

APPENDIX

Hand Calculations

Aircraft Sizing Calculations (Compiled)

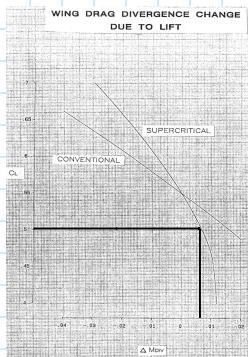
Friday, May 6, 2022 5:06 PM

1) $M = 0.82$ @ 35000ft

$$\Delta = 35$$

$$R \approx 8$$

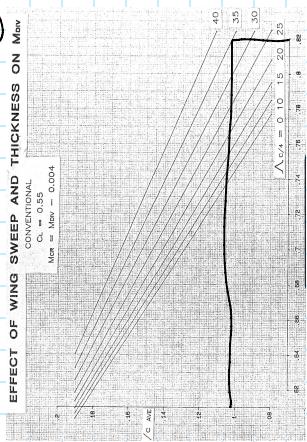
2) Assume $C_L = 0.54$, conventional



Find ΔM_{div} depending on conventional or sc

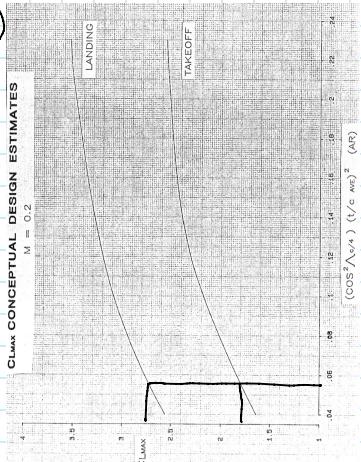
$$\begin{aligned} 3) \Delta M_{\text{div}} &= (M_{\text{crit}} + .004) - M_{\text{div}} \\ &= .0034 \end{aligned}$$

4)



Calculate t/c_{avg} based on Δ and M_{div} , $t/c = .1020$

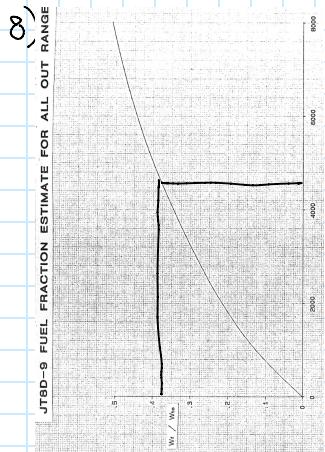
5)



Find both $C_{\text{max},s}$, $C_{\text{max,sliding}} = 2.73$, $C_{\text{max,tb}} = 1.797$

$$6) \left. \frac{W}{S} \right|_{\text{max}} = \left(\frac{V_{ap}}{1.3} \right)^2 \frac{\sigma (C_{max})_{100}}{296} = 94.8$$

$$7) V_{\text{curve}} = M \cdot a = 472,6 \\ R_{A\%} = \text{Rechabild} + 200 + (V \cdot \frac{3}{4}) = 4555$$



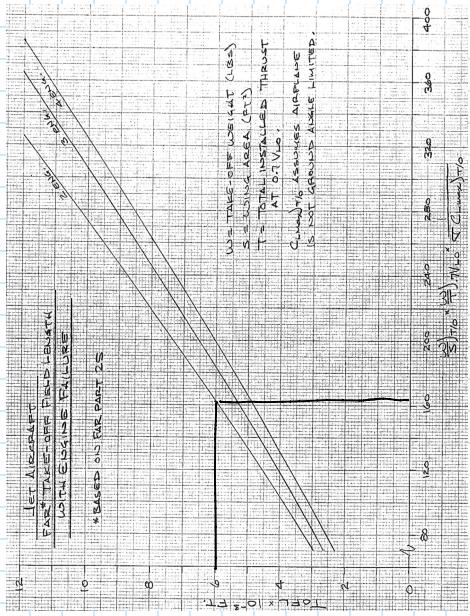
$$\frac{W_c}{W_{ho}} \Big|_{3700} = 0.3744$$

$$9) \left. \frac{w_e}{w_{b_0}} \right|_{JTBD} = \left. \frac{w_e}{w_{b_0}} \right|_{JTBD} \cdot \frac{61}{78} = 0.2928$$

$$10) \left. \frac{w}{s} \right|_{r_0} = \frac{\%s_{\infty}}{(1 - \frac{w_0}{s_{\infty}})} = 134$$

$$11) \frac{w}{s}|_k = .965 \cdot \frac{w}{s}|_b : 129$$

$$12) C_{L_c} = \frac{w_{S1ac}}{(1481 \cdot g \cdot M^2)} = 0.55, \text{ good enough}$$



$$k = 162$$

$$\frac{W}{T_{0.7V_0}} = \left(\frac{k}{\frac{W}{3_{10}}} \right) \cdot G \cdot C_{\text{harmonic}}$$

$$V_{lo} = 1.2 \cdot \sqrt{\frac{296 \cdot \frac{7\%}{10}}{\sigma C_{unw}}}} = 182.8$$

$$M_{10} = \left(\frac{189}{661} \right) / \sqrt{5} = 0.29$$

$$\frac{W}{T} = \frac{W_{T_{\text{max}}}}{T_{\text{max}}} \cdot \frac{T_{\text{max}}}{T_{\text{de}}} = 1.69$$

$$T_n = 37200$$

$$M_{10} = 37200$$

$$\frac{W}{T} = \frac{W_{T_{\text{max}}}}{T_{\text{max}}} \cdot \frac{T_{\text{max}}}{T_{\text{des}}} = 1.69$$

$$T_{\text{max}} = 37200$$

$$T_{\text{des}} = 45500$$

Weight

$$\begin{aligned} \text{Wing} : \quad & W_w = \frac{.00945 R^3 (1+\lambda)^{.15} k_w \sqrt{3.75} W_b^{1.15}}{(\frac{\lambda}{C})^4 \cos \Lambda (\frac{V_s}{S})^{.055}} , \quad \frac{1}{C} = \frac{1}{C} + 0.03 \\ & = .0085 W_b^{1.15} \end{aligned}$$

Fuselage

$$L_f = 1.76 \left(\frac{\text{PAX}}{\text{Abreast}} \right) + 33.2 = 127.2$$

$$D_f = (1.75 \text{ abreast}) + (1.58 \text{ aisle}) + 1 = 18.16$$

$$W_f = 6727 \cdot k_f \cdot L_f^{.72} \cdot D_f^{.23} \cdot W_b^{.15} = 1.723 W_b^{.15}$$

Landing Gear

$$W_b = 0.04 \cdot W_{t_0} = .04 W_b$$

Nacelle / Python

$$W_n = 0.0555 / (N_f) \cdot W_{t_0} + .0138 W_b$$

Tail Surface

$$W_b = k_t \cdot W_w = .0014 W_w$$

Power Plant

$$W_p = \frac{1}{(3.58 \cdot (\frac{\lambda}{C}))} \cdot W_b = .1699 W_b$$

Fuel

$$W_f = 1.0275 \cdot \frac{W_b}{W_{t_0}} = .313 W_b$$

Payload

$$\begin{aligned} W_p : \quad & 215 \text{ PAX} + W_c , \quad W_c = 4000 \\ & = 47000 \end{aligned}$$

Fixed Equipment

$$W_{fe} = (32 \text{ PAX}) + (300 \cdot N_{engine}) + (260 N_e) + (170 N_{shw}) + .035 W_b \cdot 28370 + .035 W_b$$

$$\begin{aligned} W : \quad & W_w + W_{t_0} + W_b + W_g + W_n + W_p + W_f + W_{fe} - 1 + W_{\text{empty}} = 0 \\ \text{solve for } & W_b \end{aligned}$$

$$W_b = 3.85e5$$

Scaling

$$S = \frac{W_b}{(\frac{W}{S_{t_0}})} = 2.93e3$$

$$b = \sqrt{\frac{R}{S}} = 143.2$$

$$\bar{c} , \frac{S}{b} = 20.46$$

$$T_{\text{total}} = \frac{W_b}{(\frac{W}{T})} = 2.34e5$$

$$T_{\text{engines}} = \frac{T_{\text{total}}}{N_{\text{engines}}} = 1.17e5$$

Drag

$$Re_1 = 2.852e6 \cdot \frac{1}{2} = 1426000$$

Wing

$$Re_w = Re_1 \cdot \bar{c} = 2.9e7$$

$$C_d = .0027$$

$$R = 7$$

$$\text{SWEEP} = 32$$

$$\text{taper} = 0.35$$

$$\frac{1}{C} = 0.096$$

Wing

$$Re_w = Re_1 \cdot \bar{c} = 2.9 \cdot 10^7$$

$$C_f = .0027$$

$$S_{wetw} = \frac{2 \cdot S \cdot 1.02}{(2 \cdot M)^{\cos \alpha}} = 5.97 \cdot 10^{-3}$$

$$z_w = \sqrt{\frac{(2 \cdot M)^{\cos \alpha}}{1 - (M^2 \cos \alpha)}} = 1.717$$

$$k_w = 1 + (z_w \cdot \frac{1}{C_f}) + 100 \left(\frac{1}{C_f}\right)^4 = 1.17$$

$$f_w = k_w \cdot C_{fw} \cdot S_{wetw} = 19.1$$

Fuselage

$$S_{wetf} = 0.9 \cdot \pi \cdot D_f \cdot L_f = 6.53 \cdot 10^{-3}$$

$$Re_{fu} = Re_1 \cdot L_f = 1.81 \cdot 10^8$$

$$C_{ffu} = .002$$

$$f_{in, fu} = \frac{L_f}{D_f} = 7$$

$$k_{fu} = 1.18$$

$$f_{fu} = k_{fu} \cdot C_{fu} \cdot S_{wetf} = 15.6$$

Tail

$$f_t = .38 f_w = 7.25$$

Nacelles

$$Re_n = Re_1 \cdot \bar{c} = 2.92 \cdot 10^7$$

$$S_{wetn} = 2.1 \cdot \sqrt{T_{\text{engines}}} \cdot N_{\text{engines}} = 1.4 \cdot 10^{-3}$$

$$C_{fn} = .0027$$

$$k_n = 1.25$$

$$f_n = k_n \cdot C_{fn} \cdot S_{wetn} = 4.9$$

Pylons

$$f_p = .2 \cdot f_n = .98$$

$$f = f_w + f_{fu} + f_t + f_n + f_p = 47.7$$

$$C_{oo} = \frac{f}{S} = .016$$

$$e = \sqrt{1.035 + 0.98 C_{oo} \pi R} = .85$$

Climb:

$$W_{wg} = (1 + .965) \cdot \frac{W_{bg}}{2} = 6.86 \cdot 10^5$$

$$h_{wg} \cdot (\frac{20}{35}) \cdot h = 20000$$

$$\sigma_d = .5702$$

$$V_{clim} = \left(\frac{12.9}{(f_{cl})^{0.6}} \right) \cdot \sqrt{\frac{W_{wg}}{(\sigma \cdot b)}} = 158.5$$

$$V_{cl} = 1.3 \cdot V_{clim} = 466.1$$

$$M_{cl} = \frac{V_{cl}}{V_{c2}} / \left(\frac{1.628}{1.628} \right) = .759$$

$$T_{regul} = (G_f \cdot \frac{V_{cl}^2}{296} \cdot (1/\sigma_d) \cdot ((\frac{W_{wg}}{b})^2 \cdot (\frac{1}{V_{cl}}))) \cdot 4.06 \cdot 10^4$$

$$T_{clif} = 1.715 \cdot 10^4$$

$$T_{clif} = 1.425 \cdot 10^4$$

$$SFC_s = .6427$$

$$I_{125} = 1.42 \times 10^4$$

$$SFC_{cl} = 0.6427$$

$$SFC_{cl} = 0.621$$

$$T_{cl} = 1.57 \times 10^4$$

$$SFC_{cl} = 0.6318$$

$$T_{all} = 3.0125 \times 10^4$$

$$\%C = (101(N_{avg} \cdot T_{all} - T_{avg})V_{cl}) / W_{avg} = 3.42 \times 10^3$$

$$T_{max,cl} = h / R_C = 10.24$$

$$Range_{cl} = V_{cl} \cdot (T_{max}/60) = 79.6$$

$$W_{fuel} = (N_{avg} \cdot T_{all}) \cdot SFC_{cl} \cdot (T_{max}/60) = 9.749$$

Range

$$W_0 \cdot W_w \cdot W_{fuel} = 6.38 \times 10^5$$

$$W_i \cdot (1 - FF_{jmo}) \cdot W_w = 4.259 \times 10^5$$

$$C_{avg} = (W_0 + W_i) / (1481 \cdot g \cdot M^2) = 4.781$$

$$C_{cl} = C_{avg}^2 / \pi R_C = 0.0107$$

$$C_{cl} = 0.001$$

$$C_0 = C_{D0} + C_{D1} + C_{D2} = 0.0261$$

$$\gamma_0 = C_{avg} / C_0 = 18.3$$

$$T_{avg} = ((W_0 + W_i)/2) / \gamma_0 = 3.05 \times 10^4$$

$$T_{max,avg} = T_{avg} / N_{avg} = 5.29 \times 10^3$$

$$SFC = 0.6224$$

$$Range_{cl} = (W_0 / SFC) \cdot \gamma_0 \cdot \ln(\frac{W_0}{W_i}) = 6.67 \times 10^3$$

$$Range = Range_{cl} + Range_{corr} = 6.75 \times 10^3$$

Compare Range to Range (all-out)
and iterate Fuel Fraction until they
match.

