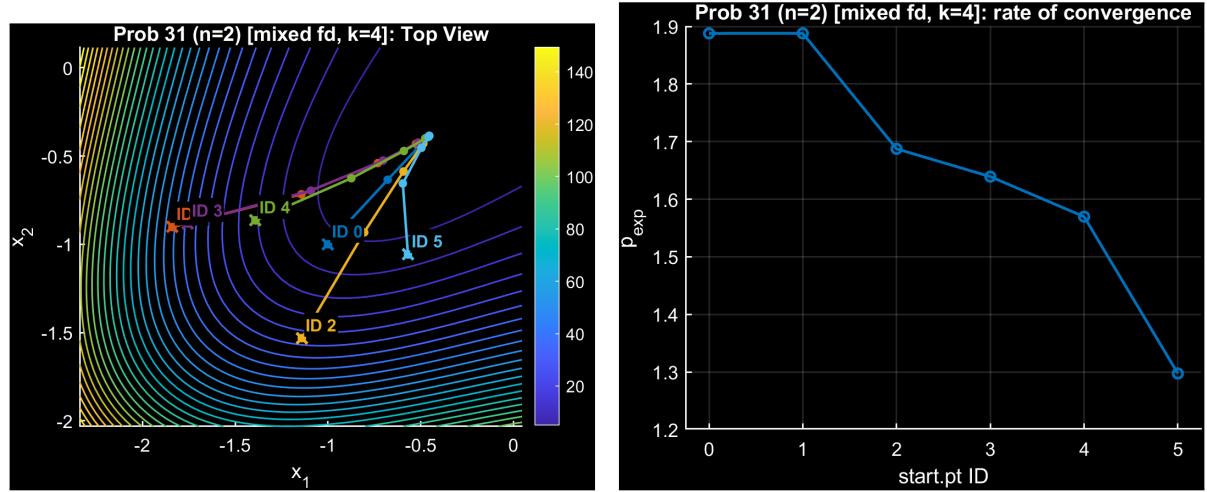


Figure 10: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

Case  $n > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd	$\bar{x}$	4	$5.08 \times 10^{-8}$	5/1000	yes		1.58	0.0053s
			1	4	$1.91 \times 10^{-10}$	10/1000	yes		1.24	0.0123s
			2	4	$4.62 \times 10^{-7}$	9/1000	yes		1.88	0.0090s
			3	4	$9.03 \times 10^{-11}$	9/1000	yes		1.21	0.0115s
			4	4	$7.51 \times 10^{-11}$	9/1000	yes		1.17	0.0113s
			5	4	$3.14 \times 10^{-10}$	9/1000	yes		1.30	0.0103s
			Avg (successes)	4	$8.55 \times 10^{-8}$	8.5/1000	6/6		1.40	0.0099s

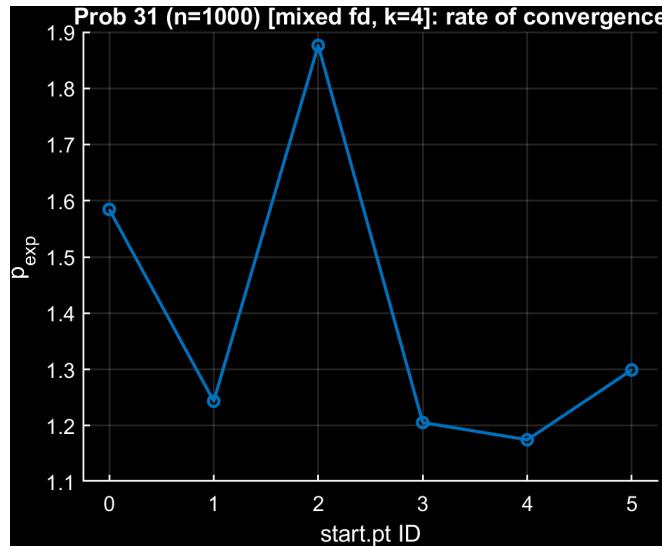


Figure 11: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd	$\bar{x}$	4	$5.85 \times 10^{-8}$	5/1000	yes		1.40	0.0368s
			1	4	$8.75 \times 10^{-10}$	10/1000	yes		1.37	0.0833s
			2	4	$1.65 \times 10^{-8}$	9/1000	yes		1.66	0.0741s
			3	4	$2.64 \times 10^{-7}$	10/1000	yes		1.90	0.0840s
			4	4	$6.23 \times 10^{-7}$	8/1000	yes		1.84	0.0683s
			5	4	$7.37 \times 10^{-7}$	10/1000	yes		1.90	0.0893s
			Avg (successes)	4	$2.83 \times 10^{-7}$	8.7/1000	6/6		1.68	0.0726s

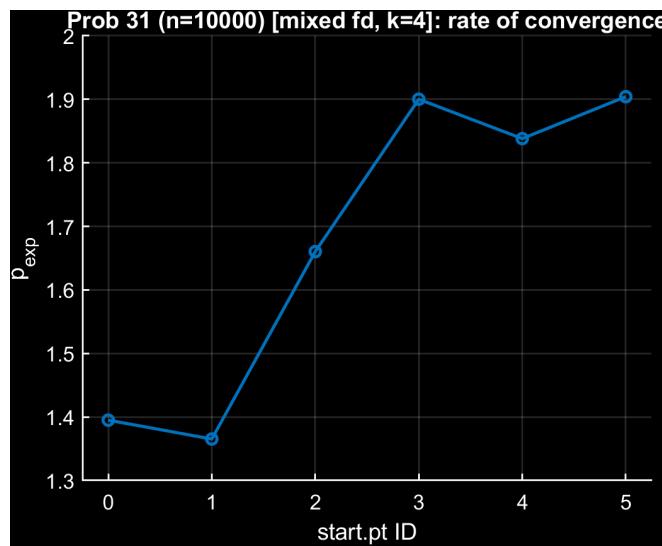


Figure 12: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd	$\bar{x}$	4	$1.09 \times 10^{-7}$	5/100	yes		1.33	0.4854s
			1	4	$2.72 \times 10^{-7}$	8/100	yes		1.81	1.04s
			2	4	$6.13 \times 10^{-8}$	12/100	yes		1.82	1.51s
			3	4	$1.56 \times 10^{-9}$	10/100	yes		1.45	1.29s
			4	4	$1.25 \times 10^{-10}$	11/100	yes		1.17	1.54s
			5	4	$1.38 \times 10^{-7}$	12/100	yes		1.84	1.68s
			<i>Avg (successes)</i>		$9.69 \times 10^{-8}$	9.7/100	6/6		1.57	1.26s

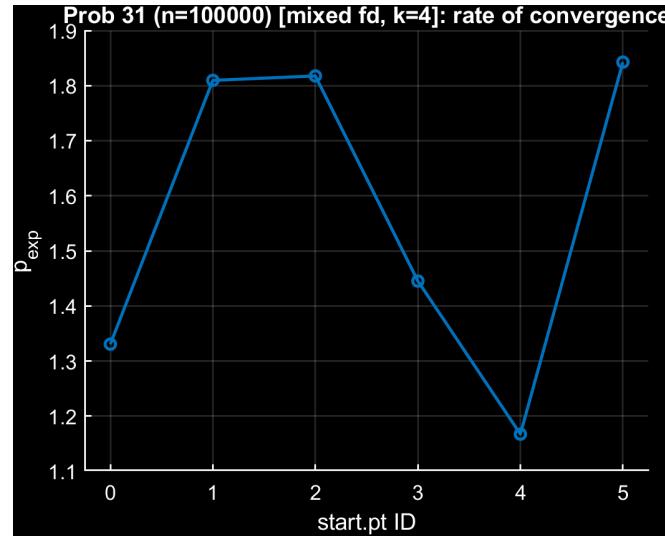


Figure 13: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

### Mixed FD (constant $h$ ), $k = 8$

#### Case $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd	$\bar{x}$	8	$1.32 \times 10^{-7}$	5/1000	yes		1.99	0.0006s
			1	8	$1.40 \times 10^{-7}$	6/1000	yes		1.98	0.0008s
			2	8	$2.17 \times 10^{-9}$	6/1000	yes		1.99	0.0010s
			3	8	$8.95 \times 10^{-10}$	6/1000	yes		1.99	0.0009s
			4	8	$2.68 \times 10^{-10}$	5/1000	yes		1.99	0.0007s
			5	8	$1.07 \times 10^{-12}$	8/1000	yes		2.00	0.0013s
			<i>Avg (successes)</i>		$4.59 \times 10^{-8}$	6.0/1000	6/6		1.99	0.0009s

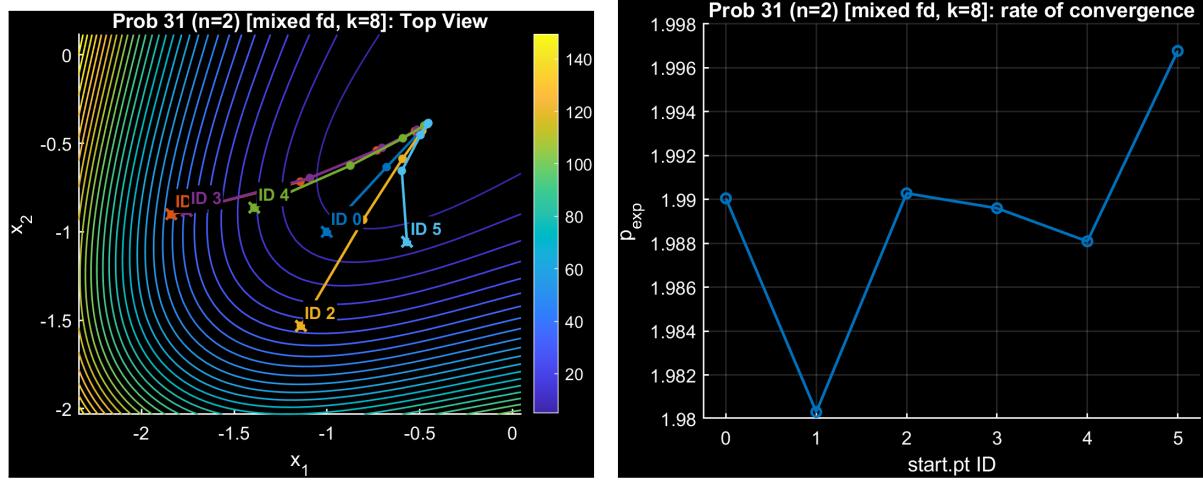


Figure 14: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $n > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.76	0.0054s
			1	8	$4.85 \times 10^{-13}$	10/1000	yes		1.98	0.0111s
			2	8	$3.30 \times 10^{-7}$	9/1000	yes		1.95	0.0085s
			3	8	$1.09 \times 10^{-13}$	9/1000	yes		1.98	0.0105s
			4	8	$8.28 \times 10^{-7}$	8/1000	yes		1.93	0.0105s
			5	8	$1.46 \times 10^{-12}$	9/1000	yes		1.99	0.0107s
			Avg (successes)	8	$1.96 \times 10^{-7}$	8.3/1000	6/6		1.93	0.0094s

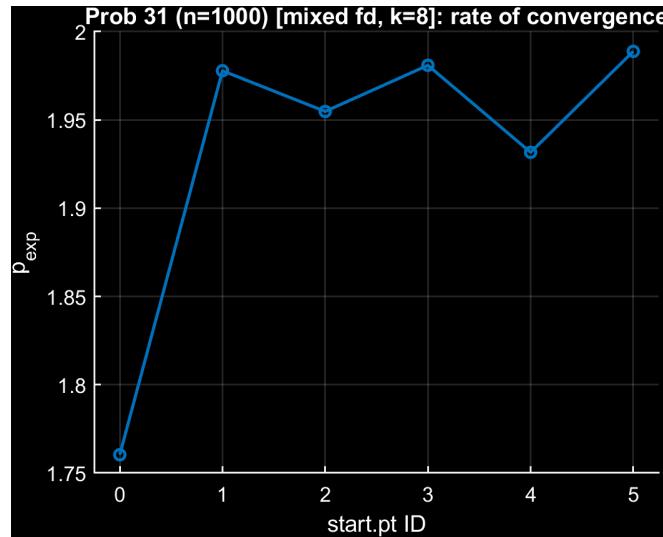


Figure 15: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.56	0.0394s
			1	8	$9.52 \times 10^{-12}$	10/1000	yes		2.00	0.0833s
			2	8	$3.12 \times 10^{-9}$	9/1000	yes		1.95	0.0735s
			3	8	$2.15 \times 10^{-7}$	10/1000	yes		1.99	0.0805s
			4	8	$4.62 \times 10^{-7}$	8/1000	yes		1.90	0.0672s
			5	8	$5.96 \times 10^{-7}$	10/1000	yes		1.96	0.0824s
			<i>Avg (successes)</i>	8	$2.16 \times 10^{-7}$	8.7/1000	6/6		1.89	0.0710s

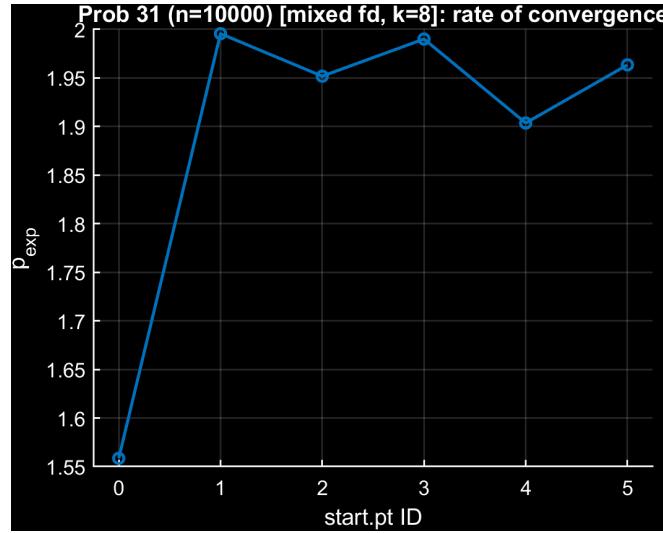


Figure 16: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/100	yes		1.56	0.5159s
			1	8	$1.73 \times 10^{-7}$	8/100	yes		1.90	1.05s
			2	8	$3.80 \times 10^{-8}$	12/100	yes		1.99	1.50s
			3	8	$3.46 \times 10^{-11}$	10/100	yes		2.00	1.26s
			4	8	$1.15 \times 10^{-13}$	11/100	yes		1.93	1.56s
			5	8	$1.23 \times 10^{-9}$	10/100	yes		2.00	1.50s
			<i>Avg (successes)</i>	8	$3.84 \times 10^{-8}$	9.3/100	6/6		1.90	1.23s

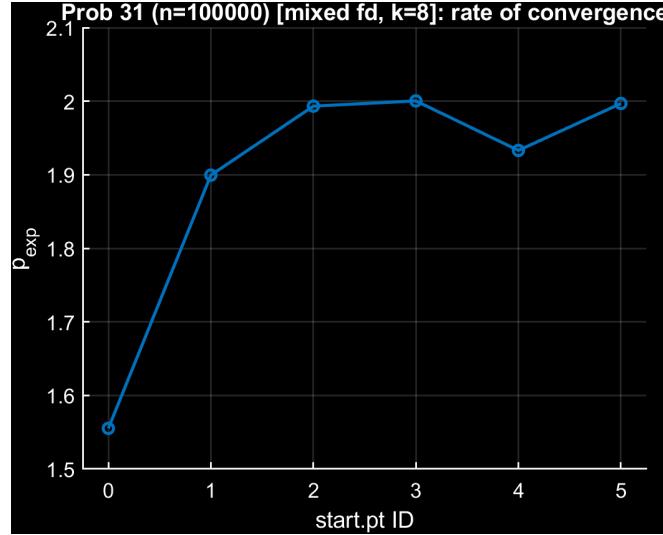


Figure 17: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

### Mixed FD (constant $h$ ), $k = 12$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd	$\bar{x}$	12	$1.32 \times 10^{-7}$	5/1000	yes		1.99	0.0007s
			1	12	$1.40 \times 10^{-7}$	6/1000	yes		1.98	0.0013s
			2	12	$2.16 \times 10^{-9}$	6/1000	yes		1.99	0.0009s
			3	12	$8.94 \times 10^{-10}$	6/1000	yes		1.99	0.0009s
			4	12	$2.67 \times 10^{-10}$	5/1000	yes		1.99	0.0009s
			5	12	$1.04 \times 10^{-12}$	8/1000	yes		2.00	0.0016s
			Avg (successes)	12	$4.59 \times 10^{-8}$	6.0/1000	6/6		1.99	0.0010s

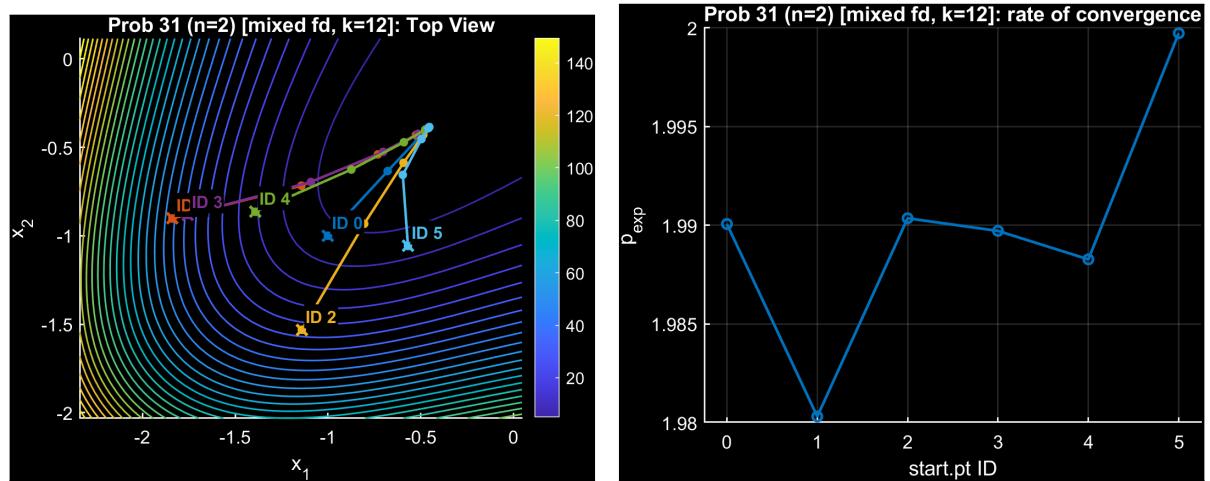


Figure 18: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/1000	yes		1.76	0.0052s
			1	12	$4.70 \times 10^{-13}$	10/1000	yes		1.98	0.0116s
			2	12	$3.30 \times 10^{-7}$	9/1000	yes		1.95	0.0090s
			3	12	$1.06 \times 10^{-13}$	9/1000	yes		1.98	0.0104s
			4	12	$8.28 \times 10^{-7}$	8/1000	yes		1.93	0.0097s
			5	12	$1.43 \times 10^{-12}$	9/1000	yes		1.99	0.0111s
			Avg (successes)	12	$1.96 \times 10^{-7}$	8.3/1000	6/6		1.93	0.0095s

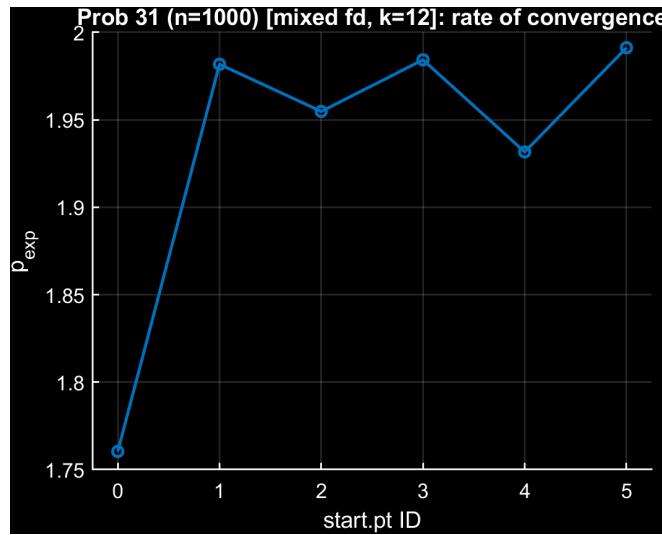


Figure 19: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/1000	yes		1.56	0.0349s
			1	12	$9.45 \times 10^{-12}$	10/1000	yes		2.00	0.0805s
			2	12	$3.12 \times 10^{-9}$	9/1000	yes		1.95	0.0751s
			3	12	$2.15 \times 10^{-7}$	10/1000	yes		1.99	0.0834s
			4	12	$4.62 \times 10^{-7}$	8/1000	yes		1.90	0.0672s
			5	12	$5.96 \times 10^{-7}$	10/1000	yes		1.96	0.0802s
			Avg (successes)	12	$2.16 \times 10^{-7}$	8.7/1000	6/6		1.89	0.0702s

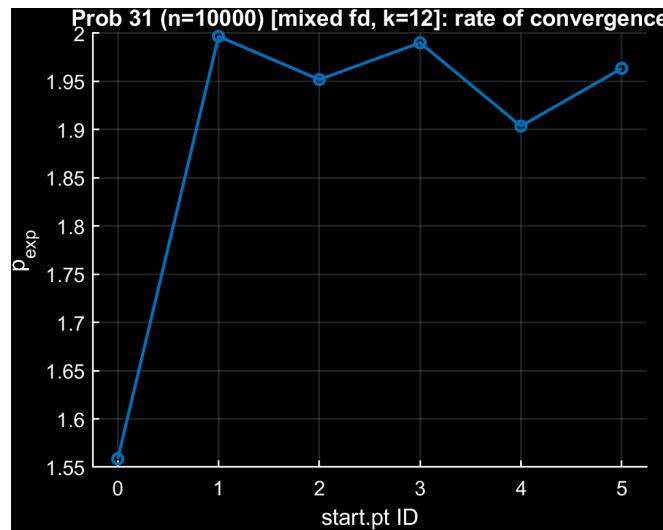


Figure 20: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/100	yes		1.56	0.5098s
			1	12	$1.73 \times 10^{-7}$	8/100	yes		1.90	1.05s
			2	12	$3.80 \times 10^{-8}$	12/100	yes		1.99	1.46s
			3	12	$3.45 \times 10^{-11}$	10/100	yes		2.00	1.24s
			4	12	$1.08 \times 10^{-13}$	11/100	yes		1.94	1.51s
			5	12	$1.23 \times 10^{-9}$	10/100	yes		2.00	1.43s
			<i>Avg (successes)</i>	12	$3.84 \times 10^{-8}$	9.3/100	6/6		1.90	1.20s

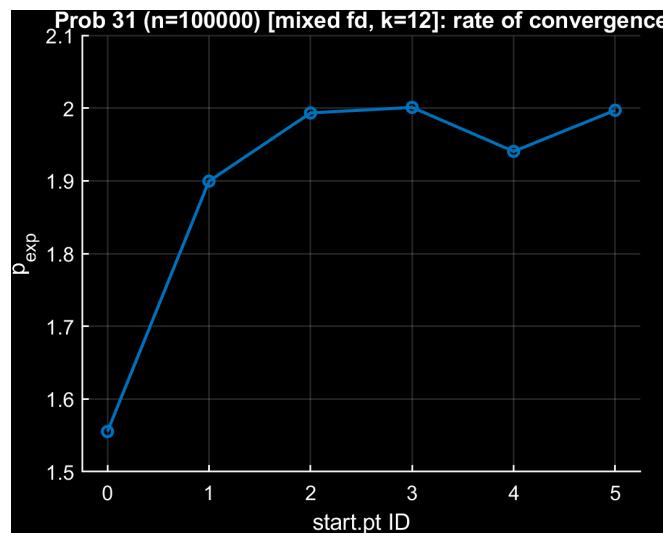


Figure 21: Problem 31, Modified Newton, mixed FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).



