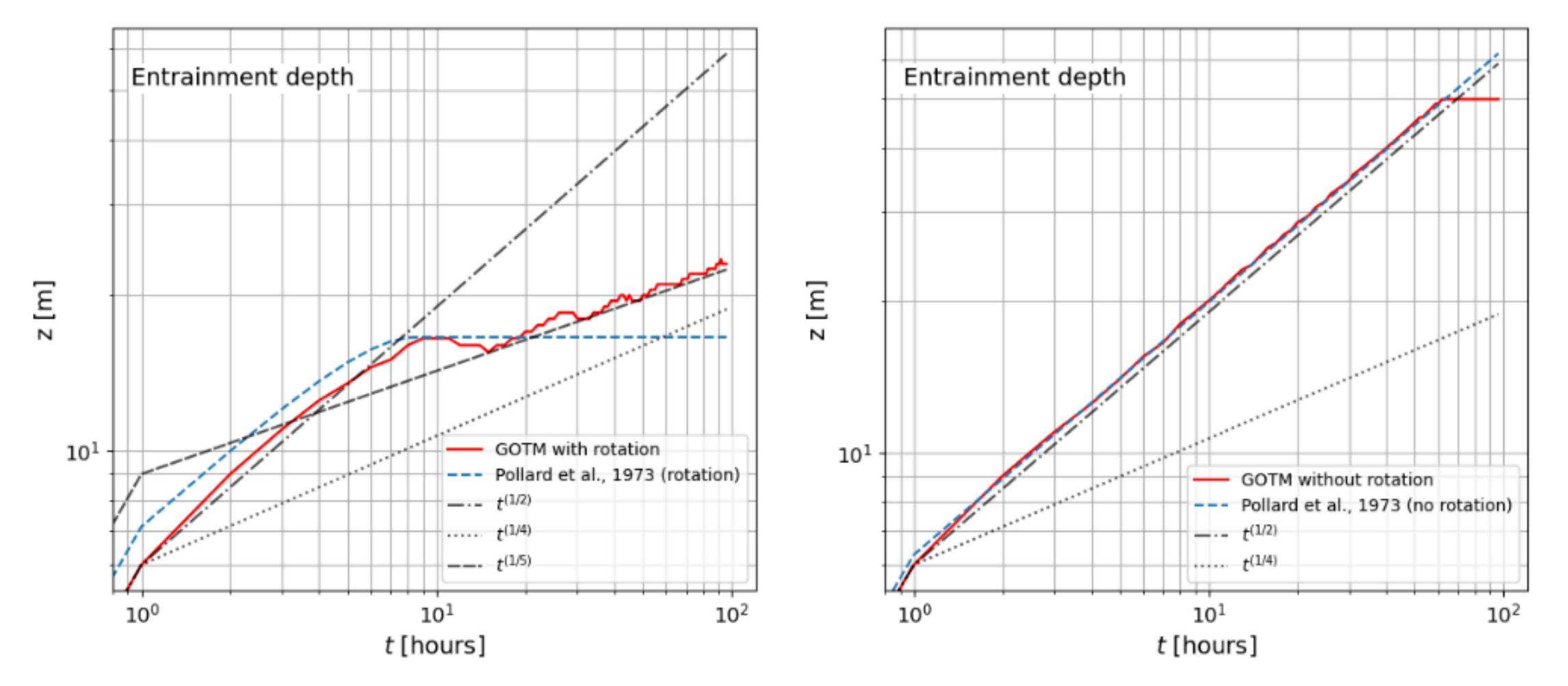
Scaling - Mixed layer depth forced by wind shear stress in rotation

Reunion LEGI - 5/12/2023

Context

Il existe une loi d'échelle qui prédit l'approfondissement sans rotation (Pollard) Avec rotation: La loi d'échelle prévoit une épaisseur constante au de la période inertiel



Loi d'échelle au-delà de période inertielle :

• Pollard [1972]