Range \rightarrow Range all-out

| Top of Climb | |
|-------------------|--|
| $C_{L, top}$ | $(W_0 + W_i)^2 / (1481 \cdot g \cdot M^2)$ |
| $C_{D, top}$ | $C_{D, top} / \pi R_C$ |
| $C_{D, top}$ | $C_{D0} + C_{D1} + 0.001$ |
| $\gamma_{D, top}$ | $C_{D, top} / C_{avg}$ |
| $T_{avg, top}$ | $W_0 / \gamma_{D, top}$ |
| $T_{avg, top}$ | $T_{avg, top} / \# \text{engines}$ |

$$\begin{aligned}
 T_{D_{\text{top}}} &:= \frac{W_0}{C_{\text{Dop}}} = 15.05 \\
 T_{\text{avg}} &:= \frac{W_0}{\gamma D_{\text{top}}} = 4.17e4 \\
 T_{\text{avg,eng}} &:= \frac{T_{\text{avg}}}{\# \text{engines}} = 1.39e4 \\
 T_{\text{avg,real}} &:= \left(\frac{T_{\text{avg}}}{T_{\text{avg}}} \right) T_{\text{real}} = 8.06e3
 \end{aligned}$$

Climb Gradients

Segment 1

$$\begin{aligned}
 C_{L1} &:= \frac{C_{\text{CL}}}{1.2} = 1.21 \\
 C_{L1}/C_{\text{CL}} &:= \frac{C_{L1}}{C_{\text{CL}}} = 0.694 \\
 C_{D1} &:= \text{see fig} \\
 L/D_1 &:= \frac{C_{L1}}{C_{D1}} = 10.7 \\
 T_{\text{avg,1}} &:= \frac{W_0}{\gamma D_1} = 5.94e4 \\
 T_{\text{clb,1}} &:= \left(\frac{T_e}{T_{\text{avg,1}}} \right) \cdot T_{\text{avg,1}} = 6.05e4 \\
 \text{Grad}_{L1} &:= \frac{((\text{deg}-1)T_{\text{clb,1}} - T_{\text{avg,1}}) 100}{W_0} = 9.69
 \end{aligned}$$

Segment 2

$$\begin{aligned}
 C_{D2} &:= C_{D0} + C_{Dp1} + \frac{C_{L1}^2}{\pi Re} = 0.098 \\
 L/D_2 &:= \frac{C_{L1}}{C_{D2}} = 12.36 \\
 T_{\text{avg,2}} &:= \frac{W_0}{\gamma D_2} = 5.15e4 \\
 \text{Grad}_{L2} &:= \frac{((\text{deg}-1)T_{\text{avg,2}} - T_{\text{avg,1}}) 100}{W_0} = 10.9
 \end{aligned}$$

Segment 3

$$\begin{aligned}
 C_{\text{CL,3}} &:= \text{see fig} \\
 V_3 &:= 1.2 \sqrt{\frac{216 \cdot W_0}{1.125 C_{\text{CL,3}}}} = 244.14 \\
 M_3 &:= \frac{V_3}{659} = 0.371 \\
 C_{L3} &:= \frac{C_{\text{CL,3}}}{1.2^2} = 0.755 \\
 C_{D3} &:= C_{D0} + \frac{C_{L3}^2}{\pi Re} = 0.0418 \\
 L/D_3 &:= \frac{C_{L3}}{C_{D3}} = 18.08 \\
 T_{\text{avg,3}} &:= \frac{W_0}{\gamma D_3} = 3.52e4 \\
 T_{\text{clb,3}} &:= \left(\frac{T_e}{T_{\text{avg,3}}} \right) \cdot T_{\text{avg,3}} = 4.63e4 \\
 \text{Grad}_{L3} &:= \frac{((\text{deg}-1)T_{\text{clb,3}} - T_{\text{avg,3}}) 100}{W_0} = 9.04
 \end{aligned}$$

Approach

$$\begin{aligned}
 C_{L4} &:= \frac{C_{\text{CL}}}{1.2^2} = 1.0288 \\
 C_{L4}/C_{\text{CL}} &:= \frac{C_{L4}}{C_{\text{CL}}} = 0.5917 \\
 C_{Dp4} &:= \text{see Pg} \\
 C_{D4} &:= C_{D0} + C_{Dp4} + \frac{C_{L4}^2}{\pi Re} = 0.0756 \\
 L/D_4 &:= \frac{C_{L4}}{C_{D4}} = 13.6 \\
 W_{\text{lift,4}} &:= \frac{W_0}{659 \cdot S} = 4.507e5 \\
 T_{\text{avg,4}} &:= \frac{W_{\text{lift,4}}}{\gamma D_4} = 3.313e4 \\
 V_A &:= \sqrt{\frac{216 \cdot W_0}{1.125 C_{L4}}} = 173.45 \\
 M_A &:= \frac{V_A}{659} = 0.263 \\
 T_{\text{clb,4}} &:= \left(\frac{T_e}{T_{\text{avg,4}}} \right) \cdot T_{\text{avg,4}} = 5.06e4 \\
 \text{Grad}_{L4} &:= \frac{((\text{deg}-1)T_{\text{clb,4}} - T_{\text{avg,4}}) 100}{W_0} = 15.1076
 \end{aligned}$$

Landing

$$\begin{aligned}
 C_{L5} &:= \frac{C_{\text{CL}}}{1.3^2} = 1.58 \\
 C_{D5} &:= \text{see fig} \\
 C_{D5} &:= C_{D0} + C_{Dp1} + C_{Dp2} + \frac{C_{L5}^2}{\pi Re} = 0.1669 \\
 L/D_5 &:= \frac{C_{L5}}{C_{D5}} = 9.46 \\
 T_{\text{avg,5}} &:= \frac{W_0}{\gamma D_5} = 4.76e4 \\
 V_L &:= \sqrt{\frac{216 \cdot W_0}{1.125 C_{L5}}} = 140 \\
 M_L &:= \frac{V_L}{659} = 0.212 \\
 T_{\text{clb,5}} &:= \left(\frac{T_e}{T_{\text{avg,5}}} \right) \cdot T_{\text{avg,5}} = 6.39e4 \\
 \text{Grad}_{L5} &:= \frac{((\text{deg}-1)T_{\text{clb,5}} - T_{\text{avg,5}}) 100}{W_0} = 31.94
 \end{aligned}$$

DOC

$$\begin{aligned}
 D &:= R_{\text{rad}} \cdot 1.15 = 6.9e3 \\
 T_{\text{g}} &:= \frac{(D/(C_{L5} + 0.04D)) / 60}{T_{\text{clb,5}}} = 0.393 \\
 T_{\text{clr}} &:= \frac{T_{\text{g}}}{60} = 0.18
 \end{aligned}$$

$$\begin{aligned}
D &= R_{\text{radiated}} \cdot 1.15 & = 6.9 \cdot 10^3 \\
T_{\text{gr}} &= \frac{(D/(1.15 + 0.04D))}{60} & = 0.393 \\
T_{\text{ctr}} &= \frac{T_{\text{gr}}}{60} & = 0.18 \\
T_d &= 0 \\
T_{\text{am}} &= 1 \\
L_a &= 0.02D & = 138 \\
D_d &= 0 \\
T_{\text{cr}} &= \frac{0 + k_{\text{am}} + 20 - (R_{\text{cr}} \cdot 1.15 + D_d)}{\sqrt{V_{\text{cr}} \cdot 1.15}} & = 12.8 \\
V_b &= D / \pi T & = 511.8 \\
F_{\text{cray}} &= T_{\text{cray}} \cdot SFC_{\text{cray}} \cdot (T_{\text{cr}} + T_{\text{am}}) & = 2.29 \cdot 10^5 \\
F_{\text{al}} &= W_{\text{al}} & = 9.18 \cdot 10^3 \\
F_b &= F_{\text{cray}} + F_{\text{al}} & = 2.38 \cdot 10^5 \\
P &= \frac{W_{\text{al}}}{2000} & = 35.6 \\
C_{\text{par}} &= 17.84 \cdot \left(\frac{V_{\text{cr}} \cdot W_{\text{al}}}{100000} \right)^3 + 40.33 = 238.1 \\
C_{\text{TMB}} &= C_{\text{par}} / V_b \cdot P & = 0.0131 \\
C_{\text{ff}} &= 0.0438 \\
C_{\text{tot}} &= 2.15 \\
C_{\text{TMB}} &= \frac{(1.02 \cdot F_b \cdot C_{\text{ff}} + \text{Heng} \cdot C_{\text{tot}} \cdot T_b \cdot 135)}{D \cdot P} & = 0.0423
\end{aligned}$$

$$\begin{aligned}
W_a &= W_b (1 - FF) - W_{\text{pl}} \cdot (W_{\text{ff}} \cdot W_{\text{to}}) & = 2.52 \cdot 10^5 \\
C_a &= 2.4 \cdot 10^6 + (87.5 \cdot W_a) & = 2.45 \cdot 10^7 \\
C_e &= 590000 + (16 \cdot T_e) & = 1.31 \cdot 10^6 \\
C_r &= (\text{Heng} \cdot C_e) + C_a & = 2.84 \cdot 10^7 \\
IR &= 0.1 \\
U &= 630 + \frac{4000}{(H \cdot (T_b + s))} & = 4.36 \cdot 10^3 \\
C_{\text{TMB}} &= IR_A \cdot C_r / (U \cdot V_b \cdot P) & = 0.0036
\end{aligned}$$

$$\begin{aligned}
K_{\text{FHa}} &= 4.9169 \cdot \log \left(\frac{W_a}{1000} \right) - 6.425 & = 5.38 \\
K_{\text{FCa}} &= 2.13 \cdot \log \left(\frac{W_a}{1000} \right)^{0.74} & = 5.62 \\
T_F &= T_b - T_{\text{gr}} & = 13.1 \\
R_L &= 8.6 \\
C_{\text{TMB}} &= \frac{(K_{\text{FHa}} \cdot T_F + K_{\text{FCa}}) \cdot R_L \cdot (1 + 2.9(M-1)^{1.5})}{(V_b \cdot T_b \cdot P)} & = 0.0025 \\
C_{\text{FHa}} &= \frac{1.58 \cdot C_a}{1000000} + 3.4 & = 42.5 \\
C_{\text{FCa}} &= \frac{1.923 \cdot C_a}{1000000} + 2.25 & = 49.3 \\
C_{\text{TMB}} &= \frac{(C_{\text{FHa}} \cdot T_b + C_{\text{FCa}})}{(V_b \cdot T_b \cdot P)} & = 0.0025 \\
K_{\text{FHa}} &= \frac{(\text{Heng} \cdot T_b / 1000)}{(327 \cdot (T_b / 1000) + 13.639)} & = 3 \\
K_{\text{FCa}} &= 2 \cdot \text{Heng} & = 0.6 \\
C_{\text{TMB}} &= \frac{(K_{\text{FHa}} \cdot T_F + K_{\text{FCa}})}{(V_b \cdot T_b \cdot P)} & = 0.0014 \\
C_{\text{FHa}} &= \frac{((23.2 \cdot C_a / 100000) - 6.5) \cdot \text{Heng}}{1000000} & = 91.8 \\
C_{\text{FCa}} &= \frac{((3.67 \cdot C_a / 1000000) + 1.36) \cdot \text{Heng}}{1000000} & = 18.6 \\
C_{\text{TMB}} &= \frac{(C_{\text{FHa}} \cdot T_b + C_{\text{FCa}})}{(V_b \cdot T_b \cdot P)} & = 0.005 \\
C_{\text{TMB}} &= 2(C_{\text{TMB}} + C_{\text{TMB}} + C_{\text{TMB}} + C_{\text{TMB}}) & = 0.0226 \\
D_a &= 14 \\
C_{\text{TMB}} &= \frac{1}{(V_b \cdot P)} \cdot \frac{(C_r + 0.06(C_r - \text{Heng} \cdot C_e) + 3 \cdot \text{Heng} \cdot C_e)}{(D_a \cdot U)} & = 0.0279 \\
\text{DOC}_{\text{min}} &= C_{\text{TMB}} + C_{\text{TMB}} + C_{\text{TMB}} + C_{\text{TMB}} + C_{\text{TMB}} & = 0.111 \\
\text{DOC}_{\text{max}} &= \text{DOC}_{\text{min}} \cdot \frac{P}{P_{\text{AX}}} & = 0.0143
\end{aligned}$$

**Code for 3D Plots and
Overall Optimizations**

```

%% Start
close all
clear
clc

%% Prompts

prompt_0 = "Is this unique (1), sample (2), or quiz (3) configuration? ";
type_inputs = input(prompt_0);

prompt_1 = "Would you like to draw graphs and fit curves? 1 for no, 2 for yes: ";
type_graph = input(prompt_1);

prompt_2 = "Please input 1 for conventional wing, 2 for supercritical: ";
type_airfoil = input(prompt_2);

prompt_3 = "Please enter what type of engine you are using, 1 for JT9D Advanced, 2 for JT9D, and 3 for JT8D";
type_engine = input(prompt_3);

prompt_4 = "Please enter how many engines the aircraft has (2, 3, or 4): ";
type_enginesqty = input(prompt_4);

if type_enginesqty == 1
    type_enginesqty = 2;
end

prompt_5 = "Are the engines mounted on the wing (1) or fuselage (2)? ";
type_mount = input(prompt_5);

prompt_6 = "Is the structure conventional (1), hybrid (2), or composites (3)? ";
type_structure = input(prompt_6);

prompt_7 = "Is this flight domestic (1) or international (2)? ";
type_flight = input(prompt_7);

if type_mount == 1
    K_w = 1;
    K_ts = 0.17;
elseif type_mount ==2
    K_w = 1.03;
    K_ts = 0.25;
end

%% Fixed Variables

l = 5; % number of lines in graphs at the end

range_AR = [8:.5:14];
range_Sweep = [20:1:38];

if type_inputs == 1 %Unique
    Taper = 0.35;

    height = 35000; %ft
    M = 0.82;
    Range_scheduled = 4000;
    FF_max = 1;
    V_approach = 135;

    TOFL = 6000;
end

```

```

PAX = 200; %passengers
Abreast = 6; %number of passengers abreast
Aisles = 2;
Weight_cargo = 4000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards
elseif type_inputs == 2 %Sample
Taper = 0.35;

height = 35000; %ft
M = 0.82;
Range_scheduled = 6000;
FF_max = .75;
V_approach = 140;
TOFL = 9000;

PAX = 275; %passengers
Abreast = 8; %number of passengers abreast
Aisles = 2;
Weight_cargo = 12000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards

type_engineqty = 3;
elseif type_inputs ==3 %Quiz
Taper = 0.35;

height = 35000; %ft
M = 0.82;
Range_scheduled = 4000;
FF_max = 1;
V_approach = 135;
TOFL = 6000;

PAX = 200; %passengers
Abreast = 6; %number of passengers abreast
Aisles = 2;
Weight_cargo = 4000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards
end

gamma = 1.4;
R = 1718;
T = 218.9; %K
rho = .023751; %lb/ft^3
sigma = .953; %Ratio between local and sea level densities
delta = .2360; %Ratio between local and sea level pressures

%a = sqrt(gamma*R*T);
a = 576.4;

%% Digitized Plots

Table = readtable('Tables.xlsx');
Table = Table{:, :};

if type_airfoil == 1
% Figure 1a: Effect of Wing Sweep and Thickness on Mdiv (Conventional)
x1 = Table(1:165,1);
y1 = Table(1:165,3);
z1 = Table(1:165,2);

```

```

[fit_TC,info_TC] = fit([x1,y1],z1,'poly23');

% Figure 1b: Effect of Wing Sweep and Thickness on Mdiv (Supercritical)
elseif type_airfoil == 2
    x2 = Table(1:211,4);
    y2 = Table(1:211,6);
    z2 = Table(1:211,5);
    [fit_TC,info_TC] = fit([x2,y2],z2,'poly35');
end

% Figure 2: Wing Drag Divergence Change Due to Lift
if type_airfoil == 1
    x3 = Table(1:25,7);
    y3 = Table(1:25,8);
    [fit_MDIVdelta,info_MDIVdelta] = fit(y3,x3,'power2');
elseif type_airfoil == 2
    x4 = Table(1:29,9);
    y4 = Table(1:29,10);
    [fit_MDIVdelta,info_MDIVdelta] = fit(y4,x4,'power2');
end

% Figure 3: CLmax Conceptual Design Estimates
x5 = Table(1:34,11);
y5 = Table(1:34,12);
[fit_CLmax_takeoff,info_CLmax_takeoff] = fit(x5,y5,'smoothingspline');
x6 = Table(1:31,13);
y6 = Table(1:31,14);
[fit_CLmax_landing,info_CLmax_landing] = fit(x6,y6,'smoothingspline');

% Figure 4: JT8D-9 Fuel Fraction Estimate for All Out Range
x7 = Table(1:41,15);
y7 = Table(1:41,16);
[fit_FF,info_FF] = fit(x7,y7,'cubicinterp'); % FF is Fuel Fraction or W_f/W_to

% Figure 5: Jet Aircraft TOFL with Engine Failure
x8 = Table(1:58,17);
y8 = Table(1:58,18);
[fit_k_2ENG,info_k_2ENG] = fit(y8,x8,'poly2');
x9 = Table(1:63,19);
y9 = Table(1:63,20);
[fit_k_3ENG,info_k_3ENG] = fit(y9,x9,'poly2');
x10 = Table(1:67,21);
y10 = Table(1:67,22);
[fit_k_4ENG,info_k_4ENG] = fit(y10,x10,'poly2');

% Cf
x11 = Table(1:50,23);
y11 = Table(1:50,24);
y11 = y11.*(1e-3);
[fit_Cf, info_Cf] = fit(x11,y11,'power2');

% Body Form Factor
x12 = Table(1:12,25);
y12 = Table(1:12,26);
[fit_k, info_k] = fit(x12,y12,'exp2');

% Max Climb Thrust @ 15000ft
x13 = Table(1:34,27);
y13 = Table(1:34,28);
[fit_T_avbl15, info_T_avbl15] = fit(x13,y13,'smoothingspline');
x14 = Table(1:9,29);
y14 = Table(1:9,30);
[fit_SFC_15, info_SFC_15] = fit(x14,y14,'smoothingspline');

