



Energy Conversion I

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Desk D216



Layout

- Non isolated choppers
- Switch mode power supplies
- **Power components**
 - Passive components
 - Coil
 - Transformer
 - Capacitor
 - Active components
 - Diodes
 - Transistors

**Passive
components**

**Active
components**

Passive components

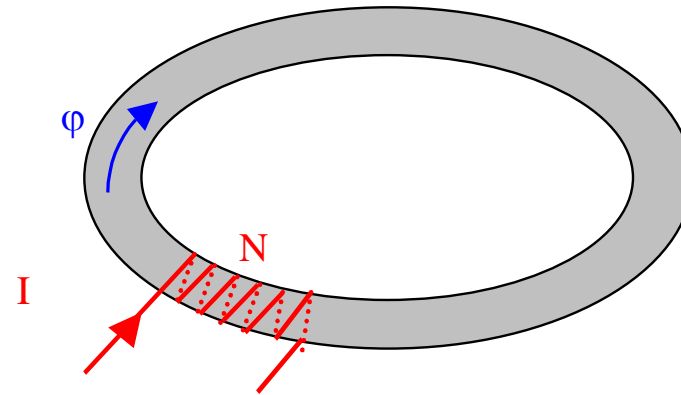
Passive components

Coil

Transformer
Capacitor

Active components

Iron core coil



$\phi = B.S$: elementary flux (real flux)

$\Phi = N.\phi = L.I$: “total flux” (sawn by the electrical circuit)

$$\int_{\text{circuit}} \mathbf{H} \cdot d\mathbf{l} = N.I$$

$$\mathbf{H} = \frac{\mathbf{B}}{\mu}$$

$$N.I = \left[\int_{\text{circuit}} \frac{dl}{\mu.S} \right] \cdot \phi = R.\phi$$

$$L_1 = \frac{N^2}{R} = N^2 \cdot A_L$$

Passive
components

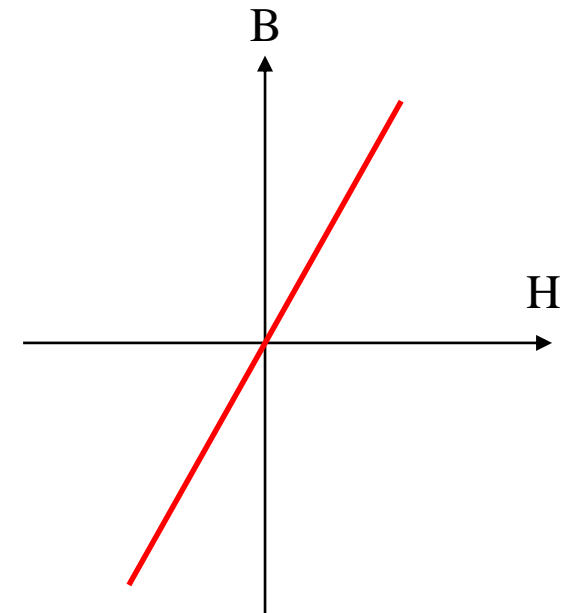
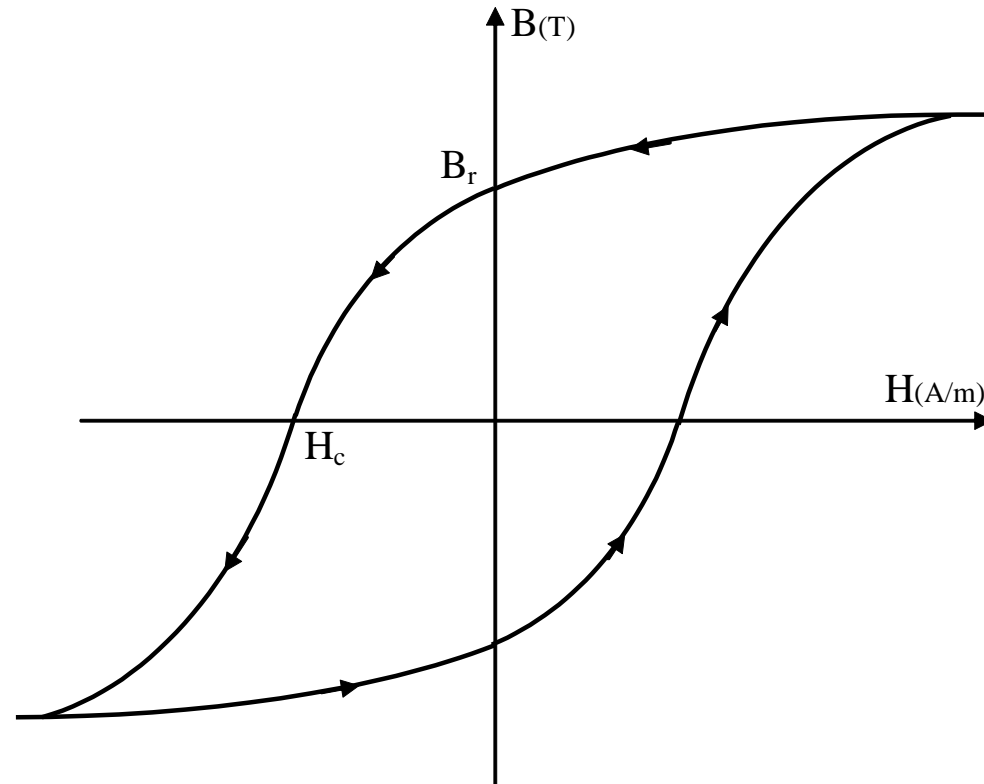
Coil

Transformer

Capacitor

Active
components

Hysteresis



*Ideal
Characteristic*

Stored energy – Air-gap

Magnetic energy density stored

$$\omega_{mag} = \frac{B^2}{2 \cdot \mu_0 \cdot \mu_r}$$

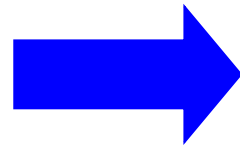
Example : Ferrinox B52

$$B = 0,4 \text{ T}$$

$$\omega_{mag} = 32 \text{ J/m}^3$$

$$\mu = \mu_0 \cdot \mu_r = 2,5 \cdot 10^{-3} \text{ H.m}^{-1}$$

$$\text{Air-gap : } \mu_0 = 4\pi \cdot 10^{-7} \text{ H.m}^{-1} \quad \omega_{mag} = 65 \text{ kJ/m}^3$$