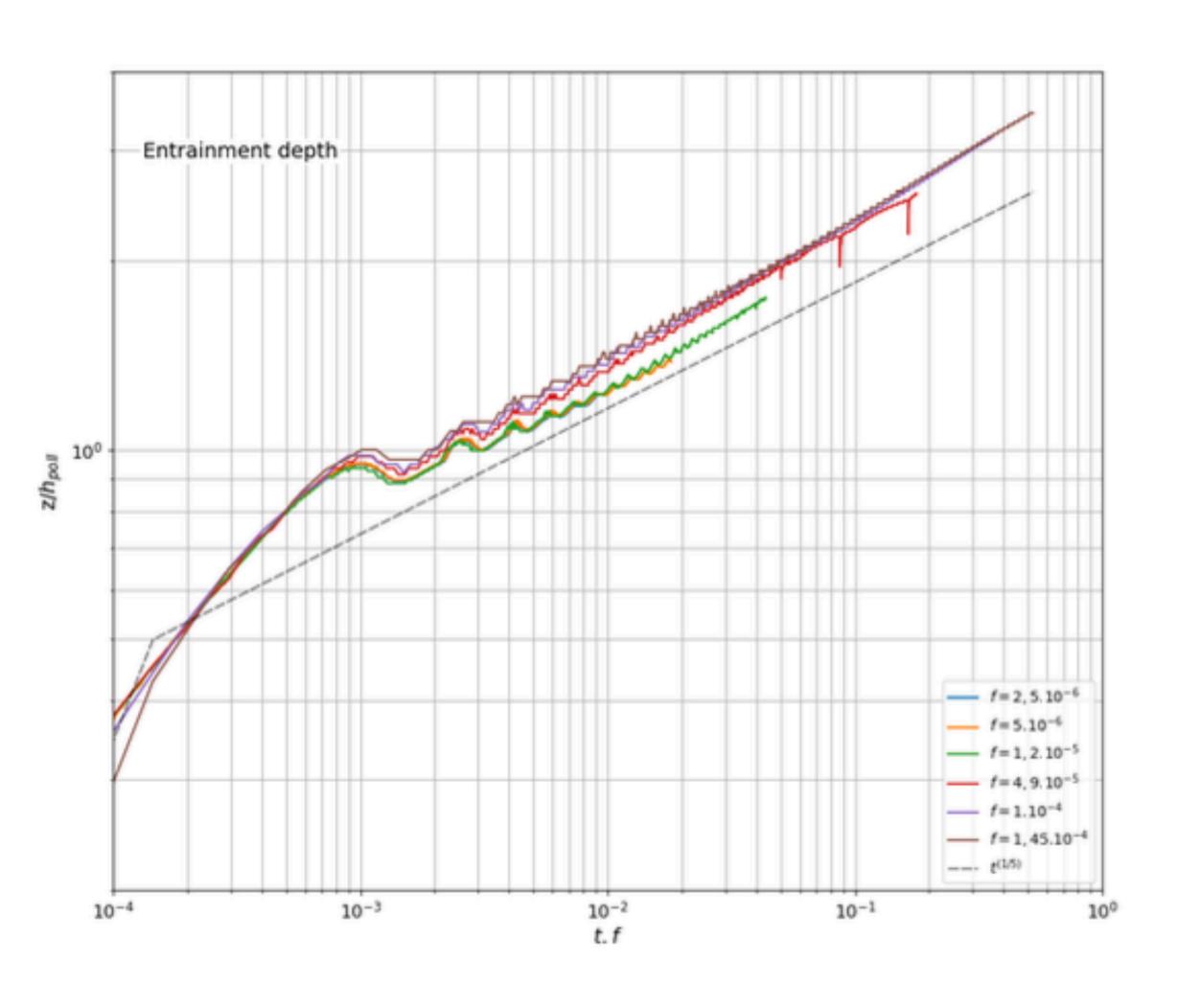
$$h(t) = h_{max} = 1.7 \left(\frac{u_*}{\sqrt{Nf}}\right)$$
 Pour $t > \pi f$