```

```
% Max Climb Thrust @ 25000ft
x15 = Table(1:30,31);
y15 = Table(1:30,32);
[fit_T_avbl25, info_T_avbl25] = fit(x15,y15,'smoothingspline');
x = Table(1:6,33);
y = Table(1:6,34);
[fit_SFC_25, info_SFC_25] = fit(x,y,'smoothingspline');

% Max Climb and Thrust @ 35000ft
x16 = Table(1:9,37);
y16 = Table(1:9,38);
[fit_SFC_35, info_SFC_35] = fit(x16,y16,'lin');

% Profile Drag at Takeoff
x17 = Table(1:60,39);
y17 = Table(1:60,40);
[fit_CDP_takeoff, info_CDP_takeoff] = fit(y17,x17,'poly5');

% Profile Drag at Landing
x18 = Table(1:60,41);
y18 = Table(1:60,42);
[fit_CDP_landing, info_CDP_landing] = fit(y18,x18,'poly5');

% Clean Wing CLmax
x19 = Table(1:69,43);
y19 = Table(1:69,45);
z19 = Table(1:69,44);
[fit_CLmax_clean, info_CLmax_clean] = fit([x19,y19],z19,'poly32');

% JT9D Dry Takeoff
x20 = Table(1:18,46);
y20 = Table(1:18,47);
[fit_JT9D_takeoffthrust, info_JT9D_takeoffthrust] = fit(x20,y20,'lin');

% JT9D Climb
x21 = Table(1:26,48);
y21 = Table(1:26,49);
[fit_JT9D_climbthrust, info_JT9D_climbthrust] = fit(x21,y21,'lin');

%% Figures

if type_graph == 2

    figure
    plot(fit_TC_conv,[x1,y1],z1);

    figure
    plot(fit_TC_sc,[x2,y2],z2);
    hold on
    ylim([0 40]);
    zlim([0.07 .2]);
    hold off

    figure
    hold on
    plot(x3,y3)
    plot(x4,y4)
    xlim([-0.04 .02])
    ylim([.4 .7])
    % plot(fit_MDIVdelta_conv)
    % plot(fit_MDIVdelta_sc)

end
```

```
% xlim([-1 2])
hold off

figure
hold on
plot(x5,y5);
plot(x6,y6);
hold off

figure
plot(fit_FF);

figure
hold on
plot(x8,y8,x9,y9,x10,y10)
hold off

figure
plot(fit_Cf,x11,y11)
hold on
set(gca,'xscale','log')
title('Skin Friction Coefficient wrt Reynolds Number')
xlabel('Reynolds Number (Re)')
ylabel('Coefficient of Skin Friction (k)')
hold off

figure
plot(fit_k,x12,y12);
hold on
title('Body Form Factor wrt Fineness Ratio')
xlabel('Fineness Ratio (l/d)')
ylabel('Body Form Factor (k)')
hold off

figure
plot(x17,y17,x18,y18)

figure
hold on
% plot([z19,x19],y19)
plot(fit_CLmax_clean)
xlim([.04 .16]);
ylim([0 35]);
zlim([.8 1.3]);
hold off
end

%% Placeholders

iteration = 1;
table3d_AR = zeros(1,(length(range_AR)*length(range_Sweep)));
table3d_Sweep = zeros(1,(length(range_AR)*length(range_Sweep)));
table3d_DOC = zeros(1,(length(range_AR)*length(range_Sweep)));
table3d_Weight = zeros(1,(length(range_AR)*length(range_Sweep)));
table_CruiseSFC = zeros(1,(length(range_AR)*length(range_Sweep)));
table_Vcruise = zeros(1,(length(range_AR)*length(range_Sweep)));
table_LDcruise = zeros(1,(length(range_AR)*length(range_Sweep)));
table_FF = zeros(1,(length(range_AR)*length(range_Sweep)));
table_Wfuel = zeros(1,(length(range_AR)*length(range_Sweep)));
table_Payload = zeros(1,(length(range_AR)*length(range_Sweep)));
table_Thrust = zeros(1,(length(range_AR)*length(range_Sweep)));
table_S = zeros(1,(length(range_AR)*length(range_Sweep)));



```

```

table_AR = zeros(length(range_Sweep),length(range_AR));
table_Sweep = zeros(length(range_Sweep),length(range_AR));
table_DOC = zeros(length(range_Sweep),length(range_AR));
table_Weight = zeros(length(range_Sweep),length(range_AR));

SFC_jt9d = 0.61;
if type_engine == 1
    SFC_jt9d = 0.9 * SFC_jt9d;
end

%% Configuration Loop

i = 1;
for Sweep = range_Sweep
    j = 1;
    for AR = range_AR
        Weightincrement = 0;
        Thrust_reqtop_JT9D = 10001;
        while Thrust_reqtop_JT9D > 10000
%% Range Loop
        Range = 0;
        Range_ao = 500000;
        Fuelincrement = 0;
        while abs(Range - Range_ao) > 2
%% CL Loop
        CL_guess = 0.5;
        CL_ic = 0;
        while abs(CL_ic - CL_guess) > 0.001
            Mdiv_delta = fit_MDIVdelta(CL_guess);
            Mdiv = (M + .004) - Mdiv_delta;
            TC = fit_TC(Mdiv,Sweep);
            CLmax_landing = fit_CLmax_landing(((cosd(Sweep))^2) * ((TC)^2) * AR);
            CLmax_takeoff = fit_CLmax_takeoff(((cosd(Sweep))^2) * ((TC)^2) * AR); %5
            WS_landing = ((V_approach/1.3)^2) * (sigma * CLmax_landing) / 296; %6
            V_cruise = M * a;
            Range_ao = Range_scheduled + 200 + (V_cruise*(3/4)); %7
            FF_jt8d = fit_FF(Range_ao); %8
            if type_inputs == 1
                FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
            elseif type_inputs == 2
                FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
            elseif type_inputs == 3
                FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
            end
            if type_engine == 1 || type_engine == 2
                FF = FF_jt9d + Fuelincrement;
            elseif type_engine == 3
                FF = FF_jt8d + Fuelincrement;
            end
            WS_takeoff = WS_landing/(1-(FF_max*FF));
            WS_ic = .965 * WS_takeoff;
            CL_ic = WS_ic / (1481 * delta * M^2);
            if abs(CL_ic - CL_guess) > 0.001
                CL_guess = (CL_guess + CL_ic)/2;
            end
        end
%% TOFL
        if type_engneqty == 2
            k_1 = fit_k_2ENG((TOFL/1000));
        elseif type_engneqty == 3
            k_1 = fit_k_3ENG((TOFL/1000));
        end
    end
end

```

```

elseif type_engineqty == 4
    k_1 = fit_k_4ENG((TOFL/1000));
end
WT_7V_lo = (k_1/WS_takeoff) * sigma * CLmax_takeoff;
V_lo = 1.2 *sqrt((296*WS_takeoff)/(sigma*CLmax_takeoff));
M_lo = V_lo/(661/sqrt(sigma));
Thrust_sls = fit_JT9D_takeoffthrust(0);
Thrust_M = fit_JT9D_takeoffthrust(M_lo*0.7);
WT = (WT_7V_lo * Thrust_M/Thrust_sls) + Weightincrement;
%% Weight
eta = 1.5*2.5;
% Wing
TC_bar = TC + 0.03;
W_w = (.00945 * (AR^0.8) * ((1+Taper)^0.25) * K_w * (eta^0.5))/((TC_bar^0.4) * cosd(Sweep) * (WS_takeoff^0.695)); %times W_takeoff^1.195
% Fuselage
K_f = 11.5;
L_f = (3.76 * (PAX/Abreast) + 33.2);
D_f = ((1.75*Abreast) + (1.58*Aisles) + 1);
if type_flight == 2
    L_f = 1.1 * L_f;
    D_f = 1.1 * D_f;
end
W_fus = 0.6727 * K_f * (L_f^0.6) * (D_f^0.72) * (eta^0.3); %times W_takeoff^0.235
% Landing Gear
W_lg = 0.04; %times W_takeoff
% Nacelle & Pylon
W_np = (0.0555/WT); %times W_takeoff
% Tail Surface
W_ts = K_ts * W_w; %times W_takeoff^1.195
% Power Plant
W_pp = 1/(3.58*WT); %times W_takeoff
if type_engine == 1
    W_pp = W_pp * 1.1;
end
% Fuel
W_f = 1.0275 * (FF);
% Payload
W_pl = 215*PAX + Weight_cargo;
% Fixed Equipment
W_fe = (132*PAX) + (300*type_engineqty) + (260*Number_flightcrew) + (170*Number_stewards);
W_fe_wto = (0.035); %times W_takeoff
if type_structure == 2
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_np = 0.8 * W_np;
elseif type_structure == 3
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_fus = 0.85 * W_fus;
    W_fe = 0.9 * W_fe;
    W_fe_wto = 0.9 * W_fe_wto;
    W_np = 0.8 * W_np;
end
a_W = W_w + W_ts;
b_W = W_fus;
c_W = W_lg + W_np + W_pp + W_f + W_fe_wto - 1;
d_W = W_pl + W_fe;
W_takeoff = 300000;
difference_1 = W_takeoff;
while abs(difference_1) > 0.1
    if abs(difference_1) > 0.5

```

```

difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
W_takeoff = W_takeoff + 4*(difference_1);
elseif abs(difference_1) <= 0.5
difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
W_takeoff = W_takeoff + (difference_1);
end
end
W_fuel = W_f * W_takeoff;

%% Wing Sizing
S = W_takeoff/WS_takeoff;
b = sqrt(AR*S);
c_bar = S/b;
Thrust_total = W_takeoff/WT;
Thrust_engine = Thrust_total/type_engineqty;

%% Drag
Re_l = 2.852e6 * 0.5; % 0.5 * rho * v / mu
% Wing
Re_w = Re_l * c_bar;
Cf_w = fit_Cf(Re_w);
Swet_w = 2 * S * 1.02;
z_w = ((2-M^2)*cosd(Sweep))/sqrt(1-((M^2).* (cosd(Sweep))));
k_w = 1+(z_w*TC)+100*(TC^4);
f_w = k_w*Cf_w*Swet_w;
% Fuselage
Swet_fus = 0.9*pi*D_f*L_f;
Re_fus = Re_l * L_f;
Cf_fus = fit_Cf(Re_fus);
fineness_fus = L_f/D_f;
k_fus = fit_k(fineness_fus);
f_fus = k_fus*Cf_fus*Swet_fus;
% Tail
f_t = 0.35*f_w;
% Nacelles
Re_n = Re_l * c_bar;
Swet_n = 2.1 * sqrt(Thrust_engine) * type_engineqty;
Cf_n = fit_Cf(Re_n);
k_n = 1.25;
f_n = k_n*Cf_n*Swet_n;
% Pylons
f_p = 0.2*f_n;
%Total
f = f_w + f_fus + f_t + f_n + f_p;
CD_overall = f/S;
e = 1/(1.035 + (.38*CD_overall*pi*AR));
CD_gear = CD_overall;

%% Climb
W_avgcl = (1.965) * W_takeoff / 2;
h_avgcl = (20/35) * height;
sigma_cl = .5702;
V_ldmax = (12.9/(f*e)^(1/4)) * sqrt(W_avgcl/(sigma_cl*b));
V_cl = 1.3 * V_ldmax;
M_cl = V_cl/(973.1/1.68781);
Thrust_reqcl = (sigma_cl*f*(V_cl^2)/296) + ((94.1/(sigma_cl*e))*((W_avgcl/b)^2)*(1/(V_cl^2)));
Thrust_cl15 = fit_T_avbl15(M_cl) * 1000;
Thrust_cl25 = fit_T_avbl25(M_cl) * 1000;
SFC_15 = fit_SFC_15(M_cl);
SFC_25 = fit_SFC_25(M_cl);
Thrust_cl = (Thrust_cl15 + Thrust_cl25)/2;
SFC_cl = (SFC_15 + SFC_25)/2;
if type_engine == 1
    SFC_cl = SFC_cl * 0.9;

```

```

    end
    Thrust_avbl = (Thrust_engine/Thrust_sls) * Thrust_cl;
    RC = (101*((type_engneqty*Thrust_avbl)-Thrust_reqcl)*V_cl)/W_avgcl;
    Time_cl = height/RC;
    Range_cl = V_cl * (Time_cl/60);
    W_fcl = (type_engneqty*Thrust_avbl) * SFC_cl * (Time_cl/60);

%% Range
    W_0 = W_takeoff-W_fcl;
    W_I = (1-FF) * W_takeoff;
    CL_avg = ((W_0+W_I)/(2*S)) / (1481*delta*(M^2));
    CD_i = (CL_avg^2)/(pi*AR*e);
    CD_c = 0.001;
    CD = CD_overall + CD_i + CD_c;
    LD = CL_avg/CD;
    Thrust_reqcr = ((W_0 + W_I)/(2*LD));
    Thrust_reqcrjt9d = Thrust_reqcr * (Thrust_sls/Thrust_engine);
    Thrust_reqcreng = Thrust_reqcrjt9d / type_engneqty;
    SFC_cr = fit_SFC_35(Thrust_reqcreng);
    if type_engine == 1
        SFC_cr = SFC_cr * 0.9;
    end
    Range_cr = (V_cruise/SFC_cr) * LD * log(W_0/W_I);
    Range = Range_cl + Range_cr;
    difference_2 = Range-Range_ao;
    if difference_2 < -200 %200 or less
        Fuelincrement = Fuelincrement + 0.01;
    elseif difference_2 >= 200 %200 or more
        Fuelincrement = Fuelincrement - 0.01;
    elseif difference_2 < -18 && (Range-Range_ao) >= -200 %Between -20 and -200
        Fuelincrement = Fuelincrement + 0.001;
    elseif difference_2 > 18 && (Range-Range_ao) <= 200 %Between 20 and 200
        Fuelincrement = Fuelincrement - 0.001;
    elseif difference_2 < -3 && (Range-Range_ao) >= -18 %Between 0 and -20
        Fuelincrement = Fuelincrement + 0.0001;
    elseif difference_2 >= 3 && (Range-Range_ao) <= 18 %Between 0 and 20
        Fuelincrement = Fuelincrement - 0.0001;
    elseif difference_2 < 0 && (Range-Range_ao) >= -3 %Between 0 and -20
        Fuelincrement = Fuelincrement + 0.00001;
    elseif difference_2 >= 0 && (Range-Range_ao) <= 3 %Between 0 and 20
        Fuelincrement = Fuelincrement - 0.00001;
    end
end
%% Top of Climb
    CL_ic_top = (W_0/S)/(1481*delta*M^2);
    CDi_top = (CL_ic_top^2) / (pi*AR*e);
    CD_top = CD_overall + CDi_top + 0.001;
    LD_top = CL_ic_top / CD_top;
    if type_inputs == 2
        LD_top = 15.05; % SAMPLE
    end
    Thrust_reqtop = W_0 / LD_top;
    Thrust_reqtop_engine = Thrust_reqtop / type_engneqty;
    Thrust_reqtop_JT9D = (Thrust_sls/Thrust_engine) * Thrust_reqtop_engine;

%% Climb Gradients
    % 1st Segment
    CL_seg1 = CLmax_takeoff/(1.2^2);
    CL_to_CLmax_to = CL_seg1/CLmax_takeoff;
    CDp_seg1 = fit_CDp_takeoff(CL_to_CLmax_to);
    CD_seg1 = CD_overall + CDp_seg1 + CD_gear + ((CL_seg1^2)/(pi*AR*e));
    LD_seg1 = CL_seg1/CD_seg1;
    Thrust_reqseg1 = W_takeoff/LD_seg1;