### 7.1.2 Truncated Newton

Mixed FD (constant  $h$ ),  $k = 4$

Table 3: Results for Problem 31.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
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31.0	2.0	FD	0.0	12.0	component-wise	$1.94e - 09$	6/1000	yes	2.0	0.0
31.0	2.0	FD	1.0	12.0	component-wise	$4.55e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	component-wise	$1.44e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	component-wise	$9.11e - 07$	5/1000	yes	1.06	0.0
31.0	2.0	FD	4.0	12.0	component-wise	$3.55e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	component-wise	$5.15e - 10$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	12.0	constant	$1.53e - 09$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	12.0	constant	$4.40e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	constant	$2.13e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	constant	$7.02e - 09$	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	12.0	constant	$1.87e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	constant	$3.80e - 10$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	4.0	component-wise	$6.17e - 11$	6/1000	yes	2.02	0.1
31.0	2.0	FD	1.0	4.0	component-wise	$9.55e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	4.0	component-wise	$2.17e - 07$	7/1000	yes	2.26	0.1
31.0	2.0	FD	3.0	4.0	component-wise	$1.62e - 12$	4/1000	yes	1.58	0.1
31.0	2.0	FD	4.0	4.0	component-wise	$8.97e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	5.0	4.0	component-wise	$4.42e - 12$	7/1000	yes	2.02	0.1
31.0	2.0	FD	0.0	4.0	constant	$6.18e - 11$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	4.0	constant	$9.56e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	4.0	constant	$2.18e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	4.0	constant	$1.15e - 12$	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	4.0	constant	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	4.0	constant	$4.45e - 12$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	component-wise	$6.18e - 11$	6/1000	yes	2.02	0.07
31.0	2.0	FD	1.0	8.0	component-wise	$9.55e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	8.0	component-wise	$2.17e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	component-wise	$2.98e - 12$	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	8.0	component-wise	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	component-wise	$4.39e - 12$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	constant	$6.17e - 11$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	8.0	constant	$9.55e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	8.0	constant	$2.17e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	constant	$1.15e - 12$	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	8.0	constant	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	constant	$4.45e - 12$	7/1000	yes	2.02	0.0
31.0	1000.0	FD	0.0	12.0	component-wise	$1.61e - 07$	11/1000	yes	2.27	0.01
31.0	1000.0	FD	1.0	12.0	component-wise	$2.40e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	12.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	component-wise	$8.53e - 08$	14/1000	yes	1.4	0.02
31.0	1000.0	FD	5.0	12.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	12.0	constant	$1.60e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	12.0	constant	$2.40e - 09$	14/1000	yes	1.59	0.01
31.0	1000.0	FD	2.0	12.0	constant	$3.42e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	constant	$8.54e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	12.0	constant	$1.23e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.22e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$1.61e - 07$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.22e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$1.61e - 07$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.22e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$1.61e - 07$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.22e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$1.61e - 07$	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.16	0.01
31.0										

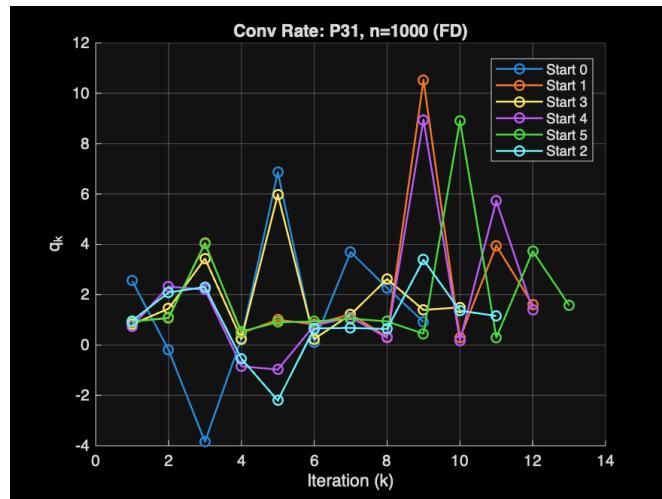


Figure 22: Problem 31, Truncated Newton, mixed FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate for converged runs ( $n = 1000$ ).



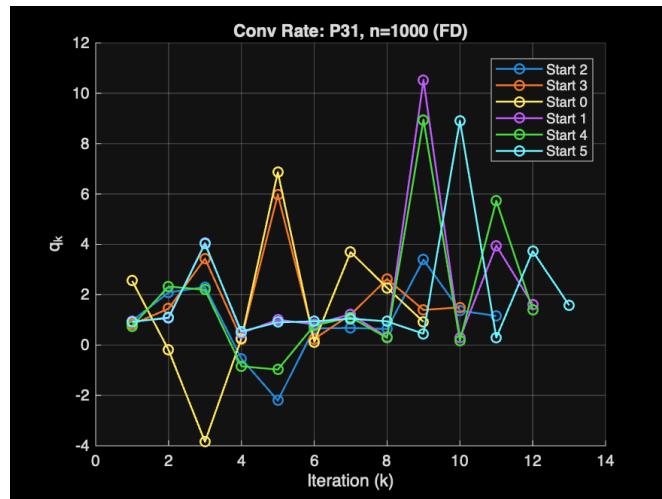


Figure 23: Problem 31, Truncated Newton, mixed FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Mixed FD (constant  $h$ ),  $k = 12$** 

Table 5: Results for Problem 31.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)	
31.0	2.0	FD	0.0	12.0	component-wise	1.94e-09	6/1000	yes	2.0	0.0	
31.0	2.0	FD	1.0	12.0	component-wise	4.55e-08	7/1000	yes	2.0	0.0	
31.0	2.0	FD	2.0	12.0	component-wise	1.44e-07	7/1000	yes	2.26	0.0	
31.0	2.0	FD	3.0	12.0	component-wise	9.11e-07	5/1000	yes	1.06	0.0	
31.0	2.0	FD	4.0	12.0	component-wise	3.55e-08	7/1000	yes	2.0	0.0	
31.0	2.0	FD	5.0	12.0	component-wise	5.15e-10	7/1000	yes	2.02	0.0	
31.0	2.0	FD	0.0	12.0	constant	1.53e-09	6/1000	yes	2.02	0.0	
31.0	2.0	FD	1.0	12.0	constant	4.40e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	2.0	12.0	constant	2.13e-07	7/1000	yes	2.26	0.0	
31.0	2.0	FD	3.0	12.0	constant	7.02e-09	4/1000	yes	1.58	0.0	
31.0	2.0	FD	4.0	12.0	constant	1.87e-08	7/1000	yes	2.0	0.0	
31.0	2.0	FD	5.0	12.0	constant	3.80e-10	7/1000	yes	2.02	0.0	
31.0	2.0	FD	0.0	4.0	component-wise	6.17e-11	6/1000	yes	2.02	0.1	
31.0	2.0	FD	1.0	4.0	component-wise	9.55e-09	7/1000	yes	2.0	0.1	
31.0	2.0	FD	2.0	4.0	component-wise	2.17e-07	7/1000	yes	2.26	0.1	
31.0	2.0	FD	3.0	4.0	component-wise	1.62e-12	4/1000	yes	1.58	0.1	
31.0	2.0	FD	4.0	4.0	component-wise	8.97e-09	7/1000	yes	2.0	0.1	
31.0	2.0	FD	5.0	4.0	component-wise	4.42e-12	7/1000	yes	2.02	0.1	
31.0	2.0	FD	0.0	4.0	constant	6.18e-11	6/1000	yes	2.02	0.0	
31.0	2.0	FD	1.0	4.0	constant	9.56e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	2.0	4.0	constant	2.18e-07	7/1000	yes	2.26	0.0	
31.0	2.0	FD	3.0	4.0	constant	1.15e-12	4/1000	yes	1.59	0.0	
31.0	2.0	FD	4.0	4.0	constant	8.97e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	5.0	4.0	constant	4.45e-12	7/1000	yes	2.02	0.0	
31.0	2.0	FD	0.0	8.0	component-wise	6.18e-11	6/1000	yes	2.02	0.07	
31.0	2.0	FD	1.0	8.0	component-wise	9.55e-09	7/1000	yes	2.0	0.1	
31.0	2.0	FD	2.0	8.0	component-wise	2.17e-07	7/1000	yes	2.26	0.0	
31.0	2.0	FD	3.0	8.0	component-wise	2.98e-12	4/1000	yes	1.58	0.0	
31.0	2.0	FD	4.0	8.0	component-wise	8.97e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	5.0	8.0	component-wise	4.39e-12	7/1000	yes	2.02	0.0	
31.0	2.0	FD	0.0	8.0	constant	6.17e-11	6/1000	yes	2.02	0.0	
31.0	2.0	FD	1.0	8.0	constant	9.55e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	2.0	8.0	constant	2.18e-07	7/1000	yes	2.26	0.0	
31.0	2.0	FD	3.0	8.0	constant	1.15e-12	4/1000	yes	1.59	0.0	
31.0	2.0	FD	4.0	8.0	constant	8.97e-09	7/1000	yes	2.0	0.0	
31.0	2.0	FD	5.0	8.0	constant	4.45e-12	7/1000	yes	2.02	0.0	
31.0	1000.0	FD	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.27	0.01	
31.0	1000.0	FD	1.0	12.0	component-wise	2.40e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	12.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	12.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	12.0	component-wise	8.53e-08	14/1000	yes	1.4	0.02	
31.0	1000.0	FD	5.0	12.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	12.0	constant	1.60e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	12.0	constant	2.40e-09	14/1000	yes	1.59	0.01	
31.0	1000.0	FD	2.0	12.0	constant	3.42e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	12.0	constant	8.54e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	12.0	constant	1.23e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	4.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	4.0	component-wise	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	4.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	4.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	4.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	4.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	4.0	constant	1.60e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	4.0	constant	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	4.0	constant	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	4.0	constant	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	4.0	constant	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.02	
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	0.0	2.0	32	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	2.0	32	component-wise	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	2.0	32	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	2.0	32	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	2.0	32	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	2.0	32	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.01	
31.0	1000.0	FD	0.0	2.0	32	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	2.0	32	component-wise	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	2.0	32	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	2.0	32	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	2.0	32	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	2.0	32	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01	
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.01	
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01	
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01	
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01	
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01	

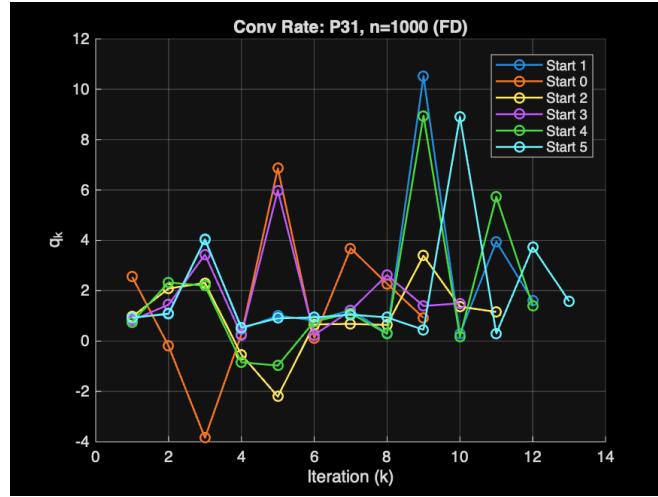


Figure 24: Problem 31, Truncated Newton, mixed FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

## 7.2 Problem 83

### 7.2.1 Modified Newton

Mixed FD (constant  $h$ ),  $k = 4$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd	$\bar{x}$	4	$1.07 \times 10^{-9}$	3/1000	yes		1.88	0.0258s
			1	4	$7.21 \times 10^{-10}$	3/1000	yes		1.98	0.0143s
			2	4	$4.13 \times 10^{-7}$	3/1000	yes		1.95	0.0137s
			3	4	$1.61 \times 10^{-9}$	3/1000	yes		2.04	0.0142s
			4	4	$7.45 \times 10^{-8}$	3/1000	yes		2.03	0.0150s
			5	4	$6.41 \times 10^{-12}$	4/1000	yes		1.24	0.0194s
			Avg (successes)	4	$8.18 \times 10^{-8}$	3.2/1000	6/6		1.85	0.0171s

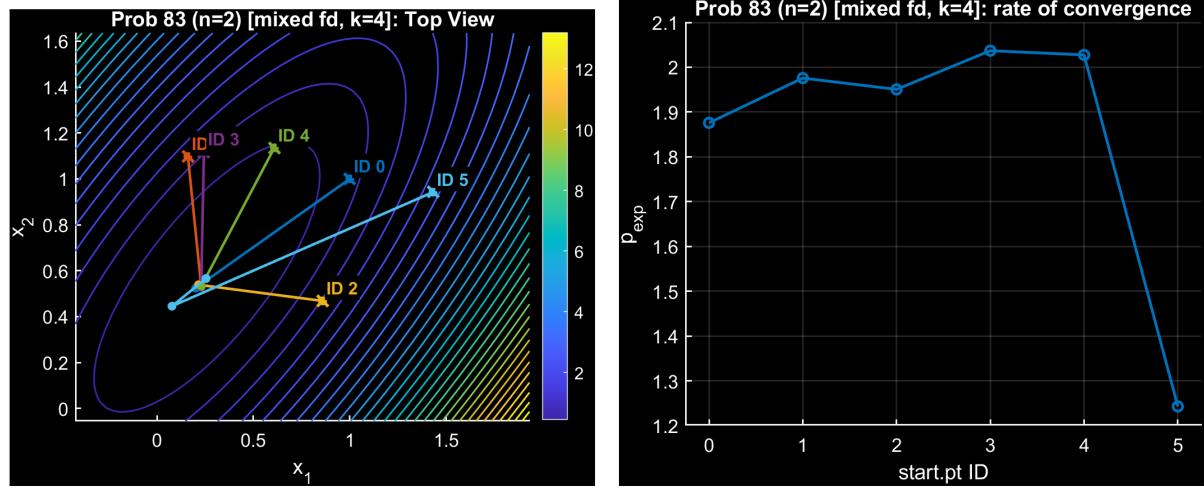


Figure 25: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $n > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	1000	mixed fd	$\bar{x}$	4	$5.71 \times 10^{-7}$	2/1000	yes		NaN	0.0159s	
			1	4	$3.32 \times 10^{-8}$	2/1000	yes		NaN	0.0160s	
			2	4	$2.02 \times 10^{-8}$	2/1000	yes		NaN	0.0149s	
			3	4	$3.18 \times 10^{-8}$	2/1000	yes		NaN	0.0154s	
			4	4	$2.70 \times 10^{-8}$	2/1000	yes		NaN	0.0152s	
			5	4	$2.73 \times 10^{-8}$	2/1000	yes		NaN	0.0148s	
			<i>Avg (successes)</i>		4	$1.18 \times 10^{-7}$	2.0/1000	6/6		NaN	0.0154s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	10000	mixed fd	$\bar{x}$	4	$1.42 \times 10^{-8}$	1/1000	yes		NaN	0.0196s	
			1	4	$7.05 \times 10^{-10}$	2/1000	yes		NaN	0.0407s	
			2	4	$9.28 \times 10^{-10}$	2/1000	yes		NaN	0.0395s	
			3	4	$2.69 \times 10^{-8}$	2/1000	yes		NaN	0.0353s	
			4	4	$4.10 \times 10^{-10}$	2/1000	yes		NaN	0.0328s	
			5	4	$3.57 \times 10^{-10}$	2/1000	yes		NaN	0.0342s	
			<i>Avg (successes)</i>		4	$7.24 \times 10^{-9}$	1.8/1000	6/6		NaN	0.0337s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	100000	mixed fd	$\bar{x}$	4	$9.67 \times 10^{-9}$	1/100	yes		NaN	0.1631s	
			1	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1678s	
			2	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1656s	
			3	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1669s	
			4	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1638s	
			5	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1726s	
			<i>Avg (successes)</i>		4	$1.41 \times 10^{-7}$	1.0/100	6/6		NaN	0.1666s

**Mixed FD (constant  $h$ ),  $k = 8$** **Case  $n = 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd	$\bar{x}$	8	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0142s
			1	8	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0149s
			2	8	$4.34 \times 10^{-7}$	3/1000	yes		1.94	0.0144s
			3	8	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0155s
			4	8	$8.39 \times 10^{-8}$	3/1000	yes		2.00	0.0158s
			5	8	$8.71 \times 10^{-15}$	4/1000	yes		1.91	0.0194s
			<i>Avg (successes)</i>	8	$8.71 \times 10^{-8}$	3.2/1000	6/6		1.94	0.0157s

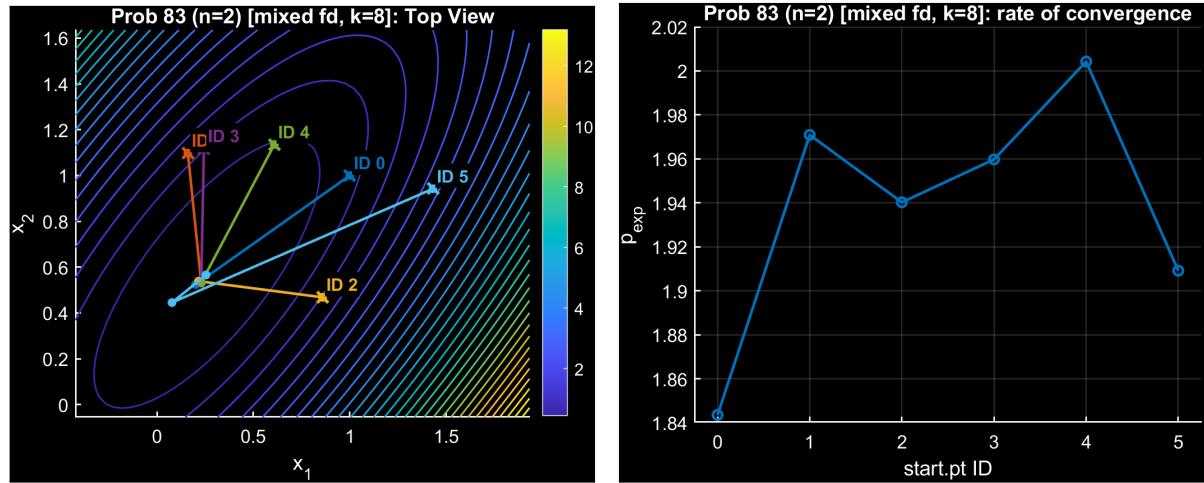


Figure 26: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	mixed fd	$\bar{x}$	8	$6.67 \times 10^{-13}$	2/1000	yes		NaN	0.0130s
			1	8	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0136s
			2	8	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0146s
			3	8	$2.80 \times 10^{-8}$	2/1000	yes		NaN	0.0147s
			4	8	$2.94 \times 10^{-8}$	2/1000	yes		NaN	0.0144s
			5	8	$2.36 \times 10^{-8}$	2/1000	yes		NaN	0.0151s
			<i>Avg (successes)</i>	8	$2.19 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0142s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	mixed fd	$\bar{x}$	8	$1.14 \times 10^{-8}$	1/1000	yes		NaN	0.0171s
			1	8	$4.65 \times 10^{-8}$	2/1000	yes		NaN	0.0412s
			2	8	$3.90 \times 10^{-8}$	2/1000	yes		NaN	0.0396s
			3	8	$2.68 \times 10^{-8}$	2/1000	yes		NaN	0.0405s
			4	8	$1.77 \times 10^{-9}$	2/1000	yes		NaN	0.0390s
			5	8	$1.50 \times 10^{-9}$	2/1000	yes		NaN	0.0393s
			<i>Avg (successes)</i>	8	$2.12 \times 10^{-8}$	1.8/1000	6/6		NaN	0.0361s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	mixed fd	$\bar{x}$	8	$1.17 \times 10^{-10}$	1/100	yes		NaN	0.1538s
			1	8	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1675s
			2	8	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1666s
			3	8	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1682s
			4	8	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1798s
			5	8	$1.67 \times 10^{-7}$	1/100	yes		NaN	0.1752s
			<i>Avg (successes)</i>	8	$1.40 \times 10^{-7}$	1.0/100	6/6		NaN	0.1685s

### Mixed FD (constant $h$ ), $k = 12$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd	$\bar{x}$	12	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0137s
			1	12	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0150s
			2	12	$4.34 \times 10^{-7}$	3/1000	yes		1.94	0.0179s
			3	12	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0145s
			4	12	$8.39 \times 10^{-8}$	3/1000	yes		2.00	0.0140s
			5	12	$9.27 \times 10^{-15}$	4/1000	yes		1.90	0.0171s
			<i>Avg (successes)</i>	12	$8.71 \times 10^{-8}$	3.2/1000	6/6		1.94	0.0154s

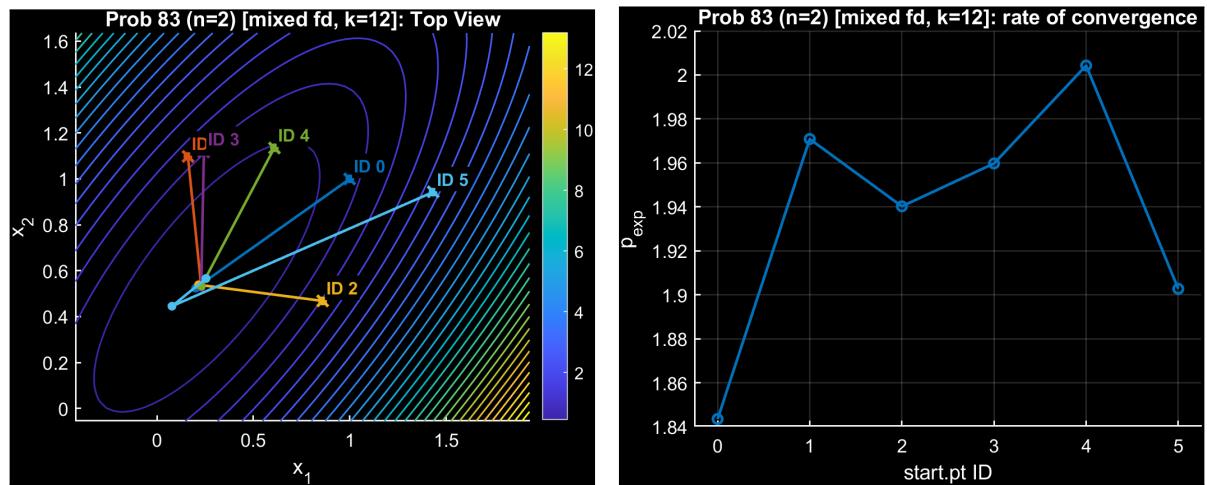


Figure 27: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	mixed fd	$\bar{x}$	12	$4.63 \times 10^{-11}$	2/1000	yes		NaN	0.0134s
			1	12	$2.62 \times 10^{-8}$	2/1000	yes		NaN	0.0161s
			2	12	$2.89 \times 10^{-8}$	2/1000	yes		NaN	0.0156s
			3	12	$2.90 \times 10^{-8}$	2/1000	yes		NaN	0.0148s
			4	12	$3.20 \times 10^{-8}$	2/1000	yes		NaN	0.0157s
			5	12	$2.64 \times 10^{-8}$	2/1000	yes		NaN	0.0145s
			<i>Avg (successes)</i>	12	$2.37 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0150s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	mixed fd	$\bar{x}$	12	$1.13 \times 10^{-8}$	1/1000	yes		NaN	0.0180s
			1	12	$5.30 \times 10^{-8}$	2/1000	yes		NaN	0.0377s
			2	12	$4.31 \times 10^{-8}$	2/1000	yes		NaN	0.0394s
			3	12	$2.90 \times 10^{-8}$	2/1000	yes		NaN	0.0385s
			4	12	$1.40 \times 10^{-7}$	2/1000	yes		NaN	0.0380s
			5	12	$1.43 \times 10^{-7}$	2/1000	yes		NaN	0.0379s
			<i>Avg (successes)</i>	12	$6.99 \times 10^{-8}$	1.8/1000	6/6		NaN	0.0349s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	mixed fd	$\bar{x}$	12	$3.23 \times 10^{-10}$	1/100	yes		NaN	0.1728s
			1	12	$1.82 \times 10^{-7}$	1/100	yes		NaN	0.1848s
			2	12	$1.82 \times 10^{-7}$	1/100	yes		NaN	0.1851s
			3	12	$1.82 \times 10^{-7}$	1/100	yes		NaN	0.1639s
			4	12	$1.83 \times 10^{-7}$	1/100	yes		NaN	0.1628s
			5	12	$1.82 \times 10^{-7}$	1/100	yes		NaN	0.1665s
			<i>Avg (successes)</i>	12	$1.52 \times 10^{-7}$	1.0/100	6/6		NaN	0.1726s