Store energy in the air-gap

Passive components

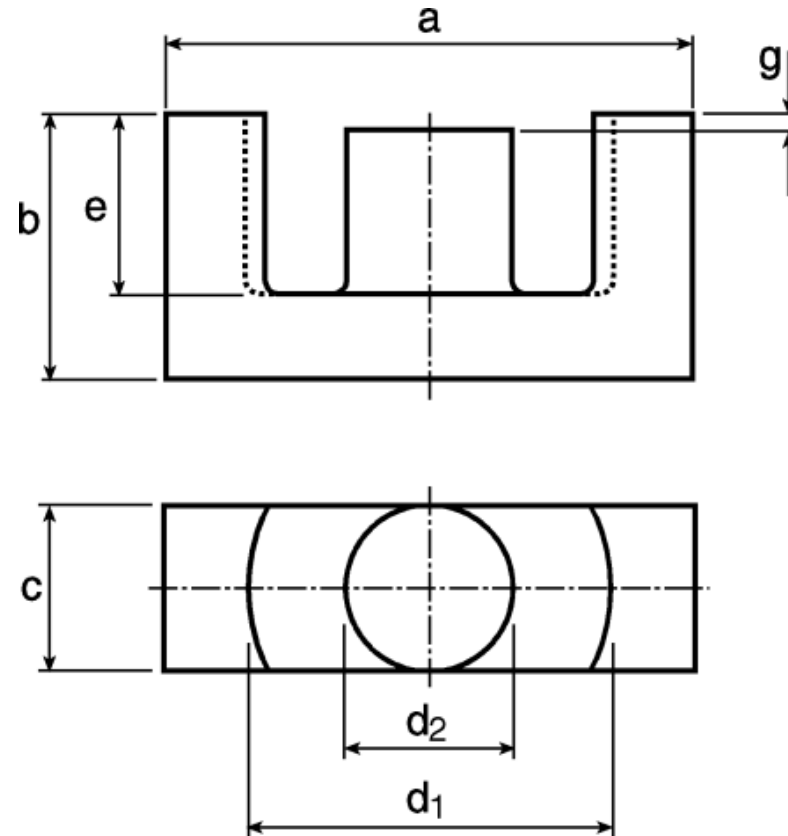
Coil

Transformer

Capacitor

Active components

Magnetic circuit example



ETD series

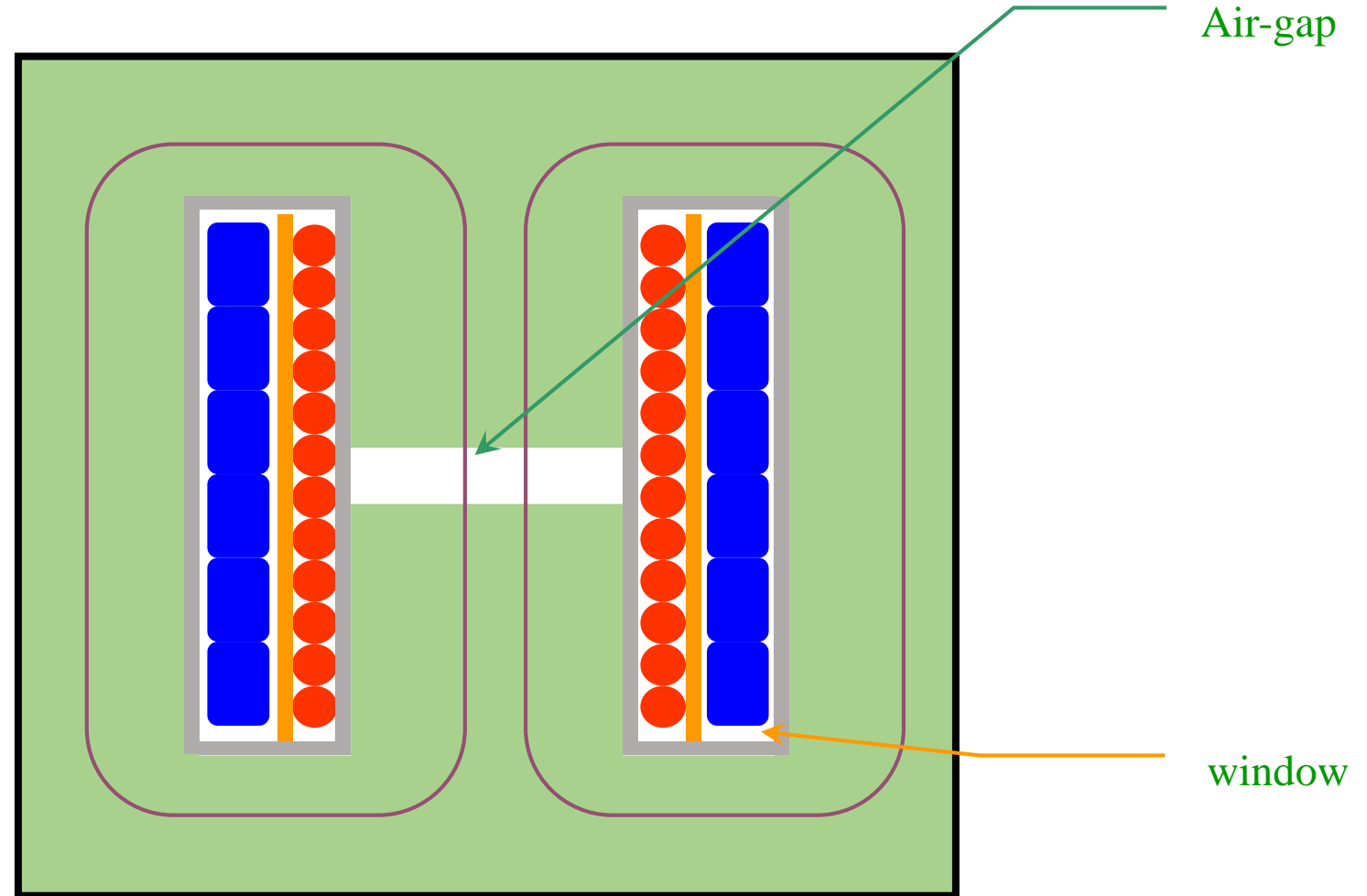


Passive components

Coil
Transformer
Capacitor

Active components

With air-gap

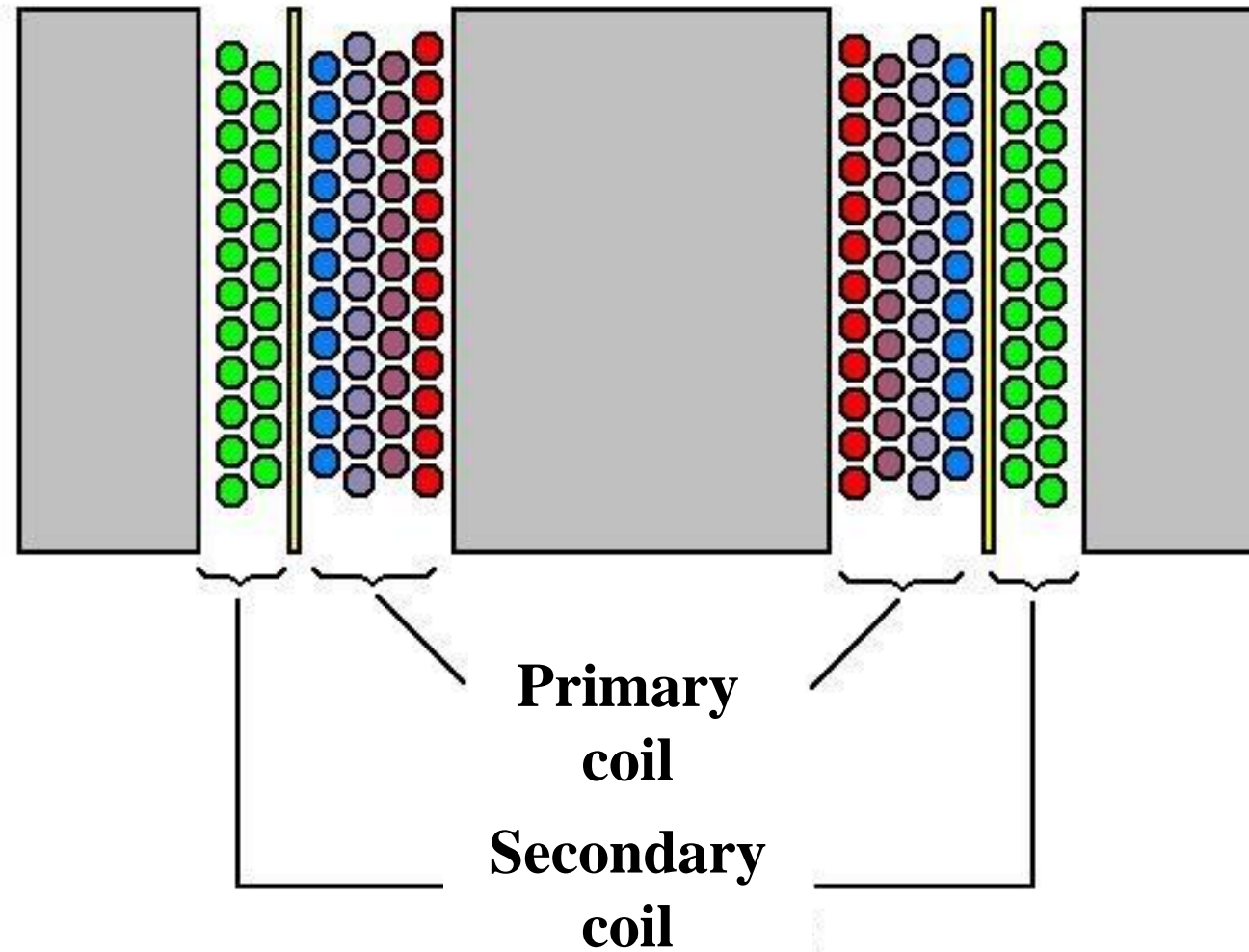


Passive components

Coil
Transformer
Capacitor

Active components

For a Forward : closed core



Passive components

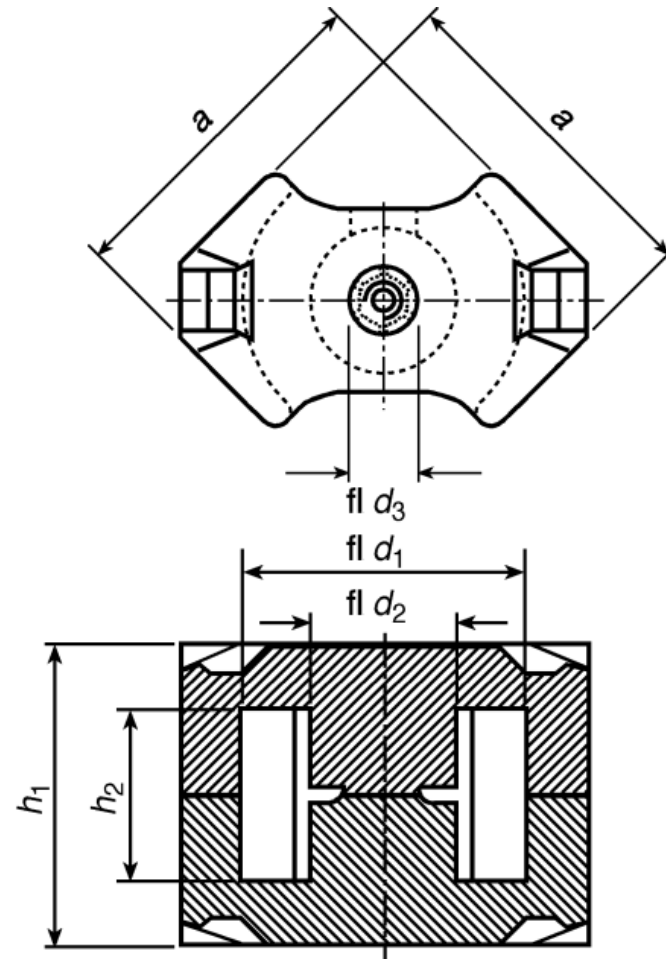
Coil

Transformer

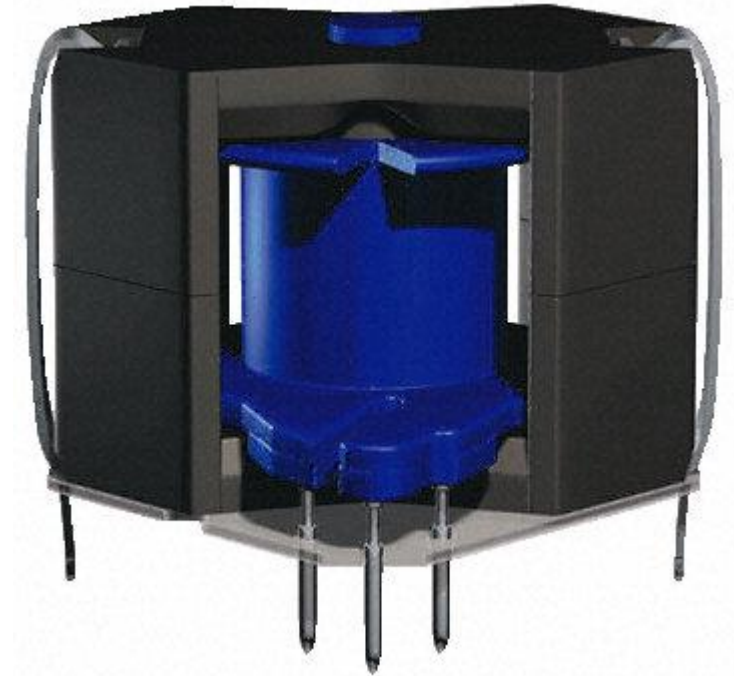
Capacitor

Active components

Magnetic pot core



RM- 8- bis RM-14-Kernstze
fr nichtlineare Drosselspulen



RM series

Passive components

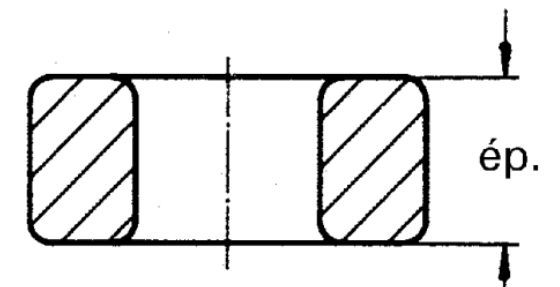
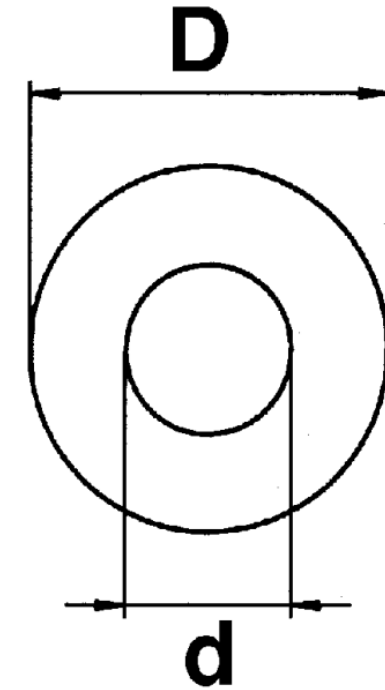
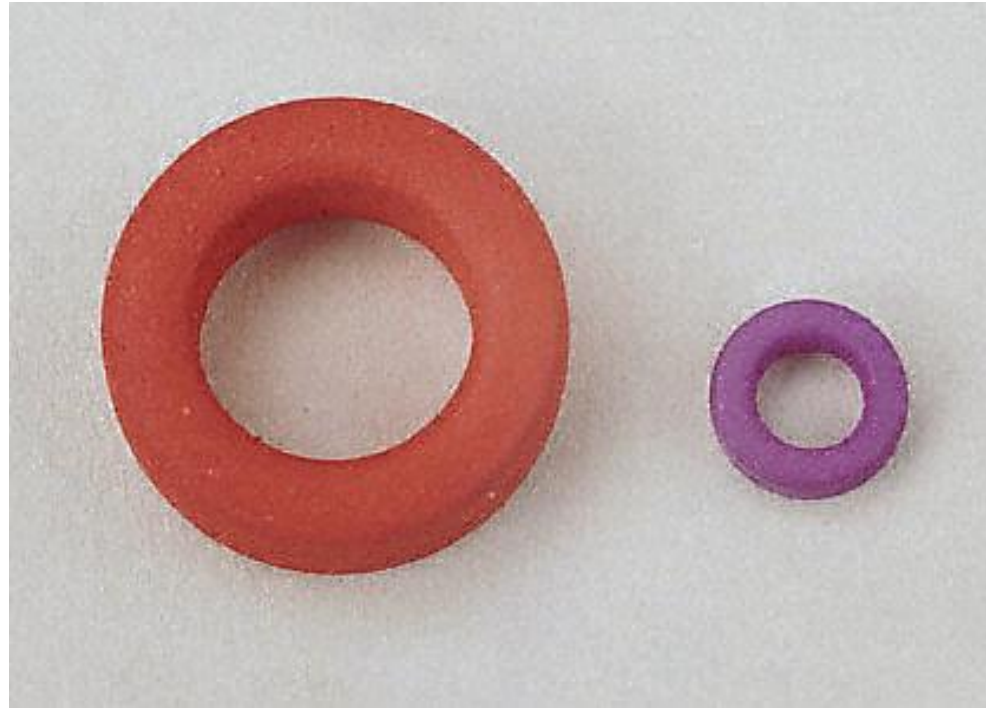
Coil

Transformer

Capacitor

Active components

Torus



Passive components

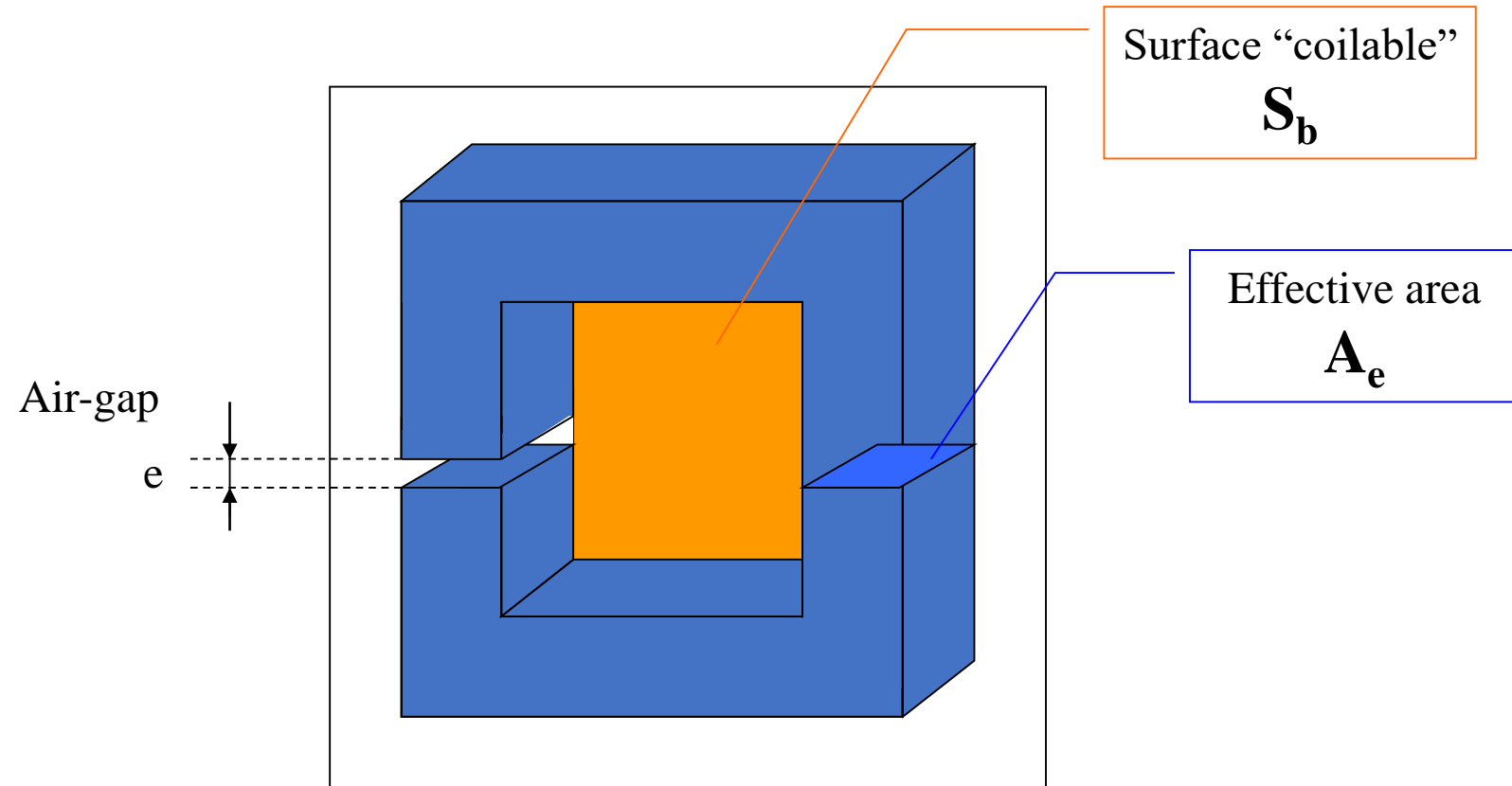
Coil

Transformer

Capacitor

Active components

Magnetic circuits parameters



Inductance factor: $\mathbf{A_L}$ = Inductance obtained with ONE loop

Passive components

Coil

Transformer

Capacitor

Active components

Critical constraints

*Induction in the material: $B < B_{sat}$
0,2 to 0,5 T for classical materials*

*Current density in the coil: $\delta < \delta_{max}$
5 A/mm² for copper*

Sizing : product $A_e \cdot S_b$

Passive components

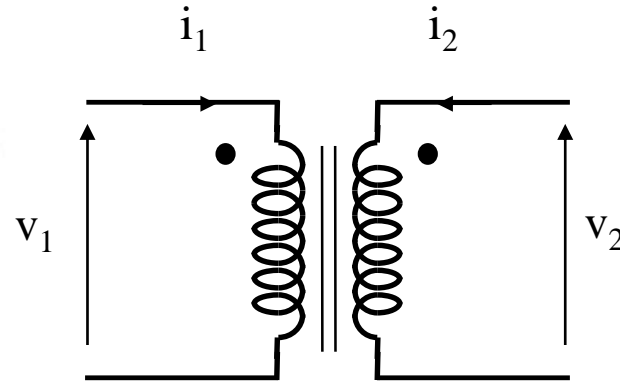
Coil

Transformer

Capacitor

Active components

Transformer



Primary : N_1 turns
Secondary : N_2 turns

Winding direction

$$v_1 = N_1 \cdot \frac{d\phi}{dt}$$

$$v_2 = N_2 \cdot \frac{d\phi}{dt}$$

$$m = \frac{N_2}{N_1} = \frac{v_2}{v_1}$$

$$\oint H \cdot dl = R \cdot \phi = N_1 \cdot i_1 + N_2 \cdot i_2$$

Magnetizing current i_{10} : Hopkinson's law

$$R \cdot \phi = N_1 \cdot i_{10}$$

$$\Phi = L_1 \cdot i_{10} \quad L_1 = \frac{N_1^2}{R}$$

$$i_1 + m \cdot i_2 = i_{10}$$

$$v_1 = L_1 \cdot \frac{di_{10}}{dt}$$

Passive components

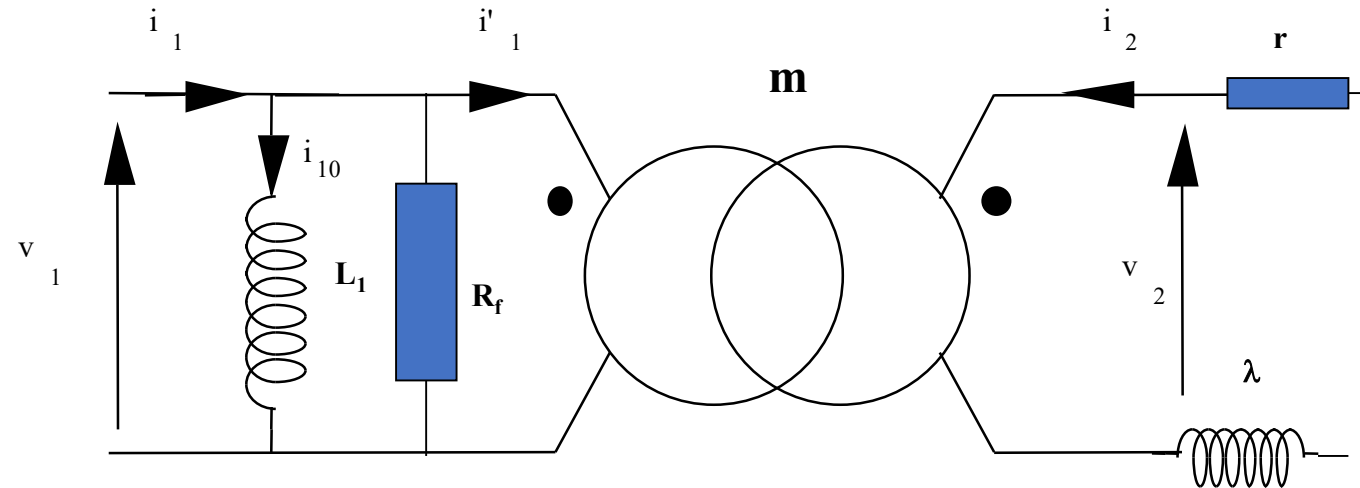
Coil

Transformer

Capacitor

Active components

Transformer : equivalent scheme



L_1 : Magnetizing inductance (at primary side)

R_f : ferromagnetic losses

r : Joule loss (or ohmic loss)