```

```

Thrust_avblseg1 = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_lo);
Grad_1 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg1)*100/W_takeoff;
% 2nd Segment
CD_seg2 = CD_overall + CDp_seg1 + ((CL_seg1^2)/(pi*AR*e));
LD_seg2 = CL_seg1/CD_seg2;
Thrust_reqseg2 = W_takeoff/LD_seg2;
Grad_2 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg2)*100/W_takeoff;
% 3rd Segment
CLmax_clean = fit_CLmax_clean(TC,Sweep);
V_seg3 = 1.2*sqrt((296*WS_takeoff)/(.925*CLmax_clean));
M_seg3 = V_seg3/659;
CL_seg3 = CLmax_clean/(1.2^2);
CD_seg3 = CD_overall + ((CL_seg3^2)/(pi*AR*e));
LD_seg3 = CL_seg3/CD_seg3;
Thrust_reqseg3 = W_takeoff/LD_seg3;
Thrust_avblseg3 = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_seg3);
Grad_3 = ((type_engneqty-1)*Thrust_avblseg3-Thrust_reqseg3)*100/W_takeoff;
% Approach
CL_approach = CLmax_takeoff/(1.3^2);
CL_approach_CLmax_landing = CL_approach/CLmax_takeoff;
CDp_approach = fit_CDp_takeoff(CL_approach_CLmax_landing);
CD_approach = CD_overall + CDp_approach + (CL_approach^2)/(pi*AR*e);
LD_approach = CL_approach/CD_approach;
W_landing = WS_landing * S;
Thrust_reqapproach = W_landing/LD_approach;
V_approach_grad = sqrt((296*WS_landing)/(.953*CL_approach));
M_approach = V_approach_grad/659;
Thrust_avblapproach = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_approach);
Grad_approach = ((type_engneqty-1)*Thrust_avblapproach-Thrust_reqapproach)*100/W_landing;
%Landing
CL_landing = CLmax_landing/1.3^2;
CDp_landing = fit_CDp_landing(1/1.3^2);
CD_landing = CD_overall + CDp_landing + CD_gear + (CL_landing^2)/(pi*AR*e);
LD_landing = CL_landing/CD_landing;
Thrust_reqlanding = W_landing/LD_landing;
V_landing = sqrt((296*WS_landing)/(0.953*CL_landing));
M_landing = V_landing/659;
Thrust_avbllanding = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_landing);
Grad_landing = ((type_engneqty*Thrust_avbllanding) - Thrust_reqlanding) * 100 / W_landing;
% Climb Requirements (pg. 39)
if type_engneqty == 2
    Grad_1_min = 0;
    Grad_2_min = 2.4;
    Grad_3_min = 1.2;
    Grad_approach_min = 2.1;
    Grad_landing_min = 3.2;
elseif type_engneqty == 3
    Grad_1_min = 0.3;
    Grad_2_min = 2.7;
    Grad_3_min = 1.5;
    Grad_approach_min = 2.4;
    Grad_landing_min = 3.2;
elseif type_engneqty == 4
    Grad_1_min = 0.5;
    Grad_2_min = 3.0;
    Grad_3_min = 1.7;
    Grad_approach_min = 2.7;
    Grad_landing_min = 3.2;
end

if Thrust_reqtop_JT9D > 10000 || Grad_1 < Grad_1_min || Grad_2 < Grad_2_min || Grad_3 < Grad_3_min || Grad_approach < Grad_approach_min || Grad_landing < Grad_landing_min

```

```

        Weightincrement = Weightincrement - 0.1;
        disp('Gradient Failed')
    end
end

%% DOC
D = Range_scheduled * 1.15;
Time_gm = (D / (11.866+0.040669*D))/60;
Time_cl_hr = Time_cl/60;
Time_d = 0;
Time_am = 0.10;
if D <= 1400
    k_a = (7+0.015*D);
elseif D > 1400
    k_a = 0.02*D;
end
D_d = 0;
Time_cr = ((D+k_a+20)-(Range_cl*1.15+D_d))/(V_cruise*1.15);
V_B = D / (Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am);
% Block Time
Time_b = Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am;
% Block Fuel
F_cr_am = Thrust_reqcr * SFC_cr * (Time_cr+Time_am);
F_cl = W_fcl;
F_b = F_cr_am + F_cl;
% Flying Operations Cost
% a. Flight Crew
P = W_pl / 2000;
if Number_flightcrew == 2
    CostPerBlockHr = 17.849 * (V_cruise*W_takeoff/1e5)^0.3 + 40.83;
else
    CostPerBlockHr = 24.261 * (V_cruise*W_takeoff/1e5)^0.3 + 57.62;
end
C_TM_FlightCrew = CostPerBlockHr / (V_B * P);
% b. Fuel and Oil
if type_flight == 1
    C_ft = 0.0438;
elseif type_flight == 2
    C_ft = 0.0625;
end
C_ot = 2.15;
C_TM_FuelOil = ( 1.02*F_b*C_ft + type_enginelqty*C_ot*Time_b*0.135 ) / (D*P);
% c. Hull Insurance Costs
W_a = W_takeoff * (1-FF) - W_pl - (W_pp*W_takeoff);
C_a = 2.4e6 + (87.5*W_a);
C_e = 590000 + (16*Thrust_engine);
if type_inputs == 2
    C_e = 1314942;
end
C_T = (type_enginelqty*C_e) + C_a;
IR_A = 0.01;
U = 630 + 4000/( 1 + 1/(Time_b + 0.5)); % block hrs/yr
C_TM_HullInsurance = IR_A * C_T / (U * V_B * P);
% Direct Maintenance
% a. Airframe-Labor
K_FHa = 4.9169 * log10(W_a/1000) - 6.425;
K_FCa = 0.21256 * log10(W_a/1000)^3.7375;
T_F = Time_b - Time_gm;
R_L = 8.6;
C_TM_a_AirframeLabor = (K_FHa * T_F + K_FCa) * R_L * (1 + 0.29*(M-1))^1.5 / (V_B * Time_b * P);
% b. Airframe Material
C_FHa = ((1.5994*C_a)/1e6) + 3.4263;

```

```

C_FCa = ((1.9229*C_a)/1e6) + 2.2504;
C_TM_b_AirframeMaterial = (C_FHa*T_F+C_FCa) / (V_B*Time_b*P);
% c. Engine Labor
K_FHe = (type_engineqty*(Thrust_engine/1e3))/(0.82715*(Thrust_engine/1e3)+ 13.639);
K_FCe = 0.2 * type_engineqty;
C_TM_c_EngineLabor = ((K_FHe*T_F+K_FCe)*R_L) / (V_B*Time_b*P);
% d. Engine Material
C_FHe = (((28.2353*C_e)/1e6) - 6.5176) * type_engineqty;
C_FCe = (((3.6698*C_e)/1e6) + 1.3685) * type_engineqty;
C_TM_d_EngineMaterial = (C_FHe*T_F+C_FCe) / (V_B*Time_b*P);
if type_engine == 1
    C_TM_d_EngineMaterial = C_TM_d_EngineMaterial * 1.1;
end
% e. Total Maintenance - Burdened
C_TM_e_Maintenance = (C_TM_a_AirframeLabor + C_TM_b_AirframeMaterial + C_TM_c_EngineLabor +
C_TM_d_EngineMaterial)*2;
% Depreciation
D_a = 14;
C_TM_Depreciation = (1/(V_B*P)) * (C_T + 0.06*(C_T-type_engineqty*C_e)+0.3*type_engineqty*C_e) *
(D_a*U);
% Total DOC
DOC_perTonMile = C_TM_FlightCrew + C_TM_FuelOil + C_TM_HullInsurance + C_TM_e_Maintenance +
C_TM_Depreciation;
DOC_perPAXMile = DOC_perTonMile * P/PAX;

%% Data Collection
% Plots
table3d_AR(iteration) = AR;
table3d_Sweep(iteration) = Sweep;
table3d_DOC(iteration) = DOC_perPAXMile;
table3d_Weight(iteration) = W_takeoff;
table_AR(i,j) = AR;
table_Sweep(i,j) = Sweep;
table_DOC(i,j) = DOC_perPAXMile;
table_Weight(i,j) = W_takeoff;
table_b(i,j) = b;

% Range Chart
table_CruiseSFC(iteration) = SFC_cr;
table_Vcruise(iteration) = V_cruise;
table_LDcruise(iteration) = LD;
table_FF(iteration) = FF;
table_Wfuel(iteration) = W_fuel;
table_Payload(iteration) = W_pl;
table_Thrust(iteration) = Thrust_engine;
table_S(iteration) = S;

iteration = iteration + 1
j = j+1;
end
i = i+1;
end

%% Results
[fit_DOC,info_DOC] = fit([table3d_AR',table3d_Sweep'],table3d_DOC','loess');
[fit_Weight,info_Weight] = fit([table3d_AR',table3d_Sweep'],table3d_Weight','loess');
[Min_DOC,optimallocation_DOC] = min(table3d_DOC);
[Min_Weight,optimallocation_Weight] = min(table3d_Weight);
optimal_DOC = table3d_DOC(optimallocation_DOC)
optimal_AR = table3d_AR(optimallocation_DOC)
optimal_Sweep = table3d_Sweep(optimallocation_DOC)

```

```

optimal_Weight = table3d_Weight(optimalallocation_DOC)
optimal_Thrust = table_Thrust(optimalallocation_DOC)
optimal_FF = table_FF(optimalallocation_DOC)
optimal_b = table_b(optimalallocation_DOC)
optimal_S = table_S(optimalallocation_DOC)
optimal_Weight_Weight = table3d_Weight(optimalallocation_Weight);
optimal_Weight_AR = table3d_AR(optimalallocation_Weight);
optimal_Weight_Sweep = table3d_Sweep(optimalallocation_Weight);

%% Range Chart

% Values
max_Weight = table3d_Weight(optimalallocation_DOC);
optimal_CruiseSFC = table_CruiseSFC(optimalallocation_DOC);
optimal_Vcruise = table_Vcruise(optimalallocation_DOC);
optimal_LDcruise = table_LDcruise(optimalallocation_DOC);
optimal_FF = table_FF(optimalallocation_DOC);
optimal_Wfuel = table_Wfuel(optimalallocation_DOC);
optimal_Payload = table_Payload(optimalallocation_DOC);
max_Payload = 52000;
delta_Payload = max_Payload - optimal_Payload;
% Point 1
p1_Weight0 = max_Weight;
p1_Payload = max_Payload;
p1_Range = 0;
% Point 2
p2_Weight0 = max_Weight;
p2_Payload = max_Payload;
p2_Wfuel = optimal_Wfuel - delta_Payload;
p2_Weight1 = p2_Weight0 - p2_Wfuel;
p2_Range = (optimal_Vcruise/optimal_CruiseSFC)*optimal_LDcruise*log(p2_Weight0/p2_Weight1);
% Point 3
p3_Weight0 = max_Weight;
p3_Payload = optimal_Payload;
p3_Wfuel = optimal_Wfuel;
p3_Weight1 = p3_Weight0 - p3_Wfuel;
p3_Range = (optimal_Vcruise/optimal_CruiseSFC)*optimal_LDcruise*log(p3_Weight0/p3_Weight1);
% Point 4
p4_Weight0 = max_Weight - optimal_Payload;
p4_Wfuel = optimal_Wfuel;
p4_Payload = 0;
p4_Weight1 = p4_Weight0 - p4_Wfuel;
p4_Range = (optimal_Vcruise/optimal_CruiseSFC)*optimal_LDcruise*log(p4_Weight0/p4_Weight1);
chart_Payload = [p1_Payload p2_Payload p3_Payload p4_Payload];
chart_Range = [p1_Range p2_Range p3_Range p4_Range];

%% Plots

% 3D DOC Plot
figure
scatter3(table3d_AR,table3d_Sweep,table3d_DOC);
hold on
plot(fit_DOC)
plot3(optimal_AR,optimal_Sweep,optimal_DOC,'r.', 'MarkerSize',30, 'DisplayName', 'Point of Lowest DOC Possible')
title('DOC vs AR and Sweep')
xlabel('Aspect Ratio')
ylabel('Sweep Angle')
zlabel('DOC ($)')
hold off
% Contour DOC Plot
figure

```

```

[mesh_AR,mesh_Sweep] = meshgrid(range_AR,range_Sweep);
mesh_DOC = griddata(table3d_AR,table3d_Sweep,table3d_DOC,mesh_AR,mesh_Sweep);
[C,h] = contourf(mesh_AR,mesh_Sweep,mesh_DOC,20);
clabel(C,h)
hold on
plot(optimal_AR,optimal_Sweep,'r.', 'MarkerSize',30, 'DisplayName',sprintf('Point of Lowest DOC Possible: %0.4f$',optimal_DOC))
plot(optimal_Weight_AR,optimal_Weight_Sweep,'y.', 'MarkerSize',30, 'DisplayName',sprintf('Point of Lowest Weight Possible: %0.4flbs',optimal_Weight_Weight))
legend
title('DOC vs AR and Sweep: Composite')
xlabel('Aspect Ratio')
ylabel('Sweep Angle')
hold off
% 3D Weight Plot
figure
scatter3(table3d_AR,table3d_Sweep,table3d_Weight);
hold on
plot(fit_Weight)
plot3(optimal_AR,optimal_Sweep,optimal_Weight,'r.', 'MarkerSize',30, 'DisplayName','Point of Lowest DOC Possible')
title('Take-off Weight vs AR and Sweep')
xlabel('Aspect Ratio')
ylabel('Sweep Angle')
zlabel('Weight (lbs)')
hold off
% Contour Weight Plot
figure
mesh_Weight = griddata(table3d_AR,table3d_Sweep,table3d_Weight,mesh_AR,mesh_Sweep);
[C,h] = contourf(mesh_AR,mesh_Sweep,mesh_Weight,20);
clabel(C,h)
hold on
plot(optimal_AR,optimal_Sweep,'r.', 'MarkerSize',30, 'DisplayName',sprintf('Point of Lowest DOC Possible: %0.1flbs',optimal_Weight))
plot(optimal_Weight_AR,optimal_Weight_Sweep,'y.', 'MarkerSize',30, 'DisplayName',sprintf('Point of Lowest Weight Possible: %0.1flbs',optimal_Weight_Weight))
legend
title('Take-off Weight vs AR and Sweep')
xlabel('Aspect Ratio')
ylabel('Sweep Angle')
hold off
% DOC wrt AR Plot
v = length(range_Sweep)/1;
figure
hold on
for i = 1:l
    plot(table_AR(round(i*v),:),table_DOC(round(i*v),:),'DisplayName',sprintf('%0.1f',range_Sweep(round(i*v))))
end
plot(optimal_AR,optimal_DOC,'r.', 'MarkerSize',30, 'DisplayName','Lowest DOC Possible')
legend
title('Sweep Angle')
title('DOC wrt Aspect Ratio: Composite')
xlabel('Aspect Ratio')
ylabel('DOC ($)')
hold off
% DOC wrt Sweep Plot
v = length(range_AR)/l;
figure
hold on
for i = 1:l
    plot(table_Sweep(:,round(i*v)),table_DOC(:,round(i*v)),'DisplayName',sprintf('%0.1f',range_AR(round(i*v))))
end