### 7.2.2 Truncated Newton

### Mixed FD (constant $h$ ), $k = 4$

Table 6: Results for Problem 83.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt	ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD		0.0	12.0	component-wise	$4.41e-07$	5/1000	yes	0.91	0.0
83.0	2.0	FD		1.0	12.0	component-wise	$4.55e-07$	4/1000	yes	1.38	0.0
83.0	2.0	FD		2.0	12.0	component-wise	$6.98e-08$	5/1000	yes	1.24	0.0
83.0	2.0	FD		3.0	12.0	component-wise	$4.97e-07$	5/1000	yes	0.78	0.0
83.0	2.0	FD		4.0	12.0	component-wise	$5.25e-07$	4/1000	yes	1.47	0.0
83.0	2.0	FD		5.0	12.0	component-wise	$4.52e-07$	4/1000	yes	1.44	0.0
83.0	2.0	FD		0.0	12.0	constant	$6.33e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		1.0	12.0	constant	$6.41e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		2.0	12.0	constant	$1.55e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		3.0	12.0	constant	$1.15e-07$	8/1000	yes	1.0	0.0
83.0	2.0	FD		4.0	12.0	constant	$8.80e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		5.0	12.0	constant	$1.85e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		0.0	4.0	component-wise	$4.40e-07$	5/1000	yes	0.91	0.04
83.0	2.0	FD		1.0	4.0	component-wise	$4.54e-07$	4/1000	yes	1.38	0.03
83.0	2.0	FD		2.0	4.0	component-wise	$6.96e-08$	5/1000	yes	1.24	0.04
83.0	2.0	FD		3.0	4.0	component-wise	$4.96e-07$	5/1000	yes	0.78	0.04
83.0	2.0	FD		4.0	4.0	component-wise	$5.24e-07$	4/1000	yes	1.47	0.04
83.0	2.0	FD		5.0	4.0	component-wise	$4.75e-07$	4/1000	yes	1.43	0.04
83.0	2.0	FD		0.0	4.0	constant	$6.32e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		1.0	4.0	constant	$6.40e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		2.0	4.0	constant	$1.54e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		3.0	4.0	constant	$1.15e-07$	8/1000	yes	1.0	0.0
83.0	2.0	FD		4.0	4.0	constant	$8.78e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		5.0	4.0	constant	$1.85e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		0.0	8.0	component-wise	$4.41e-07$	5/1000	yes	0.91	0.04
83.0	2.0	FD		1.0	8.0	component-wise	$4.55e-07$	4/1000	yes	1.38	0.03
83.0	2.0	FD		2.0	8.0	component-wise	$6.98e-08$	5/1000	yes	1.24	0.0
83.0	2.0	FD		3.0	8.0	component-wise	$4.97e-07$	5/1000	yes	0.78	0.0
83.0	2.0	FD		4.0	8.0	component-wise	$5.25e-07$	4/1000	yes	1.47	0.0
83.0	2.0	FD		5.0	8.0	component-wise	$4.52e-07$	4/1000	yes	1.44	0.0
83.0	2.0	FD		0.0	8.0	constant	$6.33e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		1.0	8.0	constant	$6.41e-07$	6/1000	yes	1.0	0.01
83.0	2.0	FD		2.0	8.0	constant	$1.55e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		3.0	8.0	constant	$1.15e-07$	8/1000	yes	1.0	0.0
83.0	2.0	FD		4.0	8.0	constant	$8.80e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		5.0	8.0	constant	$1.85e-07$	7/1000	yes	1.0	0.01
83.0	2.0	FD		0.0	2.0	constant	$1.55e-07$	7/1000	yes	1.0	0.0
83.0	2.0	FD		1.0	2.0	constant	$1.15e-07$	8/1000	yes	1.0	0.0
83.0	2.0	FD		2.0	2.0	constant	$8.80e-07$	6/1000	yes	1.0	0.0
83.0	2.0	FD		3.0	2.0	constant	$1.85e-07$	7/1000	yes	1.0	0.01
83.0	1000.0	FD		0.0	12.0	component-wise	$9.14e-07$	82/1000	yes	-0.96	0.6
83.0	1000.0	FD		1.0	12.0	component-wise	$4.06e-06$	100/1000	no	N/A	0.75
83.0	1000.0	FD		2.0	12.0	component-wise	$4.49e-06$	100/1000	no	N/A	0.89
83.0	1000.0	FD		3.0	12.0	component-wise	$4.76e-07$	39/1000	yes	-1.05	0.27
83.0	1000.0	FD		4.0	12.0	component-wise	$1.03e-05$	100/1000	no	N/A	0.85
83.0	1000.0	FD		5.0	12.0	component-wise	$8.82e-06$	100/1000	no	N/A	1.07
83.0	1000.0	FD		0.0	12.0	constant	$2.56e-06$	100/1000	no	N/A	0.83
83.0	1000.0	FD		1.0	12.0	constant	$3.05e-06$	100/1000	no	N/A	0.76
83.0	1000.0	FD		2.0	12.0	constant	$1.52e-05$	100/1000	no	N/A	0.99
83.0	1000.0	FD		3.0	12.0	constant	$5.67e-06$	100/1000	no	N/A	0.81
83.0	1000.0	FD		4.0	12.0	constant	$3.11e-06$	100/1000	no	N/A	0.73
83.0	1000.0	FD		5.0	12.0	constant	$4.37e-06$	100/1000	no	N/A	0.86
83.0	1000.0	FD		0.0	4.0	component-wise	$3.77e-06$	100/1000	no	N/A	1.07
83.0	1000.0	FD		1.0	4.0	component-wise	$2.38e-06$	100/1000	no	N/A	0.73
83.0	1000.0	FD		2.0	4.0	component-wise	$5.26e-07$	51/1000	yes	-1.06	0.48
83.0	1000.0	FD		3.0	4.0	component-wise	$2.18e-06$	100/1000	no	N/A	0.79
83.0	1000.0	FD		4.0	4.0	component-wise	$3.92e-06$	100/1000	no	N/A	0.74
83.0	1000.0	FD		5.0	4.0	component-wise	$1.13e-05$	100/1000	no	N/A	0.77
83.0	1000.0	FD		0.0	4.0	constant	$3.46e-06$	100/1000	no	N/A	0.88
83.0	1000.0	FD		1.0	4.0	constant	$6.05e-06$	100/1000	no	N/A	0.85
83.0	1000.0	FD		2.0	4.0	constant	$3.36e-06$	100/1000	no	N/A	1.0
83.0	1000.0	FD		3.0	4.0	constant	$6.66e-06$	100/1000	no	N/A	0.77
83.0	1000.0	FD		4.0	4.0	constant	$6.87e-06$	100/1000	no	N/A	0.73
83.0	1000.0	FD		5.0	4.0	constant	$3.88e-06$	100/1000	no	N/A	0.98
83.0	1000.0	FD		0.0	8.0	component-wise	$1.86e-06$	100/1000	no	N/A	0.92
83.0	1000.0	FD		1.0	8.0	component-wise	$6.70e-07$	45/1000	yes	-1.0	0.42
83.0	1000.0	FD		2.0	8.0	component-wise	$5.86e-07$	51/1000	yes	-1.09	0.4
83.0	1000.0	FD		3.0	8.0	component-wise	$5.32e-07$	41/1000	yes	-1.04	0.25
83.0	1000.0	FD		4.0	8.0	component-wise	$2.36e-05$	100/1000	no	N/A	0.83
83.0	1000.0	FD		5.0	8.0	component-wise	$1.61e-05$	100/1000	no	N/A	0.84
83.0	1000.0	FD		0.0	8.0	constant	$2.51e-06$	100/1000	no	N/A	0.89

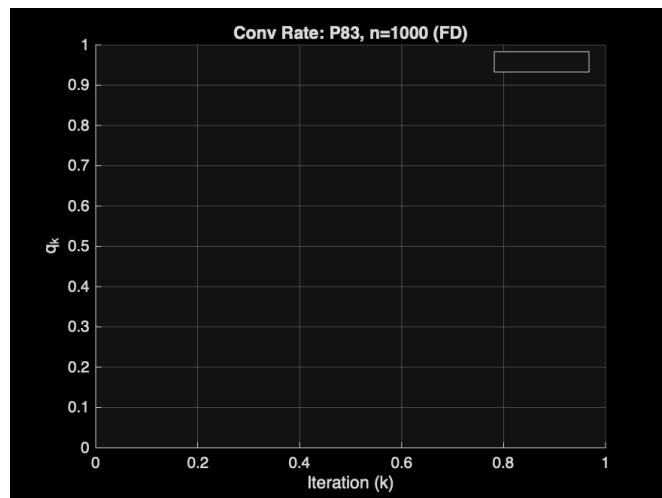


Figure 28: Problem 83, Truncated Newton, mixed FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Mixed FD (constant  $h$ ),  $k = 8$** 

Table 7: Results for Problem 83.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD	0.0	12.0	component-wise	4.41e - 07	5/1000	yes	0.91	0.0
83.0	2.0	FD	1.0	12.0	component-wise	4.55e - 07	4/1000	yes	1.38	0.0
83.0	2.0	FD	2.0	12.0	component-wise	6.98e - 08	5/1000	yes	1.24	0.0
83.0	2.0	FD	3.0	12.0	component-wise	4.97e - 07	5/1000	yes	0.78	0.0
83.0	2.0	FD	4.0	12.0	component-wise	5.25e - 07	4/1000	yes	1.47	0.0
83.0	2.0	FD	5.0	12.0	component-wise	4.52e - 07	4/1000	yes	1.44	0.0
83.0	2.0	FD	0.0	12.0	constant	6.33e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	12.0	constant	6.41e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	2.0	12.0	constant	1.55e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	12.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	12.0	constant	8.80e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	12.0	constant	1.85e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	0.0	4.0	component-wise	4.40e - 07	5/1000	yes	0.91	0.04
83.0	2.0	FD	1.0	4.0	component-wise	4.54e - 07	4/1000	yes	1.38	0.03
83.0	2.0	FD	2.0	4.0	component-wise	6.96e - 08	5/1000	yes	1.24	0.04
83.0	2.0	FD	3.0	4.0	component-wise	4.96e - 07	5/1000	yes	0.78	0.04
83.0	2.0	FD	4.0	4.0	component-wise	5.24e - 07	4/1000	yes	1.47	0.04
83.0	2.0	FD	5.0	4.0	component-wise	4.75e - 07	4/1000	yes	1.43	0.04
83.0	2.0	FD	0.0	4.0	constant	6.32e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	4.0	constant	6.40e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	2.0	4.0	constant	1.54e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	4.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	4.0	constant	8.78e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	4.0	constant	1.85e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	0.0	8.0	component-wise	4.41e - 07	5/1000	yes	0.91	0.04
83.0	2.0	FD	1.0	8.0	component-wise	4.55e - 07	4/1000	yes	1.38	0.03
83.0	2.0	FD	2.0	8.0	component-wise	6.98e - 08	5/1000	yes	1.24	0.0
83.0	2.0	FD	3.0	8.0	component-wise	4.97e - 07	5/1000	yes	0.78	0.0
83.0	2.0	FD	4.0	8.0	component-wise	5.25e - 07	4/1000	yes	1.47	0.0
83.0	2.0	FD	5.0	8.0	component-wise	4.52e - 07	4/1000	yes	1.44	0.0
83.0	2.0	FD	0.0	8.0	constant	6.33e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	8.0	constant	6.41e - 07	6/1000	yes	1.0	0.01
83.0	2.0	FD	2.0	8.0	constant	1.55e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	8.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	8.0	constant	8.80e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	8.0	constant	1.85e - 07	7/1000	yes	1.0	0.01
83.0	1000.0	FD	0.0	12.0	component-wise	9.14e - 07	82/1000	yes	-0.96	0.6
83.0	1000.0	FD	1.0	12.0	component-wise	4.06e - 06	100/1000	no	N/A	0.75
83.0	1000.0	FD	2.0	12.0	component-wise	4.49e - 06	100/1000	no	N/A	0.89
83.0	1000.0	FD	3.0	12.0	component-wise	4.76e - 07	39/1000	yes	-1.05	0.27
83.0	1000.0	FD	4.0	12.0	component-wise	1.03e - 05	100/1000	no	N/A	0.85
83.0	1000.0	FD	5.0	12.0	component-wise	8.82e - 06	100/1000	no	N/A	1.07
83.0	1000.0	FD	0.0	12.0	constant	2.56e - 06	100/1000	no	N/A	0.83
83.0	1000.0	FD	1.0	12.0	constant	3.05e - 06	100/1000	no	N/A	0.76
83.0	1000.0	FD	2.0	12.0	constant	1.52e - 05	100/1000	no	N/A	0.99
83.0	1000.0	FD	3.0	12.0	constant	5.67e - 06	100/1000	no	N/A	0.81
83.0	1000.0	FD	4.0	12.0	constant	3.11e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	5.0	12.0	constant	4.37e - 06	100/1000	no	N/A	0.86
83.0	1000.0	FD	0.0	4.0	component-wise	3.77e - 06	100/1000	no	N/A	1.07
83.0	1000.0	FD	1.0	4.0	component-wise	2.38e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	2.0	4.0	component-wise	5.26e - 07	51/1000	yes	-1.06	0.48
83.0	1000.0	FD	3.0	4.0	component-wise	2.18e - 06	100/1000	no	N/A	0.79
83.0	1000.0	FD	4.0	4.0	component-wise	3.92e - 06	100/1000	no	N/A	0.74
83.0	1000.0	FD	5.0	4.0	component-wise	1.13e - 05	100/1000	no	N/A	0.77
83.0	1000.0	FD	0.0	4.0	constant	3.46e - 06	100/1000	no	N/A	0.88
83.0	1000.0	FD	1.0	4.0	constant	6.05e - 06	100/1000	no	N/A	0.85
83.0	1000.0	FD	2.0	4.0	constant	3.36e - 06	100/1000	no	N/A	1.0
83.0	1000.0	FD	3.0	4.0	constant	6.66e - 06	100/1000	no	N/A	0.77
83.0	1000.0	FD	4.0	4.0	constant	6.87e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	5.0	4.0	constant	3.88e - 06	100/1000	no	N/A	0.98
83.0	1000.0	FD	0.0	8.0	component-wise	1.86e - 06	100/1000	no	N/A	0.92
83.0	1000.0	FD	1.0	8.0	component-wise	6.70e - 07	45/1000	yes	-1.0	0.42
83.0	1000.0	FD	2.0	8.0	component-wise	5.86e - 07	51/1000	yes	-1.09	0.4
83.0	1000.0	FD	3.0	8.0	component-wise	5.32e - 07	41/1000	yes	-1.04	0.25
83.0	1000.0	FD	4.0	8.0	component-wise	2.36e - 05	100/1000	no	N/A	0.83
83.0	1000.0	FD	5.0	8.0	component-wise	1.61e - 05	100/1000	no	N/A	0.84
83.0	1000.0	FD	0.0	8.0	constant	2.51e - 06	100/1000	no	N/A	0.89
83.0	1000.0	FD	1.0	8.0	constant	1.90e - 06	100/1000	no	N/A	0.8
83.0	1000.0	FD	2.0	8.0	constant	2.91e - 06	100/1000	no	N/A	1.01
83.0	1000.0	FD	3.0	8.0	constant	41	component-wise	2.36e - 05	100/1000	no

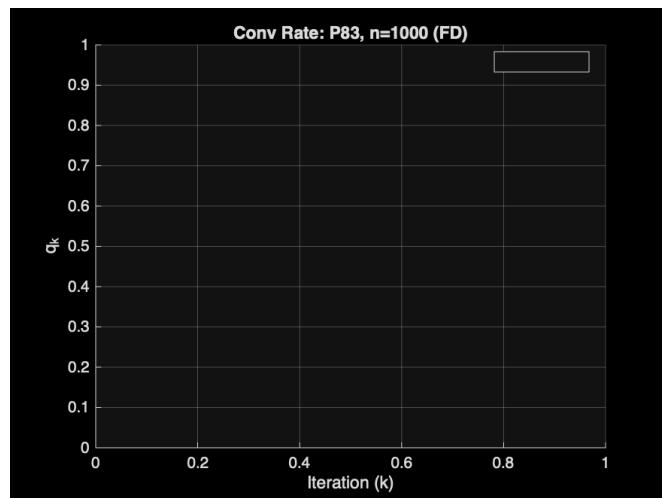


Figure 29: Problem 83, Truncated Newton, mixed FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Mixed FD (constant  $h$ ),  $k = 12$** 

Table 8: Results for Problem 83.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD	0.0	12.0	component-wise	4.41e - 07	5/1000	yes	0.91	0.0
83.0	2.0	FD	1.0	12.0	component-wise	4.55e - 07	4/1000	yes	1.38	0.0
83.0	2.0	FD	2.0	12.0	component-wise	6.98e - 08	5/1000	yes	1.24	0.0
83.0	2.0	FD	3.0	12.0	component-wise	4.97e - 07	5/1000	yes	0.78	0.0
83.0	2.0	FD	4.0	12.0	component-wise	5.25e - 07	4/1000	yes	1.47	0.0
83.0	2.0	FD	5.0	12.0	component-wise	4.52e - 07	4/1000	yes	1.44	0.0
83.0	2.0	FD	0.0	12.0	constant	6.33e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	12.0	constant	6.41e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	2.0	12.0	constant	1.55e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	12.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	12.0	constant	8.80e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	12.0	constant	1.85e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	0.0	4.0	component-wise	4.40e - 07	5/1000	yes	0.91	0.04
83.0	2.0	FD	1.0	4.0	component-wise	4.54e - 07	4/1000	yes	1.38	0.03
83.0	2.0	FD	2.0	4.0	component-wise	6.96e - 08	5/1000	yes	1.24	0.04
83.0	2.0	FD	3.0	4.0	component-wise	4.96e - 07	5/1000	yes	0.78	0.04
83.0	2.0	FD	4.0	4.0	component-wise	5.24e - 07	4/1000	yes	1.47	0.04
83.0	2.0	FD	5.0	4.0	component-wise	4.75e - 07	4/1000	yes	1.43	0.04
83.0	2.0	FD	0.0	4.0	constant	6.32e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	4.0	constant	6.40e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	2.0	4.0	constant	1.54e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	4.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	4.0	constant	8.78e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	4.0	constant	1.85e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	0.0	8.0	component-wise	4.41e - 07	5/1000	yes	0.91	0.04
83.0	2.0	FD	1.0	8.0	component-wise	4.55e - 07	4/1000	yes	1.38	0.03
83.0	2.0	FD	2.0	8.0	component-wise	6.98e - 08	5/1000	yes	1.24	0.0
83.0	2.0	FD	3.0	8.0	component-wise	4.97e - 07	5/1000	yes	0.78	0.0
83.0	2.0	FD	4.0	8.0	component-wise	5.25e - 07	4/1000	yes	1.47	0.0
83.0	2.0	FD	5.0	8.0	component-wise	4.52e - 07	4/1000	yes	1.44	0.0
83.0	2.0	FD	0.0	8.0	constant	6.33e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	1.0	8.0	constant	6.41e - 07	6/1000	yes	1.0	0.01
83.0	2.0	FD	2.0	8.0	constant	1.55e - 07	7/1000	yes	1.0	0.0
83.0	2.0	FD	3.0	8.0	constant	1.15e - 07	8/1000	yes	1.0	0.0
83.0	2.0	FD	4.0	8.0	constant	8.80e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD	5.0	8.0	constant	1.85e - 07	7/1000	yes	1.0	0.01
83.0	1000.0	FD	0.0	12.0	component-wise	9.14e - 07	82/1000	yes	-0.96	0.6
83.0	1000.0	FD	1.0	12.0	component-wise	4.06e - 06	100/1000	no	N/A	0.75
83.0	1000.0	FD	2.0	12.0	component-wise	4.49e - 06	100/1000	no	N/A	0.89
83.0	1000.0	FD	3.0	12.0	component-wise	4.76e - 07	39/1000	yes	-1.05	0.27
83.0	1000.0	FD	4.0	12.0	component-wise	1.03e - 05	100/1000	no	N/A	0.85
83.0	1000.0	FD	5.0	12.0	component-wise	8.82e - 06	100/1000	no	N/A	1.07
83.0	1000.0	FD	0.0	12.0	constant	2.56e - 06	100/1000	no	N/A	0.83
83.0	1000.0	FD	1.0	12.0	constant	3.05e - 06	100/1000	no	N/A	0.76
83.0	1000.0	FD	2.0	12.0	constant	1.52e - 05	100/1000	no	N/A	0.99
83.0	1000.0	FD	3.0	12.0	constant	5.67e - 06	100/1000	no	N/A	0.81
83.0	1000.0	FD	4.0	12.0	constant	3.11e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	5.0	12.0	constant	4.37e - 06	100/1000	no	N/A	0.86
83.0	1000.0	FD	0.0	4.0	component-wise	3.77e - 06	100/1000	no	N/A	1.07
83.0	1000.0	FD	1.0	4.0	component-wise	2.38e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	2.0	4.0	component-wise	5.26e - 07	51/1000	yes	-1.06	0.48
83.0	1000.0	FD	3.0	4.0	component-wise	2.18e - 06	100/1000	no	N/A	0.79
83.0	1000.0	FD	4.0	4.0	component-wise	3.92e - 06	100/1000	no	N/A	0.74
83.0	1000.0	FD	5.0	4.0	component-wise	1.13e - 05	100/1000	no	N/A	0.77
83.0	1000.0	FD	0.0	4.0	constant	3.46e - 06	100/1000	no	N/A	0.88
83.0	1000.0	FD	1.0	4.0	constant	6.05e - 06	100/1000	no	N/A	0.85
83.0	1000.0	FD	2.0	4.0	constant	3.36e - 06	100/1000	no	N/A	1.0
83.0	1000.0	FD	3.0	4.0	constant	6.66e - 06	100/1000	no	N/A	0.77
83.0	1000.0	FD	4.0	4.0	constant	6.87e - 06	100/1000	no	N/A	0.73
83.0	1000.0	FD	5.0	4.0	constant	3.88e - 06	100/1000	no	N/A	0.98
83.0	1000.0	FD	0.0	8.0	component-wise	1.86e - 06	100/1000	no	N/A	0.92
83.0	1000.0	FD	1.0	8.0	component-wise	6.70e - 07	45/1000	yes	-1.0	0.42
83.0	1000.0	FD	2.0	8.0	component-wise	5.86e - 07	51/1000	yes	-1.09	0.4
83.0	1000.0	FD	3.0	8.0	component-wise	5.32e - 07	41/1000	yes	-1.04	0.25
83.0	1000.0	FD	4.0	8.0	component-wise	2.36e - 05	100/1000	no	N/A	0.83
83.0	1000.0	FD	5.0	8.0	component-wise	1.61e - 05	100/1000	no	N/A	0.84
83.0	1000.0	FD	0.0	8.0	constant	2.51e - 06	100/1000	no	N/A	0.89
83.0	1000.0	FD	1.0	8.0	constant	1.90e - 06	100/1000	no	N/A	0.8
83.0	1000.0	FD	2.0	8.0	constant	2.91e - 06	100/1000	no	N/A	1.01
83.0	1000.0	FD	3.0	8.0	43 component-wise	2.36e - 05	100/1000	no	N/A	0.83

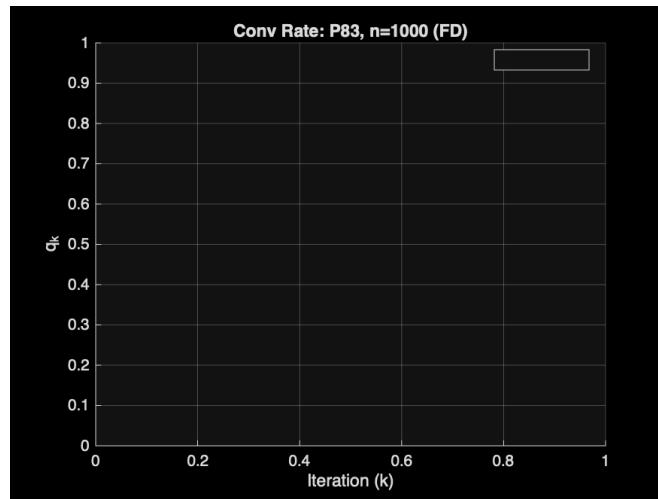


Figure 30: Problem 83, Truncated Newton, mixed FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

## 8 Results - Mixed (component-wise $h$ )

### 8.1 Problem 31

#### 8.1.1 Modified Newton

**Mixed FD (component-wise  $h$ ),  $k = 4$**

**Case  $n = 2$**

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd h prop	$\bar{x}$	4	$1.46 \times 10^{-7}$	5/1000	yes		1.97	0.0042s
			1	4	$1.55 \times 10^{-7}$	6/1000	yes		1.96	0.0009s
			2	4	$3.81 \times 10^{-9}$	6/1000	yes		1.89	0.0008s
			3	4	$2.05 \times 10^{-9}$	6/1000	yes		1.85	0.0014s
			4	4	$8.96 \times 10^{-10}$	5/1000	yes		1.79	0.0007s
			5	4	$4.23 \times 10^{-11}$	8/1000	yes		1.51	0.0010s
			<i>Avg (successes)</i>		$5.13 \times 10^{-8}$	6.0/1000	6/6		1.83	0.0015s

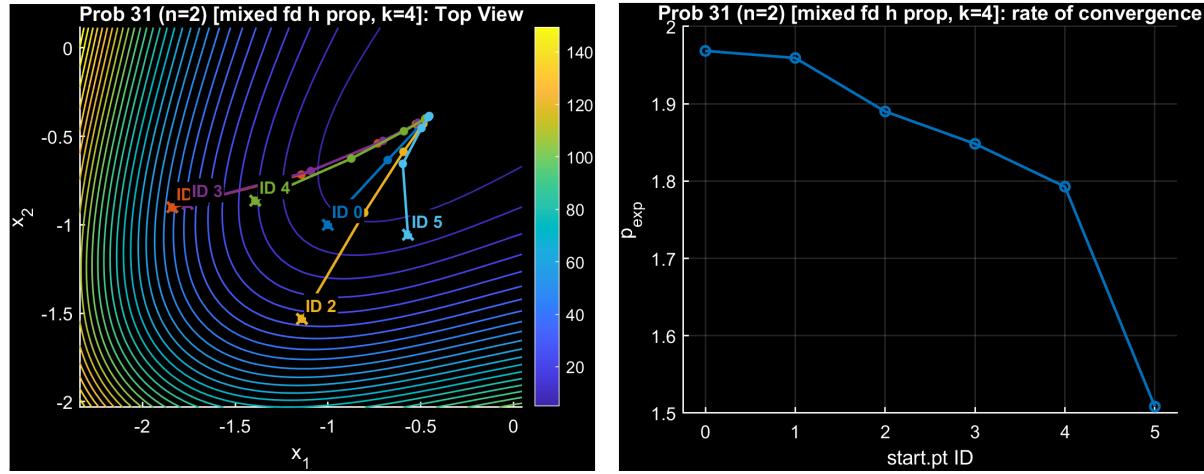


Figure 31: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $n > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd h prop	$\bar{x}$	4	$2.70 \times 10^{-8}$	5/1000	yes		1.69	0.0053s
			1	4	$9.15 \times 10^{-11}$	10/1000	yes		1.33	0.0583s
			2	4	$4.02 \times 10^{-7}$	9/1000	yes		1.91	0.0093s
			3	4	$4.01 \times 10^{-11}$	9/1000	yes		1.28	0.0107s
			4	4	$9.38 \times 10^{-7}$	8/1000	yes		1.90	0.0132s
			5	4	$1.49 \times 10^{-10}$	9/1000	yes		1.39	0.0128s
			Avg (successes)	4	$2.28 \times 10^{-7}$	8.3/1000	6/6		1.58	0.0182s