λ : leakage inductance

Passive components

Coil

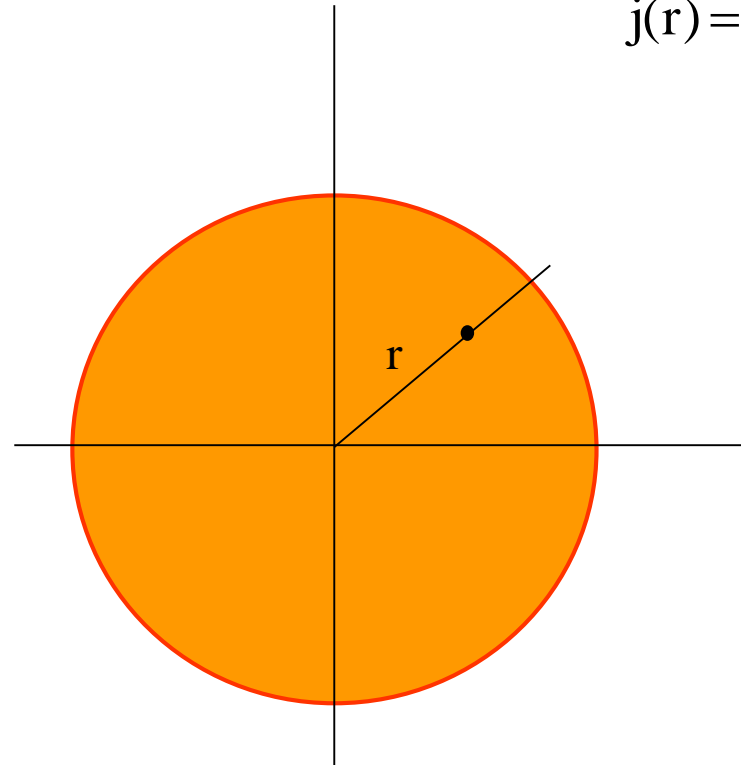
Transformer

Capacitor

Active components

Skin effect

$$j(r) = j \cdot J_0 \left(e^{i\pi \frac{r}{\delta}} \right).$$



$$\delta = \frac{1}{\sqrt{\pi \cdot \sigma \cdot \mu \cdot f}}$$

- δ : skin depth thickness
- σ : conductivity
- μ : permeability
- f : frequency

Passive components

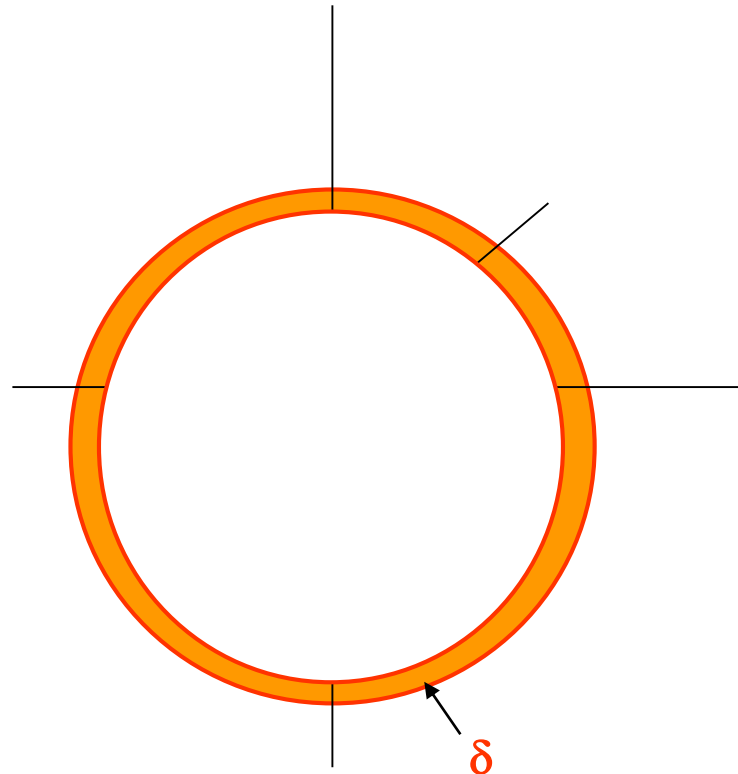
Coil

Transformer

Capacitor

Active components

Skin effect



Copper at 25°C

➤ 50 Hz : $\delta = 9,4$ mm

➤ 100 kHz : $\delta = 0,21$ mm

=> *Multi strand wire, Litz wire*

Passive components

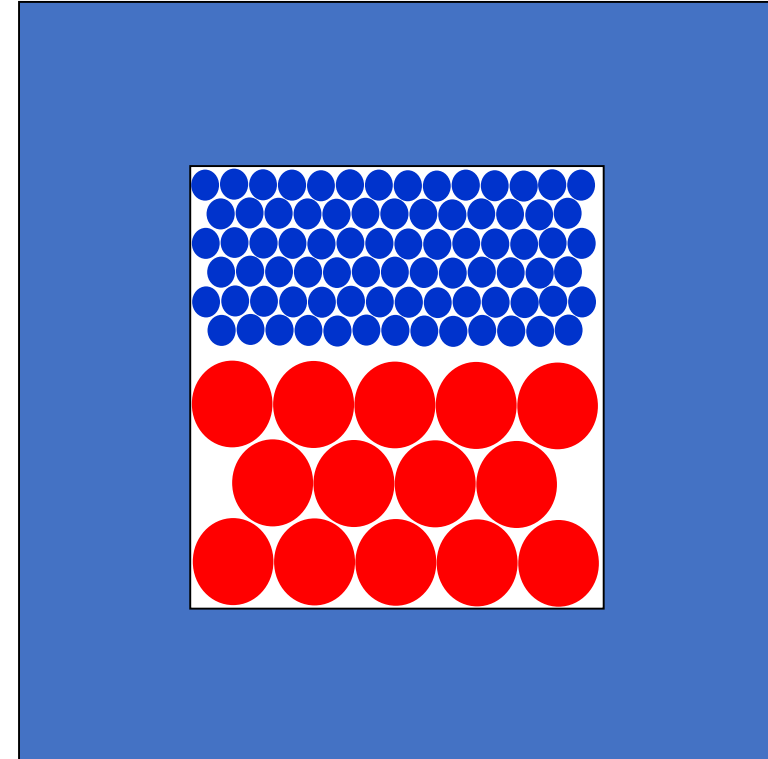
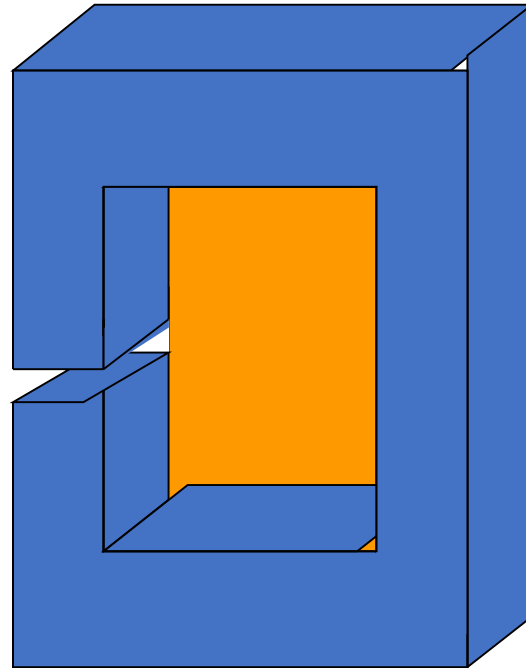
Coil

Transformer

Capacitor

Active components

Winding



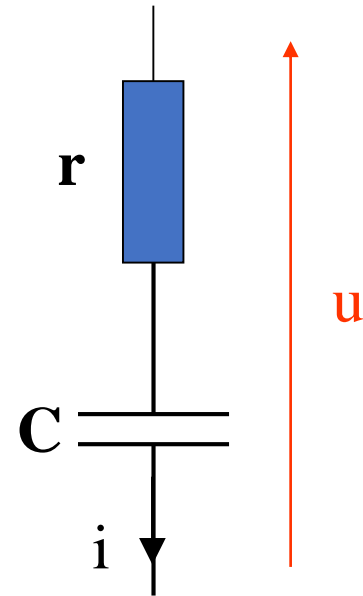
$$k_B = 0,7$$

Passive components

Coil
Transformer
Capacitor

Active components

Capacitors



Losses in the capacitor

$$P = r \cdot I_{\text{eff}}^2$$

Rated voltage: U_{eff}

r : ESR (Equivalent Series Resistor)

Multiple technologies : depends on the frequency

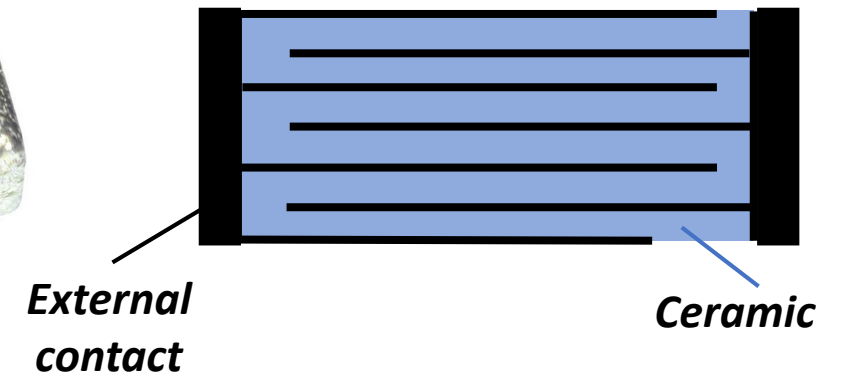
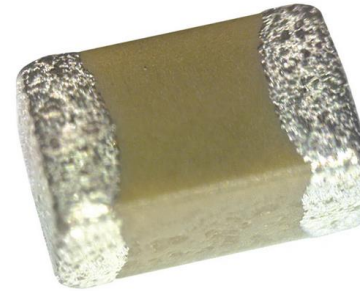
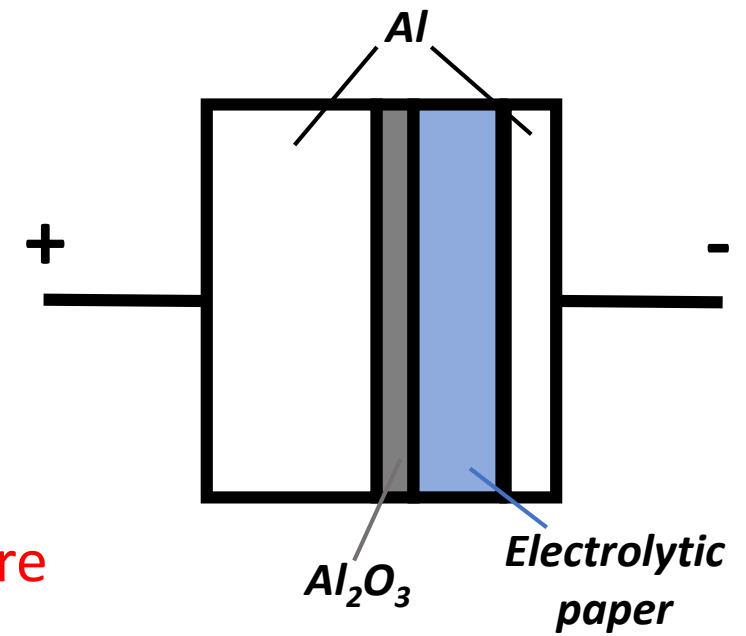
Passive components

Coil
Transformer
Capacitor

Active components

Capacitors

- Electrolytic
 - High voltage
 - Polarized -> DC voltage
 - Lifetime depends on temperature
- Ceramic
 - “low” values
 - High frequency
- Films
 - AC
 - Self-healing



Passive
components

Active
components

Active components

Passive components

Active components

Diodes

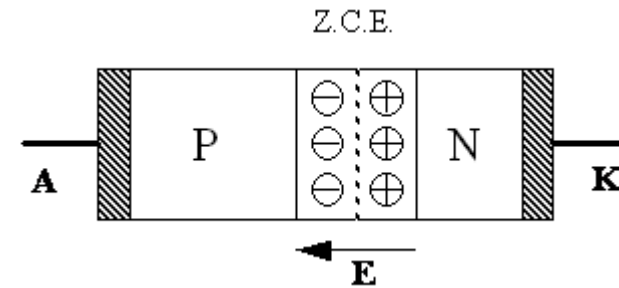
Bipolar transistor

MOS transistor

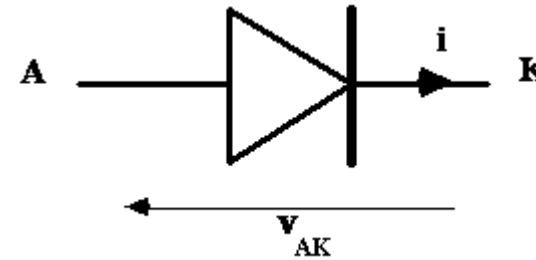
IGBT transistor

Active components

PN junction



Diode



$$i = I_S \left(e^{\frac{q \cdot v_{AK}}{k \cdot T}} - 1 \right)$$

Diode : static characteristic

I_0 : Average forward current, or I_F , I_{AV}

I_{FM} : Peak forward current

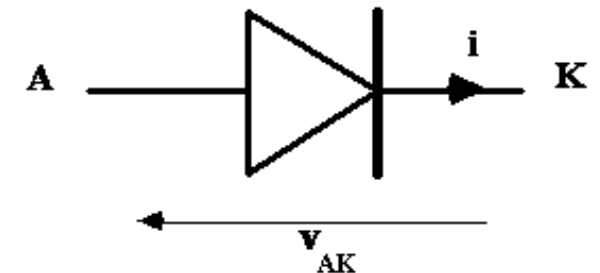
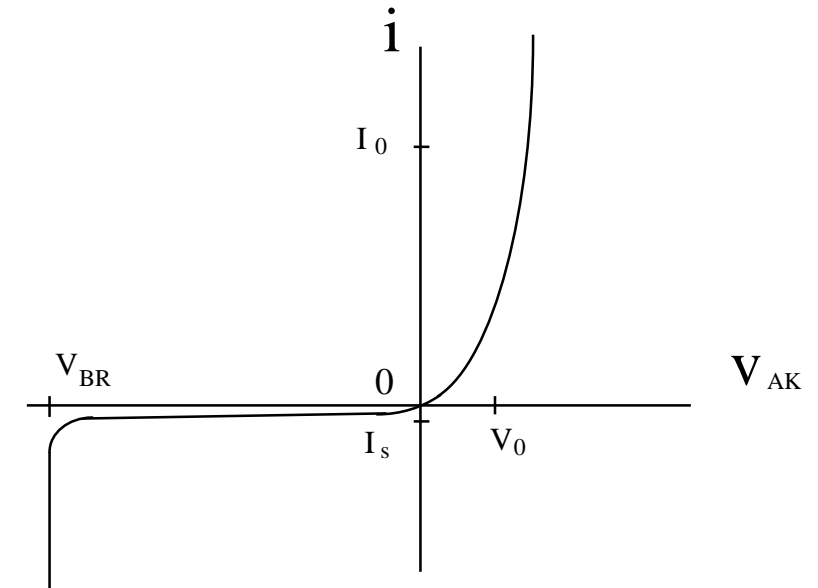
I_{FSM} : Peak forward surge current