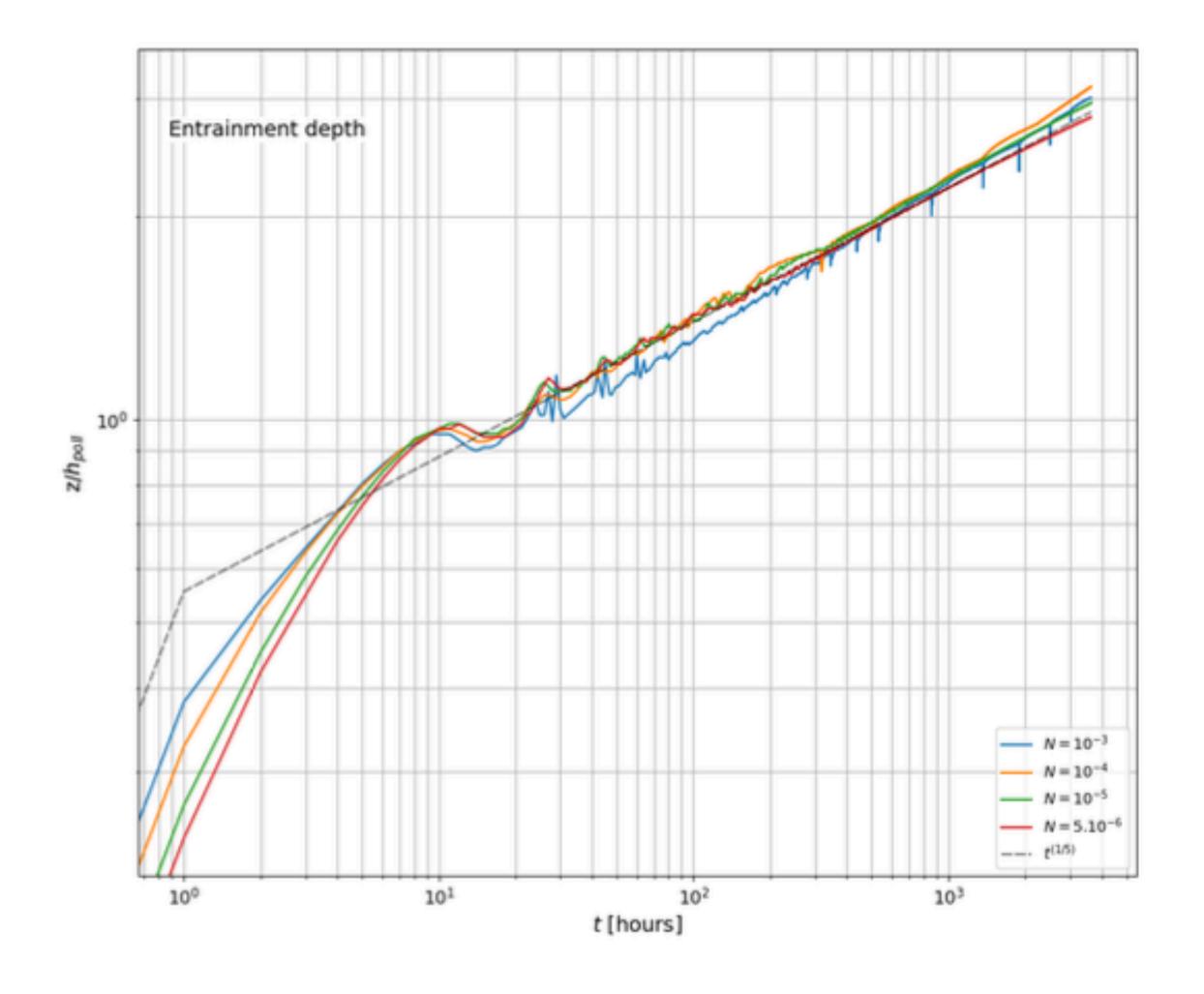
• Ushijima et al [2020]

$$h = 1.5L_{p73} \left(\frac{f}{N}\right)^{-2.2 \times 10^{-2}} \left(\frac{t}{T_f}\right)^{0.18}$$