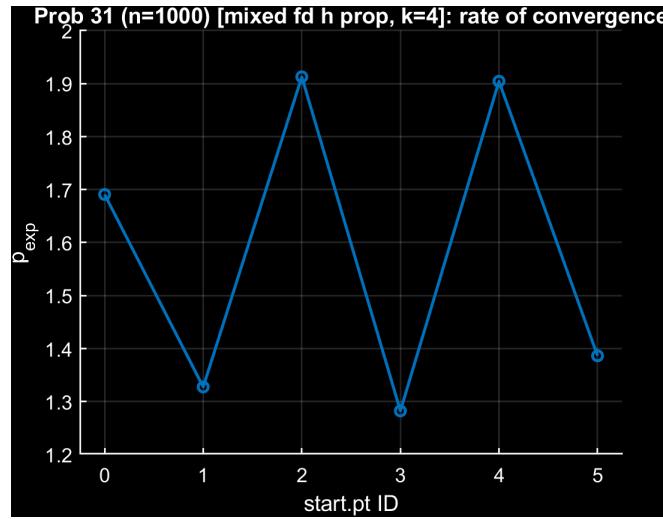


Figure 32: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd h prop	$\bar{x}$	4	$3.03 \times 10^{-8}$	5/1000	yes		1.49	0.0407s
			1	4	$4.48 \times 10^{-10}$	10/1000	yes		1.46	0.0969s
			2	4	$9.84 \times 10^{-9}$	9/1000	yes		1.75	0.0850s
			3	4	$2.64 \times 10^{-7}$	10/1000	yes		1.94	0.0935s
			4	4	$5.45 \times 10^{-7}$	8/1000	yes		1.87	0.0845s
			5	4	$6.85 \times 10^{-7}$	10/1000	yes		1.93	0.0979s
			<i>Avg (successes)</i>		4	$2.56 \times 10^{-7}$	8.7/1000	6/6	1.74	0.0831s

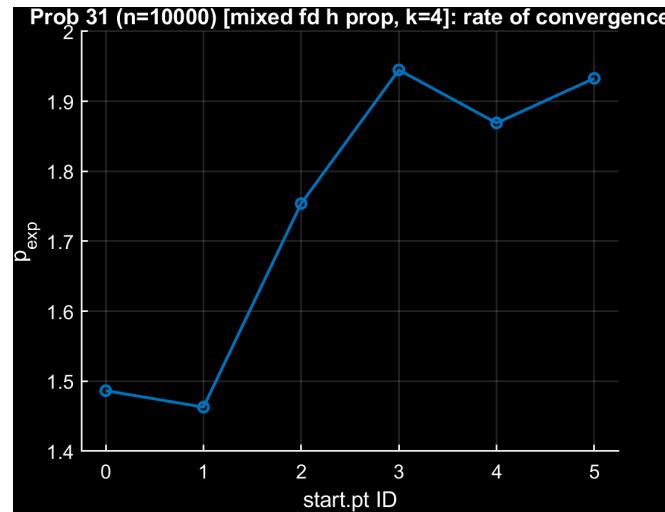


Figure 33: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd h prop	$\bar{x}$	4	$5.31 \times 10^{-8}$	5/100	yes		1.42	0.5230s
			1	4	$2.21 \times 10^{-7}$	8/100	yes		1.85	1.14s
			2	4	$5.96 \times 10^{-8}$	12/100	yes		1.90	1.54s
			3	4	$7.71 \times 10^{-10}$	10/100	yes		1.54	1.40s
			4	4	$5.39 \times 10^{-11}$	11/100	yes		1.24	1.63s
			5	4	$5.16 \times 10^{-9}$	10/100	yes		1.74	1.53s
			<i>Avg (successes)</i>		4	$5.67 \times 10^{-8}$	9.3/100	6/6	1.62	1.29s

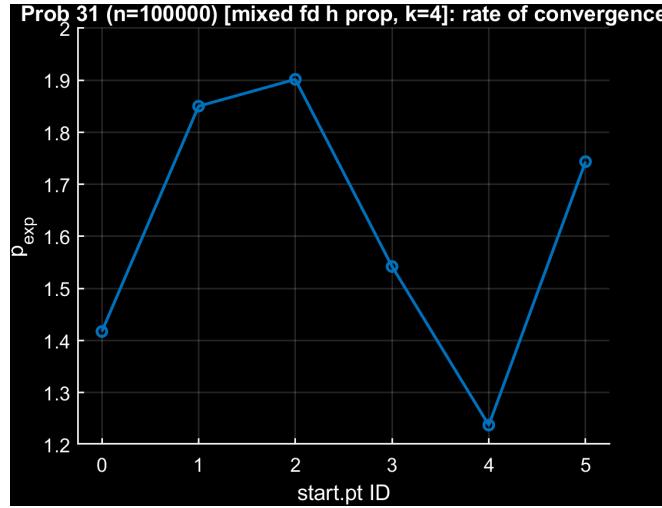


Figure 34: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

### Mixed FD (component-wise $h$ ), $k = 8$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd h prop	$\bar{x}$	8	$1.32 \times 10^{-7}$	5/1000	yes		1.99	0.0005s
			1	8	$1.40 \times 10^{-7}$	6/1000	yes		1.98	0.0008s
			2	8	$2.16 \times 10^{-9}$	6/1000	yes		1.99	0.0007s
			3	8	$8.94 \times 10^{-10}$	6/1000	yes		1.99	0.0008s
			4	8	$2.68 \times 10^{-10}$	5/1000	yes		1.99	0.0008s
			5	8	$1.05 \times 10^{-12}$	8/1000	yes		2.00	0.0009s
				Avg (successes)	8	$4.59 \times 10^{-8}$	6.0/1000	6/6	1.99	0.0008s

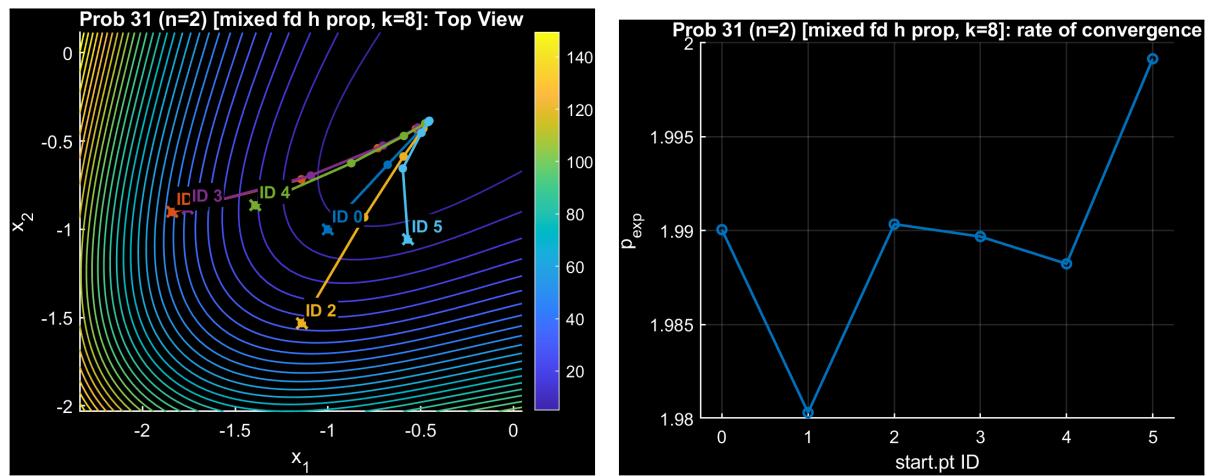


Figure 35: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd h prop	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.76	0.0053s
			1	8	$4.77 \times 10^{-13}$	10/1000	yes		1.98	0.0141s
			2	8	$3.30 \times 10^{-7}$	9/1000	yes		1.95	0.0298s
			3	8	$1.07 \times 10^{-13}$	9/1000	yes		1.98	0.0141s
			4	8	$8.28 \times 10^{-7}$	8/1000	yes		1.93	0.0119s
			5	8	$1.44 \times 10^{-12}$	9/1000	yes		1.99	0.0149s
			<i>Avg (successes)</i>		8	$1.96 \times 10^{-7}$	8.3/1000	6/6	1.93	0.0150s

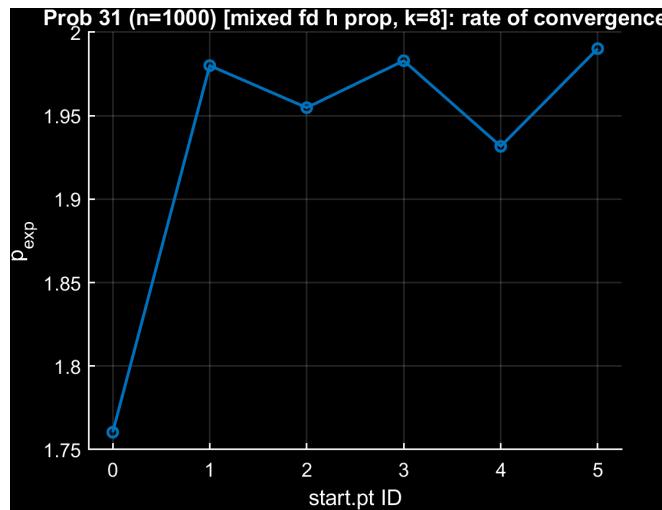


Figure 36: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd h prop	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.56	0.0384s
			1	8	$9.49 \times 10^{-12}$	10/1000	yes		2.00	0.0912s
			2	8	$3.12 \times 10^{-9}$	9/1000	yes		1.95	0.0961s
			3	8	$2.15 \times 10^{-7}$	10/1000	yes		1.99	0.0964s
			4	8	$4.62 \times 10^{-7}$	8/1000	yes		1.90	0.0708s
			5	8	$5.96 \times 10^{-7}$	10/1000	yes		1.96	0.0930s
			<i>Avg (successes)</i>		8	$2.16 \times 10^{-7}$	8.7/1000	6/6	1.89	0.0810s

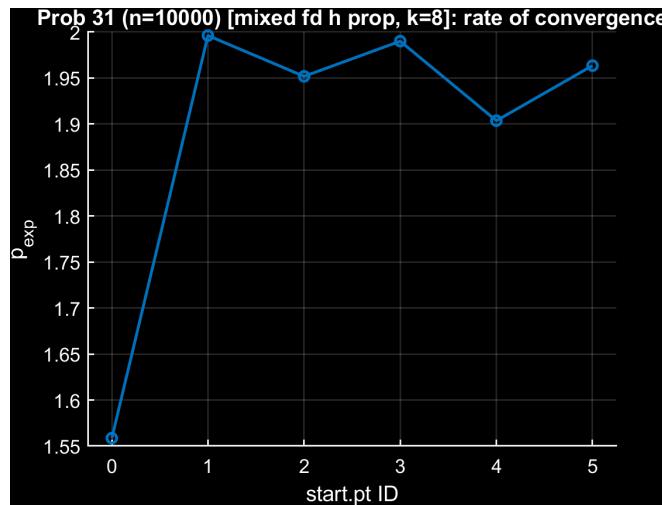


Figure 37: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd h prop	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/100	yes		1.56	0.7282s
			1	8	$1.73 \times 10^{-7}$	8/100	yes		1.90	1.79s
			2	8	$3.80 \times 10^{-8}$	12/100	yes		1.99	1.73s
			3	8	$3.45 \times 10^{-11}$	10/100	yes		2.00	1.70s
			4	8	$1.12 \times 10^{-13}$	11/100	yes		1.94	2.10s
			5	8	$1.23 \times 10^{-9}$	10/100	yes		2.00	1.57s
			Avg (successes)	8	$3.84 \times 10^{-8}$	9.3/100	6/6		1.90	1.60s

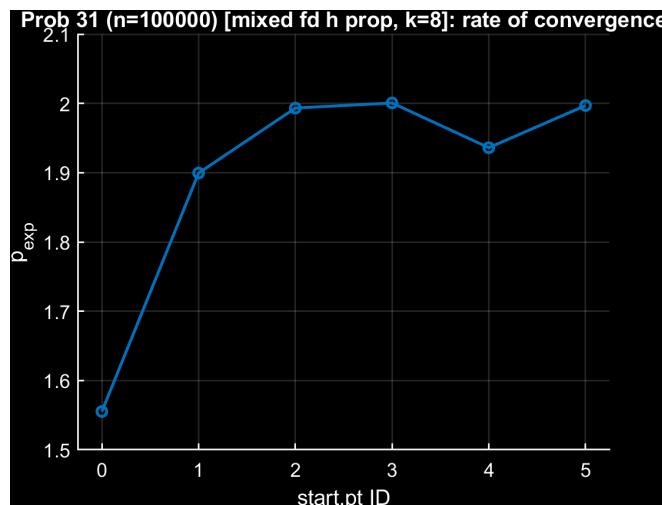


Figure 38: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

**Mixed FD (component-wise  $h$ ),  $k = 12$** **Case  $n = 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	mixed fd h prop	$\bar{x}$	12	$1.32 \times 10^{-7}$	5/1000	yes		1.99	0.0005s
			1	12	$1.40 \times 10^{-7}$	6/1000	yes		1.98	0.0008s
			2	12	$2.16 \times 10^{-9}$	6/1000	yes		1.99	0.0007s
			3	12	$8.94 \times 10^{-10}$	6/1000	yes		1.99	0.0007s
			4	12	$2.67 \times 10^{-10}$	5/1000	yes		1.99	0.0008s
			5	12	$1.04 \times 10^{-12}$	8/1000	yes		2.00	0.0009s
			<i>Avg (successes)</i>	12	$4.59 \times 10^{-8}$	6.0/1000	6/6		1.99	0.0008s

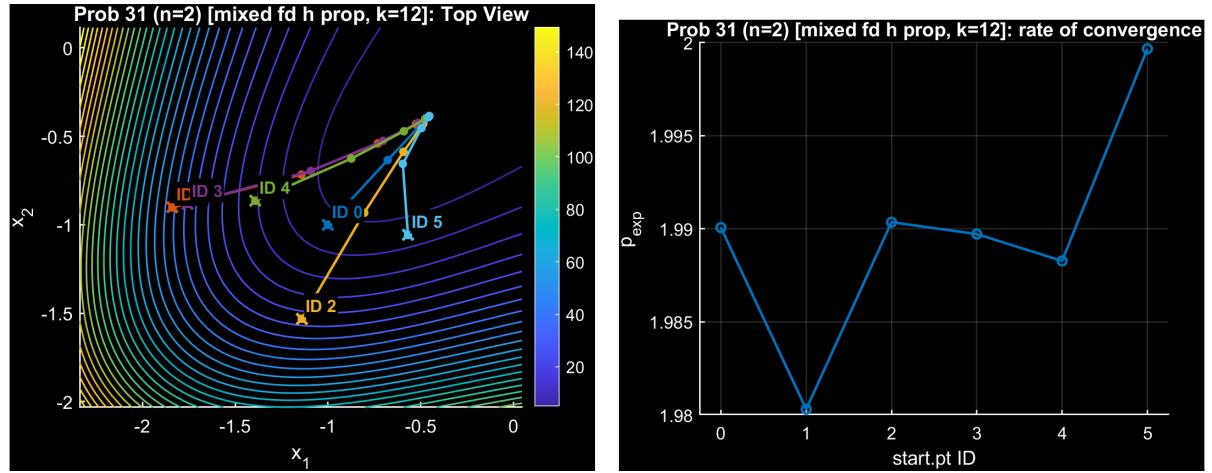


Figure 39: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	mixed fd h prop	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/1000	yes		1.76	0.0086s
			1	12	$4.69 \times 10^{-13}$	10/1000	yes		1.98	0.0115s
			2	12	$3.30 \times 10^{-7}$	9/1000	yes		1.95	0.0101s
			3	12	$1.08 \times 10^{-13}$	9/1000	yes		1.98	0.0102s
			4	12	$8.28 \times 10^{-7}$	8/1000	yes		1.93	0.0091s
			5	12	$1.43 \times 10^{-12}$	9/1000	yes		1.99	0.0101s
			<i>Avg (successes)</i>	12	$1.96 \times 10^{-7}$	8.3/1000	6/6		1.93	0.0099s

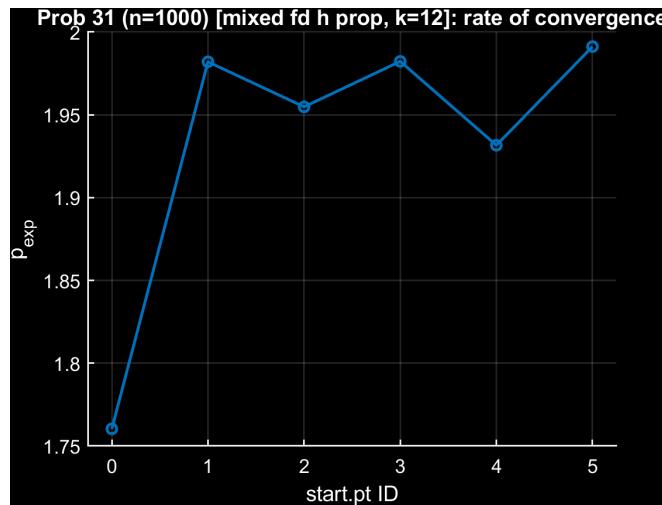


Figure 40: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	mixed fd h prop	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/1000	yes		1.56	0.0407s
			1	12	$9.45 \times 10^{-12}$	10/1000	yes		2.00	0.0851s
			2	12	$3.12 \times 10^{-9}$	9/1000	yes		1.95	0.0805s
			3	12	$2.15 \times 10^{-7}$	10/1000	yes		1.99	0.1016s
			4	12	$4.62 \times 10^{-7}$	8/1000	yes		1.90	0.0726s
			5	12	$5.96 \times 10^{-7}$	10/1000	yes		1.96	0.0850s
			Avg (successes)	12	$2.16 \times 10^{-7}$	8.7/1000	6/6		1.89	0.0776s

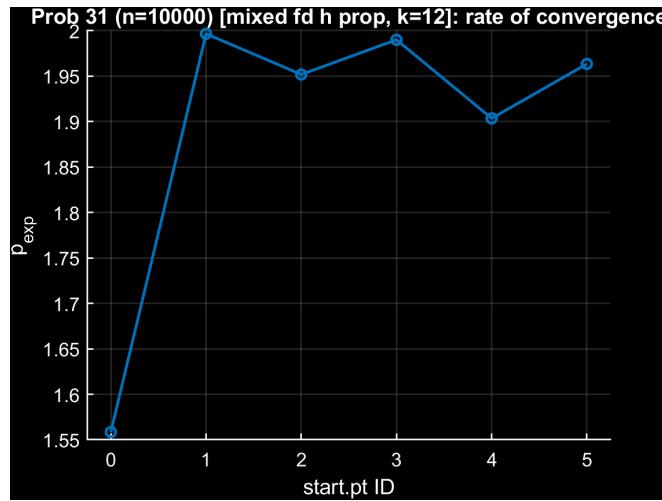


Figure 41: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	mixed fd h prop	$\bar{x}$	12	$1.79 \times 10^{-8}$	5/100	yes		1.56	0.6381s
			1	12	$1.73 \times 10^{-7}$	8/100	yes		1.90	1.60s
			2	12	$3.80 \times 10^{-8}$	12/100	yes		1.99	1.72s
			3	12	$3.45 \times 10^{-11}$	10/100	yes		2.00	1.45s
			4	12	$1.08 \times 10^{-13}$	11/100	yes		1.94	1.77s
			5	12	$1.23 \times 10^{-9}$	10/100	yes		2.00	1.51s
			<i>Avg (successes)</i>		12	$3.84 \times 10^{-8}$	9.3/100	6/6	1.90	1.45s

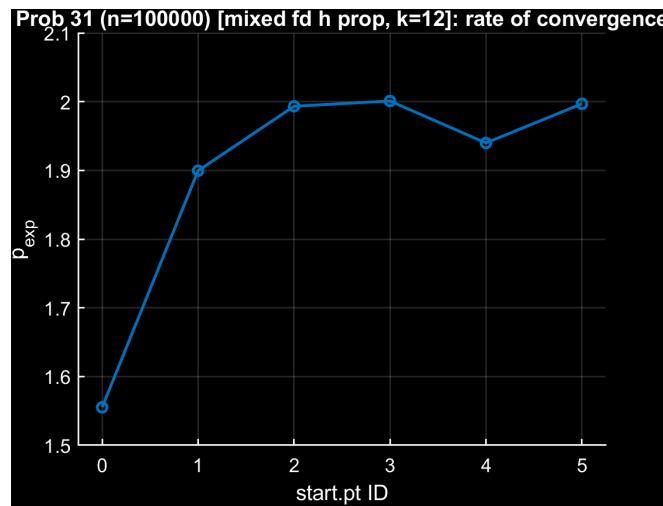


Figure 42: Problem 31, Modified Newton, mixed FD (component-wise  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).