I_{RRM} : Reverse repetitive current

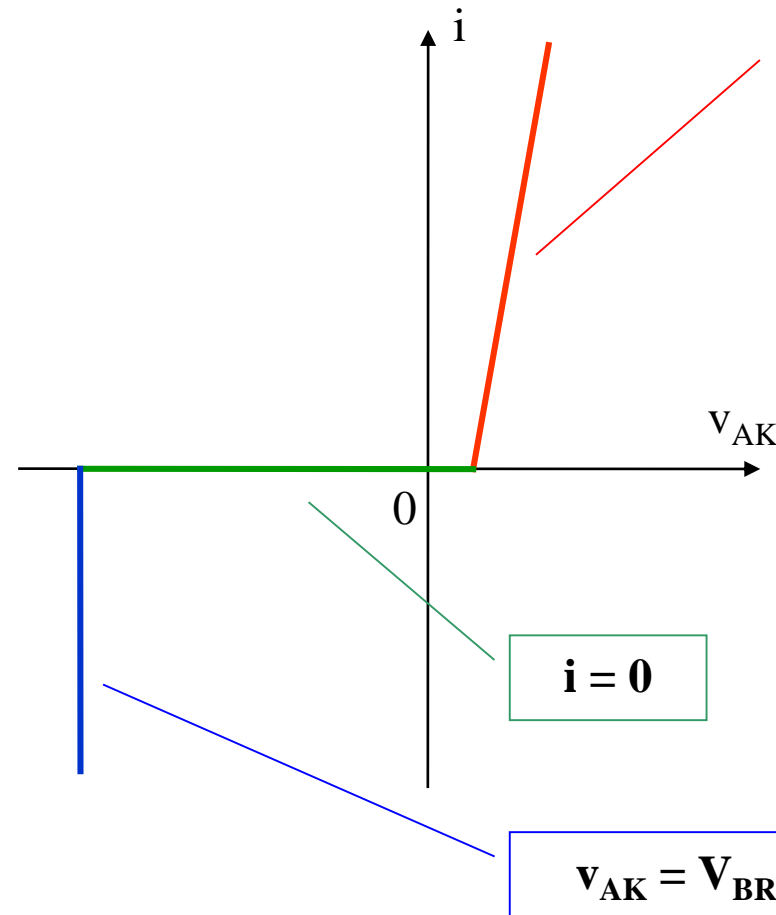
V_0 : Forward voltage or V_{FM}

V_{BR} : Breakdown reverse voltage

V_{RRM} : Peak repetitive reverse voltage



Diode : simplified static characteristics



$$V_{AK} = r_{on} \cdot i + V_0$$

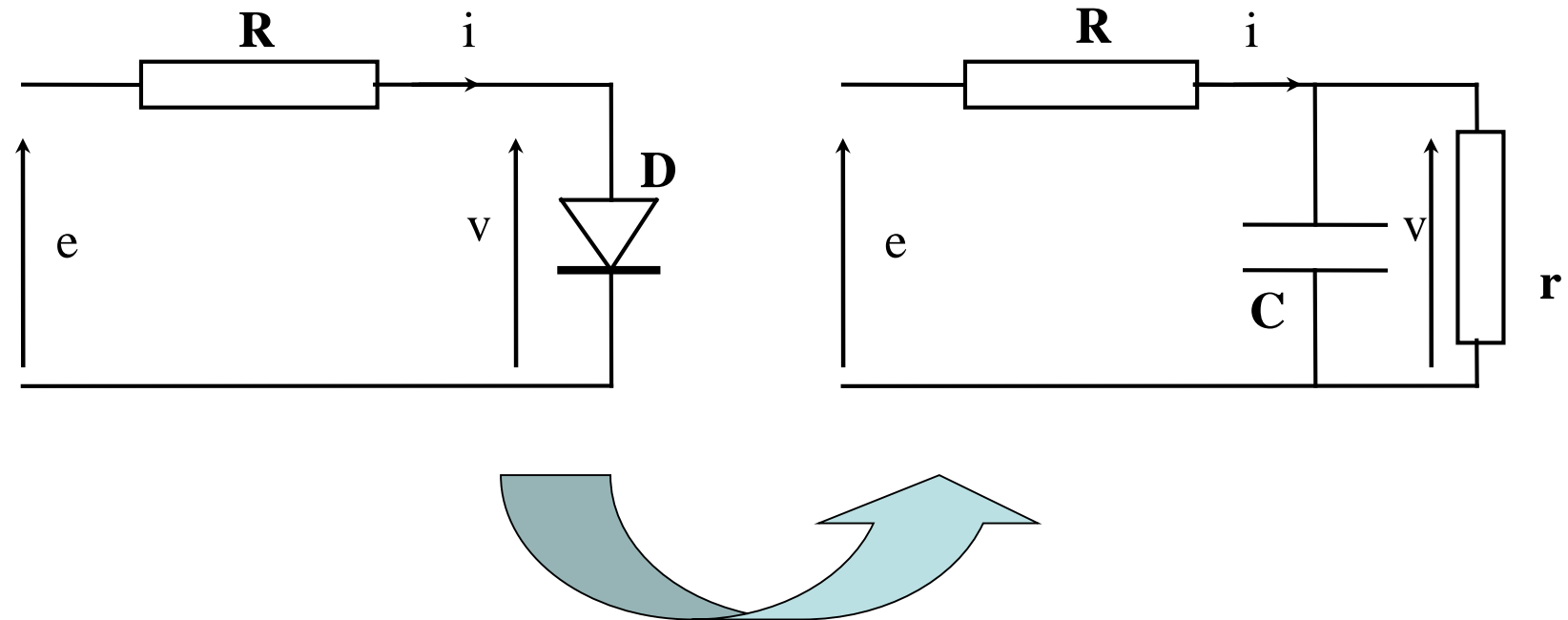
*Linearized characteristic
3 segments*



Conduction loss calculation

$$P_c = r_{on} \cdot I_{eff}^2 + V_0 \cdot I_{av}$$

Diode on commutation mode: equivalent scheme



Passive components

Active components

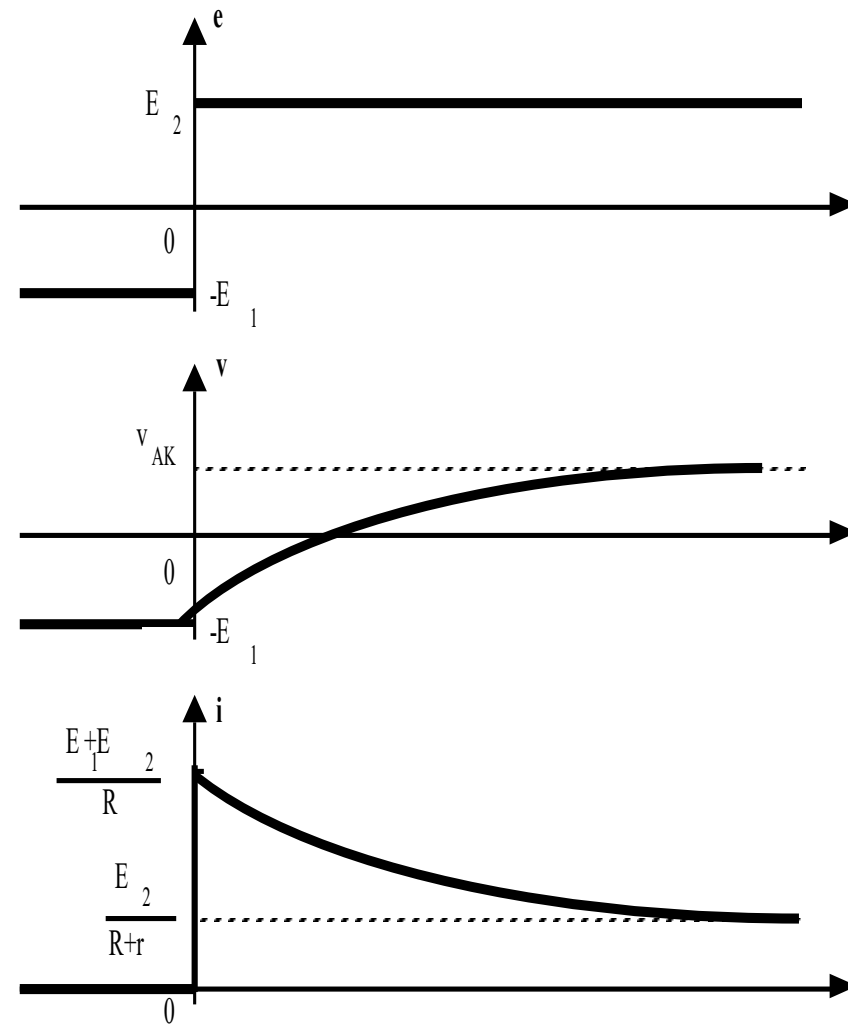
Diodes

Bipolar transistor

MOS transistor

IGBT transistor

Conduction switch



Passive components

Active components

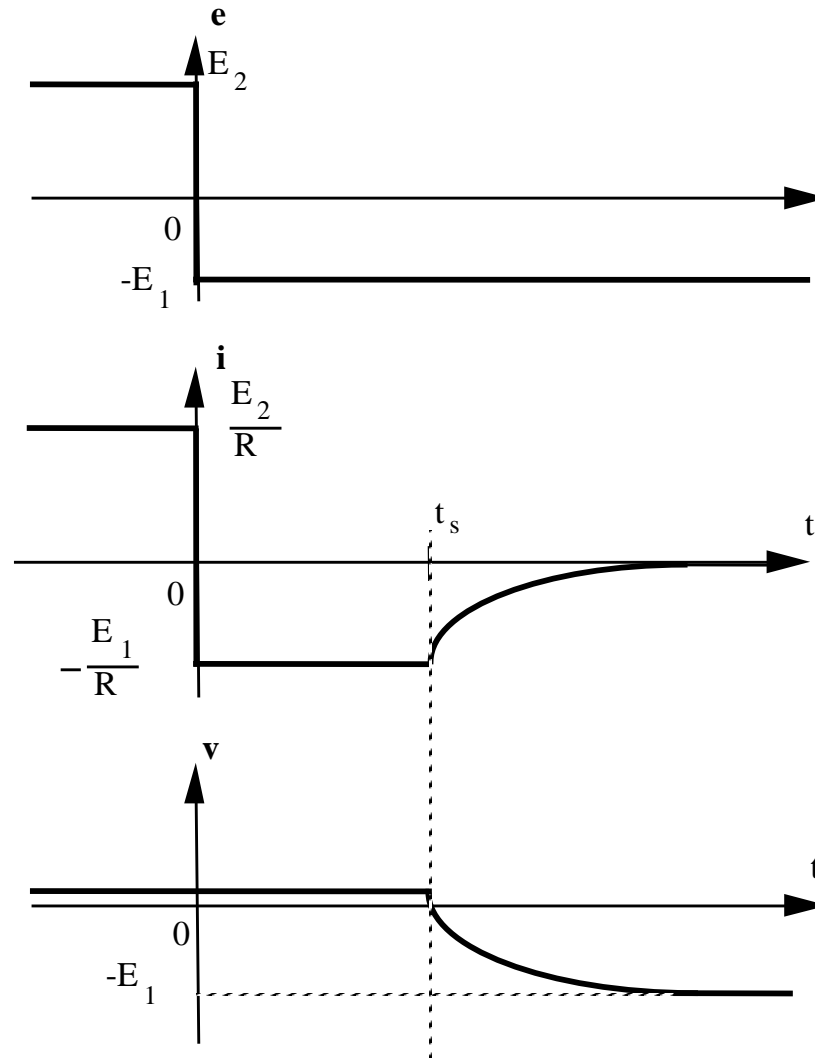
Diodes

Bipolar transistor

MOS transistor

IGBT transistor

« Ideal » turn off diode with voltage source



Passive components

Active components

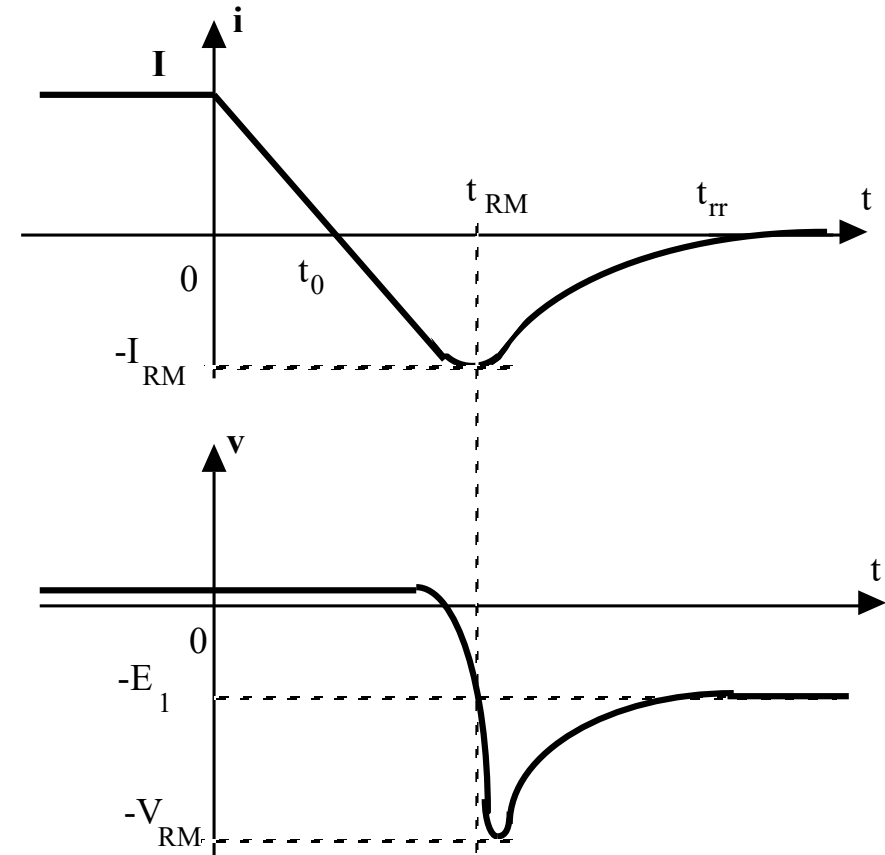
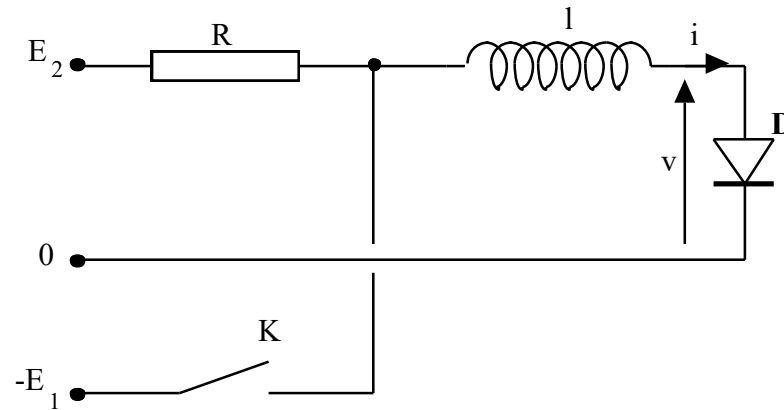
Diodes