```

```
(i*v)))
end
plot(optimal_Sweep,optimal_DOC,'r.', 'MarkerSize',30,'DisplayName','Lowest DOC Possible')
legend
title(legend,'Aspect Ratio')
title('DOC wrt Sweep Angle: Composite')
xlabel('Sweep Angle')
ylabel('DOC ($)')
hold off
% Weight wrt AR Plot
v = length(range_Sweep)/l;
figure
hold on
for i = 1:l
    plot(table_AR(round(i*v),:),table_Weight(round(i*v),:),'DisplayName',sprintf('%0.1f',range_Sweep(round(i*v))))
end
plot(optimal_AR,optimal_Weight,'r.', 'MarkerSize',30,'DisplayName','Lowest DOC Possible')
legend
title(legend,'Sweep Angle')
title('Weight wrt Aspect Ratio')
xlabel('Aspect Ratio')
ylabel('Weight (lbs)')
hold off
% Weight wrt Sweep Plot
v = length(range_AR)/l;
figure
hold on
for i = 1:l
    plot(table_Sweep(:,round(i*v)),table_Weight(:,round(i*v)),'DisplayName',sprintf('%0.1f',range_AR(round(i*v))))
end
plot(optimal_Sweep,optimal_Weight,'r.', 'MarkerSize',30,'DisplayName','Lowest DOC Possible')
legend
title(legend,'Aspect Ratio')
title('Weight wrt Sweep Angle')
xlabel('Sweep Angle')
ylabel('Weight (lbs)')
hold off
% Range Chart
figure
plot(chart_Range,chart_Payload);
hold on
title('Effect of Payload Weight on Range')
xlabel('Range (mi)')
ylabel('Payload (lbs)')
hold off
```

**Code for Comparison
Plots for DOC**

```

%% Start
close all
clear
clc

%% Prompts

prompt_0 = "Is this unique (1), sample (2), or quiz (3) configuration? ";
type_inputs = input(prompt_0);

prompt_1 = "Would you like to draw graphs and fit curves? 1 for no, 2 for yes: ";
type_graph = input(prompt_1);

prompt_2 = "Please input 1 for conventional wing, 2 for supercritical: ";
type_airfoil = input(prompt_2);

prompt_3 = "Please enter what type of engine you are using, 1 for JT9D Advanced, 2 for JT9D, and 3 for JT8D";
type_engine = input(prompt_3);

prompt_4 = "Please enter how many engines the aircraft has (2, 3, or 4): ";
type_enginesqty = input(prompt_4);

if type_enginesqty == 1
    type_enginesqty = 2;
end

prompt_5 = "Are the engines mounted on the wing (1) or fuselage (2)? ";
type_mount = input(prompt_5);

prompt_6 = "Is the structure conventional (1), hybrid (2), or composites (3)? ";
type_structure = input(prompt_6);

prompt_7 = "Is this flight domestic (1) or international (2)? ";
type_flight = input(prompt_7);

if type_mount == 1
    K_w = 1;
    K_ts = 0.17;
elseif type_mount ==2
    K_w = 1.03;
    K_ts = 0.25;
end

%% Fixed Variables

l = 5; % number of lines in graphs at the end

range_AR = [6:.5:14];
Sweep = 36;

if type_inputs == 1 %Unique
    Taper = 0.35;

    height = 35000; %ft
    M = 0.82;
    Range_scheduled = 4000;
    FF_max = 1;
    V_approach = 135;

    TOFL = 6000;
end

```

```

PAX = 200; %passengers
Abreast = 6; %number of passengers abreast
Aisles = 1;
Weight_cargo = 4000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards
elseif type_inputs == 2 %Sample
Taper = 0.35;

height = 35000; %ft
M = 0.82;
Range_scheduled = 6000;
FF_max = .75;
V_approach = 140;
TOFL = 9000;

PAX = 275; %passengers
Abreast = 8; %number of passengers abreast
Aisles = 2;
Weight_cargo = 12000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards

type_engineqty = 3;
elseif type_inputs ==3 %Quiz
Taper = 0.35;

height = 35000; %ft
M = 0.82;
Range_scheduled = 4000;
FF_max = 1;
V_approach = 135;
TOFL = 6000;

PAX = 200; %passengers
Abreast = 6; %number of passengers abreast
Aisles = 2;
Weight_cargo = 4000; %weight of cargo
Number_flightcrew = 2; %number of flight crew
Number_stewards = round((PAX/50)+0.49); %number of stewards
end

gamma = 1.4;
R = 1718;
T = 218.9; %K
rho = .023751; %lb/ft^3
sigma = .953; %Ratio between local and sea level densities
delta = .2360; %Ratio between local and sea level pressures

%a = sqrt(gamma*R*T);
a = 576.4;

%% Digitized Plots

Table = readtable('Tables.xlsx');
Table = Table{::,:};

if type_airfoil == 1
% Figure 1a: Effect of Wing Sweep and Thickness on Mdiv (Conventional)
x1 = Table(1:165,1);
y1 = Table(1:165,3);
z1 = Table(1:165,2);

```

```

[fit_TC,info_TC] = fit([x1,y1],z1,'poly23');

% Figure 1b: Effect of Wing Sweep and Thickness on Mdiv (Supercritical)
elseif type_airfoil == 2
    x2 = Table(1:211,4);
    y2 = Table(1:211,6);
    z2 = Table(1:211,5);
    [fit_TC,info_TC] = fit([x2,y2],z2,'poly35');
end

% Figure 2: Wing Drag Divergence Change Due to Lift
if type_airfoil == 1
    x3 = Table(1:25,7);
    y3 = Table(1:25,8);
    [fit_MDIVdelta,info_MDIVdelta] = fit(y3,x3,'power2');
elseif type_airfoil == 2
    x4 = Table(1:29,9);
    y4 = Table(1:29,10);
    [fit_MDIVdelta,info_MDIVdelta] = fit(y4,x4,'power2');
end

% Figure 3: CLmax Conceptual Design Estimates
x5 = Table(1:34,11);
y5 = Table(1:34,12);
[fit_CLmax_takeoff,info_CLmax_takeoff] = fit(x5,y5,'smoothingspline');
x6 = Table(1:31,13);
y6 = Table(1:31,14);
[fit_CLmax_landing,info_CLmax_landing] = fit(x6,y6,'smoothingspline');

% Figure 4: JT8D-9 Fuel Fraction Estimate for All Out Range
x7 = Table(1:41,15);
y7 = Table(1:41,16);
[fit_FF,info_FF] = fit(x7,y7,'cubicinterp'); % FF is Fuel Fraction or W_f/W_to

% Figure 5: Jet Aircraft TOFL with Engine Failure
x8 = Table(1:58,17);
y8 = Table(1:58,18);
[fit_k_2ENG,info_k_2ENG] = fit(y8,x8,'poly2');
x9 = Table(1:63,19);
y9 = Table(1:63,20);
[fit_k_3ENG,info_k_3ENG] = fit(y9,x9,'poly2');
x10 = Table(1:67,21);
y10 = Table(1:67,22);
[fit_k_4ENG,info_k_4ENG] = fit(y10,x10,'poly2');

% Cf
x11 = Table(1:50,23);
y11 = Table(1:50,24);
y11 = y11.*(1e-3);
[fit_Cf, info_Cf] = fit(x11,y11,'power2');

% Body Form Factor
x12 = Table(1:12,25);
y12 = Table(1:12,26);
[fit_k, info_k] = fit(x12,y12,'exp2');

% Max Climb Thrust @ 15000ft
x13 = Table(1:34,27);
y13 = Table(1:34,28);
[fit_T_avbl15, info_T_avbl15] = fit(x13,y13,'smoothingspline');
x14 = Table(1:9,29);
y14 = Table(1:9,30);
[fit_SFC_15, info_SFC_15] = fit(x14,y14,'smoothingspline');

```

```
% Max Climb Thrust @ 25000ft
x15 = Table(1:30,31);
y15 = Table(1:30,32);
[fit_T_avbl25, info_T_avbl25] = fit(x15,y15,'smoothingspline');
x = Table(1:6,33);
y = Table(1:6,34);
[fit_SFC_25, info_SFC_25] = fit(x,y,'smoothingspline');

% Max Climb and Thrust @ 35000ft
x16 = Table(1:9,37);
y16 = Table(1:9,38);
[fit_SFC_35, info_SFC_35] = fit(x16,y16,'lin');

% Profile Drag at Takeoff
x17 = Table(1:60,39);
y17 = Table(1:60,40);
[fit_CDP_takeoff, info_CDP_takeoff] = fit(y17,x17,'poly5');

% Profile Drag at Landing
x18 = Table(1:60,41);
y18 = Table(1:60,42);
[fit_CDP_landing, info_CDP_landing] = fit(y18,x18,'poly5');

% Clean Wing CLmax
x19 = Table(1:69,43);
y19 = Table(1:69,45);
z19 = Table(1:69,44);
[fit_CLmax_clean, info_CLmax_clean] = fit([x19,y19],z19,'poly32');

% JT9D Dry Takeoff
x20 = Table(1:18,46);
y20 = Table(1:18,47);
[fit_JT9D_takeoffthrust, info_JT9D_takeoffthrust] = fit(x20,y20,'lin');

% JT9D Climb
x21 = Table(1:26,48);
y21 = Table(1:26,49);
[fit_JT9D_climbthrust, info_JT9D_climbthrust] = fit(x21,y21,'lin');

%% Figures

if type_graph == 2

    figure
    plot(fit_TC_conv,[x1,y1],z1);

    figure
    plot(fit_TC_sc,[x2,y2],z2);
    hold on
    ylim([0 40]);
    zlim([0.07 .2]);
    hold off

    figure
    hold on
    plot(x3,y3)
    plot(x4,y4)
    xlim([-0.04 .02])
    ylim([.4 .7])
    % plot(fit_MDIVdelta_conv)
    % plot(fit_MDIVdelta_sc)

end
```

```
% xlim([-1 2])
hold off

figure
hold on
plot(x5,y5);
plot(x6,y6);
hold off

figure
plot(fit_FF);

figure
hold on
plot(x8,y8,x9,y9,x10,y10)
hold off

figure
plot(fit_Cf,x11,y11)
hold on
set(gca,'xscale','log')
title('Skin Friction Coefficient wrt Reynolds Number')
xlabel('Reynolds Number (Re)')
ylabel('Coefficient of Skin Friction (k)')
hold off

figure
plot(fit_k,x12,y12);
hold on
title('Body Form Factor wrt Fineness Ratio')
xlabel('Fineness Ratio (l/d)')
ylabel('Body Form Factor (k)')
hold off

figure
plot(x17,y17,x18,y18)

figure
hold on
% plot([z19,x19],y19)
plot(fit_CLmax_clean)
xlim([.04 .16]);
ylim([0 35]);
zlim([.8 1.3]);
hold off
end

%% Placeholders

iteration = 1;

% table_engineqty_AR = AR;
% table_engineqty_EngineQty = type_engineqty;
% table_engineqty_DOC = DOC_perPAXMile;
% table_engineqty_Weight = W_takeoff;

SFC_jt9d = 0.61;
if type_engine == 1
    SFC_jt9d = 0.9 * SFC_jt9d;
end

%% Configuration Loop: Engine
```

```

i = 1;
for type_engineqty = 2:1:4
j = 1;
for AR = range_AR
    Weightincrement = 0;
    Thrust_reqtop_JT9D = 10001;
    while Thrust_reqtop_JT9D > 10000
%% Range Loop
    Range = 0;
    Range_ao = 500000;
    Fuelincrement = 0;
    while abs(Range - Range_ao) > 2
%% CL Loop
    CL_guess = 0.5;
    CL_ic = 0;
    while abs(CL_ic - CL_guess) > 0.001
        Mdiv_delta = fit_MDIVdelta(CL_guess);
        Mdiv = (M + .004) - Mdiv_delta;
        TC = fit_TC(Mdiv,Sweep);
        CLmax_landing = fit_CLmax_landing(((cosd(Sweep))^2)*((TC)^2)*AR));
        CLmax_takeoff = fit_CLmax_takeoff(((cosd(Sweep))^2)*((TC)^2)*AR));%5
        WS_landing = ((V_approach/1.3)^2) * (sigma * CLmax_landing) / 296;%6
        V_cruise = M * a;
        Range_ao = Range_scheduled + 200 + (V_cruise*(3/4));%7
        FF_jt8d = fit_FF(Range_ao); %8
        if type_inputs == 1
            FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
        elseif type_inputs == 2
            FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
        elseif type_inputs == 3
            FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
        end
        if type_engine == 1 || type_engine == 2
            FF = FF_jt9d + Fuelincrement;
        elseif type_engine == 3
            FF = FF_jt8d + Fuelincrement;
        end
        WS_takeoff = WS_landing/(1-(FF_max*FF));
        WS_ic = .965 * WS_takeoff;
        CL_ic = WS_ic / (1481 * delta * M^2);
        if abs(CL_ic - CL_guess) > 0.001
            CL_guess = (CL_guess + CL_ic)/2;
        end
    end
%% TOFL
    if type_engineqty == 2
        k_1 = fit_k_2ENG((TOFL/1000));
    elseif type_engineqty == 3
        k_1 = fit_k_3ENG((TOFL/1000));
    elseif type_engineqty == 4
        k_1 = fit_k_4ENG((TOFL/1000));
    end
    WT_7V_lo = (k_1/WS_takeoff) * sigma * CLmax_takeoff;
    V_lo = 1.2 *sqrt((296*WS_takeoff)/(sigma*CLmax_takeoff));
    M_lo = V_lo/(661/sqrt(sigma));
    Thrust_sls = fit_JT9D_takeoffthrust(0);
    Thrust_M = fit_JT9D_takeoffthrust(M_lo*0.7);
    WT = (WT_7V_lo * Thrust_M/Thrust_sls) + Weightincrement;
%% Weight
    eta = 1.5*2.5;
    % Wing
    TC_bar = TC + 0.03;

```

```

W_w = (.00945 * (AR^0.8) * ((1+Taper)^0.25) * K_w * (eta^0.5)) / ((TC_bar^0.4) * cosd(Sweep) * WS_takeoff^0.695); %times W_takeoff^1.195
% Fuselage
K_f = 11.5;
L_f = (3.76 * (PAX/Abreast) + 33.2);
D_f = ((1.75*Abreast) + (1.58*Aisles) + 1);
if type_flight == 2
    L_f = 1.1 * L_f;
    D_f = 1.1 * D_f;
end
W_fus = 0.6727 * K_f * (L_f^0.6) * (D_f^0.72) * (eta^0.3); %times W_takeoff^0.235
% Landing Gear
W_lg = 0.04; %times W_takeoff
% Nacelle & Pylon
W_np = (0.0555/WT); %times W_takeoff
% Tail Surface
W_ts = K_ts * W_w; %times W_takeoff^1.195
% Power Plant
W_pp = 1/(3.58*WT); %times W_takeoff
if type_engine == 1
    W_pp = W_pp * 1.1;
end
% Fuel
W_f = 1.0275 * (FF);
% Payload
W_pl = 215*PAX + Weight_cargo;
% Fixed Equipment
W_fe = (132*PAX) + (300*type_engineqty) + (260*Number_flightcrew) + (170*Number_stewards);
W_fe_wto = (0.035); %times W_takeoff
if type_structure == 2
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_np = 0.8 * W_np;
elseif type_structure == 3
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_fus = 0.85 * W_fus;
    W_fe = 0.9 * W_fe;
    W_fe_wto = 0.9 * W_fe_wto;
    W_np = 0.8 * W_np;
end
a_W = W_w + W_ts;
b_W = W_fus;
c_W = W_lg + W_np + W_pp + W_f + W_fe_wto - 1;
d_W = W_pl + W_fe;
W_takeoff = 300000;
difference_1 = W_takeoff;
while abs(difference_1) > 0.1
    if abs(difference_1) > 0.5
        difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
        W_takeoff = W_takeoff + 4*(difference_1);
    elseif abs(difference_1) <= 0.5
        difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
        W_takeoff = W_takeoff + (difference_1);
    end
end
W_fuel = W_f * W_takeoff;
%% Wing Sizing
S = W_takeoff/WS_takeoff;
b = sqrt(AR*S);
c_bar = S/b;
Thrust_total = W_takeoff/WT;