### 8.1.2 Truncated Newton

**Mixed FD (component-wise  $h$ ),  $k = 4$**

Table 9: Results for Problem 31.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD	0.0	12.0	component-wise	$1.94e - 09$	6/1000	yes	2.0	0.0
31.0	2.0	FD	1.0	12.0	component-wise	$4.55e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	component-wise	$1.44e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	component-wise	$9.11e - 07$	5/1000	yes	1.06	0.0
31.0	2.0	FD	4.0	12.0	component-wise	$3.55e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	component-wise	$5.15e - 10$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	12.0	constant	$1.53e - 09$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	12.0	constant	$4.40e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	constant	$2.13e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	constant	$7.02e - 09$	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	12.0	constant	$1.87e - 08$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	constant	$3.80e - 10$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	4.0	component-wise	$6.17e - 11$	6/1000	yes	2.02	0.1
31.0	2.0	FD	1.0	4.0	component-wise	$9.55e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	4.0	component-wise	$2.17e - 07$	7/1000	yes	2.26	0.1
31.0	2.0	FD	3.0	4.0	component-wise	$1.62e - 12$	4/1000	yes	1.58	0.1
31.0	2.0	FD	4.0	4.0	component-wise	$8.97e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	5.0	4.0	component-wise	$4.42e - 12$	7/1000	yes	2.02	0.1
31.0	2.0	FD	0.0	4.0	constant	$6.18e - 11$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	4.0	constant	$9.56e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	4.0	constant	$2.18e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	4.0	constant	$1.15e - 12$	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	4.0	constant	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	4.0	constant	$4.45e - 12$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	component-wise	$6.18e - 11$	6/1000	yes	2.02	0.07
31.0	2.0	FD	1.0	8.0	component-wise	$9.55e - 09$	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	8.0	component-wise	$2.17e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	component-wise	$2.98e - 12$	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	8.0	component-wise	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	component-wise	$4.39e - 12$	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	constant	$6.17e - 11$	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	8.0	constant	$9.55e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	8.0	constant	$2.18e - 07$	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	constant	$1.15e - 12$	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	8.0	constant	$8.97e - 09$	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	constant	$4.45e - 12$	7/1000	yes	2.02	0.0
31.0	1000.0	FD	0.0	12.0	component-wise	$1.61e - 07$	11/1000	yes	2.27	0.01
31.0	1000.0	FD	1.0	12.0	component-wise	$2.40e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	12.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	component-wise	$8.53e - 08$	14/1000	yes	1.4	0.02
31.0	1000.0	FD	5.0	12.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	12.0	constant	$1.60e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	12.0	constant	$2.40e - 09$	14/1000	yes	1.59	0.01
31.0	1000.0	FD	2.0	12.0	constant	$3.42e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	constant	$8.54e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	12.0	constant	$1.23e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	$8.52e - 08$	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	$1.22e - 09$	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	$1.61e - 07$	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	$2.39e - 09$	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	component-wise	$3.41e - 07$	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	$3.81e - 07$	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	$8.52e - 08$	14/1000	yes	1.4	

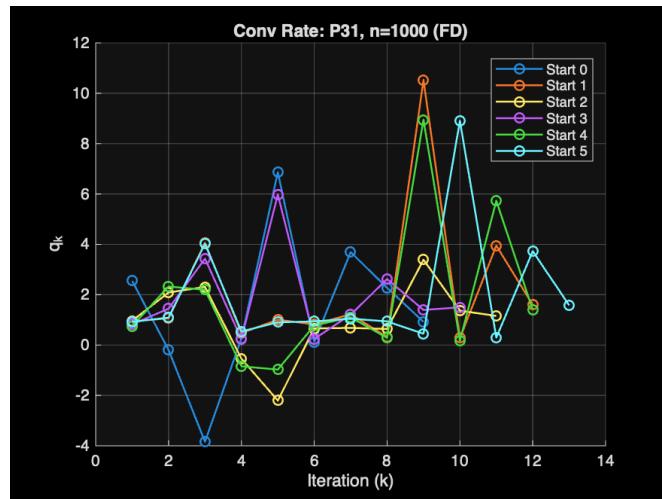


Figure 43: Problem 31, Truncated Newton, mixed FD (component-wise  $h$ ,  $k = 4$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Mixed FD (component-wise  $h$ ),  $k = 8$** 

Table 10: Results for Problem 31.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD	0.0	12.0	component-wise	1.94e-09	6/1000	yes	2.0	0.0
31.0	2.0	FD	1.0	12.0	component-wise	4.55e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	component-wise	1.44e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	component-wise	9.11e-07	5/1000	yes	1.06	0.0
31.0	2.0	FD	4.0	12.0	component-wise	3.55e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	component-wise	5.15e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	12.0	constant	1.53e-09	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	12.0	constant	4.40e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	constant	2.13e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	constant	7.02e-09	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	12.0	constant	1.87e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	constant	3.80e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	4.0	component-wise	6.17e-11	6/1000	yes	2.02	0.1
31.0	2.0	FD	1.0	4.0	component-wise	9.55e-09	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	4.0	component-wise	2.17e-07	7/1000	yes	2.26	0.1
31.0	2.0	FD	3.0	4.0	component-wise	1.62e-12	4/1000	yes	1.58	0.1
31.0	2.0	FD	4.0	4.0	component-wise	8.97e-09	7/1000	yes	2.0	0.1
31.0	2.0	FD	5.0	4.0	component-wise	4.42e-12	7/1000	yes	2.02	0.1
31.0	2.0	FD	0.0	4.0	constant	6.18e-11	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	4.0	constant	9.56e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	4.0	constant	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	4.0	constant	1.15e-12	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	4.0	constant	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	4.0	constant	4.45e-12	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	component-wise	6.18e-11	6/1000	yes	2.02	0.07
31.0	2.0	FD	1.0	8.0	component-wise	9.55e-09	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	8.0	component-wise	2.17e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	component-wise	2.98e-12	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	8.0	component-wise	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	component-wise	4.39e-12	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	constant	6.17e-11	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	8.0	constant	9.55e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	8.0	constant	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	constant	1.15e-12	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	8.0	constant	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	constant	4.45e-12	7/1000	yes	2.02	0.0
31.0	1000.0	FD	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.27	0.01
31.0	1000.0	FD	1.0	12.0	component-wise	2.40e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	12.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	component-wise	8.53e-08	14/1000	yes	1.4	0.02
31.0	1000.0	FD	5.0	12.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	12.0	constant	1.60e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	12.0	constant	2.40e-09	14/1000	yes	1.59	0.01
31.0	1000.0	FD	2.0	12.0	constant	3.42e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	constant	8.54e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	12.0	constant	1.23e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	component-wise	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	constant	1.60e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	constant	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	constant	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	constant	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	constant	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0</						

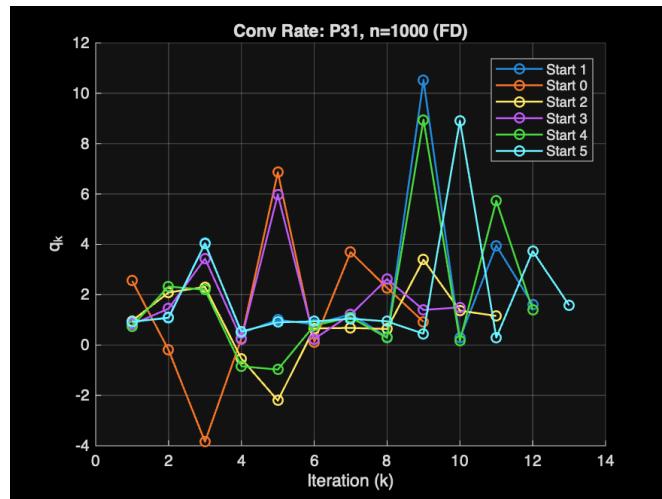


Figure 44: Problem 31, Truncated Newton, mixed FD (component-wise  $h$ ,  $k = 8$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Mixed FD (component-wise  $h$ ),  $k = 12$** 

Table 11: Results for Problem 31.0 - FD

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD	0.0	12.0	component-wise	1.94e - 09	6/1000	yes	2.0	0.0
31.0	2.0	FD	1.0	12.0	component-wise	4.55e - 08	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	component-wise	1.44e - 07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	component-wise	9.11e - 07	5/1000	yes	1.06	0.0
31.0	2.0	FD	4.0	12.0	component-wise	3.55e - 08	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	component-wise	5.15e - 10	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	12.0	constant	1.53e - 09	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	12.0	constant	4.40e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	12.0	constant	2.13e - 07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	12.0	constant	7.02e - 09	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	12.0	constant	1.87e - 08	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	12.0	constant	3.80e - 10	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	4.0	component-wise	6.17e - 11	6/1000	yes	2.02	0.1
31.0	2.0	FD	1.0	4.0	component-wise	9.55e - 09	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	4.0	component-wise	2.17e - 07	7/1000	yes	2.26	0.1
31.0	2.0	FD	3.0	4.0	component-wise	1.62e - 12	4/1000	yes	1.58	0.1
31.0	2.0	FD	4.0	4.0	component-wise	8.97e - 09	7/1000	yes	2.0	0.1
31.0	2.0	FD	5.0	4.0	component-wise	4.42e - 12	7/1000	yes	2.02	0.1
31.0	2.0	FD	0.0	4.0	constant	6.18e - 11	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	4.0	constant	9.56e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	4.0	constant	2.18e - 07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	4.0	constant	1.15e - 12	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	4.0	constant	8.97e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	4.0	constant	4.45e - 12	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	component-wise	6.18e - 11	6/1000	yes	2.02	0.07
31.0	2.0	FD	1.0	8.0	component-wise	9.55e - 09	7/1000	yes	2.0	0.1
31.0	2.0	FD	2.0	8.0	component-wise	2.17e - 07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	component-wise	2.98e - 12	4/1000	yes	1.58	0.0
31.0	2.0	FD	4.0	8.0	component-wise	8.97e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	component-wise	4.39e - 12	7/1000	yes	2.02	0.0
31.0	2.0	FD	0.0	8.0	constant	6.17e - 11	6/1000	yes	2.02	0.0
31.0	2.0	FD	1.0	8.0	constant	9.55e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	2.0	8.0	constant	2.18e - 07	7/1000	yes	2.26	0.0
31.0	2.0	FD	3.0	8.0	constant	1.15e - 12	4/1000	yes	1.59	0.0
31.0	2.0	FD	4.0	8.0	constant	8.97e - 09	7/1000	yes	2.0	0.0
31.0	2.0	FD	5.0	8.0	constant	4.45e - 12	7/1000	yes	2.02	0.0
31.0	1000.0	FD	0.0	12.0	component-wise	1.61e - 07	11/1000	yes	2.27	0.01
31.0	1000.0	FD	1.0	12.0	component-wise	2.40e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	12.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	component-wise	8.53e - 08	14/1000	yes	1.4	0.02
31.0	1000.0	FD	5.0	12.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	12.0	constant	1.60e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	12.0	constant	2.40e - 09	14/1000	yes	1.59	0.01
31.0	1000.0	FD	2.0	12.0	constant	3.42e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	12.0	constant	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	12.0	constant	8.54e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	12.0	constant	1.23e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	component-wise	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	component-wise	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	component-wise	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	4.0	constant	1.60e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	4.0	constant	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	4.0	constant	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	4.0	constant	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	4.0	constant	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	4.0	constant	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e - 09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e - 09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e - 09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	constant	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	constant	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	constant	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	component-wise	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	component-wise	2.39e - 09	14/1000	yes	1.6	0.02
31.0	1000.0	FD	2.0	8.0	component-wise	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0	8.0	component-wise	3.81e - 07	12/1000	yes	1.39	0.01
31.0	1000.0	FD	4.0	8.0	component-wise	8.52e - 08	14/1000	yes	1.4	0.01
31.0	1000.0	FD	5.0	8.0	component-wise	1.22e - 09	15/1000	yes	1.58	0.01
31.0	1000.0	FD	0.0	8.0	constant	1.61e - 07	11/1000	yes	2.28	0.01
31.0	1000.0	FD	1.0	8.0	constant	2.39e - 09	14/1000	yes	1.6	0.01
31.0	1000.0	FD	2.0	8.0	constant	3.41e - 07	13/1000	yes	1.16	0.01
31.0	1000.0	FD	3.0							

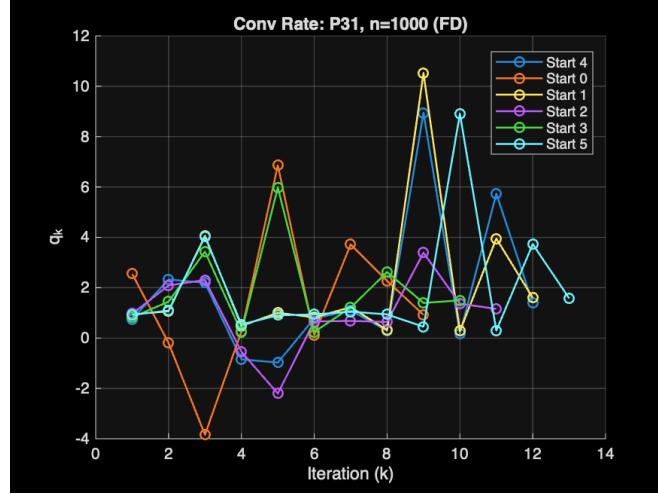


Figure 45: Problem 31, Truncated Newton, mixed FD (component-wise  $h$ ,  $k = 12$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

## 8.2 Problem 83

### 8.2.1 Modified Newton

Mixed FD (component-wise  $h$ ),  $k = 4$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd h prop	$\bar{x}$	4	$9.20 \times 10^{-10}$	3/1000	yes		1.90	0.0172s
			1	4	$4.53 \times 10^{-10}$	3/1000	yes		2.05	0.0150s
			2	4	$4.27 \times 10^{-7}$	3/1000	yes		1.94	0.0140s
			3	4	$2.03 \times 10^{-9}$	3/1000	yes		2.00	0.0135s
			4	4	$8.07 \times 10^{-8}$	3/1000	yes		2.01	0.0142s
			5	4	$1.03 \times 10^{-12}$	4/1000	yes		1.42	0.0171s
			Avg (successes)	4	$8.52 \times 10^{-8}$	3.2/1000	6/6		1.89	0.0152s

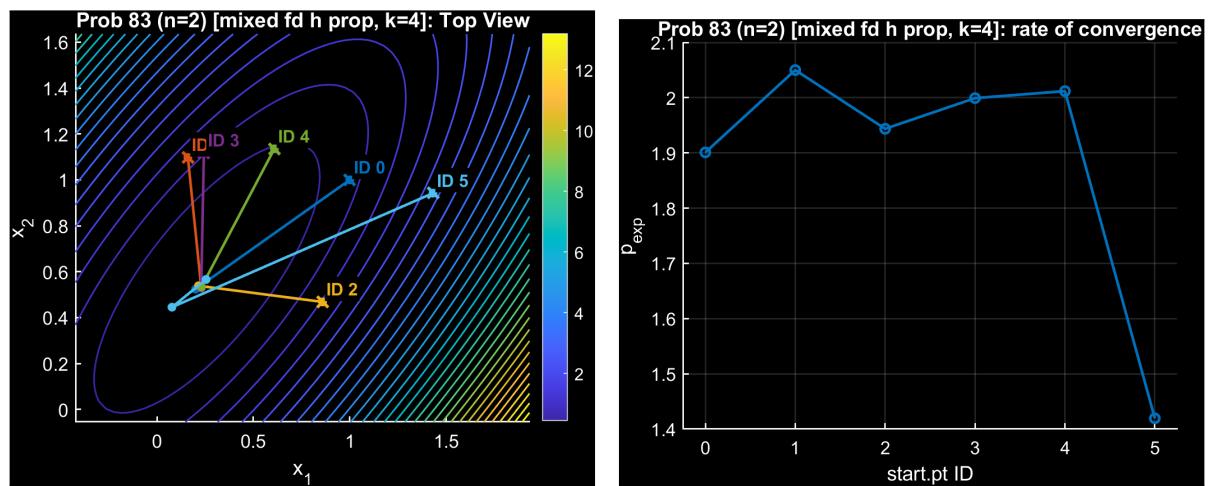


Figure 46: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $N > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	mixed fd h prop	$\bar{x}$	4	$1.68 \times 10^{-10}$	2/1000	yes		NaN	0.0139s
			1	4	$3.54 \times 10^{-8}$	2/1000	yes		NaN	0.0143s
			2	4	$2.03 \times 10^{-8}$	2/1000	yes		NaN	0.0145s
			3	4	$2.52 \times 10^{-8}$	2/1000	yes		NaN	0.0153s
			4	4	$1.44 \times 10^{-8}$	2/1000	yes		NaN	0.0148s
			5	4	$1.35 \times 10^{-8}$	2/1000	yes		NaN	0.0143s
			<i>Avg (successes)</i>	4	$1.82 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0145s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	mixed fd h prop	$\bar{x}$	4	$1.42 \times 10^{-8}$	1/1000	yes		NaN	0.0160s
			1	4	$4.58 \times 10^{-8}$	2/1000	yes		NaN	0.0366s
			2	4	$3.89 \times 10^{-8}$	2/1000	yes		NaN	0.0343s
			3	4	$2.67 \times 10^{-8}$	2/1000	yes		NaN	0.0333s
			4	4	$3.20 \times 10^{-8}$	2/1000	yes		NaN	0.0356s
			5	4	$3.15 \times 10^{-8}$	2/1000	yes		NaN	0.0337s
			<i>Avg (successes)</i>	4	$3.15 \times 10^{-8}$	1.8/1000	6/6		NaN	0.0316s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	mixed fd h prop	$\bar{x}$	4	$9.67 \times 10^{-9}$	1/100	yes		NaN	0.1614s
			1	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1675s
			2	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1637s
			3	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1637s
			4	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1689s
			5	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.1631s
			<i>Avg (successes)</i>	4	$1.41 \times 10^{-7}$	1.0/100	6/6		NaN	0.1647s

**Mixed FD (component-wise  $h$ ),  $k = 8$** **Case  $n = 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd h prop	$\bar{x}$	8	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0120s
			1	8	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0146s
			2	8	$4.34 \times 10^{-7}$	3/1000	yes		1.94	0.0135s
			3	8	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0146s
			4	8	$8.39 \times 10^{-8}$	3/1000	yes		2.00	0.0146s
			5	8	$9.22 \times 10^{-15}$	4/1000	yes		1.90	0.0169s
			<i>Avg (successes)</i>	8	$8.71 \times 10^{-8}$	3.2/1000	6/6		1.94	0.0144s

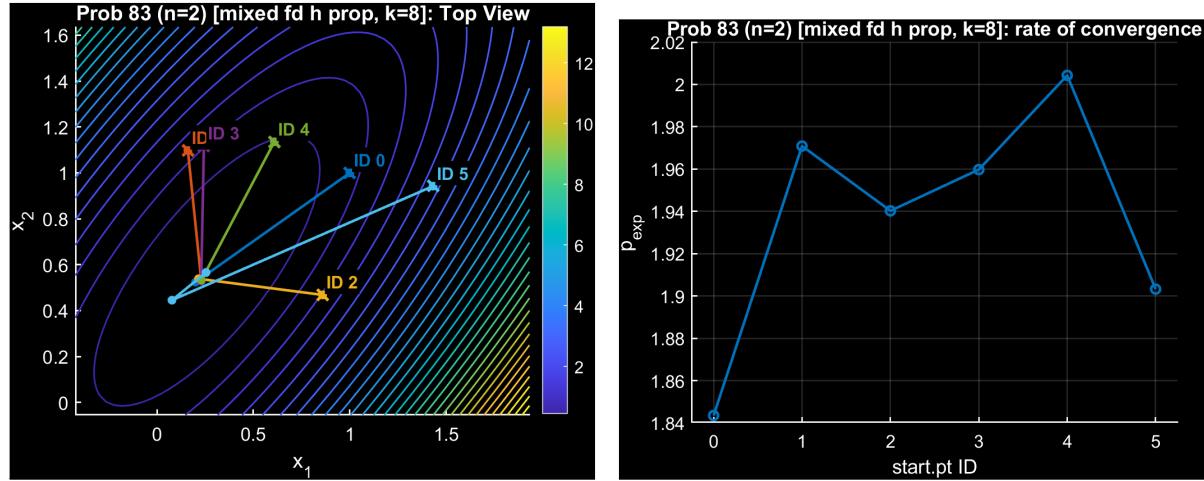


Figure 47: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $n > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	mixed fd h prop	$\bar{x}$	8	$3.19 \times 10^{-12}$	2/1000	yes		NaN	0.0126s
			1	8	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0157s
			2	8	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0131s
			3	8	$2.80 \times 10^{-8}$	2/1000	yes		NaN	0.0142s
			4	8	$2.94 \times 10^{-8}$	2/1000	yes		NaN	0.0136s
			5	8	$2.36 \times 10^{-8}$	2/1000	yes		NaN	0.0146s
			Avg (successes)	8	$2.19 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0140s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	mixed fd h prop	$\bar{x}$	8	$1.14 \times 10^{-8}$	1/1000	yes		NaN	0.0151s
			1	8	$4.64 \times 10^{-8}$	2/1000	yes		NaN	0.0378s
			2	8	$3.94 \times 10^{-8}$	2/1000	yes		NaN	0.0336s
			3	8	$2.75 \times 10^{-8}$	2/1000	yes		NaN	0.0372s
			4	8	$9.42 \times 10^{-10}$	2/1000	yes		NaN	0.0331s
			5	8	$6.53 \times 10^{-10}$	2/1000	yes		NaN	0.0336s
			Avg (successes)	8	$2.11 \times 10^{-8}$	1.8/1000	6/6		NaN	0.0317s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	mixed fd h prop	$\bar{x}$	8	$1.17 \times 10^{-10}$	1/100	yes		NaN	0.1458s
			1	8	$2.48 \times 10^{-7}$	1/100	yes		NaN	0.1649s
			2	8	$2.10 \times 10^{-7}$	1/100	yes		NaN	0.1728s
			3	8	$7.93 \times 10^{-10}$	2/100	yes		NaN	0.3251s
			4	8	$1.59 \times 10^{-9}$	2/100	yes		NaN	0.2990s
			5	8	$2.11 \times 10^{-7}$	1/100	yes		NaN	0.1681s
			Avg (successes)	8	$1.12 \times 10^{-7}$	1.3/100	6/6		NaN	0.2126s

**Mixed FD (component-wise  $h$ ),  $k = 12$** **Case  $n = 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	mixed fd h prop	$\bar{x}$	12	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0123s
			1	12	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0144s
			2	12	$4.34 \times 10^{-7}$	3/1000	yes		1.94	0.0159s
			3	12	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0144s
			4	12	$8.39 \times 10^{-8}$	3/1000	yes		2.00	0.0141s
			5	12	$9.37 \times 10^{-15}$	4/1000	yes		1.90	0.0180s
			Avg (successes)	12	$8.71 \times 10^{-8}$	3.2/1000	6/6		1.94	0.0148s

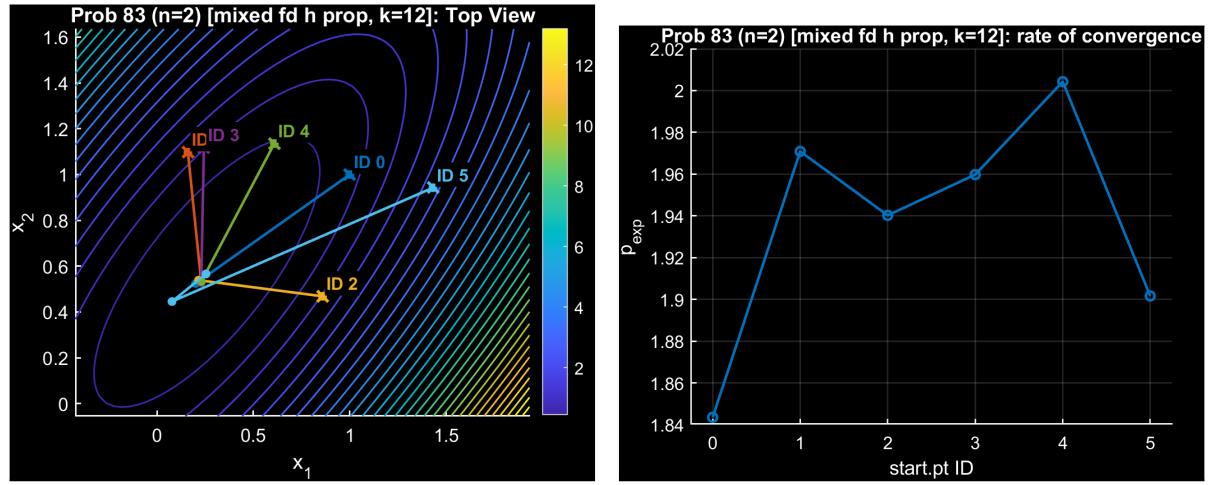


Figure 48: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $n > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	mixed fd h prop	$\bar{x}$	12	$3.02 \times 10^{-10}$	2/1000	yes		NaN	0.0112s
			1	12	$2.92 \times 10^{-8}$	2/1000	yes		NaN	0.0144s
			2	12	$2.98 \times 10^{-8}$	2/1000	yes		NaN	0.0149s
			3	12	$3.18 \times 10^{-8}$	2/1000	yes		NaN	0.0176s
			4	12	$3.36 \times 10^{-8}$	2/1000	yes		NaN	0.0147s
			5	12	$3.01 \times 10^{-8}$	2/1000	yes		NaN	0.0144s
			Avg (successes)	12	$2.58 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0146s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	mixed fd h prop	$\bar{x}$	12	$1.13 \times 10^{-8}$	1/1000	yes		NaN	0.0153s
			1	12	$8.14 \times 10^{-8}$	2/1000	yes		NaN	0.0359s
			2	12	$8.88 \times 10^{-9}$	2/1000	yes		NaN	0.0311s
			3	12	$3.68 \times 10^{-8}$	2/1000	yes		NaN	0.0357s
			4	12	$1.70 \times 10^{-8}$	2/1000	yes		NaN	0.0317s
			5	12	$1.23 \times 10^{-7}$	2/1000	yes		NaN	0.0334s
			Avg (successes)	12	$4.65 \times 10^{-8}$	1.8/1000	6/6		NaN	0.0305s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	100000	mixed fd h prop	$\bar{x}$	12	$3.23 \times 10^{-10}$	1/100	yes		NaN	0.1602s	
			1	12	$7.28 \times 10^{-8}$	2/100	yes		NaN	0.4280s	
			2	12	$2.66 \times 10^{-8}$	2/100	yes		NaN	0.3932s	
			3	12	$1.53 \times 10^{-8}$	2/100	yes		NaN	0.4486s	
			4	12	$1.64 \times 10^{-8}$	2/100	yes		NaN	0.5788s	
			5	12	$8.69 \times 10^{-8}$	2/100	yes		NaN	0.4401s	
			<i>Avg (successes)</i>		12	$3.64 \times 10^{-8}$	1.8/100	6/6		NaN	0.4081s

### 8.2.2 Truncated Newton

## 9 Results - Full FD (constant $h$ )

### 9.1 Problem 31

#### 9.1.1 Modified Newton

Full FD (constant  $h$ ),  $k = 4$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	full fd	$\bar{x}$	4	$1.73 \times 10^{-7}$	5/1000	yes		1.93	0.0066s
			1	4	$1.78 \times 10^{-7}$	6/1000	yes		1.93	0.0008s
			2	4	$7.12 \times 10^{-9}$	6/1000	yes		1.78	0.0009s
			3	4	$3.99 \times 10^{-9}$	6/1000	yes		1.74	0.0007s
			4	4	$1.95 \times 10^{-9}$	5/1000	yes		1.67	0.0007s
			5	4	$1.20 \times 10^{-10}$	8/1000	yes		1.38	0.0011s
			<i>Avg (successes)</i>	4	$6.06 \times 10^{-8}$	6.0/1000	6/6		1.74	0.0018s