Bipolar transistor

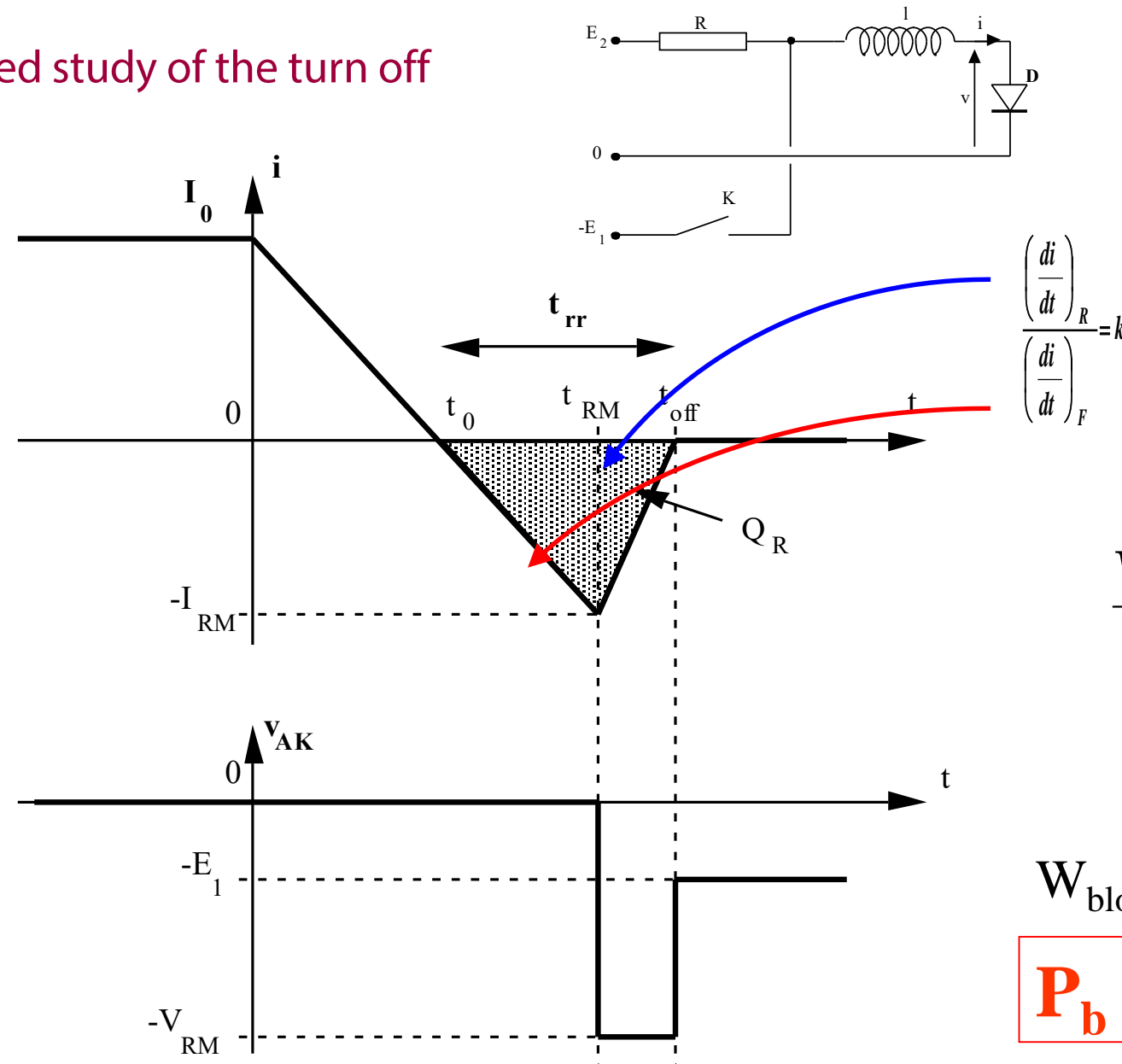
MOS transistor

IGBT transistor

Diode : « real » turn off



Simplified study of the turn off



$$\frac{V_{RM}}{E_1} = 1 + k$$

$$W_{bloc} = E_1 \cdot Q_R$$

$$P_b = f \cdot E_1 \cdot Q_R$$

Passive components

Active components

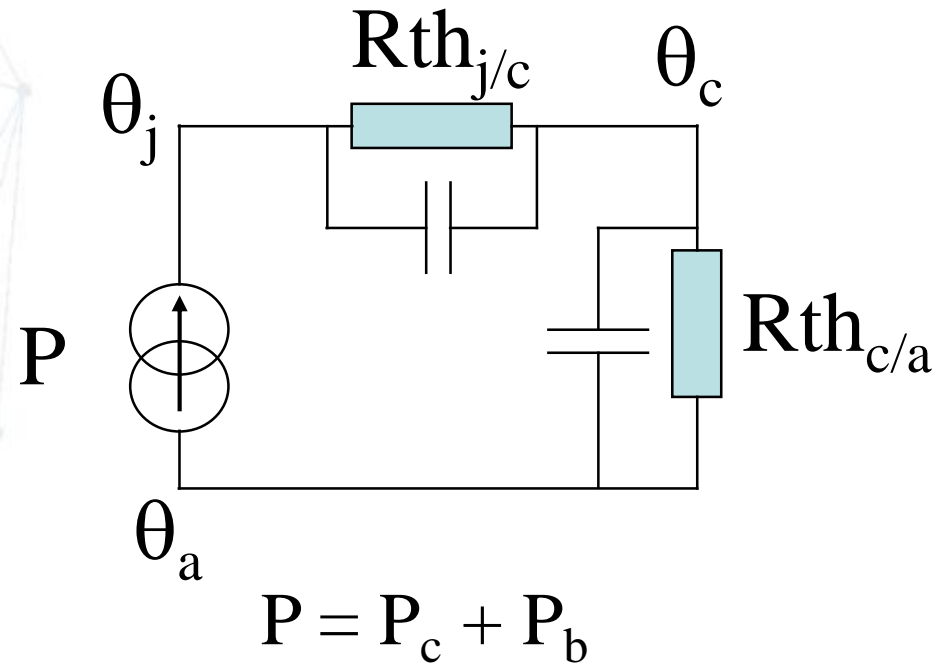
Diodes

Bipolar transistor

MOS transistor

IGBT transistor

Heat sink



$$\theta_j < \theta_{jmax}$$

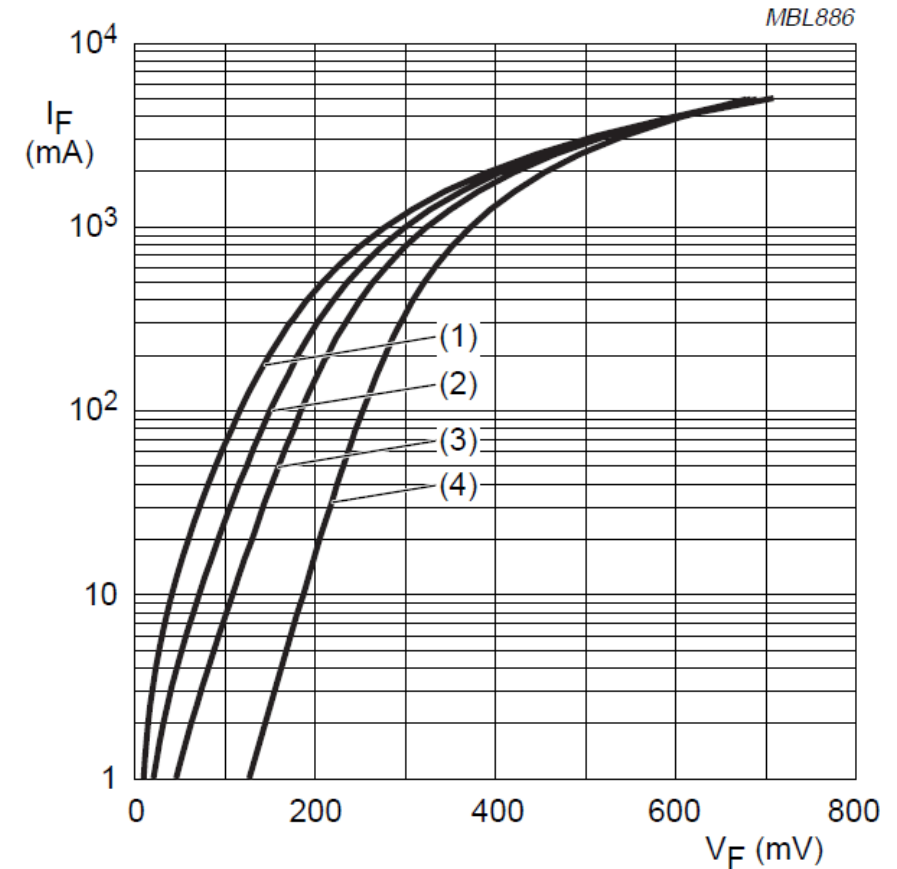
$Rth_{c/a}$ calculation



Specific diode

- *Low threshold diode: Schottky diode*
- *High voltage diode*
- *Power Zener diodes (« Transient-voltage-suppression diode »)*
- *Fast diodes (low Q_R)*
- *Light-emitting diodes (high threshold)*

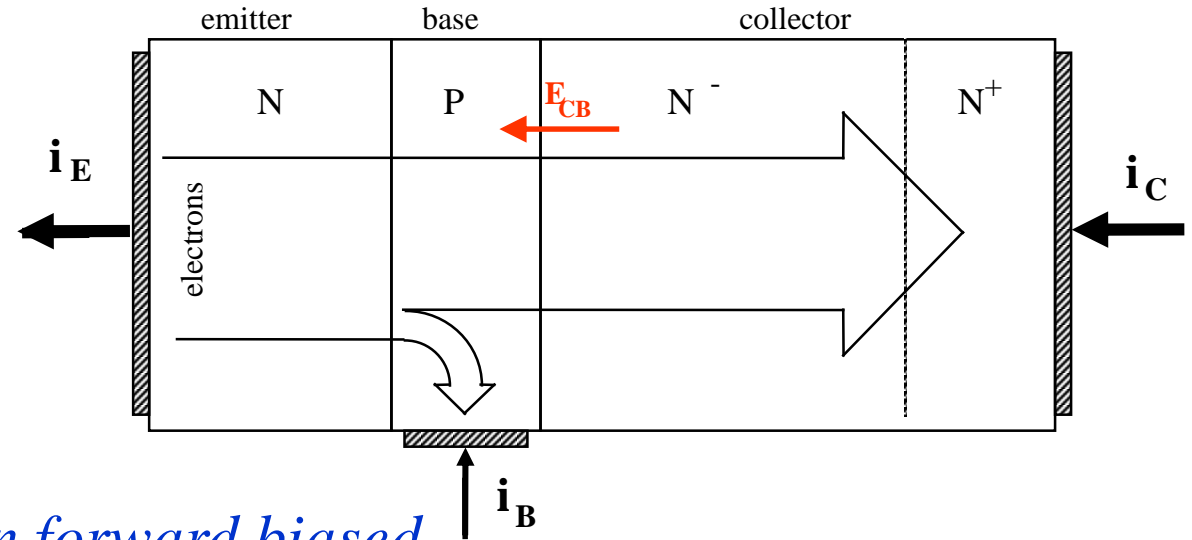
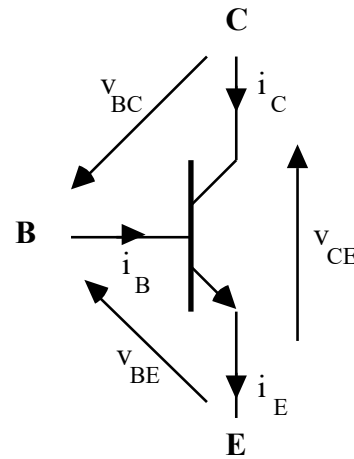
Schottky diode



- (1) $T_{amb} = 125\text{ }^{\circ}\text{C}.$
- (2) $T_{amb} = 100\text{ }^{\circ}\text{C}.$
- (3) $T_{amb} = 75\text{ }^{\circ}\text{C}.$
- (4) $T_{amb} = 25\text{ }^{\circ}\text{C}.$

Fig.2 Forward current as a function of forward voltage; typical values.