```

```

Thrust_engine = Thrust_total/type_engineqty;

%% Drag
Re_l = 2.852e6 * 0.5; % 0.5 * rho * v / mu
% Wing
Re_w = Re_l * c_bar;
Cf_w = fit_Cf(Re_w);
Swet_w = 2 * S * 1.02;
z_w = ((2-M^2)*cosd(Sweep))/sqrt(1-(M^2).*cosd(Sweep)));
k_w = 1+(z_w*TC)+100*(TC^4);
f_w = k_w*Cf_w*Swet_w;
% Fuselage
Swet_fus = 0.9*pi*D_f*L_f;
Re_fus = Re_l * L_f;
Cf_fus = fit_Cf(Re_fus);
fineness_fus = L_f/D_f;
k_fus = fit_k(fineness_fus);
f_fus = k_fus*Cf_fus*Swet_fus;
% Tail
f_t = 0.35*f_w;
% Nacelles
Re_n = Re_l * c_bar;
Swet_n = 2.1 * sqrt(Thrust_engine) * type_engineqty;
Cf_n = fit_Cf(Re_n);
k_n = 1.25;
f_n = k_n*Cf_n*Swet_n;
% Pylons
f_p = 0.2*f_n;
% Total
f = f_w + f_fus + f_t + f_n + f_p;
CD_overall = f/S;
e = 1/(1.035 + (.38*CD_overall*pi*AR));
CD_gear = CD_overall;

%% Climb
W_avgcl = (1.965) * W_takeoff / 2;
h_avgcl = (20/35) * height;
sigma_cl = .5702;
V_ldmax = (12.9/(f*e)^(1/4)) * sqrt(W_avgcl/(sigma_cl*b));
V_cl = 1.3 * V_ldmax;
M_cl = V_cl/(973.1/1.68781);
Thrust_reqcl = (sigma_cl*f*(V_cl^2)/296) + ((94.1/(sigma_cl*e))*((W_avgcl/b)^2)*(1/4*(V_cl^2)));
Thrust_c115 = fit_T_avbl15(M_cl) * 1000;
Thrust_c125 = fit_T_avbl25(M_cl) * 1000;
SFC_15 = fit_SFC_15(M_cl);
SFC_25 = fit_SFC_25(M_cl);
Thrust_cl = (Thrust_c115 + Thrust_c125)/2;
SFC_cl = (SFC_15 + SFC_25)/2;
if type_engine == 1
    SFC_cl = SFC_cl * 0.9;
end
Thrust_avbl = (Thrust_engine/Thrust_sls) * Thrust_cl;
RC = (101*((type_engineqty*Thrust_avbl)-Thrust_reqcl)*V_cl)/W_avgcl;
Time_cl = height/RC;
Range_cl = V_cl * (Time_cl/60);
W_fcl = (type_engineqty*Thrust_avbl) * SFC_cl * (Time_cl/60);

%% Range
W_0 = W_takeoff-W_fcl;
W_I = (1-FF) * W_takeoff;
CL_avg = ((W_0+W_I)/(2*S)) / (1481*delta*(M^2));
CD_i = (CL_avg^2)/(pi*AR*e);
CD_c = 0.001;
CD = CD_overall + CD_i + CD_c;

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LD = CL_avg/CD;
Thrust_reqcr = ((W_0 + W_I)/(2*LD));
Thrust_reqcrjt9d = Thrust_reqcr * (Thrust_sls/Thrust_engine);
Thrust_reqcreng = Thrust_reqcrjt9d / type_engneqty;
SFC_cr = fit_SFC_35(Thrust_reqcreng);
if type_engine == 1
    SFC_cr = SFC_cr * 0.9;
end
Range_cr = (V_cruise/SFC_cr) * LD * log(W_0/W_I);
Range = Range_cl + Range_cr;
difference_2 = Range - Range_ao;
if difference_2 < -200 %200 or less
    Fuelincrement = Fuelincrement + 0.01;
elseif difference_2 >= 200 %200 or more
    Fuelincrement = Fuelincrement - 0.01;
elseif difference_2 < -18 && (Range - Range_ao) >= -200 %Between -20 and -200
    Fuelincrement = Fuelincrement + 0.001;
elseif difference_2 > 18 && (Range - Range_ao) <= 200 %Between 20 and 200
    Fuelincrement = Fuelincrement - 0.001;
elseif difference_2 < -3 && (Range - Range_ao) >= -18 %Between 0 and -20
    Fuelincrement = Fuelincrement + 0.0001;
elseif difference_2 >= 3 && (Range - Range_ao) <= 18 %Between 0 and 20
    Fuelincrement = Fuelincrement - 0.0001;
elseif difference_2 < 0 && (Range - Range_ao) >= -3 %Between 0 and -20
    Fuelincrement = Fuelincrement + 0.00001;
elseif difference_2 >= 0 && (Range - Range_ao) <= 3 %Between 0 and 20
    Fuelincrement = Fuelincrement - 0.00001;
end
end
%% Top of Climb
CL_ic_top = (W_0/S)/(1481*delta*M^2);
CDi_top = (CL_ic_top^2) / (pi*AR*e);
CD_top = CD_overall + CDi_top + 0.001;
LD_top = CL_ic_top / CD_top;
if type_inputs == 2
    LD_top = 15.05; % SAMPLE
end
Thrust_reqtop = W_0 / LD_top;
Thrust_reqtop_engine = Thrust_reqtop / type_engneqty;
Thrust_reqtop_JT9D = (Thrust_sls/Thrust_engine) * Thrust_reqtop_engine;

%% Climb Gradients
% 1st Segment
CL_seg1 = CLmax_takeoff/(1.2^2);
CL_to_CLmax_to = CL_seg1/CLmax_takeoff;
CDp_seg1 = fit_CDp_takeoff(CL_to_CLmax_to);
CD_seg1 = CD_overall + CDp_seg1 + CD_gear + ((CL_seg1^2)/(pi*AR*e));
LD_seg1 = CL_seg1/CD_seg1;
Thrust_reqseg1 = W_takeoff/LD_seg1;
Thrust_avblseg1 = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_lo);
Grad_1 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg1)*100/W_takeoff;
% 2nd Segment
CD_seg2 = CD_overall + CDp_seg1 + ((CL_seg1^2)/(pi*AR*e));
LD_seg2 = CL_seg1/CD_seg2;
Thrust_reqseg2 = W_takeoff/LD_seg2;
Grad_2 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg2)*100/W_takeoff;
% 3rd Segment
CLmax_clean = fit_CLmax_clean(TC,Sweep);
V_seg3 = 1.2*sqrt((296*WS_takeoff)/(.925*CLmax_clean));
M_seg3 = V_seg3/659;
CL_seg3 = CLmax_clean/(1.2^2);
CD_seg3 = CD_overall + ((CL_seg3^2)/(pi*AR*e));

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LD_seg3 = CL_seg3/CD_seg3;
Thrust_reqseg3 = W_takeoff/LD_seg3;
Thrust_avblseg3 = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_seg3);
Grad_3 = ((type_engneqty-1)*Thrust_avblseg3-Thrust_reqseg3)*100/W_takeoff;
% Approach
CL_approach = CLmax_takeoff/(1.3^2);
CL_approach_CLmax_landing = CL_approach/CLmax_takeoff;
CDp_approach = fit_CDp_takeoff(CL_approach_CLmax_landing);
CD_approach = CD_overall + CDp_approach + (CL_approach^2)/(pi*AR*e);
LD_approach = CL_approach/CD_approach;
W_landing = WS_landing * S;
Thrust_reqapproach = W_landing/LD_approach;
V_approach_grad = sqrt((296*WS_landing)/(0.953*CL_approach));
M_approach = V_approach_grad/659;
Thrust_avblapproach = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_approach);
Grad_approach = ((type_engneqty-1)*Thrust_avblapproach-Thrust_reqapproach)*100/W_landing;
% Landing
CL_landing = CLmax_landing/1.3^2;
CDp_landing = fit_CDp_landing(1/1.3^2);
CD_landing = CD_overall + CDp_landing + CD_gear + (CL_landing^2)/(pi*AR*e);
LD_landing = CL_landing/CD_landing;
Thrust_reqlanding = W_landing/LD_landing;
V_landing = sqrt((296*WS_landing)/(0.953*CL_landing));
M_landing = V_landing/659;
Thrust_avbllanding = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_landing);
Grad_landing = ((type_engneqty*Thrust_avbllanding) - Thrust_reqlanding) * 100 / W_landing;
% Climb Requirements (pg. 39)
if type_engneqty == 2
    Grad_1_min = 0;
    Grad_2_min = 2.4;
    Grad_3_min = 1.2;
    Grad_approach_min = 2.1;
    Grad_landing_min = 3.2;
elseif type_engneqty == 3
    Grad_1_min = 0.3;
    Grad_2_min = 2.7;
    Grad_3_min = 1.5;
    Grad_approach_min = 2.4;
    Grad_landing_min = 3.2;
elseif type_engneqty == 4
    Grad_1_min = 0.5;
    Grad_2_min = 3.0;
    Grad_3_min = 1.7;
    Grad_approach_min = 2.7;
    Grad_landing_min = 3.2;
end
if Thrust_reqtop_JT9D > 10000 || Grad_1 < Grad_1_min || Grad_2 < Grad_2_min || Grad_3 <
Grad_3_min || Grad_approach < Grad_approach_min || Grad_landing < Grad_landing_min
    Weightincrement = Weightincrement - 0.1;
    disp('Gradient Failed')
end
%% DOC
D = Range_scheduled * 1.15;
%Time_gm = (D / (11.866+0.040669*D))/60;
Time_gm = 0.25;
Time_c1_hr = Time_c1/60;
Time_d = 0;
Time_am = 0.10;
if D <= 1400

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k_a = (7+0.015*D);
elseif D > 1400
    k_a = 0.02*D;
end
D_d = 0;
Time_cr = ((D+k_a+20)-(Range_cl*1.15+D_d))/(V_cruise*1.15);
V_B = D / (Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am);
% Block Time
Time_b = Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am;
% Block Fuel
F_cr_am = Thrust_reqcr * SFC_cr * (Time_cr+Time_am);
F_cl = W_fcl;
F_b = F_cr_am + F_cl;
% Flying Operations Cost
% a. Flight Crew
P = W_pl / 2000;
if Number_flightcrew == 2
    CostPerBlockHr = 17.849 * (V_cruise*W_takeoff/1e5)^0.3 + 40.83;
else
    CostPerBlockHr = 24.261 * (V_cruise*W_takeoff/1e5)^0.3 + 57.62;
end
C_TM_FlightCrew = CostPerBlockHr / (V_B * P);
% b. Fuel and Oil
if type_flight == 1
    C_ft = 0.0438;
elseif type_flight == 2
    C_ft = 0.0625;
end
C_ot = 2.15;
C_TM_FuelOil = ( 1.02*F_b*C_ft + type_engneqty*C_ot*Time_b*0.135 ) / (D*P);
% c. Hull Insurance Costs
W_a = W_takeoff * (1-FF) - W_pl - (W_pp*W_takeoff);
C_a = 2.4e6 + (87.5*W_a);
C_e = 590000 + (16*Thrust_engine);
if type_inputs == 2
    C_e = 1314942;
end
C_T = (type_engneqty*C_e) + C_a;
IR_A = 0.01;
U = 630 + 4000/( 1 + 1/(Time_b + 0.5)); % block hrs/yr
C_TM_HullInsurance = IR_A * C_T / (U * V_B * P);
% Direct Maintenance
% a. Airframe-Labor
K_FHa = 4.9169 * log10(W_a/1000) - 6.425;
K_FCa = 0.21256 * log10(W_a/1000)^3.7375;
T_F = Time_b - Time_gm;
R_L = 8.6;
C_TM_a_AirframeLabor = (K_FHa * T_F + K_FCa) * R_L * (1 + 0.29*(M-1))^1.5 / (V_B * Time_b * P);
% b. Airframe Material
C_FHa = ((1.5994*C_a)/1e6) + 3.4263;
C_FCa = ((1.9229*C_a)/1e6) + 2.2504;
C_TM_b_AirframeMaterial = (C_FHa*T_F+C_FCa) / (V_B*Time_b*P);
% c. Engine Labor
K_FHe = (type_engneqty*(Thrust_engine/1e3))/(0.82715*(Thrust_engine/1e3)+ 13.639);
K_FCe = 0.2 * type_engneqty;
C_TM_c_EngineLabor = ((K_FHe*T_F+K_FCe)*R_L) / (V_B*Time_b*P);
% d. Engine Material
C_FHe = (((28.2353*C_e)/1e6) - 6.5176) * type_engneqty;
C_FCe = (((3.6698*C_e)/1e6) + 1.3685) * type_engneqty;
C_TM_d_EngineMaterial = (C_FHe*T_F+C_FCe) / (V_B*Time_b*P);
if type_engine == 1
    C_TM_d_EngineMaterial = C_TM_d_EngineMaterial * 1.1;

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```

    end
    % e. Total Maintenance - Burdened
    C_TM_e_Maintenance = (C_TM_a_AirframeLabor + C_TM_b_AirframeMaterial + C_TM_c_EngineLabor + %
C_TM_d_EngineMaterial)*2;
    % Depreciation
    D_a = 14;
    C_TM_Depreciation = (1/(V_B*P)) * (C_T + 0.06*(C_T-type_engineqty*C_e)+0.3*type_engineqty*C_e) %
(D_a*U);
    % Total DOC
    DOC_perTonMile = C_TM_FlightCrew + C_TM_FuelOil + C_TM_HullInsurance + C_TM_e_Maintenance +
C_TM_Depreciation;
    DOC_perPAXMile = DOC_perTonMile * P/PAX;

    %% Data Collection
    % Plots
    table_engineqty_AR(i,j) = AR;
    table_engineqty_EngineQty(i,j) = type_engineqty;
    table_engineqty_DOC(i,j) = DOC_perPAXMile;
    table_engineqty_Weight(i,j) = W_takeoff;
    table_engineqty_EngineMaterialCost(i,j) = C_TM_d_EngineMaterial;
    table_engineqty_EngineLabor(i,j) = C_TM_c_EngineLabor;

    iteration = iteration + 1;
    j = j+1;
end
i = i+1;
end

figure
hold on
for i = [1:1:(type_engineqty-1)]
    plot(table_engineqty_AR(i,:),table_engineqty_DOC(i,:))
end
legend('2','3','4')
title(legend,'Engine Quantity')
title('DOC wrt Engine Quantity')
xlabel('Aspect Ratio')
ylabel('DOC ($)')
hold off

figure
hold on
for i = [1:1:(type_engineqty-1)]
    plot(table_engineqty_AR(i,:),table_engineqty_EngineMaterialCost(i,:))
end
legend('2','3','4')
title(legend,'Engine Quantity')
title('Engine Material Costs wrt Engine Quantity')
xlabel('Aspect Ratio')
ylabel('Material Costs ($)')
hold off

figure
hold on
for i = [1:1:(type_engineqty-1)]
    plot(table_engineqty_AR(i,:),table_engineqty_EngineLabor(i,:))
end
legend('2','3','4')
title(legend,'Engine Quantity')
title('Engine Labor Costs wrt Engine Quantity')
xlabel('Aspect Ratio')
ylabel('Labor Costs ($)')