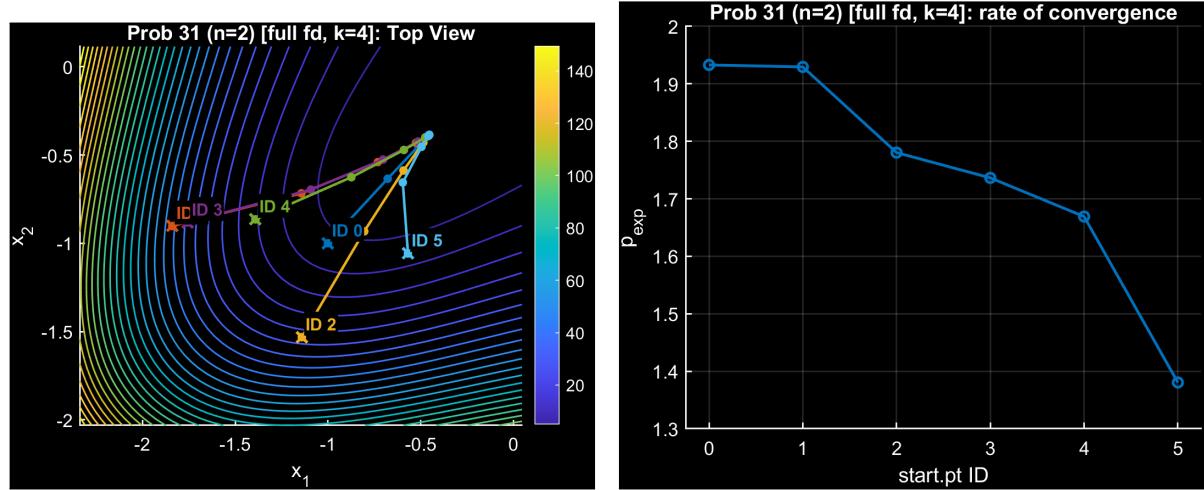


Figure 49: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

Case  $N > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	full fd	$\bar{x}$	4	$3.39 \times 10^{-8}$	5/1000	yes		1.65	0.0800s
			1	4	$8.94 \times 10^{-11}$	10/1000	yes		1.33	0.1612s
			2	4	$3.95 \times 10^{-7}$	9/1000	yes		1.91	0.1535s
			3	4	$4.01 \times 10^{-11}$	9/1000	yes		1.28	0.1548s
			4	4	$9.29 \times 10^{-7}$	8/1000	yes		1.90	0.1424s
			5	4	$1.48 \times 10^{-10}$	9/1000	yes		1.39	0.1430s
			<i>Avg (successes)</i>	4	$2.26 \times 10^{-7}$	8.3/1000	6/6		1.58	0.1392s

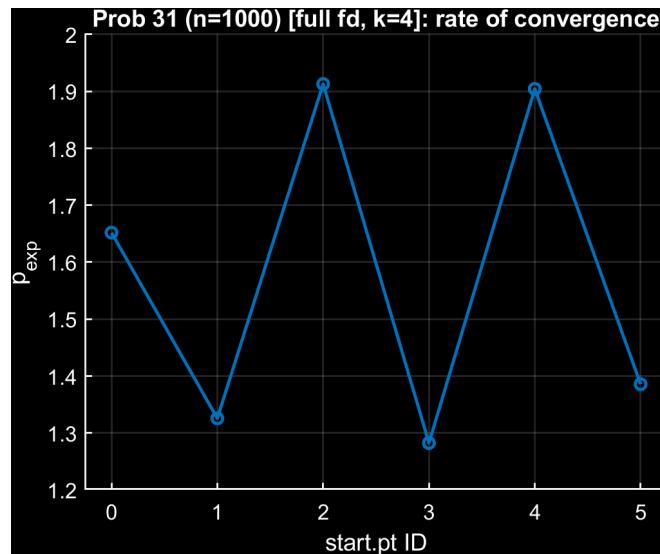


Figure 50: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	full fd	$\bar{x}$	4	$3.66 \times 10^{-8}$	5/1000	yes		1.46	0.9511s
			1	4	$4.34 \times 10^{-10}$	10/1000	yes		1.46	2.50s
			2	4	$9.71 \times 10^{-9}$	9/1000	yes		1.75	1.56s
			3	4	$2.40 \times 10^{-7}$	10/1000	yes		1.94	1.44s
			4	4	$5.41 \times 10^{-7}$	8/1000	yes		1.87	1.13s
			5	4	$6.67 \times 10^{-7}$	10/1000	yes		1.93	1.41s
			<i>Avg (successes)</i>	4	$2.49 \times 10^{-7}$	8.7/1000	6/6		1.74	1.50s

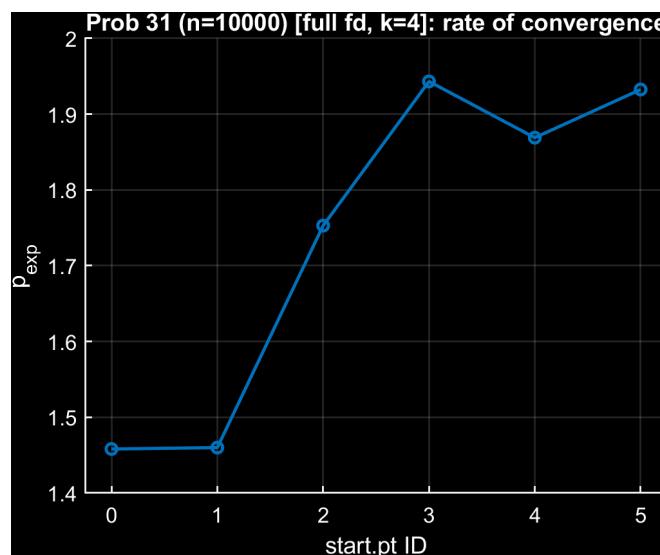


Figure 51: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	full fd	$\bar{x}$	4	$5.69 \times 10^{-8}$	5/100	yes		1.41	7.05s
			1	4	$2.22 \times 10^{-7}$	8/100	yes		1.85	11.40s
			2	4	$5.06 \times 10^{-8}$	12/100	yes		1.90	16.74s
			3	4	$7.71 \times 10^{-10}$	10/100	yes		1.54	14.08s
			4	4	$5.39 \times 10^{-11}$	11/100	yes		1.24	15.54s
			5	4	$1.06 \times 10^{-7}$	12/100	yes		1.90	16.89s
			Avg (successes)	4	$7.26 \times 10^{-8}$	9.7/100	6/6		1.64	13.62s

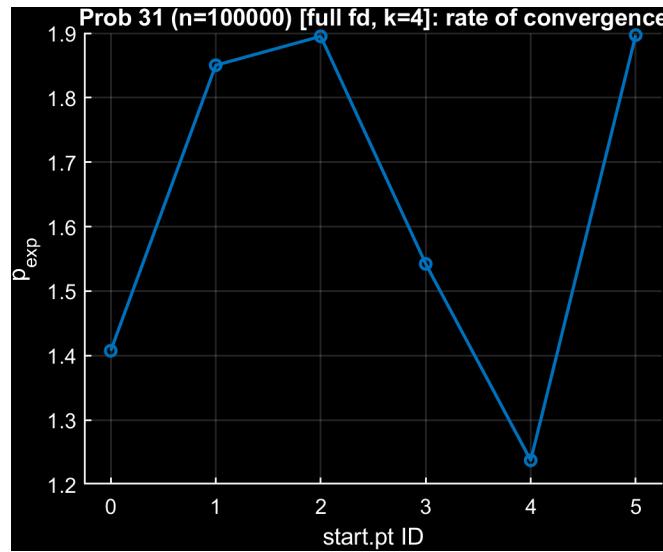


Figure 52: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

**Full FD (constant  $h$ ),  $k = 8$**

**Case  $n = 2$**

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	2	full fd	$\bar{x}$	8	$1.32 \times 10^{-7}$	5/1000	yes		1.99	0.0006s
			1	8	$1.40 \times 10^{-7}$	6/1000	yes		1.98	0.0010s
			2	8	$2.16 \times 10^{-9}$	6/1000	yes		1.99	0.0009s
			3	8	$8.95 \times 10^{-10}$	6/1000	yes		1.99	0.0008s
			4	8	$2.68 \times 10^{-10}$	5/1000	yes		1.99	0.0006s
			5	8	$1.06 \times 10^{-12}$	8/1000	yes		2.00	0.0008s
			Avg (successes)	8	$4.59 \times 10^{-8}$	6.0/1000	6/6		1.99	0.0008s

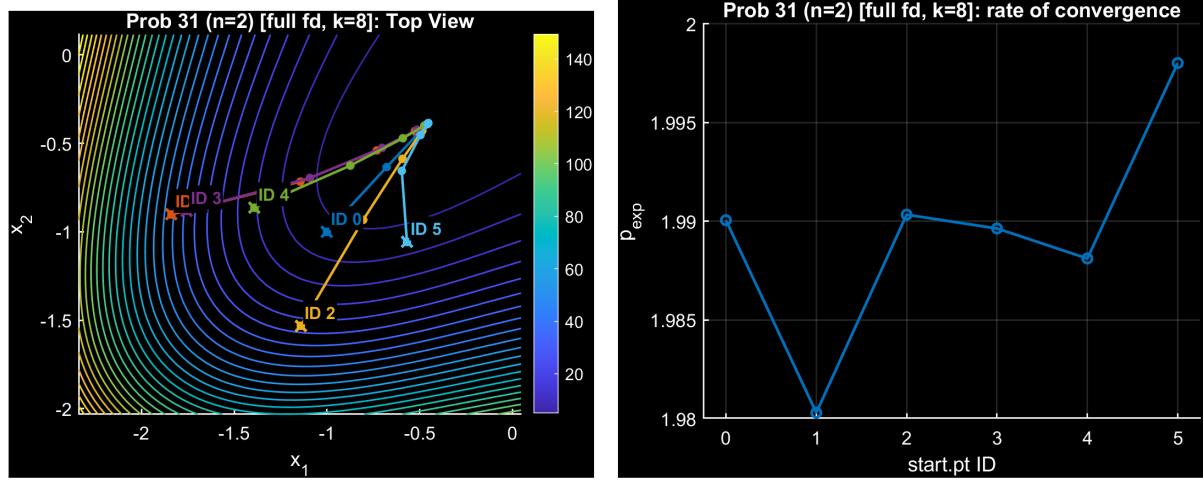


Figure 53: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $N > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	full fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.76	0.0867s
			1	8	$4.57 \times 10^{-13}$	10/1000	yes		1.99	0.1477s
			2	8	$3.30 \times 10^{-7}$	9/1000	yes		1.95	0.1456s
			3	8	$1.33 \times 10^{-13}$	9/1000	yes		1.96	0.1354s
			4	8	$8.28 \times 10^{-7}$	8/1000	yes		1.93	0.1241s
			5	8	$1.43 \times 10^{-12}$	9/1000	yes		1.99	0.1547s
			<i>Avg (successes)</i>	8	$1.96 \times 10^{-7}$	8.3/1000	6/6		1.93	0.1324s

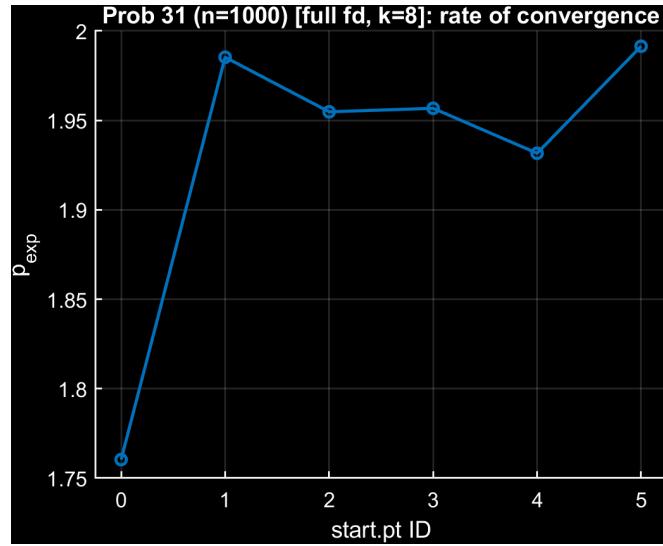


Figure 54: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	full fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/1000	yes		1.56	0.7164s
			1	8	$9.41 \times 10^{-12}$	10/1000	yes		2.00	1.40s
			2	8	$3.12 \times 10^{-9}$	9/1000	yes		1.95	1.27s
			3	8	$2.15 \times 10^{-7}$	10/1000	yes		1.99	1.39s
			4	8	$4.62 \times 10^{-7}$	8/1000	yes		1.90	1.13s
			5	8	$5.96 \times 10^{-7}$	10/1000	yes		1.96	1.41s
			Avg (successes)	8	$2.16 \times 10^{-7}$	8.7/1000	6/6		1.89	1.22s

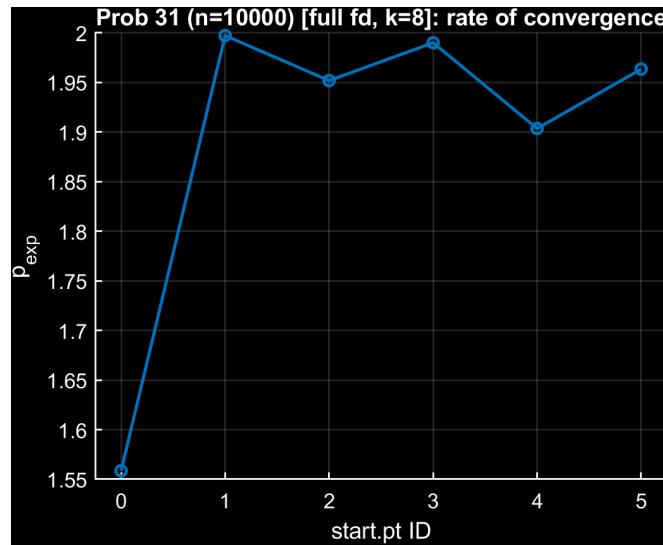


Figure 55: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	full fd	$\bar{x}$	8	$1.79 \times 10^{-8}$	5/100	yes		1.56	7.02s
			1	8	$1.73 \times 10^{-7}$	8/100	yes		1.90	11.36s
			2	8	$3.80 \times 10^{-8}$	12/100	yes		1.99	16.69s
			3	8	$3.45 \times 10^{-11}$	10/100	yes		2.00	13.91s
			4	8	$7.23 \times 10^{-13}$	11/100	yes		1.71	15.46s
			5	8	$1.23 \times 10^{-9}$	10/100	yes		2.00	14.19s
			Avg (successes)	8	$3.84 \times 10^{-8}$	9.3/100	6/6		1.86	13.11s

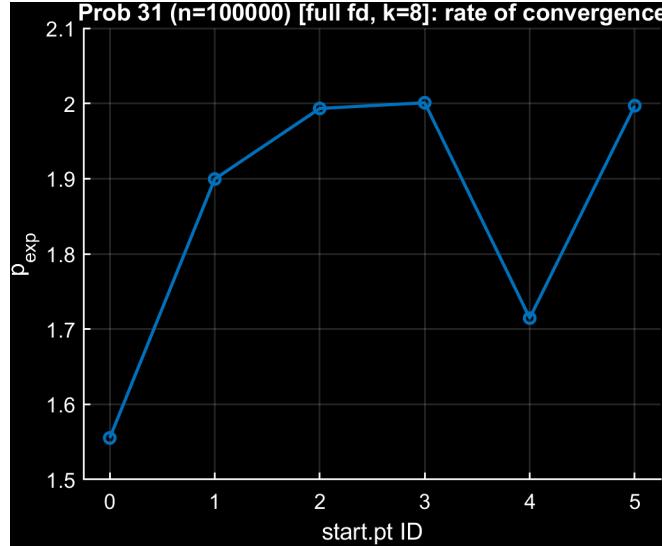


Figure 56: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).

**Full FD (constant  $h$ ),  $k = 12$**

**Case  $n = 2$**

Prob.	Dim.	Mode	start.pt ID	$k$	grad.norm	iters/max	succ.	flag	rate	time
31	2	full fd	$\bar{x}$	12	$1.83 \times 10^{-7}$	5/1000	yes		1.92	0.0010s
			1	12	$1.92 \times 10^{-7}$	6/1000	yes		1.91	0.0008s
			2	12	$4.71 \times 10^{-9}$	6/1000	yes		1.86	0.0011s
			3	12	$3.89 \times 10^{-9}$	6/1000	yes		1.74	0.0007s
			4	12	$5.00 \times 10^{-10}$	5/1000	yes		1.89	0.0006s
			5	12	$7.56 \times 10^{-11}$	8/1000	yes		1.39	0.0010s
			Avg (successes)	12	$6.41 \times 10^{-8}$	6.0/1000	6/6		1.78	0.0009s

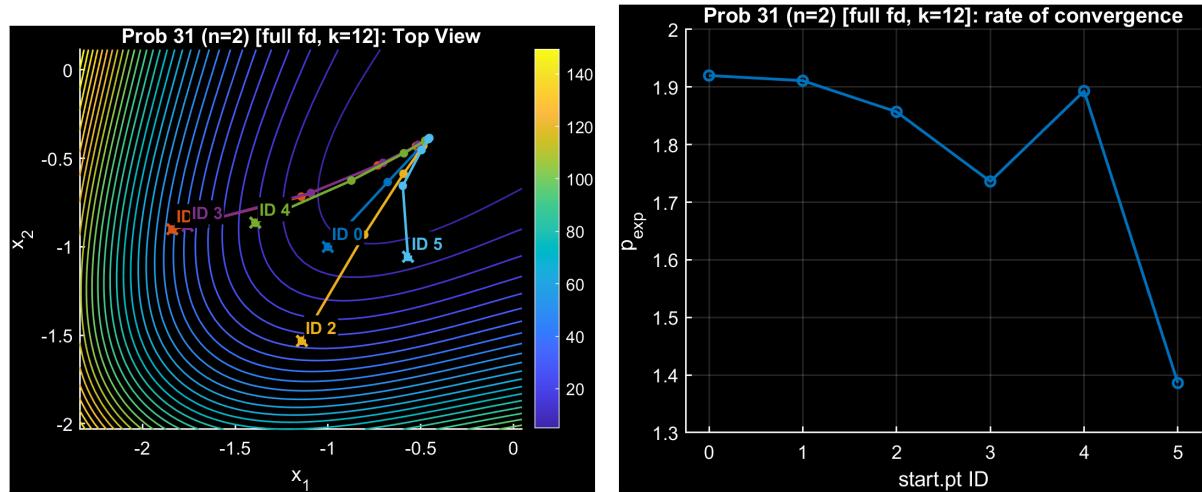


Figure 57: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $N > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	1000	full fd	$\bar{x}$	12	$3.10 \times 10^{-8}$	5/1000	yes		1.67	0.0746s
			1	12	$1.40 \times 10^{-10}$	10/1000	yes		1.25	0.1717s
			2	12	$7.21 \times 10^{-7}$	9/1000	yes		1.92	0.1393s
			3	12	$2.62 \times 10^{-11}$	9/1000	yes		1.29	0.1529s
			4	12	$7.52 \times 10^{-7}$	8/1000	yes		1.96	0.1346s
			5	12	$2.03 \times 10^{-10}$	9/1000	yes		1.36	0.1941s
			Avg (successes)	12	$2.51 \times 10^{-7}$	8.3/1000	6/6		1.57	0.1446s

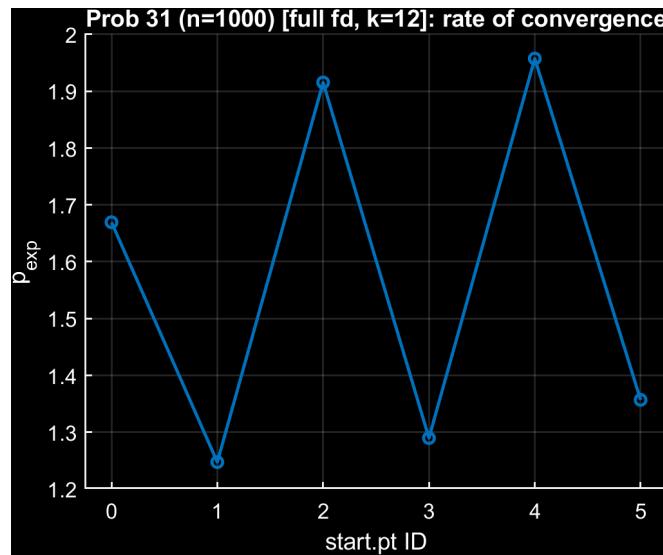


Figure 58: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 1000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	10000	full fd	$\bar{x}$	12	$3.12 \times 10^{-8}$	5/1000	yes		1.49	0.7128s
			1	12	$4.94 \times 10^{-10}$	10/1000	yes		1.47	1.41s
			2	12	$1.57 \times 10^{-8}$	9/1000	yes		1.67	1.28s
			3	12	$4.10 \times 10^{-7}$	10/1000	yes		1.91	1.40s
			4	12	$6.31 \times 10^{-7}$	8/1000	yes		1.85	1.13s
			5	12	$7.05 \times 10^{-7}$	10/1000	yes		1.97	1.41s
			Avg (successes)	12	$2.99 \times 10^{-7}$	8.7/1000	6/6		1.73	1.22s

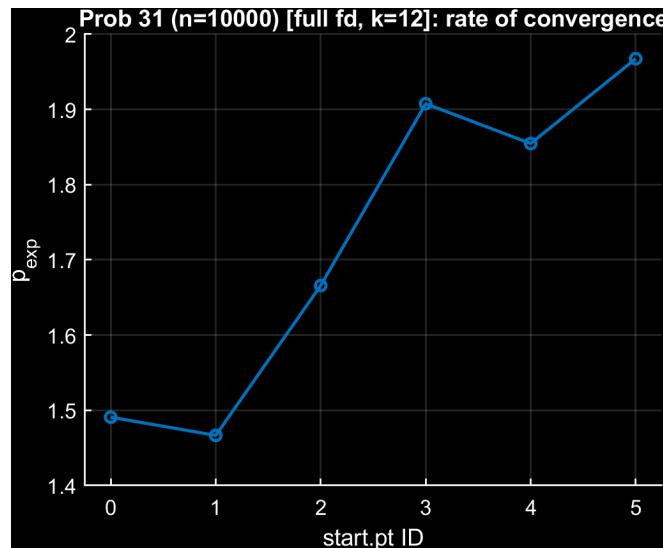


Figure 59: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 10000$ ).

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
31	100000	full fd	$\bar{x}$	12	$3.23 \times 10^{-8}$	5/100	yes		1.51	7.23s
			1	12	$1.98 \times 10^{-7}$	8/100	yes		1.85	13.42s
			2	12	$1.70 \times 10^{-8}$	11/100	yes		1.73	15.48s
			3	12	$1.13 \times 10^{-9}$	10/100	yes		1.48	13.58s
			4	12	$3.92 \times 10^{-7}$	10/100	yes		1.99	13.65s
			5	12	$2.15 \times 10^{-10}$	11/100	yes		1.09	14.92s
			Avg (successes)	12	$1.07 \times 10^{-7}$	9.2/100	6/6		1.61	13.05s

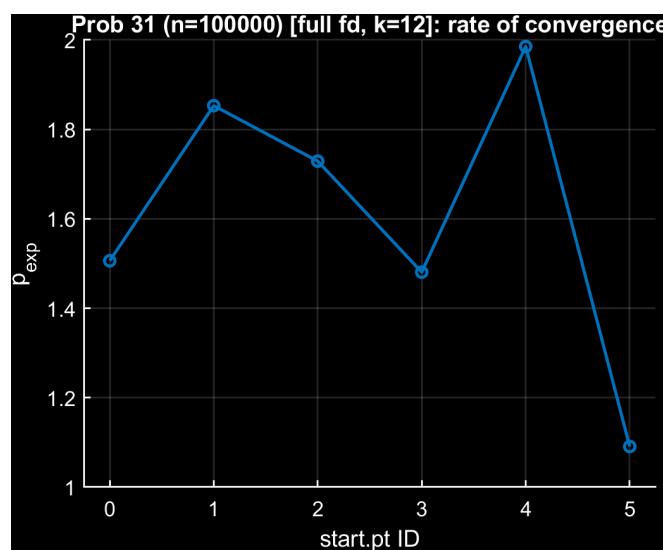


Figure 60: Problem 31, Modified Newton, full FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate  $p_{exp}$  for converged runs ( $n = 100000$ ).