Bipolar power transistor



Base-emitter junction forward biased

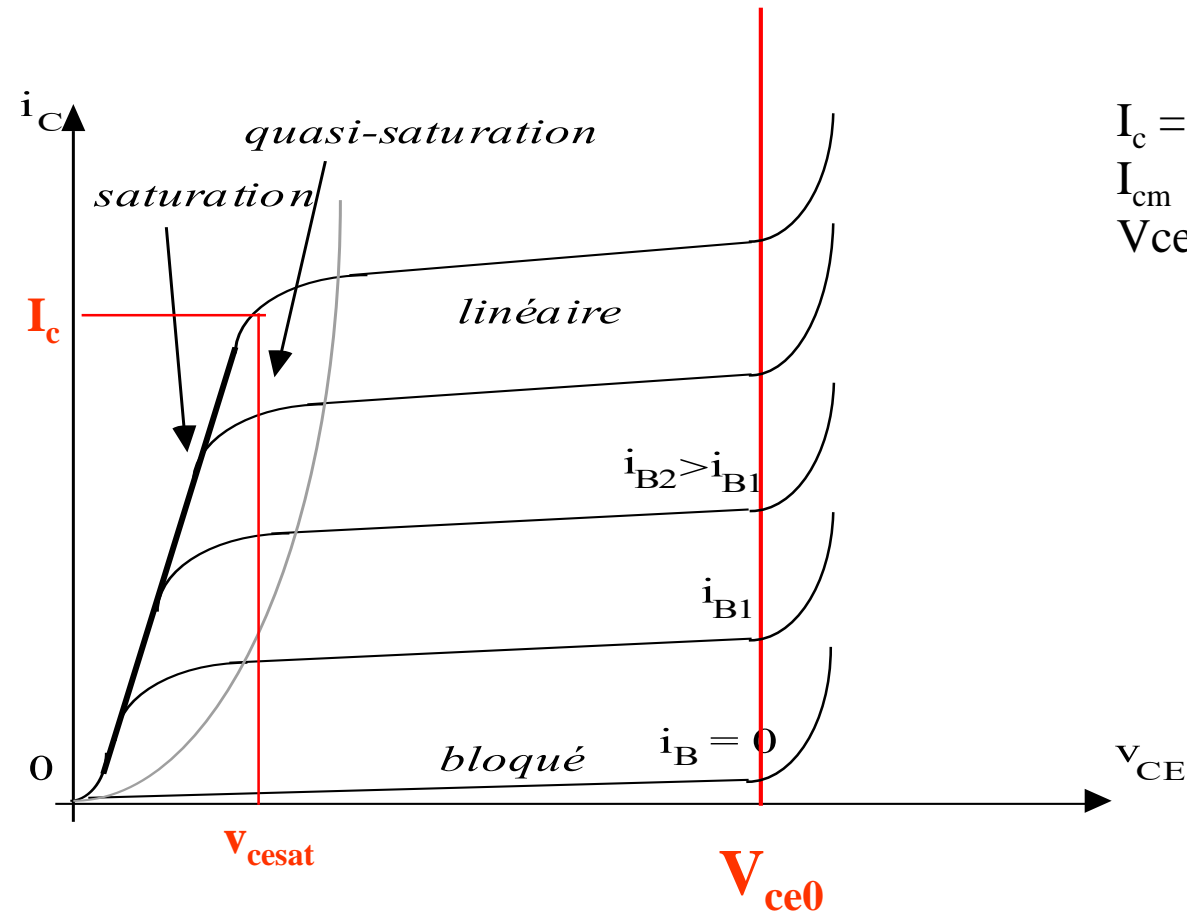
Base-collector junction reverse biased

$$i_C = \alpha \cdot i_E ; i_B = (1 - \alpha) \cdot i_E \quad \longrightarrow$$

$$\beta = \frac{\alpha}{1 - \alpha}$$

$$i_C = \beta \cdot i_B$$

Transistor characteristic



I_c = average current

I_{cm} : maximum forward current

$V_{ce_{sat}}$: saturation voltage

Conduction loss

$$P_c = V_{ce_{sat}} I_c \alpha$$

Passive components

Active components

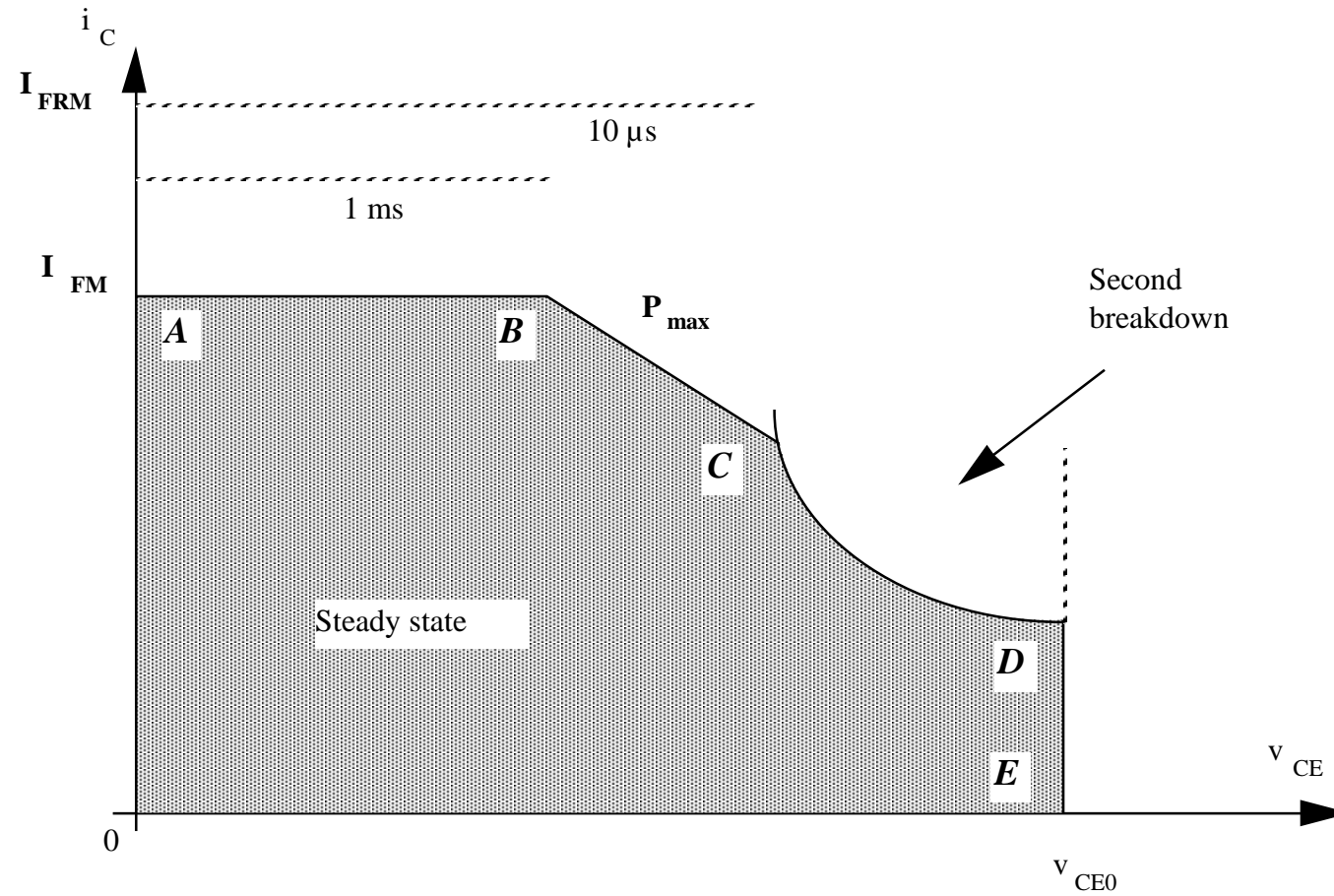
Diodes

Bipolar transistor

MOS transistor

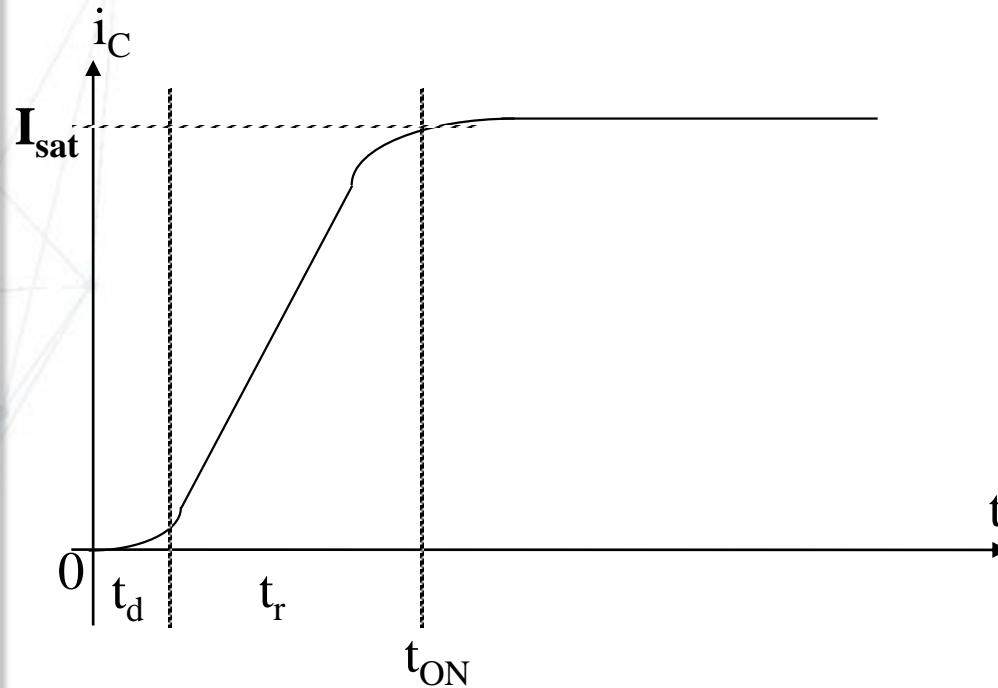
IGBT transistor

Transistor safety area

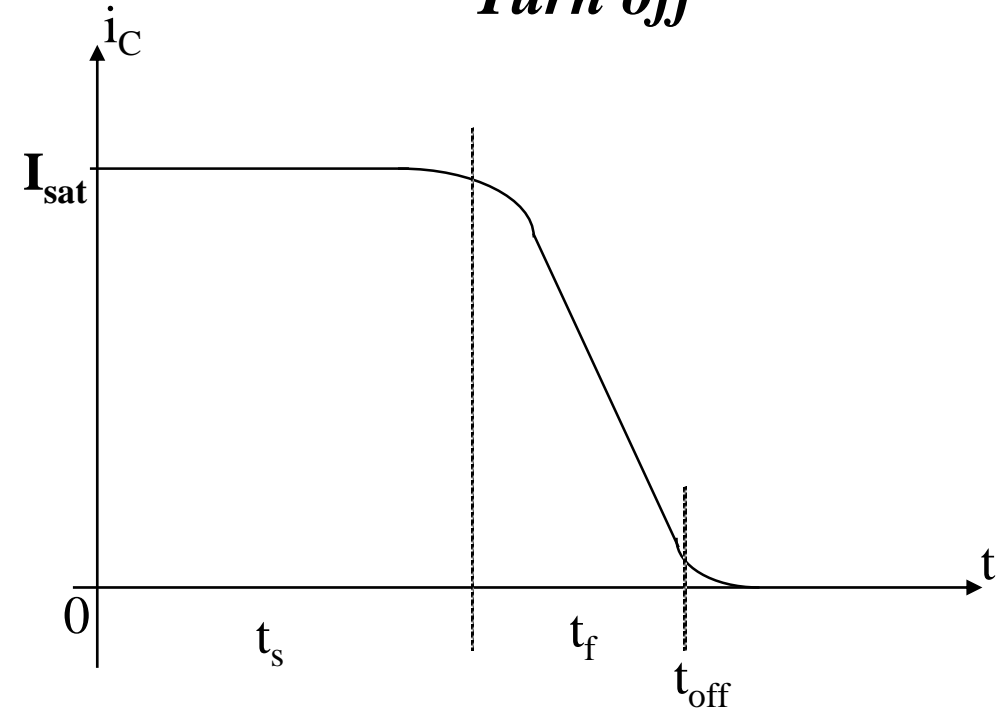


Transistor switching

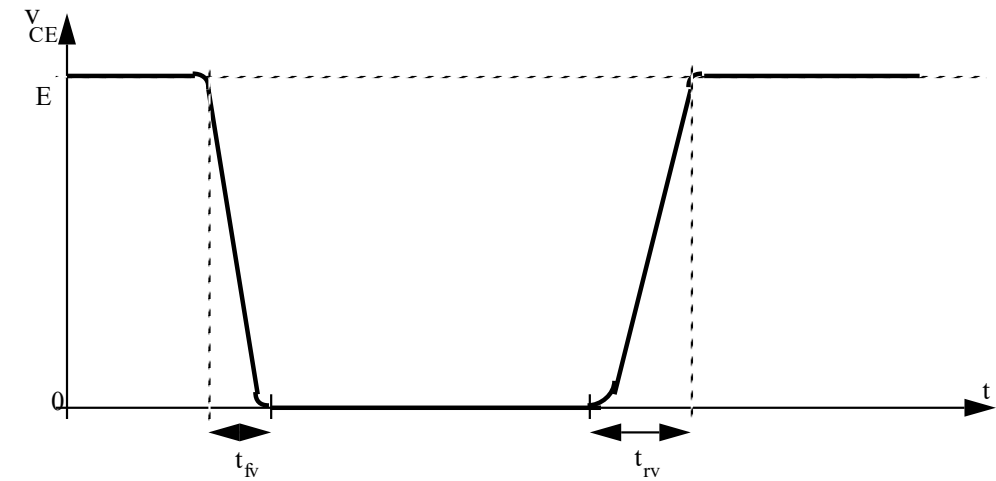
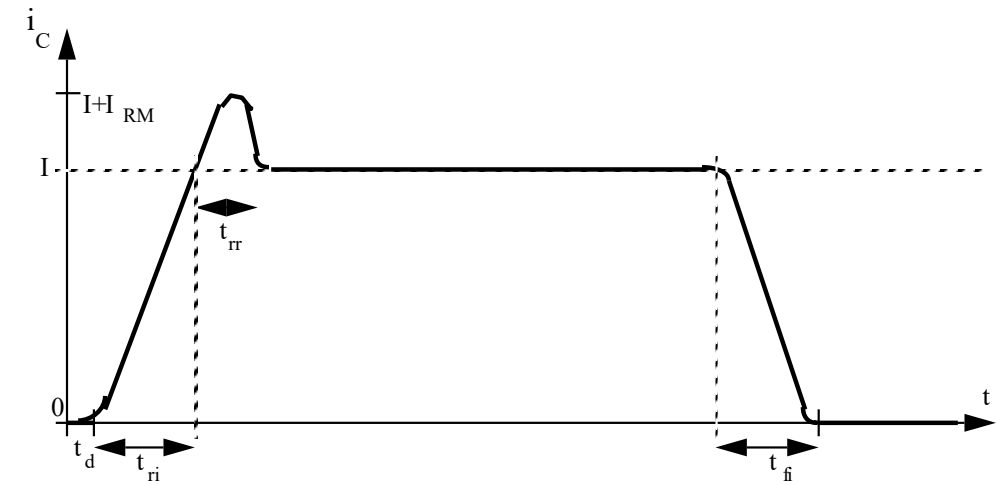
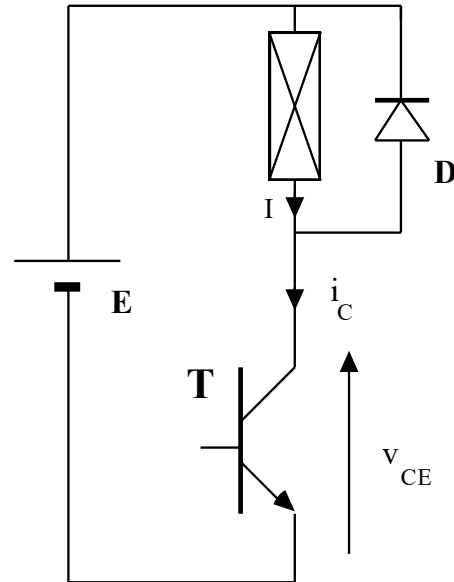
Turn on



Turn off



Switching cycle



$$P_f = \frac{1}{2} \cdot EI \cdot (t_{fv} + t_{ri}) \cdot f$$
$$P_b = \frac{1}{2} \cdot EI \cdot (t_{fi} + t_{rv}) \cdot f$$

Passive components

Active components

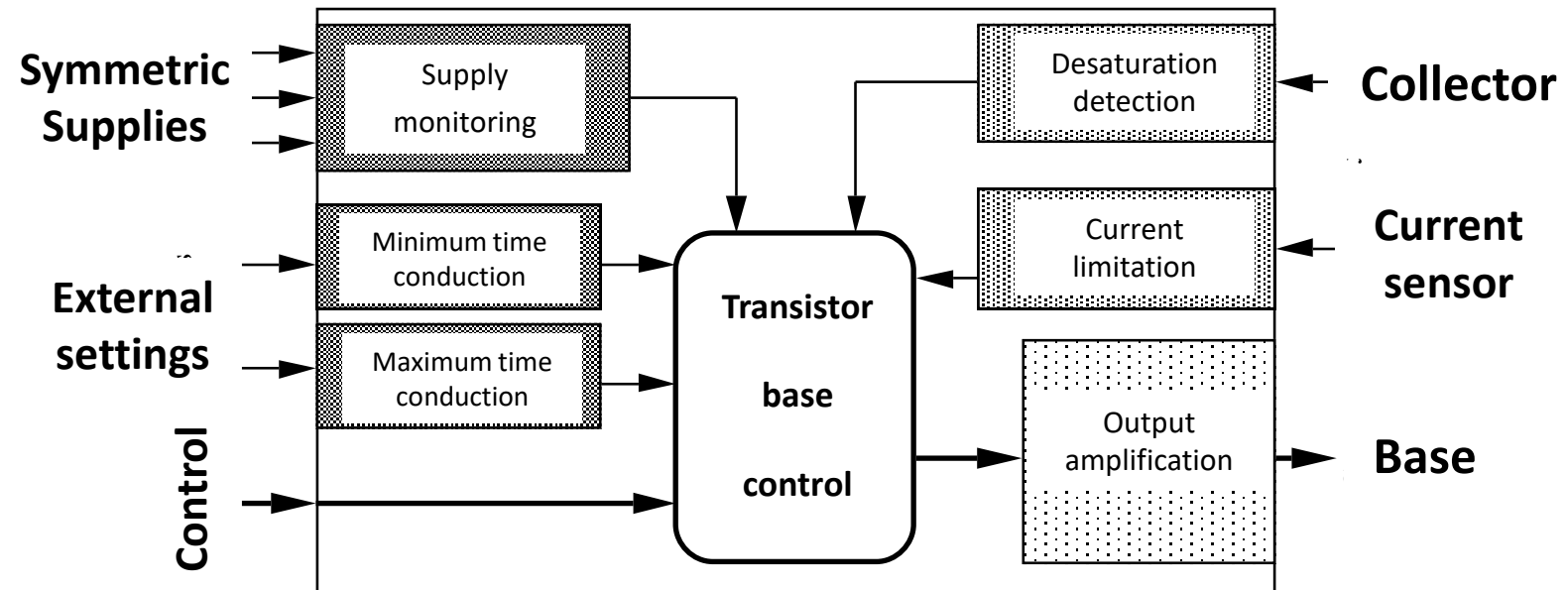
Diodes

Bipolar transistor

MOS transistor

IGBT transistor

Control circuit: driver



Passive components

Active components

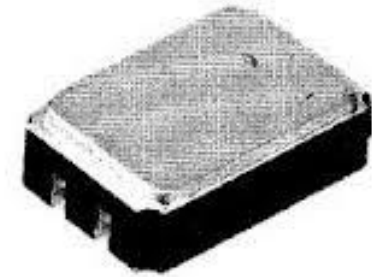
Diodes

Bipolar transistor

MOS transistor

IGBT transistor

Cases

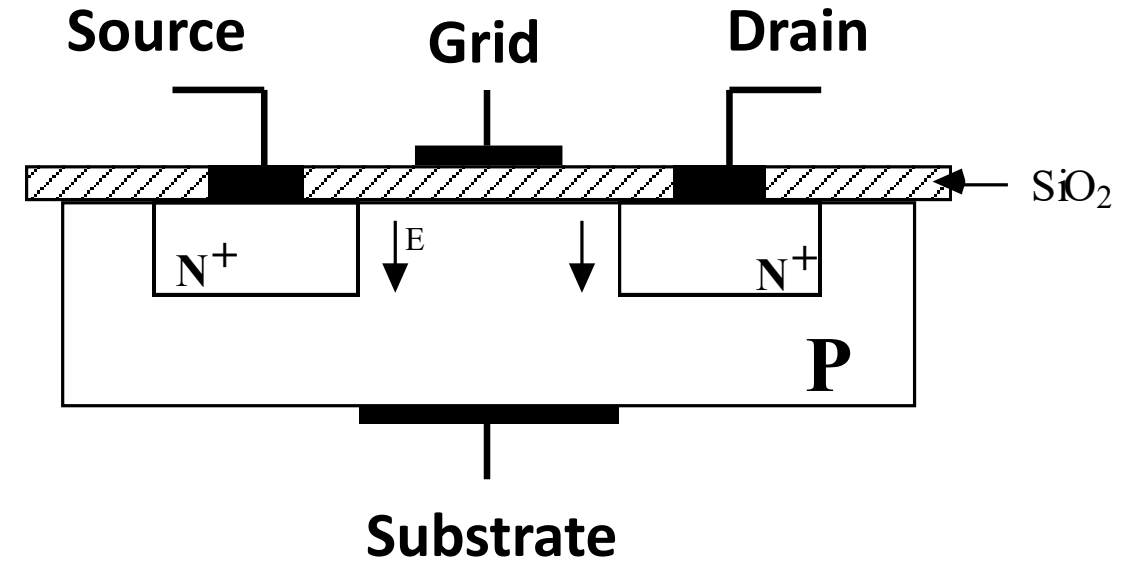
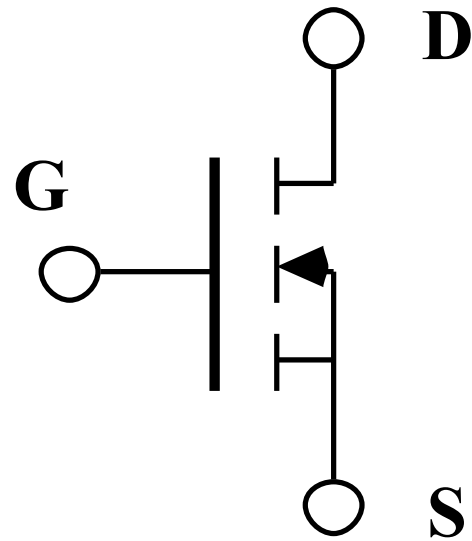