```

```

hold off

%% Configuration Loop: Airfoil Shape
iteration = 1;
type_engineqty = 2;
i = 1;
for type_airfoil = 1:2
    if type_airfoil == 1
        % Figure 1a: Effect of Wing Sweep and Thickness on Mdiv (Conventional)
        x1 = Table(1:165,1);
        y1 = Table(1:165,3);
        z1 = Table(1:165,2);
        [fit_TC,info_TC] = fit([x1,y1],z1,'poly23');

        % Figure 1b: Effect of Wing Sweep and Thickness on Mdiv (Supercritical)
    elseif type_airfoil == 2
        x2 = Table(1:211,4);
        y2 = Table(1:211,6);
        z2 = Table(1:211,5);
        [fit_TC,info_TC] = fit([x2,y2],z2,'poly35');
    end
    j = 1;
    for AR = range_AR
        Weightincrement = 0;
        Thrust_reqtop_JT9D = 10001;
        while Thrust_reqtop_JT9D > 10000
            %% Range Loop
            Range = 0;
            Range_ao = 500000;
            Fuelincrement = 0;
            while abs(Range - Range_ao) > 2
                %% CL Loop
                CL_guess = 0.5;
                CL_ic = 0;
                while abs(CL_ic - CL_guess) > 0.001
                    Mdiv_delta = fit_MDIVdelta(CL_guess);
                    Mdiv = (M + .004) - Mdiv_delta;
                    TC = fit_TC(Mdiv,Sweep);
                    CLmax_landing = fit_CLmax_landing(((cosd(Sweep))^2)*((TC)^2)*AR));
                    CLmax_takeoff = fit_CLmax_takeoff(((cosd(Sweep))^2)*((TC)^2)*AR));%5
                    WS_landing = ((V_approach/1.3)^2) * (sigma * CLmax_landing) / 296;%6
                    V_cruise = M * a;
                    Range_ao = Range_scheduled + 200 + (V_cruise*(3/4));%7
                    FF_jt8d = fit_FF(Range_ao); %8
                    if type_inputs == 1
                        FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
                    elseif type_inputs == 2
                        FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
                    elseif type_inputs == 3
                        FF_jt9d = (FF_jt8d * (SFC_jt9d/.78)); %9
                    end
                    if type_engine == 1 || type_engine == 2
                        FF = FF_jt9d + Fuelincrement;
                    elseif type_engine == 3
                        FF = FF_jt8d + Fuelincrement;
                    end
                    WS_takeoff = WS_landing/(1-(FF_max*FF));
                    WS_ic = .965 * WS_takeoff;
                    CL_ic = WS_ic / (1481 * delta * M^2);
                    if abs(CL_ic - CL_guess) > 0.001
                        CL_guess = (CL_guess + CL_ic)/2;
                    end
                end
            end
        end
    end
end

```

```

    end
%% TOFL
if type_engineqty == 2
    k_1 = fit_k_2ENG((TOFL/1000));
elseif type_engineqty == 3
    k_1 = fit_k_3ENG((TOFL/1000));
elseif type_engineqty == 4
    k_1 = fit_k_4ENG((TOFL/1000));
end
WT_7V_lo = (k_1/WS_takeoff) * sigma * CLmax_takeoff;
V_lo = 1.2 * sqrt((296*WS_takeoff)/(sigma*CLmax_takeoff));
M_lo = V_lo/(661/sqrt(sigma));
Thrust_sls = fit_JT9D_takeoffthrust(0);
Thrust_M = fit_JT9D_takeoffthrust(M_lo*0.7);
WT = (WT_7V_lo * Thrust_M/Thrust_sls) + Weightincrement;

%% Weight
eta = 1.5*2.5;
% Wing
TC_bar = TC + 0.03;
W_w = (.00945 * (AR^0.8) * ((1+Taper)^0.25) * K_w * (eta^0.5))/((TC_bar^0.4) * cosd(Sweep) ↵
(WS_takeoff^0.695)); %times W_takeoff^1.195
% Fuselage
K_f = 11.5;
L_f = (3.76 * (PAX/Abreast) + 33.2);
D_f = ((1.75*Abreast) + (1.58*Aisles) + 1);
if type_flight == 2
    L_f = 1.1 * L_f;
    D_f = 1.1 * D_f;
end
W_fus = 0.6727 * K_f * (L_f^0.6) * (D_f^0.72) * (eta^0.3); %times W_takeoff^0.235
% Landing Gear
W_lg = 0.04; %times W_takeoff
% Nacelle & Pylon
W_np = (0.0555/WT); %times W_takeoff
% Tail Surface
W_ts = K_ts * W_w; %times W_takeoff^1.195
% Power Plant
W_pp = 1/(3.58*WT); %times W_takeoff
if type_engine == 1
    W_pp = W_pp * 1.1;
end
% Fuel
W_f = 1.0275 * (FF);
% Payload
W_pl = 215*PAX + Weight_cargo;
% Fixed Equipment
W_fe = (132*PAX) + (300*type_engineqty) + (260*Number_flightcrew) + (170*Number_stewards);
W_fe_wto = (0.035); %times W_takeoff
if type_structure == 2
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_np = 0.8 * W_np;
elseif type_structure == 3
    W_w = 0.7 * W_w;
    W_ts = 0.7 * W_ts;
    W_fus = 0.85 * W_fus;
    W_fe = 0.9 * W_fe;
    W_fe_wto = 0.9 * W_fe_wto;
    W_np = 0.8 * W_np;
end
a_W = W_w + W_ts;
b_W = W_fus;

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```

c_W = W_lg + W_np + W_pp + W_f + W_fe_wto - 1;
d_W = W_pl + W_fe;
W_takeoff = 300000;
difference_1 = W_takeoff;
while abs(difference_1) > 0.1
    if abs(difference_1) > 0.5
        difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
        W_takeoff = W_takeoff + 4*(difference_1);
    elseif abs(difference_1) <= 0.5
        difference_1 = a_W*(W_takeoff^1.195) + b_W*(W_takeoff^0.235) + c_W*W_takeoff + d_W;
        W_takeoff = W_takeoff + (difference_1);
    end
end
W_fuel = W_f * W_takeoff;
%% Wing Sizing
S = W_takeoff/WS_takeoff;
b = sqrt(AR*S);
c_bar = S/b;
Thrust_total = W_takeoff/WT;
Thrust_engine = Thrust_total/type_engineqty;
%% Drag
Re_l = 2.852e6 * 0.5; % 0.5 * rho * v / mu
% Wing
Re_w = Re_l * c_bar;
Cf_w = fit_Cf(Re_w);
Swet_w = 2 * S * 1.02;
z_w = ((2-M^2)*cosd(Sweep))/sqrt(1-(M^2).* (cosd(Sweep)));
k_w = 1+(z_w*TC)+100*(TC^4);
f_w = k_w*Cf_w*Swet_w;
% Fuselage
Swet_fus = 0.9*pi*D_f*L_f;
Re_fus = Re_l * L_f;
Cf_fus = fit_Cf(Re_fus);
fineness_fus = L_f/D_f;
k_fus = fit_k(fineness_fus);
f_fus = k_fus*Cf_fus*Swet_fus;
% Tail
f_t = 0.35*f_w;
% Nacelles
Re_n = Re_l * c_bar;
Swet_n = 2.1 * sqrt(Thrust_engine) * type_engineqty;
Cf_n = fit_Cf(Re_n);
k_n = 1.25;
f_n = k_n*Cf_n*Swet_n;
% Pylons
f_p = 0.2*f_n;
%Total
f = f_w + f_fus + f_t + f_n + f_p;
CD_overall = f/S;
e = 1/(1.035 + (.38*CD_overall*pi*AR));
CD_gear = CD_overall;
%% Climb
W_avgcl = (1.965) * W_takeoff / 2;
h_avgcl = (20/35) * height;
sigma_cl = .5702;
V_ldmax = (12.9/(f*e)^(1/4)) * sqrt(W_avgcl/(sigma_cl*b));
V_cl = 1.3 * V_ldmax;
M_cl = V_cl/(973.1/1.68781);
Thrust_reqcl = (sigma_cl*f*(V_cl^2)/296) + ((94.1/(sigma_cl*e))*((W_avgcl/b)^2)*(1/2*(V_cl^2)));
Thrust_cl15 = fit_T_avbl15(M_cl) * 1000;
Thrust_cl25 = fit_T_avbl25(M_cl) * 1000;

```

```

SFC_15 = fit_SFC_15(M_cl);
SFC_25 = fit_SFC_25(M_cl);
Thrust_cl = (Thrust_cl15 + Thrust_cl25)/2;
SFC_cl = (SFC_15 + SFC_25)/2;
if type_engine == 1
    SFC_cl = SFC_cl * 0.9;
end
Thrust_avbl = (Thrust_engine/Thrust_sls) * Thrust_cl;
RC = (101*((type_engneqty*Thrust_avbl)-Thrust_reqcl)*V_cl)/W_avgcl;
Time_cl = height/RC;
Range_cl = V_cl * (Time_cl/60);
W_fcl = (type_engneqty*Thrust_avbl) * SFC_cl * (Time_cl/60);

%% Range
W_0 = W_takeoff-W_fcl;
W_I = (1-FF) * W_takeoff;
CL_avg = ((W_0+W_I)/(2*S)) / (1481*delta*(M^2));
CD_i = (CL_avg^2)/(pi*AR*e);
CD_c = 0.001;
CD = CD_overall + CD_i + CD_c;
LD = CL_avg/CD;
Thrust_reqcr = ((W_0 + W_I)/(2*LD));
Thrust_reqcrjt9d = Thrust_reqcr * (Thrust_sls/Thrust_engine);
Thrust_reqcreng = Thrust_reqcrjt9d / type_engneqty;
SFC_cr = fit_SFC_35(Thrust_reqcreng);
if type_engine == 1
    SFC_cr = SFC_cr * 0.9;
end
Range_cr = (V_cruise/SFC_cr) * LD * log(W_0/W_I);
Range = Range_cl + Range_cr;
difference_2 = Range-Range_ao;
if difference_2 < -200 %200 or less
    Fuelincrement = Fuelincrement + 0.01;
elseif difference_2 >= 200 %200 or more
    Fuelincrement = Fuelincrement - 0.01;
elseif difference_2 < -18 && (Range-Range_ao) >= -200 %Between -20 and -200
    Fuelincrement = Fuelincrement + 0.001;
elseif difference_2 > 18 && (Range-Range_ao) <= 200 %Between 20 and 200
    Fuelincrement = Fuelincrement - 0.001;
elseif difference_2 < -3 && (Range-Range_ao) >= -18 %Between 0 and -20
    Fuelincrement = Fuelincrement + 0.0001;
elseif difference_2 >= 3 && (Range-Range_ao) <= 18 %Between 0 and 20
    Fuelincrement = Fuelincrement - 0.0001;
elseif difference_2 < 0 && (Range-Range_ao) >= -3 %Between 0 and -20
    Fuelincrement = Fuelincrement + 0.00001;
elseif difference_2 >= 0 && (Range-Range_ao) <= 3 %Between 0 and 20
    Fuelincrement = Fuelincrement - 0.00001;
end
end
%% Top of Climb
CL_ic_top = (W_0/S)/(1481*delta*M^2);
CDi_top = (CL_ic_top^2) / (pi*AR*e);
CD_top = CD_overall + CDi_top + 0.001;
LD_top = CL_ic_top / CD_top;
if type_inputs == 2
    LD_top = 15.05; % SAMPLE
end
Thrust_reqtop = W_0 / LD_top;
Thrust_reqtop_engine = Thrust_reqtop / type_engneqty;
Thrust_reqtop_JT9D = (Thrust_sls/Thrust_engine) * Thrust_reqtop_engine;

%% Climb Gradients
% 1st Segment

```

```

CL_seg1 = CLmax_takeoff/(1.2^2);
CL_to_CLmax_to = CL_seg1/CLmax_takeoff;
CDp_seg1 = fit_CDp_takeoff(CL_to_CLmax_to);
CD_seg1 = CD_overall + CDp_seg1 + CD_gear + ((CL_seg1^2)/(pi*AR*e));
LD_seg1 = CL_seg1/CD_seg1;
Thrust_reqseg1 = W_takeoff/LD_seg1;
Thrust_avblseg1 = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_lo);
Grad_1 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg1)*100/W_takeoff;
% 2nd Segment
CD_seg2 = CD_overall + CDp_seg1 + ((CL_seg1^2)/(pi*AR*e));
LD_seg2 = CL_seg1/CD_seg2;
Thrust_reqseg2 = W_takeoff/LD_seg2;
Grad_2 = ((type_engneqty-1)*Thrust_avblseg1-Thrust_reqseg2)*100/W_takeoff;
% 3rd Segment
CLmax_clean = fit_CLmax_clean(TC,Sweep);
V_seg3 = 1.2*sqrt((296*WS_takeoff)/(.925*CLmax_clean));
M_seg3 = V_seg3/659;
CL_seg3 = CLmax_clean/(1.2^2);
CD_seg3 = CD_overall + ((CL_seg3^2)/(pi*AR*e));
LD_seg3 = CL_seg3/CD_seg3;
Thrust_reqseg3 = W_takeoff/LD_seg3;
Thrust_avblseg3 = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_seg3);
Grad_3 = ((type_engneqty-1)*Thrust_avblseg3-Thrust_reqseg3)*100/W_takeoff;
% Approach
CL_approach = CLmax_takeoff/(1.3^2);
CL_approach_CLmax_landing = CL_approach/CLmax_takeoff;
CDp_approach = fit_CDp_takeoff(CL_approach_CLmax_landing);
CD_approach = CD_overall + CDp_approach + (CL_approach^2)/(pi*AR*e);
LD_approach = CL_approach/CD_approach;
W_landing = WS_landing * S;
Thrust_reqapproach = W_landing/LD_approach;
V_approach_grad = sqrt((296*WS_landing)/(.953*CL_approach));
M_approach = V_approach_grad/659;
Thrust_avblapproach = (Thrust_engine/Thrust_sls) * fit_JT9D_climbthrust(M_approach);
Grad_approach = ((type_engneqty-1)*Thrust_avblapproach-Thrust_reqapproach)*100/W_landing;
% Landing
CL_landing = CLmax_landing/1.3^2;
CDp_landing = fit_CDp_landing(1/1.3^2);
CD_landing = CD_overall + CDp_landing + CD_gear + (CL_landing^2)/(pi*AR*e);
LD_landing = CL_landing/CD_landing;
Thrust_reqlanding = W_landing/LD_landing;
V_landing = sqrt((296*WS_landing)/(0.953*CL_landing));
M_landing = V_landing/659;
Thrust_avbl_landing = (Thrust_engine/Thrust_sls) * fit_JT9D_takeoffthrust(M_landing);
Grad_landing = ((type_engneqty*Thrust_avbl_landing) - Thrust_reqlanding) * 100 / W_landing;
% Climb Requirements (pg. 39)
if type_engneqty == 2
    Grad_1_min = 0;
    Grad_2_min = 2.4;
    Grad_3_min = 1.2;
    Grad_approach_min = 2.1;
    Grad_landing_min = 3.2;
elseif type_engneqty == 3
    Grad_1_min = 0.3;
    Grad_2_min = 2.7;
    Grad_3_min = 1.5;
    Grad_approach_min = 2.4;
    Grad_landing_min = 3.2;
elseif type_engneqty == 4
    Grad_1_min = 0.5;
    Grad_2_min = 3.0;
    Grad_3_min = 1.7;