### 9.1.2 Truncated Newton

**Full FD (constant  $h$ ),  $k = 4$**

Table 12: Results for Problem 31.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD_all	0.0	12.0	component-wise	9.69e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	component-wise	2.82e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	component-wise	3.40e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	component-wise	5.07e-08	5/1000	yes	0.08	0.0
31.0	2.0	FD_all	4.0	12.0	component-wise	2.74e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	component-wise	4.12e-10	7/1000	yes	2.03	0.0
31.0	2.0	FD_all	0.0	12.0	constant	1.26e-09	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	constant	2.39e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	constant	2.24e-10	6/1000	yes	1.15	0.0
31.0	2.0	FD_all	4.0	12.0	constant	1.52e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	constant	1.56e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	4.0	component-wise	2.01e-10	6/1000	yes	2.01	0.03
31.0	2.0	FD_all	1.0	4.0	component-wise	1.13e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	4.0	component-wise	2.27e-07	7/1000	yes	2.26	0.03
31.0	2.0	FD_all	3.0	4.0	component-wise	2.07e-10	4/1000	yes	1.59	0.03
31.0	2.0	FD_all	4.0	4.0	component-wise	1.06e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	5.0	4.0	component-wise	4.56e-11	7/1000	yes	2.02	0.03
31.0	2.0	FD_all	0.0	4.0	constant	9.04e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	4.0	constant	2.00e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	4.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	4.0	constant	3.56e-07	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	4.0	constant	1.90e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	4.0	constant	2.34e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	component-wise	6.16e-11	6/1000	yes	2.02	0.03
31.0	2.0	FD_all	1.0	8.0	component-wise	9.56e-09	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	8.0	component-wise	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	component-wise	2.32e-08	5/1000	yes	0.51	0.0
31.0	2.0	FD_all	4.0	8.0	component-wise	8.96e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	component-wise	4.43e-12	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	constant	6.17e-11	6/1000	yes	2.02	0.0
31.0	2.0	FD_all	1.0	8.0	constant	9.55e-09	7/1000	yes	2.0	0.01
31.0	2.0	FD_all	2.0	8.0	constant	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	constant	1.40e-12	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	8.0	constant	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	constant	4.44e-12	7/1000	yes	2.02	0.0
31.0	1000.0	FD_all	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.28	0.48
31.0	1000.0	FD_all	1.0	12.0	component-wise	2.39e-09	14/1000	yes	1.6	0.6
31.0	1000.0	FD_all	2.0	12.0	component-wise	3.42e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	12.0	component-wise	3.80e-07	12/1000	yes	1.4	0.49
31.0	1000.0	FD_all	4.0	12.0	component-wise	8.55e-08	14/1000	yes	1.4	0.48
31.0	1000.0	FD_all	5.0	12.0	component-wise	1.23e-09	15/1000	yes	1.58	0.68
31.0	1000.0	FD_all	0.0	12.0	constant	1.61e-07	11/1000	yes	2.27	0.51
31.0	1000.0	FD_all	1.0	12.0	constant	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	12.0	constant	3.42e-07	13/1000	yes	1.16	0.58
31.0	1000.0	FD_all	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.52
31.0	1000.0	FD_all	4.0	12.0	constant	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	12.0	constant	1.23e-09	15/1000	yes	1.58	0.64
31.0	1000.0	FD_all	0.0	4.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	4.0	component-wise	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	4.0	component-wise	3.41e-07	13/1000	yes	1.16	0.59
31.0	1000.0	FD_all	3.0	4.0	component-wise	3.81e-07	12/1000	yes	1.39	0.51
31.0	1000.0	FD_all	4.0	4.0	component-wise	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	4.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	4.0	constant	1.61e-07	11/1000	yes	2.27	0.46
31.0	1000.0	FD_all	1.0	4.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	4.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	4.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	4.0	constant	8.51e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	4.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.27	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	8.0	constant	8.51e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	12.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	12.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	12.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	12.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	12.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	12.0	constant	1.61e-07	11/1000	yes	2.27	0.47
31.0	1000.0	FD_all	1.0	12.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	12.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	12.0	constant	8.51e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	12.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.27	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	12.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	12.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	12.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	12.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	12.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	12.0	constant	1.61e-07	11/1000	yes	2.27	0.47
31.0	1000.0	FD_all	1.0	12.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	12.0	constant	3.4				

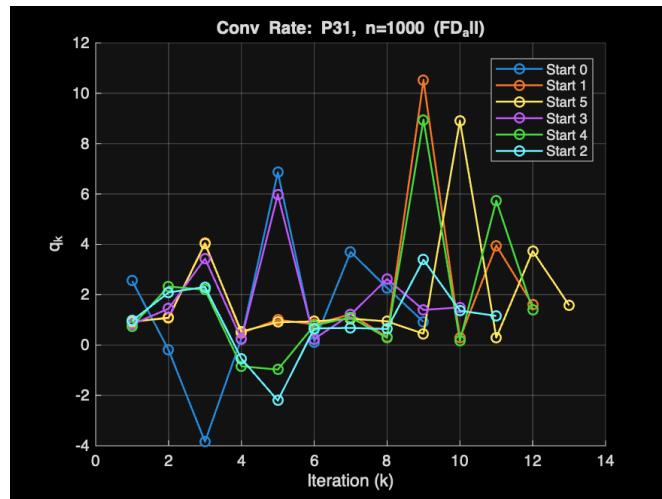


Figure 61: Problem 31, Truncated Newton, full FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Full FD (constant  $h$ ),  $k = 8$** Table 13: Results for Problem 31.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD_all	0.0	12.0	component-wise	9.69e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	component-wise	2.82e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	component-wise	3.40e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	component-wise	5.07e-08	5/1000	yes	0.08	0.0
31.0	2.0	FD_all	4.0	12.0	component-wise	2.74e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	component-wise	4.12e-10	7/1000	yes	2.03	0.0
31.0	2.0	FD_all	0.0	12.0	constant	1.26e-09	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	constant	2.39e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	constant	2.24e-10	6/1000	yes	1.15	0.0
31.0	2.0	FD_all	4.0	12.0	constant	1.52e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	constant	1.56e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	4.0	component-wise	2.01e-10	6/1000	yes	2.01	0.03
31.0	2.0	FD_all	1.0	4.0	component-wise	1.13e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	4.0	component-wise	2.27e-07	7/1000	yes	2.26	0.03
31.0	2.0	FD_all	3.0	4.0	component-wise	2.07e-10	4/1000	yes	1.59	0.03
31.0	2.0	FD_all	4.0	4.0	component-wise	1.06e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	5.0	4.0	component-wise	4.56e-11	7/1000	yes	2.02	0.03
31.0	2.0	FD_all	0.0	4.0	constant	9.04e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	4.0	constant	2.00e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	4.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	4.0	constant	3.56e-07	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	4.0	constant	1.90e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	4.0	constant	2.34e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	component-wise	6.16e-11	6/1000	yes	2.02	0.03
31.0	2.0	FD_all	1.0	8.0	component-wise	9.56e-09	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	8.0	component-wise	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	component-wise	2.32e-08	5/1000	yes	0.51	0.0
31.0	2.0	FD_all	4.0	8.0	component-wise	8.96e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	component-wise	4.43e-12	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	constant	6.17e-11	6/1000	yes	2.02	0.0
31.0	2.0	FD_all	1.0	8.0	constant	9.55e-09	7/1000	yes	2.0	0.01
31.0	2.0	FD_all	2.0	8.0	constant	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	constant	1.40e-12	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	8.0	constant	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	constant	4.44e-12	7/1000	yes	2.02	0.0
31.0	1000.0	FD_all	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.28	0.48
31.0	1000.0	FD_all	1.0	12.0	component-wise	2.39e-09	14/1000	yes	1.6	0.6
31.0	1000.0	FD_all	2.0	12.0	component-wise	3.42e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	12.0	component-wise	3.80e-07	12/1000	yes	1.4	0.49
31.0	1000.0	FD_all	4.0	12.0	component-wise	8.55e-08	14/1000	yes	1.4	0.48
31.0	1000.0	FD_all	5.0	12.0	component-wise	1.23e-09	15/1000	yes	1.58	0.68
31.0	1000.0	FD_all	0.0	12.0	constant	1.61e-07	11/1000	yes	2.27	0.51
31.0	1000.0	FD_all	1.0	12.0	constant	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	12.0	constant	3.42e-07	13/1000	yes	1.16	0.58
31.0	1000.0	FD_all	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.52
31.0	1000.0	FD_all	4.0	12.0	constant	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	12.0	constant	1.23e-09	15/1000	yes	1.58	0.64
31.0	1000.0	FD_all	0.0	4.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	4.0	component-wise	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	4.0	component-wise	3.41e-07	13/1000	yes	1.16	0.59
31.0	1000.0	FD_all	3.0	4.0	component-wise	3.81e-07	12/1000	yes	1.39	0.51
31.0	1000.0	FD_all	4.0	4.0	component-wise	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	4.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	4.0	constant	1.61e-07	11/1000	yes	2.27	0.46
31.0	1000.0	FD_all	1.0	4.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	4.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	4.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	4.0	constant	8.51e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	4.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.54
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.47
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all								

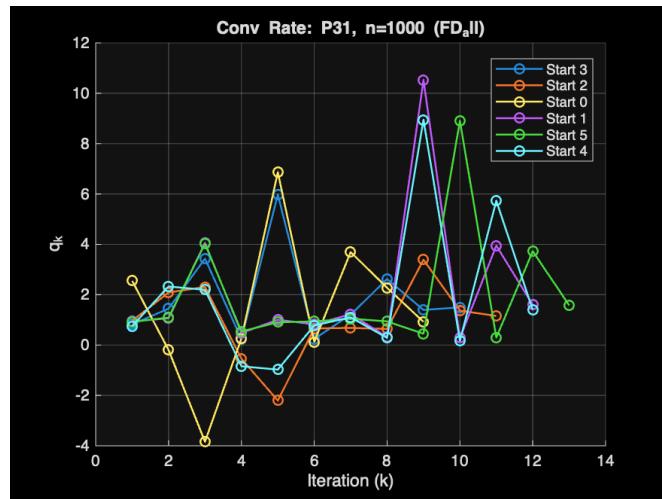


Figure 62: Problem 31, Truncated Newton, full FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Full FD (constant  $h$ ),  $k = 12$** Table 14: Results for Problem 31.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
31.0	2.0	FD_all	0.0	12.0	component-wise	9.69e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	component-wise	2.82e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	component-wise	3.40e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	component-wise	5.07e-08	5/1000	yes	0.08	0.0
31.0	2.0	FD_all	4.0	12.0	component-wise	2.74e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	component-wise	4.12e-10	7/1000	yes	2.03	0.0
31.0	2.0	FD_all	0.0	12.0	constant	1.26e-09	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	12.0	constant	2.39e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	12.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	12.0	constant	2.24e-10	6/1000	yes	1.15	0.0
31.0	2.0	FD_all	4.0	12.0	constant	1.52e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	12.0	constant	1.56e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	4.0	component-wise	2.01e-10	6/1000	yes	2.01	0.03
31.0	2.0	FD_all	1.0	4.0	component-wise	1.13e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	4.0	component-wise	2.27e-07	7/1000	yes	2.26	0.03
31.0	2.0	FD_all	3.0	4.0	component-wise	2.07e-10	4/1000	yes	1.59	0.03
31.0	2.0	FD_all	4.0	4.0	component-wise	1.06e-08	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	5.0	4.0	component-wise	4.56e-11	7/1000	yes	2.02	0.03
31.0	2.0	FD_all	0.0	4.0	constant	9.04e-10	6/1000	yes	2.01	0.0
31.0	2.0	FD_all	1.0	4.0	constant	2.00e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	2.0	4.0	constant	2.67e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	4.0	constant	3.56e-07	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	4.0	constant	1.90e-08	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	4.0	constant	2.34e-10	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	component-wise	6.16e-11	6/1000	yes	2.02	0.03
31.0	2.0	FD_all	1.0	8.0	component-wise	9.56e-09	7/1000	yes	2.0	0.03
31.0	2.0	FD_all	2.0	8.0	component-wise	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	component-wise	2.32e-08	5/1000	yes	0.51	0.0
31.0	2.0	FD_all	4.0	8.0	component-wise	8.96e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	component-wise	4.43e-12	7/1000	yes	2.02	0.0
31.0	2.0	FD_all	0.0	8.0	constant	6.17e-11	6/1000	yes	2.02	0.0
31.0	2.0	FD_all	1.0	8.0	constant	9.55e-09	7/1000	yes	2.0	0.01
31.0	2.0	FD_all	2.0	8.0	constant	2.18e-07	7/1000	yes	2.26	0.0
31.0	2.0	FD_all	3.0	8.0	constant	1.40e-12	4/1000	yes	1.58	0.0
31.0	2.0	FD_all	4.0	8.0	constant	8.97e-09	7/1000	yes	2.0	0.0
31.0	2.0	FD_all	5.0	8.0	constant	4.44e-12	7/1000	yes	2.02	0.0
31.0	1000.0	FD_all	0.0	12.0	component-wise	1.61e-07	11/1000	yes	2.28	0.48
31.0	1000.0	FD_all	1.0	12.0	component-wise	2.39e-09	14/1000	yes	1.6	0.6
31.0	1000.0	FD_all	2.0	12.0	component-wise	3.42e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	12.0	component-wise	3.80e-07	12/1000	yes	1.4	0.49
31.0	1000.0	FD_all	4.0	12.0	component-wise	8.55e-08	14/1000	yes	1.4	0.48
31.0	1000.0	FD_all	5.0	12.0	component-wise	1.23e-09	15/1000	yes	1.58	0.68
31.0	1000.0	FD_all	0.0	12.0	constant	1.61e-07	11/1000	yes	2.27	0.51
31.0	1000.0	FD_all	1.0	12.0	constant	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	12.0	constant	3.42e-07	13/1000	yes	1.16	0.58
31.0	1000.0	FD_all	3.0	12.0	constant	3.81e-07	12/1000	yes	1.39	0.52
31.0	1000.0	FD_all	4.0	12.0	constant	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	12.0	constant	1.23e-09	15/1000	yes	1.58	0.64
31.0	1000.0	FD_all	0.0	4.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	4.0	component-wise	2.39e-09	14/1000	yes	1.6	0.62
31.0	1000.0	FD_all	2.0	4.0	component-wise	3.41e-07	13/1000	yes	1.16	0.59
31.0	1000.0	FD_all	3.0	4.0	component-wise	3.81e-07	12/1000	yes	1.39	0.51
31.0	1000.0	FD_all	4.0	4.0	component-wise	8.52e-08	14/1000	yes	1.4	0.6
31.0	1000.0	FD_all	5.0	4.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	4.0	constant	1.61e-07	11/1000	yes	2.27	0.46
31.0	1000.0	FD_all	1.0	4.0	constant	2.39e-09	14/1000	yes	1.59	0.6
31.0	1000.0	FD_all	2.0	4.0	constant	3.41e-07	13/1000	yes	1.16	0.57
31.0	1000.0	FD_all	3.0	4.0	constant	3.81e-07	12/1000	yes	1.39	0.53
31.0	1000.0	FD_all	4.0	4.0	constant	8.51e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	4.0	constant	1.22e-09	15/1000	yes	1.58	0.65
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.46
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.49
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.55
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.49
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	constant	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	constant	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	constant	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	component-wise	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	component-wise	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	component-wise	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all	3.0	8.0	component-wise	3.81e-07	12/1000	yes	1.39	0.65
31.0	1000.0	FD_all	4.0	8.0	component-wise	8.52e-08	14/1000	yes	1.4	0.61
31.0	1000.0	FD_all	5.0	8.0	component-wise	1.22e-09	15/1000	yes	1.58	0.66
31.0	1000.0	FD_all	0.0	8.0	constant	1.61e-07	11/1000	yes	2.28	0.47
31.0	1000.0	FD_all	1.0	8.0	constant	2.39e-09	14/1000	yes	1.6	0.57
31.0	1000.0	FD_all	2.0	8.0	constant	3.41e-07	13/1000	yes	1.16	0.61
31.0	1000.0	FD_all</td								

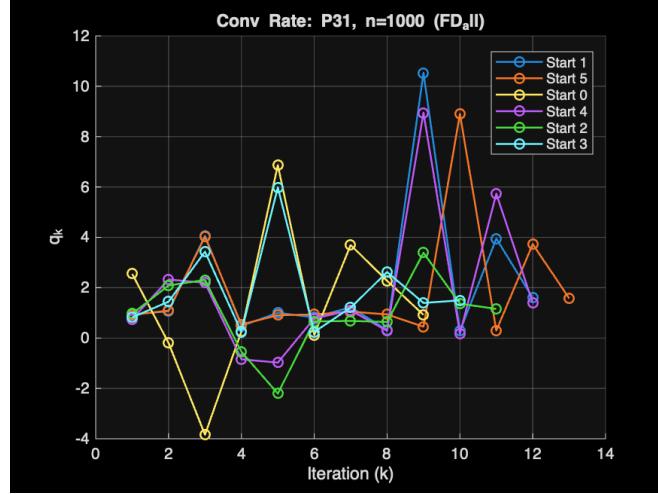


Figure 63: Problem 31, Truncated Newton, full FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

## 9.2 Problem 83

### 9.2.1 Modified Newton

Full FD (constant  $h$ ),  $k = 4$

Case  $n = 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	full fd	$\bar{x}$	4	$9.49 \times 10^{-10}$	3/1000	yes		1.90	0.0179s
			1	4	$4.70 \times 10^{-10}$	3/1000	yes		2.04	0.0007s
			2	4	$4.27 \times 10^{-7}$	3/1000	yes		1.94	0.0005s
			3	4	$2.02 \times 10^{-9}$	3/1000	yes		2.00	0.0006s
			4	4	$8.05 \times 10^{-8}$	3/1000	yes		2.01	0.0005s
			5	4	$2.11 \times 10^{-12}$	4/1000	yes		1.35	0.0008s
			Avg (successes)	4	$8.51 \times 10^{-8}$	3.2/1000	6/6		1.87	0.0035s

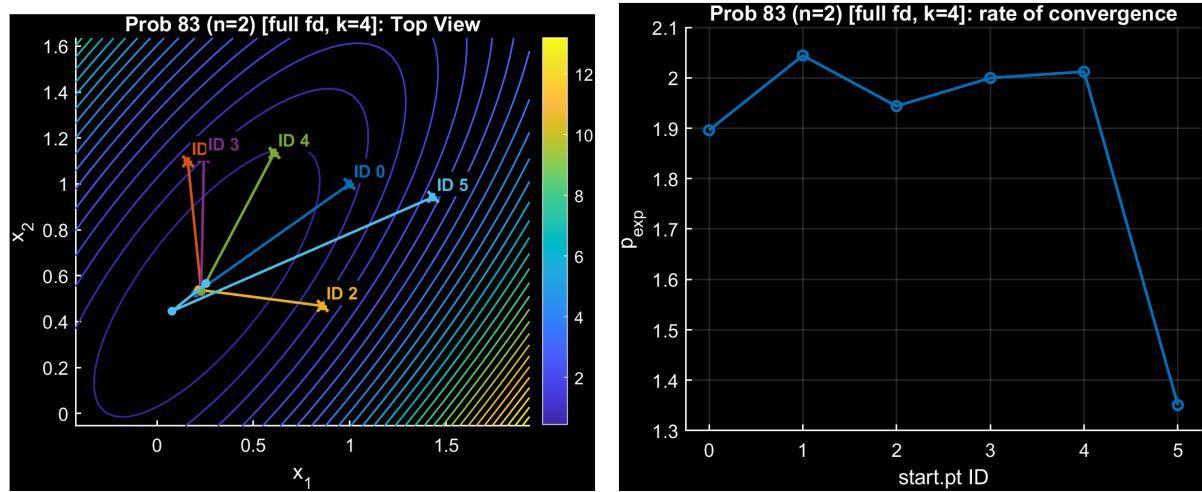


Figure 64: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

### Case $N > 2$

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	full fd	$\bar{x}$	4	$5.29 \times 10^{-13}$	2/1000	yes		NaN	0.0291s
			1	4	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0339s
			2	4	$2.51 \times 10^{-8}$	2/1000	yes		NaN	0.0262s
			3	4	$2.80 \times 10^{-8}$	2/1000	yes		NaN	0.0263s
			4	4	$2.94 \times 10^{-8}$	2/1000	yes		NaN	0.0253s
			5	4	$2.36 \times 10^{-8}$	2/1000	yes		NaN	0.0250s
				Avg (successes)	4	$2.19 \times 10^{-8}$	2.0/1000	6/6	NaN	0.0276s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	full fd	$\bar{x}$	4	$1.14 \times 10^{-8}$	1/1000	yes		NaN	0.0971s
			1	4	$6.73 \times 10^{-10}$	2/1000	yes		NaN	0.1870s
			2	4	$5.35 \times 10^{-10}$	2/1000	yes		NaN	0.1873s
			3	4	$1.56 \times 10^{-10}$	2/1000	yes		NaN	0.1873s
			4	4	$4.33 \times 10^{-10}$	2/1000	yes		NaN	0.1883s
			5	4	$2.88 \times 10^{-10}$	2/1000	yes		NaN	0.1924s
				Avg (successes)	4	$2.25 \times 10^{-9}$	1.8/1000	6/6	NaN	0.1732s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	full fd	$\bar{x}$	4	$9.67 \times 10^{-9}$	1/100	yes		NaN	1.03s
			1	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.9743s
			2	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.9779s
			3	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	1.01s
			4	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.9861s
			5	4	$1.68 \times 10^{-7}$	1/100	yes		NaN	0.9875s
				Avg (successes)	4	$1.41 \times 10^{-7}$	1.0/100	6/6	NaN	0.9943s

**Full FD (constant  $h$ ),  $k = 8$** Case  $n = 2$ 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	2	full fd	$\bar{x}$	8	$1.34 \times 10^{-9}$	3/1000	yes		1.84	0.0012s
			1	8	$7.49 \times 10^{-10}$	3/1000	yes		1.97	0.0007s
			2	8	$4.34 \times 10^{-7}$	3/1000	yes		1.94	0.0007s
			3	8	$2.58 \times 10^{-9}$	3/1000	yes		1.96	0.0005s
			4	8	$8.39 \times 10^{-8}$	3/1000	yes		2.00	0.0007s
			5	8	$1.02 \times 10^{-14}$	4/1000	yes		1.89	0.0006s
			<i>Avg (successes)</i>	8	$8.71 \times 10^{-8}$	3.2/1000	6/6		1.94	0.0008s

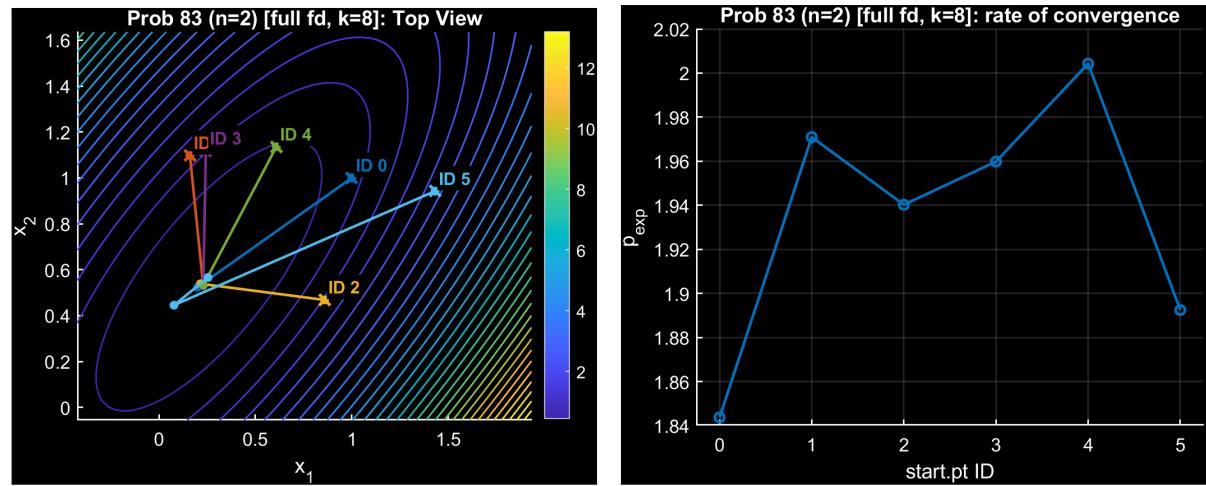


Figure 65: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

Case  $N > 2$ 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	full fd	$\bar{x}$	8	$1.36 \times 10^{-12}$	2/1000	yes		NaN	0.0223s
			1	8	$2.09 \times 10^{-8}$	2/1000	yes		NaN	0.0226s
			2	8	$3.77 \times 10^{-8}$	2/1000	yes		NaN	0.0219s
			3	8	$2.61 \times 10^{-8}$	2/1000	yes		NaN	0.0215s
			4	8	$2.70 \times 10^{-8}$	2/1000	yes		NaN	0.0218s
			5	8	$2.50 \times 10^{-8}$	2/1000	yes		NaN	0.0205s
			<i>Avg (successes)</i>	8	$2.28 \times 10^{-8}$	2.0/1000	6/6		NaN	0.0218s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	10000	full fd	$\bar{x}$	8	$3.43 \times 10^{-8}$	1/1000	yes		NaN	0.0981s	
			1	8	$1.32 \times 10^{-9}$	2/1000	yes		NaN	0.1870s	
			2	8	$8.09 \times 10^{-11}$	2/1000	yes		NaN	0.1894s	
			3	8	$1.15 \times 10^{-10}$	2/1000	yes		NaN	0.1925s	
			4	8	$1.96 \times 10^{-8}$	2/1000	yes		NaN	0.1961s	
			5	8	$9.33 \times 10^{-11}$	2/1000	yes		NaN	0.2042s	
			<i>Avg (successes)</i>		8	$9.26 \times 10^{-9}$	1.8/1000	6/6		NaN	0.1779s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	100000	full fd	$\bar{x}$	8	$2.96 \times 10^{-8}$	1/100	yes		NaN	0.9861s	
			1	8	$4.21 \times 10^{-8}$	2/100	yes		NaN	1.94s	
			2	8	$4.93 \times 10^{-8}$	2/100	yes		NaN	1.96s	
			3	8	$5.21 \times 10^{-8}$	2/100	yes		NaN	1.95s	
			4	8	$1.08 \times 10^{-7}$	2/100	yes		NaN	1.94s	
			5	8	$6.41 \times 10^{-8}$	2/100	yes		NaN	1.96s	
			<i>Avg (successes)</i>		8	$5.75 \times 10^{-8}$	1.8/100	6/6		NaN	1.79s

**Full FD (constant  $h$ ),  $k = 12$**

**Case  $n = 2$**

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time	
83	2	full fd	$\bar{x}$	12	$6.53 \times 10^{-9}$	3/1000	yes		1.60	0.0012s	
			1	12	$9.82 \times 10^{-9}$	3/1000	yes		1.56	0.0007s	
			2	12	$3.45 \times 10^{-7}$	3/1000	yes		1.99	0.0006s	
			3	12	$2.04 \times 10^{-8}$	3/1000	yes		1.62	0.0006s	
			4	12	$1.04 \times 10^{-7}$	3/1000	yes		1.96	0.0005s	
			5	12	$4.98 \times 10^{-7}$	3/1000	yes		2.36	0.0005s	
			<i>Avg (successes)</i>		12	$1.64 \times 10^{-7}$	3.0/1000	6/6		1.85	0.0007s

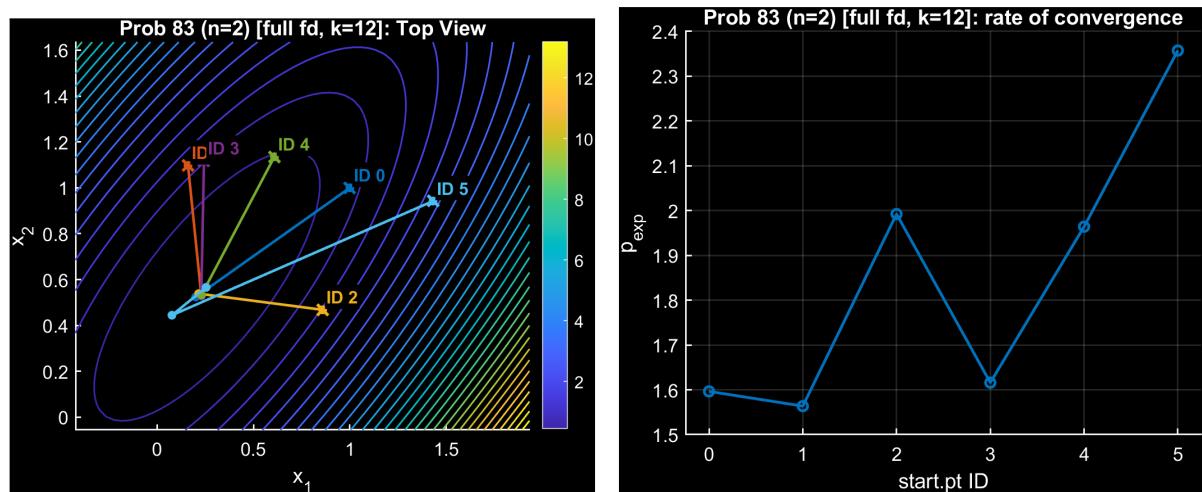


Figure 66: (Left) Top view of the objective level sets with the optimization paths from the different starting points; (right) experimental convergence rate for converged runs.