Passive components

Active components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

Power MOS

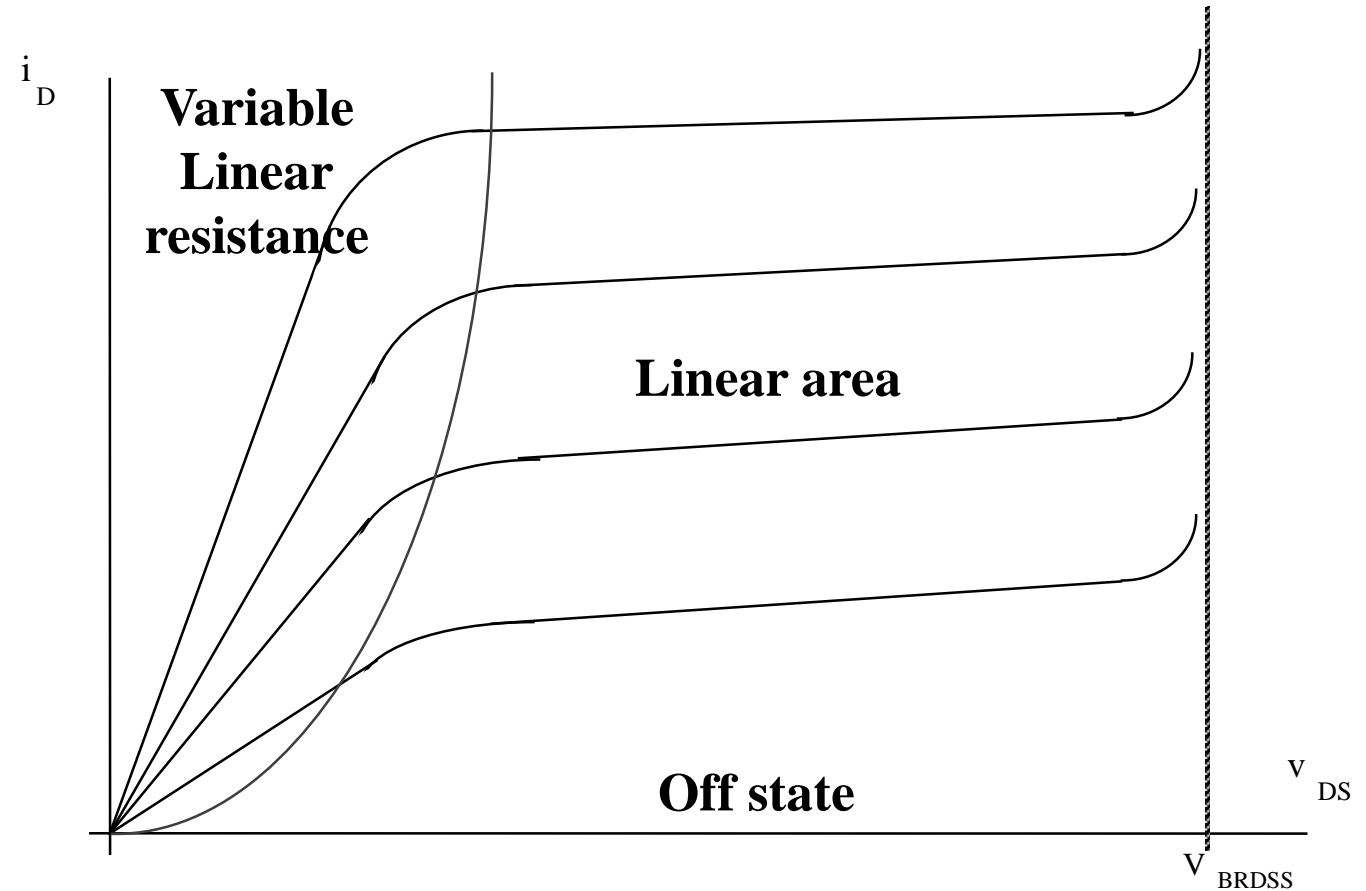


Passive components

Active components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

MOSFET characteristics

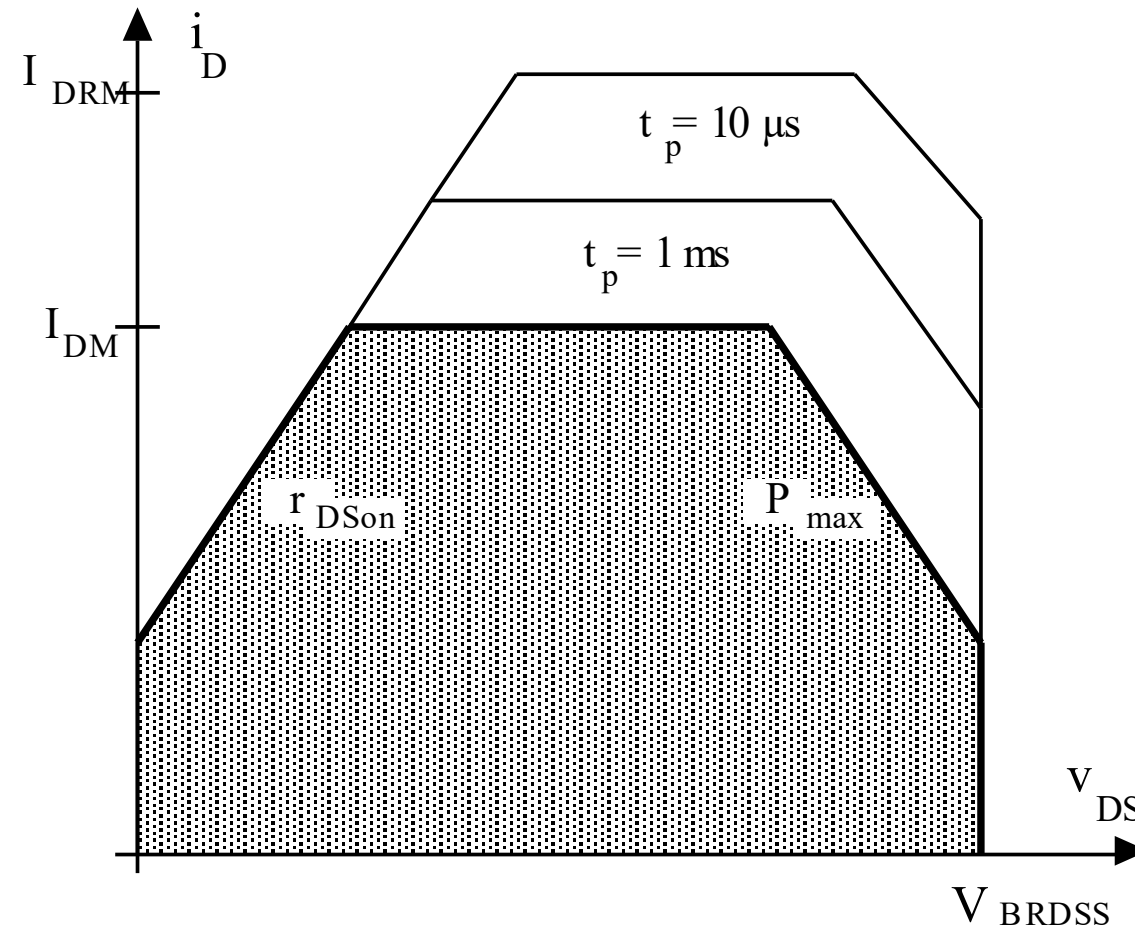


Passive components

Active components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

MOS safety area



Passive components

Active components

Diodes

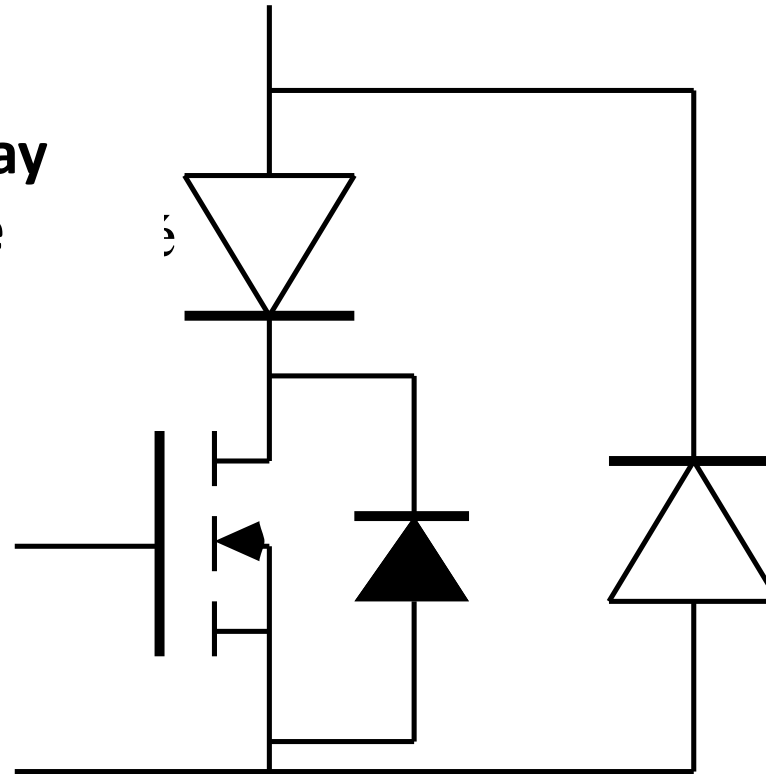
Bipolar transistor

MOS transistor

IGBT transistor

MOS parasitic diode

One-way diode



Free-wheeling diode

Passive
components

Active
components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

Bipolar-MOS comparison

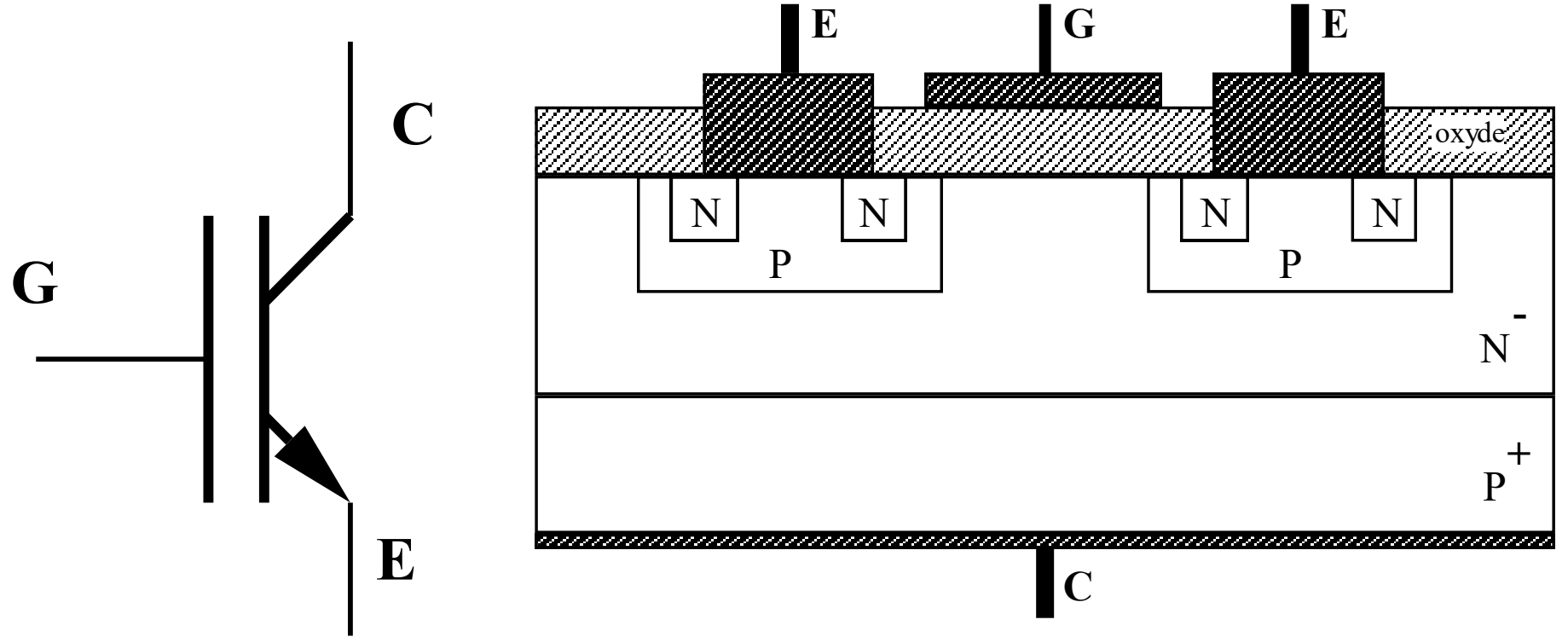
Criteria	Bipolar		MOSFET
Voltage withstand	1000 V	>	500 V
Switched current	few 100 A	>	few 10 A
Control speed	few kHz	<	few MHz
Ease of control	Current	<	Voltage
Safety circuit	Snubber	<	Zener
Conduction loss	few W	<	r_{DSon}
Switching loss (at fixed frequency)	few 10 W	>	few W

Passive components

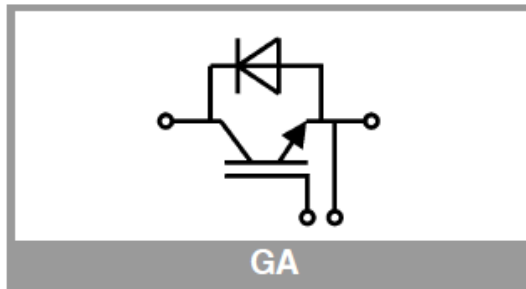
Active components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

I.G.B.T. : Insulated-Gate Bipolar Transistor

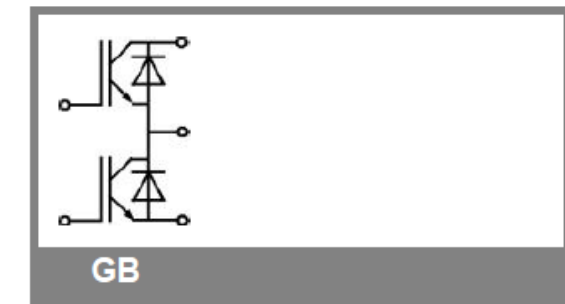


Power IGBT



Absolute Maximum Ratings				
Symbol	Conditions		Values	Unit
IGBT				
V _{CES}	T _j = 25 °C		1200	V
I _C	T _j = 175 °C	T _c = 25 °C	1305	A
		T _c = 80 °C	1003	A
I _{Cnom}			900	A

I.G.B.T. half bridge



Absolute Maximum Ratings				
Symbol	Conditions		Values	Unit
IGBT				
V_{CES}	$T_j = 25\text{ }^{\circ}\text{C}$		1200	V
I_C	$T_j = 175\text{ }^{\circ}\text{C}$	$T_c = 25\text{ }^{\circ}\text{C}$	422	A
		$T_c = 80\text{ }^{\circ}\text{C}$	324	A
I_{Cnom}			300	A
I_{CRM}	$I_{CRM} = 3 \times I_{Cnom}$		900	A

Characteristics						
Symbol	Conditions		min.	typ.	max.	Unit
$t_{d(on)}$	$V_{CC} = 600\text{ V}$	$T_j = 150\text{ }^{\circ}\text{C}$		220		ns
t_r	$I_C = 300\text{ A}$	$T_j = 150\text{ }^{\circ}\text{C}$		44		ns
E_{on}	$V_{GE} = \pm 15\text{ V}$	$T_j = 150\text{ }^{\circ}\text{C}$		27		mJ
$t_{d(off)}$	$R_{G\ on} = 1.5\ \Omega$	$T_j = 150\text{ }^{\circ}\text{C}$		520		ns
t_f	$di/dt_{on} = 6100\text{ A}/\mu\text{s}$	$T_j = 150\text{ }^{\circ}\text{C}$		117		ns
E_{off}	$di/dt_{off} = 3000\text{ A}/\mu\text{s}$	$T_j = 150\text{ }^{\circ}\text{C}$		39		mJ
$R_{th(j-c)}$	per IGBT				0.11	K/W

Passive components

Active components

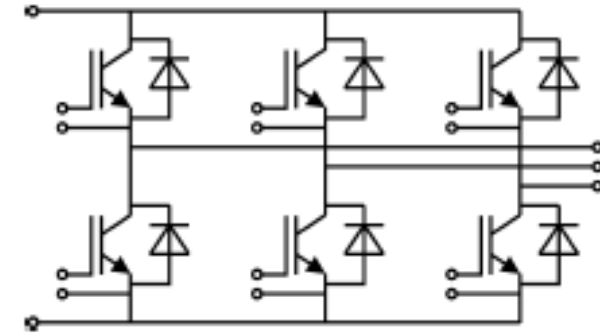
Diodes
Bipolar transistor
MOS transistor
IGBT transistor

Modules



SEMTRANS® 6

1200 V – 39 A at 25°C – $t_f < 200\text{ns}$



GD



SEMiX® 13

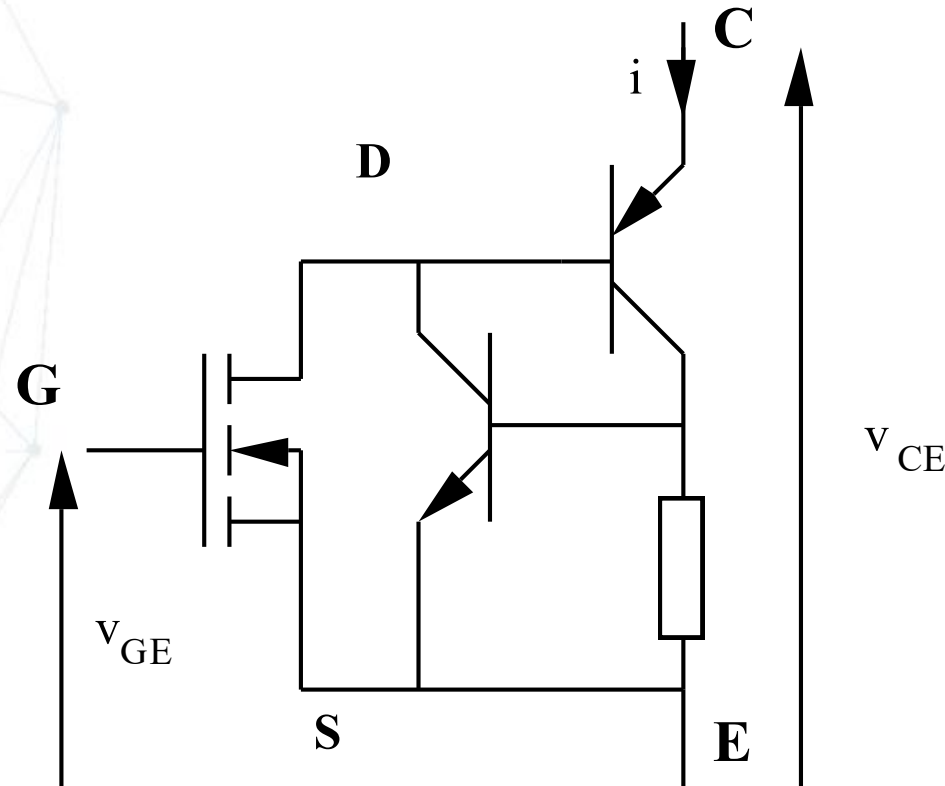
1200 V – 231 A at 25°C – $t_f < 500\text{ns}$