```

```

        Grad_approach_min = 2.7;
        Grad_landing_min = 3.2;
    end

    if Thrust_reqtop_JT9D > 10000 || Grad_1 < Grad_1_min || Grad_2 < Grad_2_min || Grad_3 <
Grad_3_min || Grad_approach < Grad_approach_min || Grad_landing < Grad_landing_min
        Weightincrement = Weightincrement - 0.1;
        disp('Gradient Failed')
    end
end

%% DOC
D = Range_scheduled * 1.15;
Time_gm = (D / (11.866+0.040669*D))/60;
Time_cl_hr = Time_cl/60;
Time_d = 0;
Time_am = 0.10;
if D <= 1400
    k_a = (7+0.015*D);
elseif D > 1400
    k_a = 0.02*D;
end
D_d = 0;
Time_cr = ((D+k_a+20)-(Range_cl*1.15+D_d))/(V_cruise*1.15);
V_B = D / (Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am);
% Block Time
Time_b = Time_gm + Time_cl_hr + Time_d + Time_cr + Time_am;
% Block Fuel
F_cr_am = Thrust_reqcr * SFC_cr * (Time_cr+Time_am);
F_cl = W_fcl;
F_b = F_cr_am + F_cl;
% Flying Operations Cost
% a. Flight Crew
P = W_pl / 2000;
if Number_flightcrew == 2
    CostPerBlockHr = 17.849 * (V_cruise*W_takeoff/1e5)^0.3 + 40.83;
else
    CostPerBlockHr = 24.261 * (V_cruise*W_takeoff/1e5)^0.3 + 57.62;
end
C_TM_FlightCrew = CostPerBlockHr / (V_B * P);
% b. Fuel and Oil
if type_flight == 1
    C_ft = 0.0438;
elseif type_flight == 2
    C_ft = 0.0625;
end
C_ot = 2.15;
C_TM_FuelOil = ( 1.02*F_b*C_ft + type_enginelqty*C_ot*Time_b*0.135 ) / (D*P);
% c. Hull Insurance Costs
W_a = W_takeoff * (1-FF) - W_pl - (W_pp*W_takeoff);
C_a = 2.4e6 + (87.5*W_a);
C_e = 590000 + (16*Thrust_engine);
if type_inputs == 2
    C_e = 1314942;
end
C_T = (type_enginelqty*C_e) + C_a;
IR_A = 0.01;
U = 630 + 4000/( 1 + 1/(Time_b + 0.5)); % block hrs/yr
C_TM_HullInsurance = IR_A * C_T / (U * V_B * P);
% Direct Maintenance
% a. Airframe-Labor
K_FHa = 4.9169 * log10(W_a/1000) - 6.425;

```

```

K_FCa = 0.21256 * log10(W_a/1000)^3.7375;
T_F = Time_b - Time_gm;
R_L = 8.6;
C_TM_a_AirframeLabor = (K_FHa * T_F + K_FCa) * R_L * (1 + 0.29*(M-1))^1.5 / (V_B * Time_b * P);
% b. Airframe Material
C_FHa = ((1.5994*C_a)/1e6) + 3.4263;
C_FCa = ((1.9229*C_a)/1e6) + 2.2504;
C_TM_b_AirframeMaterial = (C_FHa*T_F+C_FCa) / (V_B*Time_b*P);
% c. Engine Labor
K_FHe = (type_engineqty*(Thrust_engine/1e3))/(0.82715*(Thrust_engine/1e3)+ 13.639);
K_FCe = 0.2 * type_engineqty;
C_TM_c_EngineLabor = ((K_FHe*T_F+K_FCe)*R_L) / (V_B*Time_b*P);
% d. Engine Material
C_FHe = (((28.2353*C_e)/1e6) - 6.5176) * type_engineqty;
C_FCe = (((3.6698*C_e)/1e6) + 1.3685) * type_engineqty;
C_TM_d_EngineMaterial = (C_FHe*T_F+C_FCe) / (V_B*Time_b*P);
if type_engine == 1
    C_TM_d_EngineMaterial = C_TM_d_EngineMaterial * 1.1;
end
% e. Total Maintenance - Burdened
C_TM_e_Maintenance = (C_TM_a_AirframeLabor + C_TM_b_AirframeMaterial + C_TM_c_EngineLabor +
C_TM_d_EngineMaterial)*2;
% Depreciation
D_a = 14;
C_TM_Depreciation = (1/(V_B*P)) * (C_T + 0.06*(C_T-type_engineqty*C_e)+0.3*type_engineqty*C_e) *
(D_a*U);
% Total DOC
DOC_perTonMile = C_TM_FlightCrew + C_TM_FuelOil + C_TM_HullInsurance + C_TM_e_Maintenance +
C_TM_Depreciation;
DOC_perPAXMile = DOC_perTonMile * P/PAX;

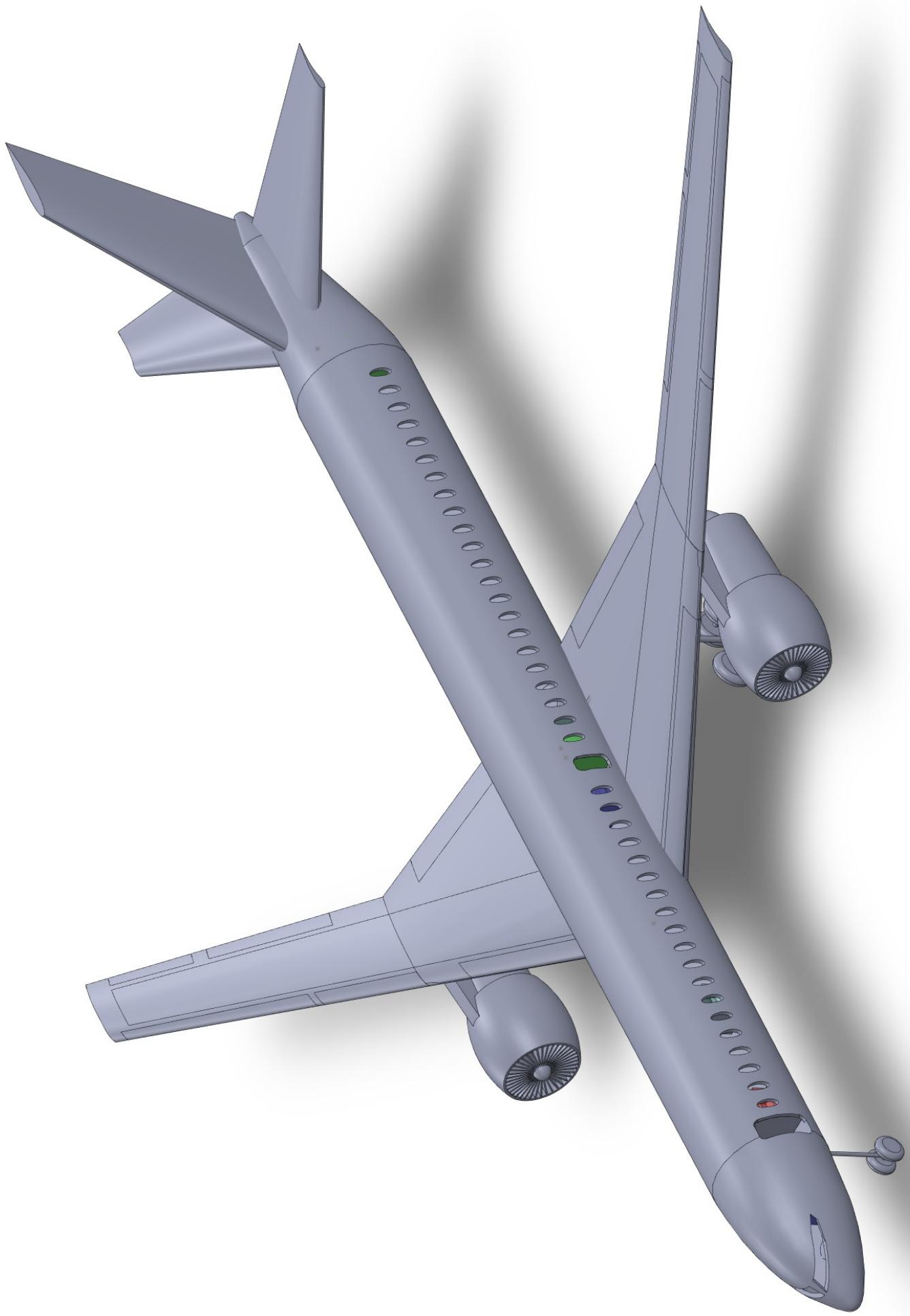
%% Data Collection
% Plots
table_airfoil_AR(i,j) = AR;
table_airfoil_AirfoilType(i,j) = type_airfoil;
table_airfoil_DOC(i,j) = DOC_perPAXMile;
table_airfoil_Weight(i,j) = W_takeoff;

iteration = iteration + 1
j = j+1;
end
i = i+1
end

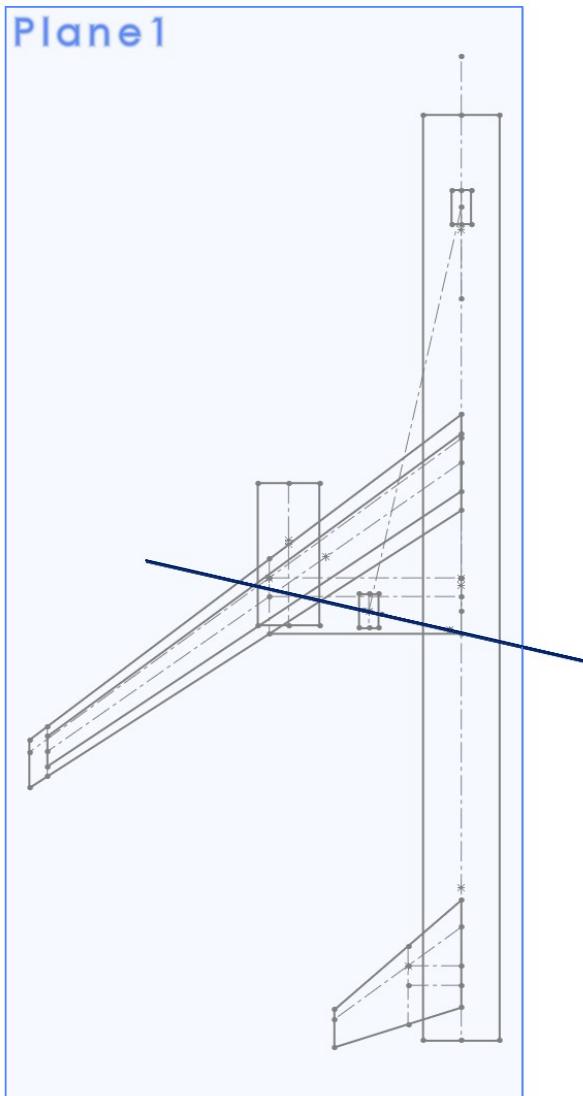
figure
hold on
for i = [1:type_airfoil]
    plot(table_airfoil_AR(i,:),table_airfoil_DOC(i,:))
end
legend('Conventional','Supercritical')
title(legend,'Airfoil Type')
title('DOC wrt Airfoil Type')
xlabel('Aspect Ratio')
ylabel('DOC ($)')
hold off

```

3D Model



Sketch of Dimensions



Tables

| Wing Sizing | |
|------------------------------|-----------------------------|
| AR | 12 |
| Sweep | 36 |
| MAC | 147.72 |
| H Tail Sizing | |
| AR | 3.5 |
| Taper | 0.35 |
| Volume Coeff | 2.25 |
| Tail Arm | 646.9453 |
| S | 77670.26 |
| b | 521.3884 |
| C_root | 1902 |
| C_tip | 157.2 |
| Thickness/Chord | 0.5 |
| Engine dry | 0.136 |
| Abreast | 2 |
| Aisles | 6 |
| V Tail Sizing | |
| AR | 3.5 |
| Taper | 0.35 |
| Volume Coeff | 2.25 |
| Tail Arm | 646.9453 |
| S | 77670.26 |
| b | 521.3884 |
| C_root | 2206.995 |
| C_tip | 77.24273 |
| Sweep | 36 |
| MAC | 160.4796 |
| Engine Sizing | |
| Thrust Max | 1.6 |
| Bypass Ratio | 0.5 |
| Fan Diameter | 0.079 |
| Fan Length | 646.9453 |
| Nacelle Diameter | 56801.37 |
| Nacelle Inlet Length | 150.7334 |
| Nacelle Total Length | 502.4445 |
| y_Engine | 251.2223 |
| Engine Offset | 36 |
| MAC | 390.7902 |
| Wing Parameters | |
| t/c | 72790 |
| Taper | 5 |
| Root Chord | 115 |
| Weight of Fuel | 183 |
| Fuel (Gallons) | 12163.65 |
| Fuel (in^3) | 281090 |
| Fuel Per Tank | 1405045 |
| Tank Height | 80.5 |
| Volume of Tank | 292.05 |
| Front Spar Location | 354.7781 |
| Rear Spar Location | 126.5 |
| Fuel Tip Chord | 102.6545 |
| Fuselage | |
| Base Height | 0.1366 |
| Base Width | 0.5 |
| A_1 | 197.099 |
| Root Chord | 197.099 |
| Tip Height | 81619 |
| Tip Width | 12163.65 |
| A_2 | 61.59271 |
| Length of Tank | 777.3213 |
| Volume of Tank | 850 |
| Centroid location | 145624.4 |
| Front Spar from Leading Edge | -49978.9 |
| Rear Spar from Leading Edge | 338.5885 (negative is good) |
| Fuel Weight | 30.65984 |

| Rectangular Frustum Parameter | |
|-------------------------------|----------|
| Base Height | 24.23135 |
| Base Width | 118.2594 |
| A_1 | 2865.584 |
| Afterbody length | 12.62035 |
| Wing 1/4 MAC Position | 951 |
| Fuselage | |
| Fuselage Length | 1902 |
| Fuselage Diameter | 157.2 |
| Nose Length | 235.8 |
| Afterbody length | 314.4 |
| Wing 1/4 MAC Position | 951 |

If negative, move stuff back

Landing Gear
W_takeoff Main Gear per Wheel
Nose Gear per Wheel

| Length | Weight | Moment |
|-------------|--------|----------|
| 0 | 288610 | 0 |
| -15.3299191 | 288610 | -4424368 |
| 15.3299191 | 28861 | 4424368 |

| | |
|-----------------------|-----------------|
| Passengers | 200 |
| First Class Seats | 16 |
| Abreast | 4 |
| Rows | 4 |
| LAV | 2 38in x 40in |
| Galley Carts | 4.8 12in x 34in |
| Seat Pitch | 40in |
| Depth/Recline | 28in/36in |
| Bulkhead to seat nose | 24in |
| Aisle Width | 20in |
| Economy Seats | 184 |
| Abreast | 6 |
| Rows | 30.66667 |
| LAV | 3.68 |
| Galley Carts | 14.72 |
| Seat Pitch | 32in |
| Depth/Recline | 28in/36in |
| Bulkhead to seat nose | 18in |
| Aisle Width | 18in |
| LDW Volume | 84 |
| Cargo Weight | 4000 |
| Cargo Density | 10 |
| Cargo Volume | 400 |
| Containers Required | 4.761905 |