**Case  $N > 2$** 

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	1000	full fd	$\bar{x}$	12	$4.77 \times 10^{-7}$	4/1000	yes		0.29	0.0407s
			1	12	$3.91 \times 10^{-7}$	9/1000	yes		NaN	0.0901s
			2	12	$1.16 \times 10^{-7}$	5/1000	yes		2.17	0.0510s
			3	12	$1.52 \times 10^{-7}$	3/1000	yes		0.69	0.0304s
			4	12	$1.47 \times 10^{-8}$	4/1000	yes		1.42	0.0395s
			5	12	$2.86 \times 10^{-7}$	3/1000	yes		0.60	0.0304s
			<i>Avg (successes)</i>	12	$2.40 \times 10^{-7}$	4.7/1000	6/6		1.03	0.0470s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	10000	full fd	$\bar{x}$	12	$3.26 \times 10^{-7}$	2/1000	yes		NaN	0.1895s
			1	12	$1.26 \times 10^{-8}$	4/1000	yes		1.39	0.3876s
			2	12	$1.47 \times 10^{-7}$	3/1000	yes		0.66	0.3044s
			3	12	$5.91 \times 10^{-7}$	5/1000	yes		1.12	0.4783s
			4	12	$1.26 \times 10^{-7}$	3/1000	yes		0.62	0.3019s
			5	12	$1.23 \times 10^{-7}$	3/1000	yes		0.66	0.3028s
			<i>Avg (successes)</i>	12	$2.21 \times 10^{-7}$	3.3/1000	6/6		0.89	0.3274s

Prob.	Dim.	Mode	start.pt ID	k	grad.norm	iters/max	succ.	flag	rate	time
83	100000	full fd	$\bar{x}$	12	$8.31 \times 10^{-7}$	6/100	yes		0.90	5.83s
			1	12	$3.14 \times 10^{-7}$	3/100	yes		0.68	3.28s
			2	12	$1.10 \times 10^{-7}$	4/100	yes		0.58	4.23s
			3	12	$1.83 \times 10^{-8}$	5/100	yes		1.00	5.20s
			4	12	$3.23 \times 10^{-7}$	3/100	yes		0.67	3.25s
			5	12	$7.10 \times 10^{-7}$	3/100	yes		0.59	3.28s
			<i>Avg (successes)</i>	12	$3.84 \times 10^{-7}$	4.0/100	6/6		0.74	4.18s



### 9.2.2 Truncated Newton

**Full FD (constant  $h$ ),  $k = 4$**

Table 15: Results for Problem 83.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD_all	0.0	12.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.0
83.0	2.0	FD_all	1.0	12.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	2.0	12.0	component-wise	5.05e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	12.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	12.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	12.0	component-wise	1.27e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	12.0	constant	3.34e - 07	12/1000	yes	0.91	0.0
83.0	2.0	FD_all	1.0	12.0	constant	0.0281	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	12.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	12.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	12.0	constant	0.0641	100/1000	no	N/A	0.01
83.0	2.0	FD_all	5.0	12.0	constant	0.0169	100/1000	no	N/A	0.01
83.0	2.0	FD_all	0.0	4.0	component-wise	1.90e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	4.0	component-wise	1.77e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	4.0	component-wise	5.32e - 08	7/1000	yes	0.98	0.01
83.0	2.0	FD_all	3.0	4.0	component-wise	2.25e - 07	6/1000	yes	0.94	0.01
83.0	2.0	FD_all	4.0	4.0	component-wise	2.07e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	4.0	component-wise	1.11e - 07	5/1000	yes	0.95	0.01
83.0	2.0	FD_all	0.0	4.0	constant	4.37e - 07	7/1000	yes	-2.31	0.0
83.0	2.0	FD_all	1.0	4.0	constant	0.0282	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	4.0	constant	1.17e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	4.0	constant	0.074	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	4.0	constant	0.0644	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	4.0	constant	0.0173	100/1000	no	N/A	0.02
83.0	2.0	FD_all	0.0	8.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	8.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	8.0	component-wise	5.06e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	8.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	8.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	5.0	8.0	component-wise	1.26e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	8.0	constant	3.35e - 07	9/1000	yes	0.06	0.0
83.0	2.0	FD_all	1.0	8.0	constant	0.0281	100/1000	no	N/A	0.02
83.0	2.0	FD_all	2.0	8.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	8.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	8.0	constant	0.0641	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	8.0	constant	0.0169	100/1000	no	N/A	0.02
83.0	1000.0	FD_all	0.0	12.0	component-wise	1.00e - 03	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	1.0	12.0	component-wise	1.55e - 03	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	2.0	12.0	component-wise	5.25e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	3.0	12.0	component-wise	9.26e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	4.0	12.0	component-wise	7.38e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	5.0	12.0	component-wise	7.86e - 04	100/1000	no	N/A	2.43
83.0	1000.0	FD_all	0.0	12.0	constant	9.39e - 04	100/1000	no	N/A	2.22
83.0	1000.0	FD_all	1.0	12.0	constant	8.57e - 04	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	2.0	12.0	constant	6.44e - 04	100/1000	no	N/A	2.31
83.0	1000.0	FD_all	3.0	12.0	constant	8.04e - 04	100/1000	no	N/A	2.19
83.0	1000.0	FD_all	4.0	12.0	constant	6.72e - 04	100/1000	no	N/A	2.16
83.0	1000.0	FD_all	5.0	12.0	constant	7.45e - 04	100/1000	no	N/A	2.02
83.0	1000.0	FD_all	0.0	4.0	component-wise	1.05e - 03	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	1.0	4.0	component-wise	1.62e - 03	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	2.0	4.0	component-wise	5.22e - 04	100/1000	no	N/A	2.45
83.0	1000.0	FD_all	3.0	4.0	component-wise	9.54e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	4.0	4.0	component-wise	7.10e - 04	100/1000	no	N/A	2.47
83.0	1000.0	FD_all	5.0	4.0	component-wise	7.93e - 04	100/1000	no	N/A	2.23
83.0	1000.0	FD_all	0.0	4.0	constant	9.36e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	1.0	4.0	constant	8.87e - 04	100/1000	no	N/A	2.5
83.0	1000.0	FD_all	2.0	4.0	constant	6.83e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	3.0	4.0	constant	9.16e - 04	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	4.0	4.0	constant	6.62e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	5.0	4.0	constant	7.78e - 04	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	0.0	8.0	component-wise	9.84e - 04	100/1000	no	N/A	2.44
83.0	1000.0	FD_all	1.0	8.0	component-wise	1.56e - 03	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	2.0	8.0	component-wise	5.18e - 04	100/1000	no	N/A	2.17
83.0	1000.0	FD_all	3.0	8.0	component-wise	9.96e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	4.0	8.0	component-wise	7.31e - 04	100/1000	no	N/A	2.34
83.0	1000.0	FD_all	5.0	8.0	component-wise	8.18e - 04	100/1000	no	N/A	2.3
83.0	1000.0	FD_all	0.0	8.0	constant	9.58e - 04	100/1000	no	N/A	2.18

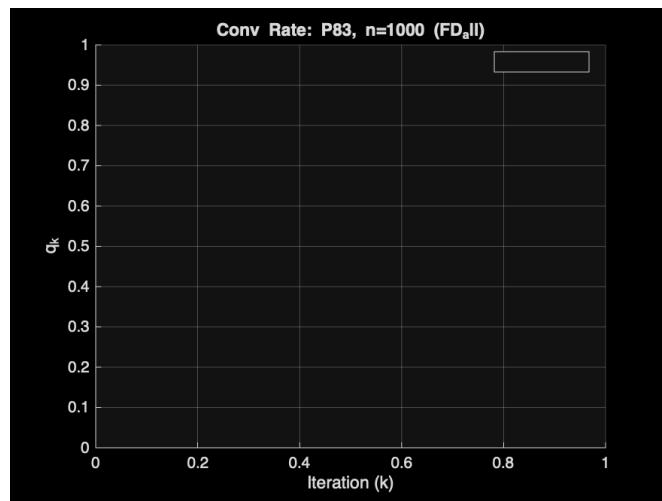


Figure 67: Problem 83, Truncated Newton, full FD (constant  $h$ ,  $k = 4$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Full FD (constant  $h$ ),  $k = 8$** Table 16: Results for Problem 83.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD_all	0.0	12.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.0
83.0	2.0	FD_all	1.0	12.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	2.0	12.0	component-wise	5.05e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	12.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	12.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	12.0	component-wise	1.27e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	12.0	constant	3.34e - 07	12/1000	yes	0.91	0.0
83.0	2.0	FD_all	1.0	12.0	constant	0.0281	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	12.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	12.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	12.0	constant	0.0641	100/1000	no	N/A	0.01
83.0	2.0	FD_all	5.0	12.0	constant	0.0169	100/1000	no	N/A	0.01
83.0	2.0	FD_all	0.0	4.0	component-wise	1.90e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	4.0	component-wise	1.77e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	4.0	component-wise	5.32e - 08	7/1000	yes	0.98	0.01
83.0	2.0	FD_all	3.0	4.0	component-wise	2.25e - 07	6/1000	yes	0.94	0.01
83.0	2.0	FD_all	4.0	4.0	component-wise	2.07e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	4.0	component-wise	1.11e - 07	5/1000	yes	0.95	0.01
83.0	2.0	FD_all	0.0	4.0	constant	4.37e - 07	7/1000	yes	-2.31	0.0
83.0	2.0	FD_all	1.0	4.0	constant	0.0282	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	4.0	constant	1.17e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	4.0	constant	0.074	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	4.0	constant	0.0644	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	4.0	constant	0.0173	100/1000	no	N/A	0.02
83.0	2.0	FD_all	0.0	8.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	8.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	8.0	component-wise	5.06e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	8.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	8.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	5.0	8.0	component-wise	1.26e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	8.0	constant	3.35e - 07	9/1000	yes	0.06	0.0
83.0	2.0	FD_all	1.0	8.0	constant	0.0281	100/1000	no	N/A	0.02
83.0	2.0	FD_all	2.0	8.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	8.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	8.0	constant	0.0641	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	8.0	constant	0.0169	100/1000	no	N/A	0.02
83.0	1000.0	FD_all	0.0	12.0	component-wise	1.00e - 03	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	1.0	12.0	component-wise	1.55e - 03	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	2.0	12.0	component-wise	5.25e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	3.0	12.0	component-wise	9.26e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	4.0	12.0	component-wise	7.38e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	5.0	12.0	component-wise	7.86e - 04	100/1000	no	N/A	2.43
83.0	1000.0	FD_all	0.0	12.0	constant	9.39e - 04	100/1000	no	N/A	2.22
83.0	1000.0	FD_all	1.0	12.0	constant	8.57e - 04	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	2.0	12.0	constant	6.44e - 04	100/1000	no	N/A	2.31
83.0	1000.0	FD_all	3.0	12.0	constant	8.04e - 04	100/1000	no	N/A	2.19
83.0	1000.0	FD_all	4.0	12.0	constant	6.72e - 04	100/1000	no	N/A	2.16
83.0	1000.0	FD_all	5.0	12.0	constant	7.45e - 04	100/1000	no	N/A	2.02
83.0	1000.0	FD_all	0.0	4.0	component-wise	1.05e - 03	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	1.0	4.0	component-wise	1.62e - 03	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	2.0	4.0	component-wise	5.22e - 04	100/1000	no	N/A	2.45
83.0	1000.0	FD_all	3.0	4.0	component-wise	9.54e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	4.0	4.0	component-wise	7.10e - 04	100/1000	no	N/A	2.47
83.0	1000.0	FD_all	5.0	4.0	component-wise	7.93e - 04	100/1000	no	N/A	2.23
83.0	1000.0	FD_all	0.0	4.0	constant	9.36e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	1.0	4.0	constant	8.87e - 04	100/1000	no	N/A	2.5
83.0	1000.0	FD_all	2.0	4.0	constant	6.83e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	3.0	4.0	constant	9.16e - 04	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	4.0	4.0	constant	6.62e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	5.0	4.0	constant	7.78e - 04	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	0.0	8.0	component-wise	9.84e - 04	100/1000	no	N/A	2.44
83.0	1000.0	FD_all	1.0	8.0	component-wise	1.56e - 03	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	2.0	8.0	component-wise	5.18e - 04	100/1000	no	N/A	2.17
83.0	1000.0	FD_all	3.0	8.0	component-wise	9.96e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	4.0	8.0	component-wise	7.31e - 04	100/1000	no	N/A	2.34
83.0	1000.0	FD_all	5.0	8.0	component-wise	8.18e - 04	100/1000	no	N/A	2.3
83.0	1000.0	FD_all	0.0	8.0	constant	9.58e - 04	100/1000	no	N/A	2.18
83.0	1000.0	FD_all	1.0	8.0	constant	8.60e - 04	100/1000	no	N/A	2.14
83.0	1000.0	FD_all	2.0	8.0	constant	7.59e - 04	100/1000	no	N/A	2.26

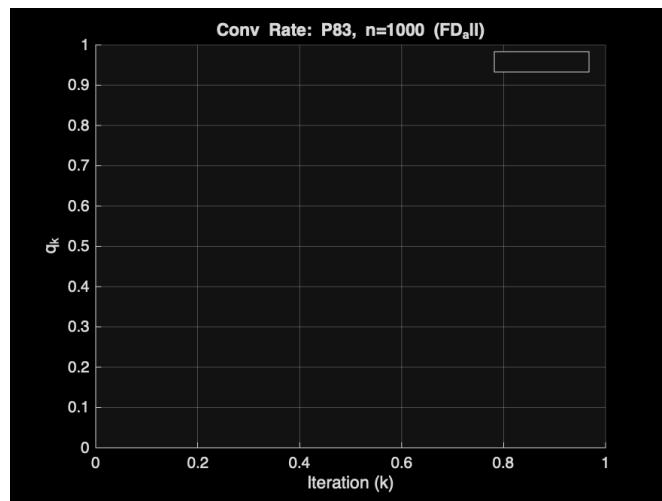


Figure 68: Problem 83, Truncated Newton, full FD (constant  $h$ ,  $k = 8$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

**Full FD (constant  $h$ ),  $k = 12$** Table 17: Results for Problem 83.0 - FD<sub>all</sub>

PROBLEM	DIMENSION	derivative_type	start.pt ID	k_exp	fd_strategy	grad.norm	iters/max	success	rate(exp)	time(s)
83.0	2.0	FD_all	0.0	12.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.0
83.0	2.0	FD_all	1.0	12.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	2.0	12.0	component-wise	5.05e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	12.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	12.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	12.0	component-wise	1.27e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	12.0	constant	3.34e - 07	12/1000	yes	0.91	0.0
83.0	2.0	FD_all	1.0	12.0	constant	0.0281	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	12.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	12.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	12.0	constant	0.0641	100/1000	no	N/A	0.01
83.0	2.0	FD_all	5.0	12.0	constant	0.0169	100/1000	no	N/A	0.01
83.0	2.0	FD_all	0.0	4.0	component-wise	1.90e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	4.0	component-wise	1.77e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	4.0	component-wise	5.32e - 08	7/1000	yes	0.98	0.01
83.0	2.0	FD_all	3.0	4.0	component-wise	2.25e - 07	6/1000	yes	0.94	0.01
83.0	2.0	FD_all	4.0	4.0	component-wise	2.07e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	5.0	4.0	component-wise	1.11e - 07	5/1000	yes	0.95	0.01
83.0	2.0	FD_all	0.0	4.0	constant	4.37e - 07	7/1000	yes	-2.31	0.0
83.0	2.0	FD_all	1.0	4.0	constant	0.0282	100/1000	no	N/A	0.01
83.0	2.0	FD_all	2.0	4.0	constant	1.17e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	4.0	constant	0.074	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	4.0	constant	0.0644	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	4.0	constant	0.0173	100/1000	no	N/A	0.02
83.0	2.0	FD_all	0.0	8.0	component-wise	1.84e - 07	6/1000	yes	0.99	0.01
83.0	2.0	FD_all	1.0	8.0	component-wise	1.72e - 07	5/1000	yes	0.99	0.01
83.0	2.0	FD_all	2.0	8.0	component-wise	5.06e - 08	7/1000	yes	0.98	0.0
83.0	2.0	FD_all	3.0	8.0	component-wise	2.21e - 07	6/1000	yes	0.94	0.0
83.0	2.0	FD_all	4.0	8.0	component-wise	2.01e - 07	5/1000	yes	0.99	0.0
83.0	2.0	FD_all	5.0	8.0	component-wise	1.26e - 07	5/1000	yes	0.96	0.0
83.0	2.0	FD_all	0.0	8.0	constant	3.35e - 07	9/1000	yes	0.06	0.0
83.0	2.0	FD_all	1.0	8.0	constant	0.0281	100/1000	no	N/A	0.02
83.0	2.0	FD_all	2.0	8.0	constant	1.07e - 07	6/1000	yes	1.0	0.0
83.0	2.0	FD_all	3.0	8.0	constant	0.0738	100/1000	no	N/A	0.02
83.0	2.0	FD_all	4.0	8.0	constant	0.0641	100/1000	no	N/A	0.02
83.0	2.0	FD_all	5.0	8.0	constant	0.0169	100/1000	no	N/A	0.02
83.0	1000.0	FD_all	0.0	12.0	component-wise	1.00e - 03	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	1.0	12.0	component-wise	1.55e - 03	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	2.0	12.0	component-wise	5.25e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	3.0	12.0	component-wise	9.26e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	4.0	12.0	component-wise	7.38e - 04	100/1000	no	N/A	2.39
83.0	1000.0	FD_all	5.0	12.0	component-wise	7.86e - 04	100/1000	no	N/A	2.43
83.0	1000.0	FD_all	0.0	12.0	constant	9.39e - 04	100/1000	no	N/A	2.22
83.0	1000.0	FD_all	1.0	12.0	constant	8.57e - 04	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	2.0	12.0	constant	6.44e - 04	100/1000	no	N/A	2.31
83.0	1000.0	FD_all	3.0	12.0	constant	8.04e - 04	100/1000	no	N/A	2.19
83.0	1000.0	FD_all	4.0	12.0	constant	6.72e - 04	100/1000	no	N/A	2.16
83.0	1000.0	FD_all	5.0	12.0	constant	7.45e - 04	100/1000	no	N/A	2.02
83.0	1000.0	FD_all	0.0	4.0	component-wise	1.05e - 03	100/1000	no	N/A	2.32
83.0	1000.0	FD_all	1.0	4.0	component-wise	1.62e - 03	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	2.0	4.0	component-wise	5.22e - 04	100/1000	no	N/A	2.45
83.0	1000.0	FD_all	3.0	4.0	component-wise	9.54e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	4.0	4.0	component-wise	7.10e - 04	100/1000	no	N/A	2.47
83.0	1000.0	FD_all	5.0	4.0	component-wise	7.93e - 04	100/1000	no	N/A	2.23
83.0	1000.0	FD_all	0.0	4.0	constant	9.36e - 04	100/1000	no	N/A	2.29
83.0	1000.0	FD_all	1.0	4.0	constant	8.87e - 04	100/1000	no	N/A	2.5
83.0	1000.0	FD_all	2.0	4.0	constant	6.83e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	3.0	4.0	constant	9.16e - 04	100/1000	no	N/A	2.28
83.0	1000.0	FD_all	4.0	4.0	constant	6.62e - 04	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	5.0	4.0	constant	7.78e - 04	100/1000	no	N/A	2.26
83.0	1000.0	FD_all	0.0	8.0	component-wise	9.84e - 04	100/1000	no	N/A	2.44
83.0	1000.0	FD_all	1.0	8.0	component-wise	1.56e - 03	100/1000	no	N/A	2.4
83.0	1000.0	FD_all	2.0	8.0	component-wise	5.18e - 04	100/1000	no	N/A	2.17
83.0	1000.0	FD_all	3.0	8.0	component-wise	9.96e - 04	100/1000	no	N/A	2.33
83.0	1000.0	FD_all	4.0	8.0	component-wise	7.31e - 04	100/1000	no	N/A	2.34
83.0	1000.0	FD_all	5.0	8.0	component-wise	8.18e - 04	100/1000	no	N/A	2.3
83.0	1000.0	FD_all	0.0	8.0	constant	9.58e - 04	100/1000	no	N/A	2.18
83.0	1000.0	FD_all	1.0	8.0	constant	8.60e - 04	100/1000	no	N/A	2.14
83.0	1000.0	FD_all	2.0	8.0	constant	7.59e - 04	100/1000	no	N/A	2.26

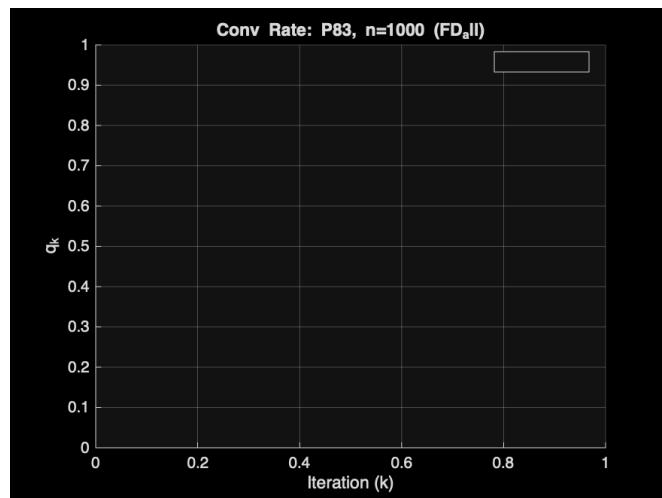


Figure 69: Problem 83, Truncated Newton, full FD (constant  $h$ ,  $k = 12$ ): experimental convergence rate for converged runs ( $n = 1000$ ).

## 10 Analysis of the results

## References

- [1] Jorge Nocedal and Stephen Wright. *Numerical Optimization*. Springer Science & Business Media, 2006.