Passive
components

Active
components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

IGBT equivalent scheme



Control: MOS's one
Forward voltage: bipolar
Voltage withstand: MOS

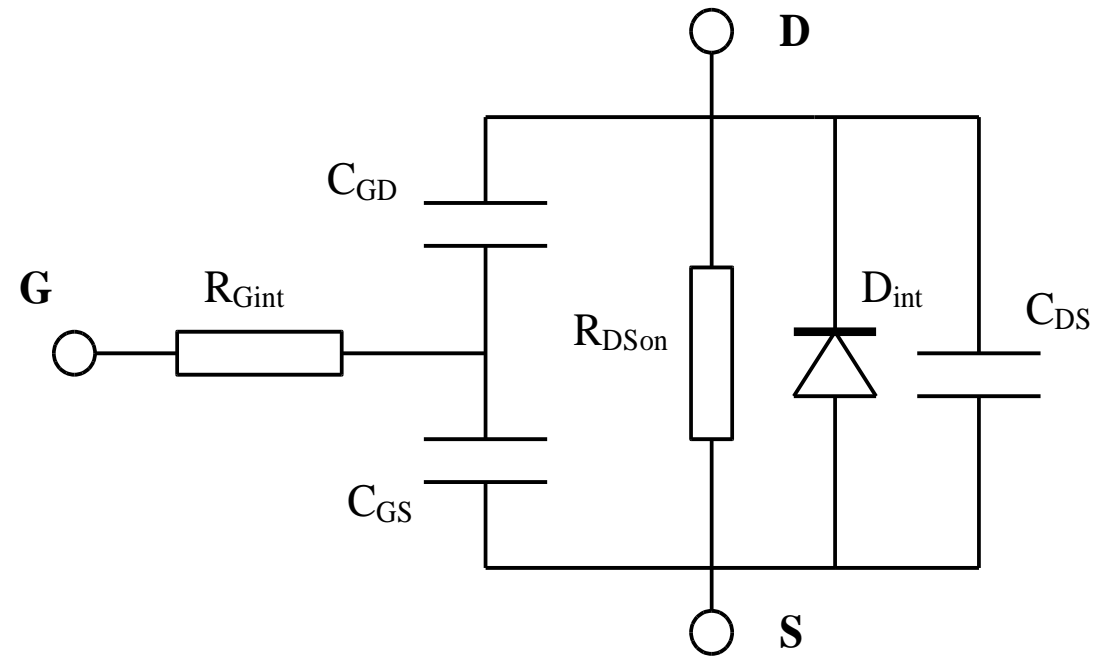
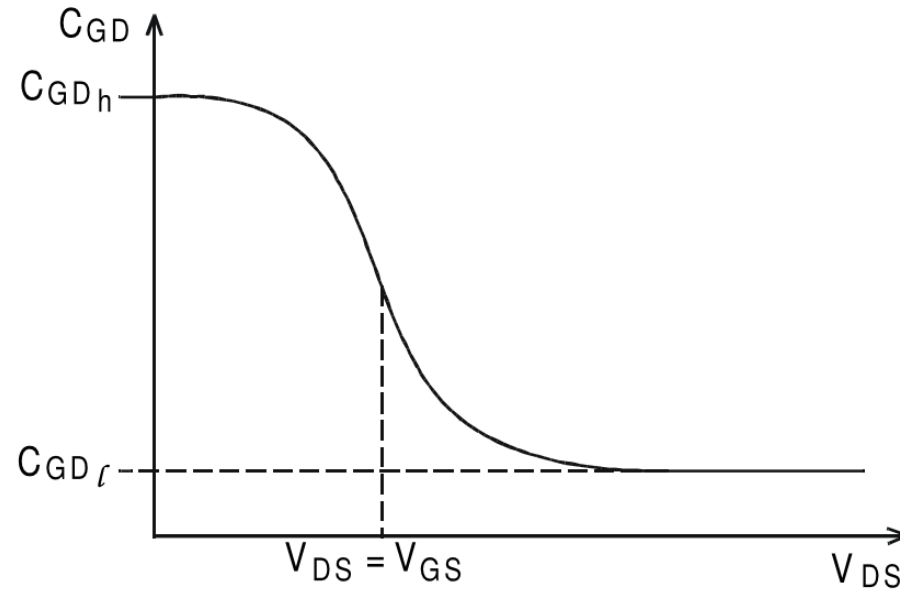
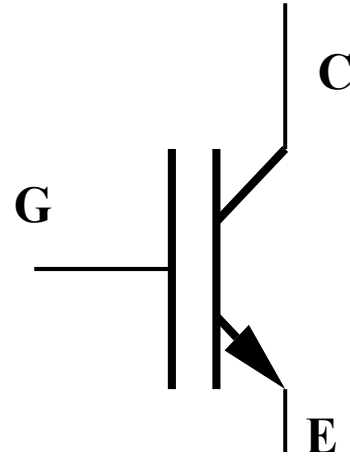
Switch off : MOS
Switch on : bipolar (dragging)

Passive
components

Active
components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

IGBT model: commutation mode

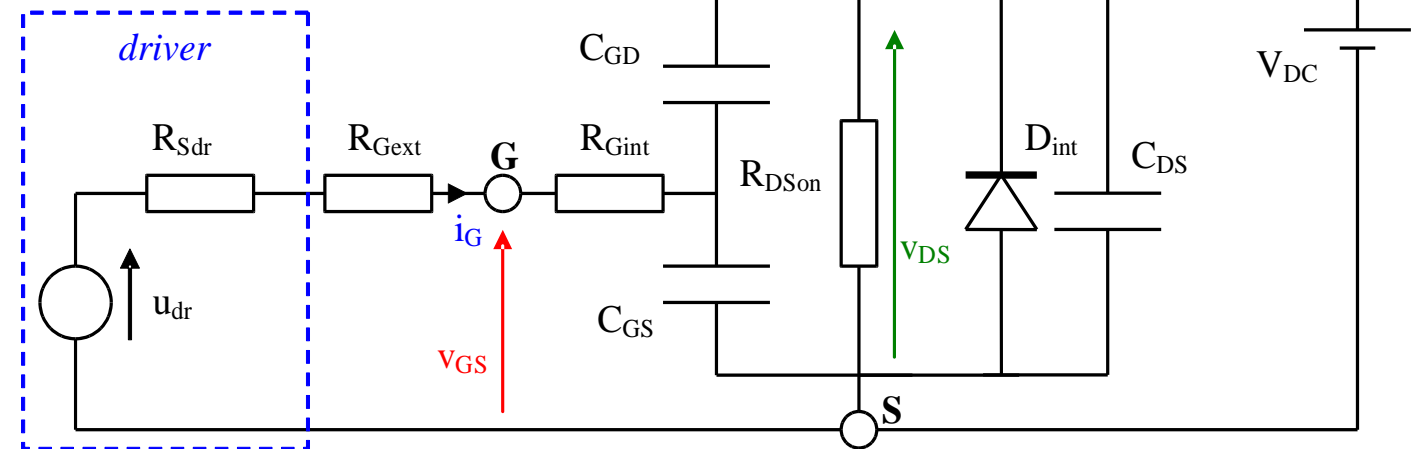
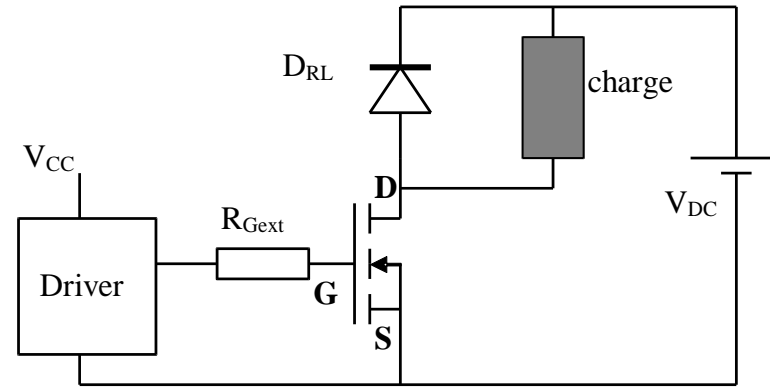


Passive
components

Active
components

Diodes
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Commutation on a BUCK chopper



Passive
components

Active
components

Diodes
Bipolar transistor
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IGBT transistor

Commutation on a BUCK chopper: Turn on

$[0..t_1]$: the transistor is still off state

$$t_1 : V_{GS} = V_{GSTH}$$

$[t_1..t_2]$: v_{GS} and i_G are still evolving

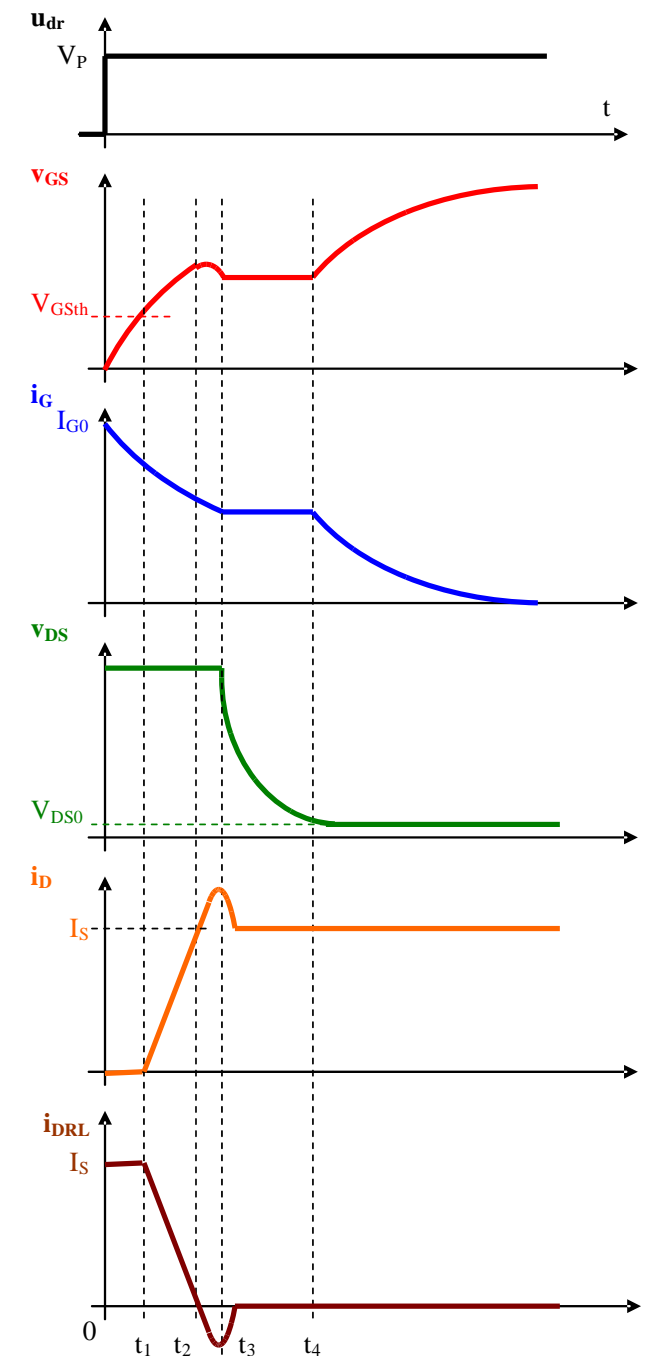
$$t_2 : i_{DRL} = 0$$

$[t_2..t_3]$: diode reverse recovery

t_3 : end of recovery

$[t_3..t_4]$: v_{DS} relaxation

t_4 : end of switching i_D, v_{DS}



Commutation on a BUCK chopper: Turn off

$[0..t'_1]$: the transistor is still on state

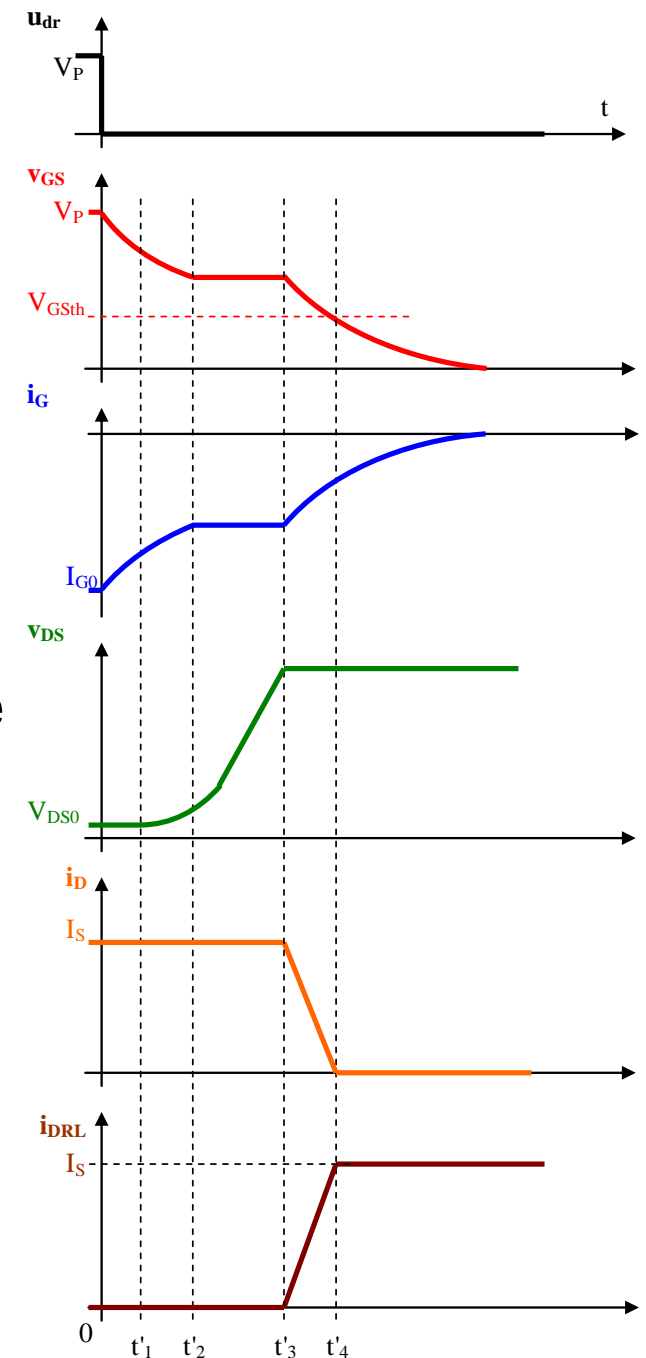
$$V_{DS} = V_{DSO}$$

$[t'_1..t'_3]$: v_{DS} increases, transistor on state

t'_3 : DRL forwards

$[t'_3..t'_4]$: i_D decreases

t'_4 : end of switching

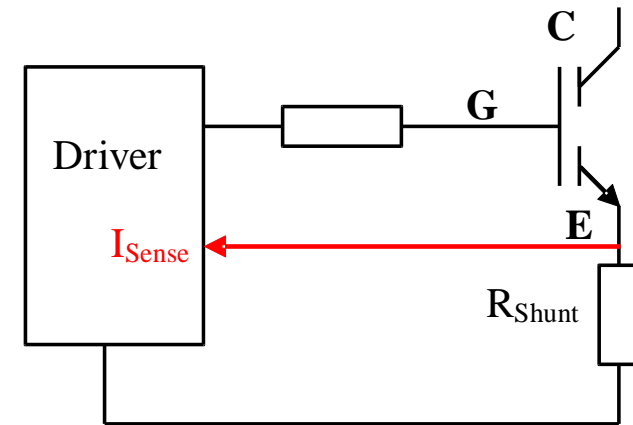
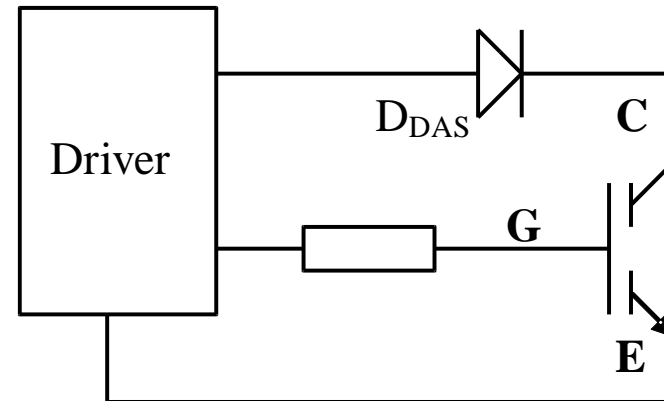
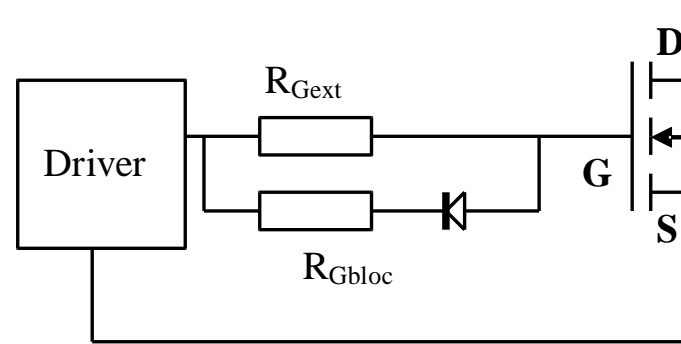


Passive components

Active components

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IGBT transistor

Control specificity



Passive
components

Active
components

Diodes
Bipolar transistor
MOS transistor
IGBT transistor

Driver MC33153