Cette étude -> LES => n'avance pas d'argument physique

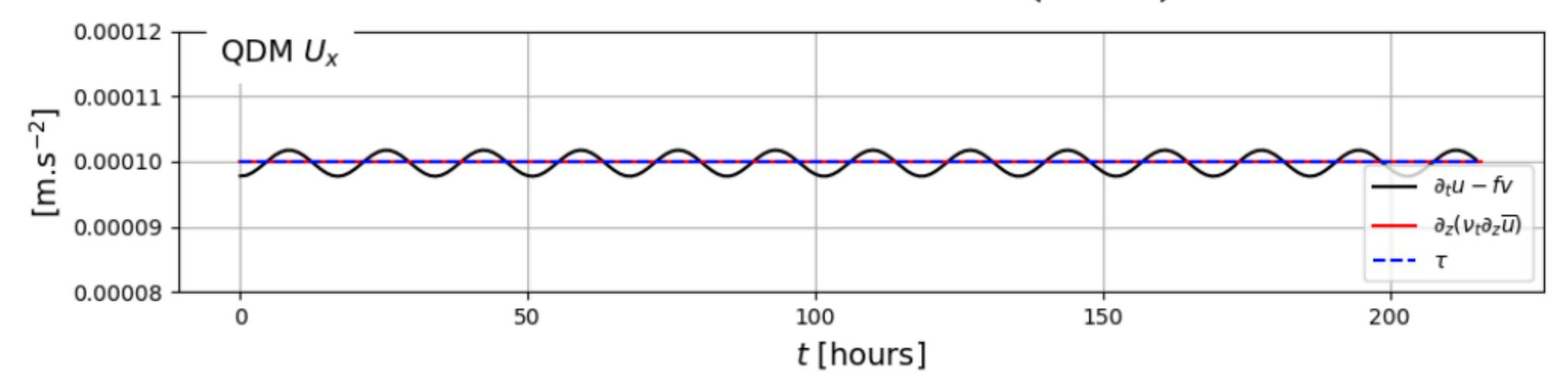
On cherche une loi en t^1/5

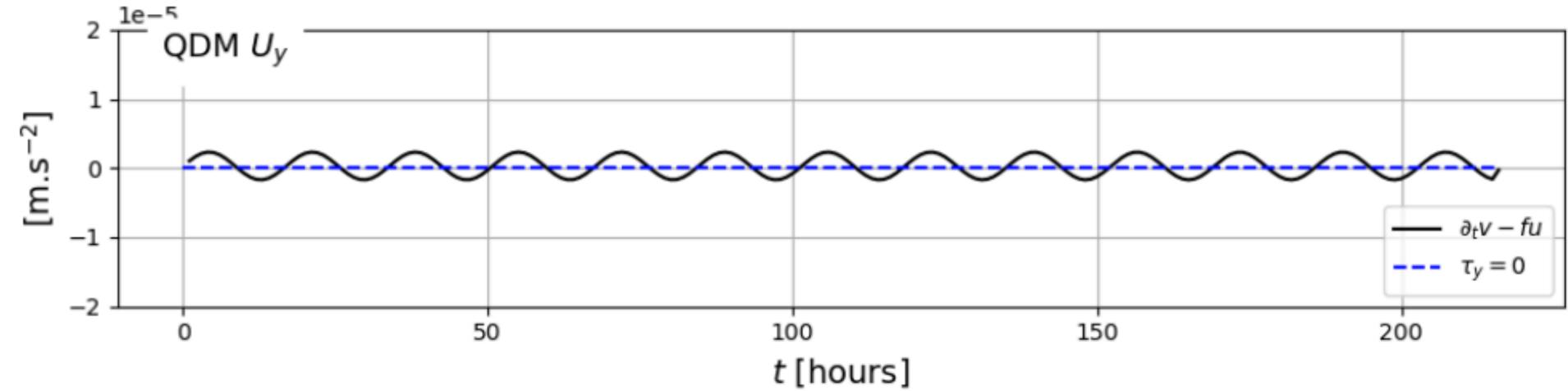




Bilan de QDM

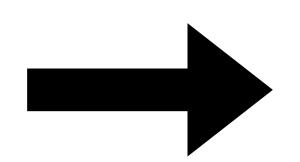
$$\begin{cases} \frac{\partial \overline{u}}{\partial t} - f \overline{v} = \frac{\partial}{\partial z} \left(\nu_t \frac{\partial \overline{u}}{\partial z} \right) \\ \frac{\partial \overline{v}}{\partial t} + f \overline{u} = \frac{\partial}{\partial z} \left(\nu_t \frac{\partial \overline{v}}{\partial z} \right) \end{cases}$$



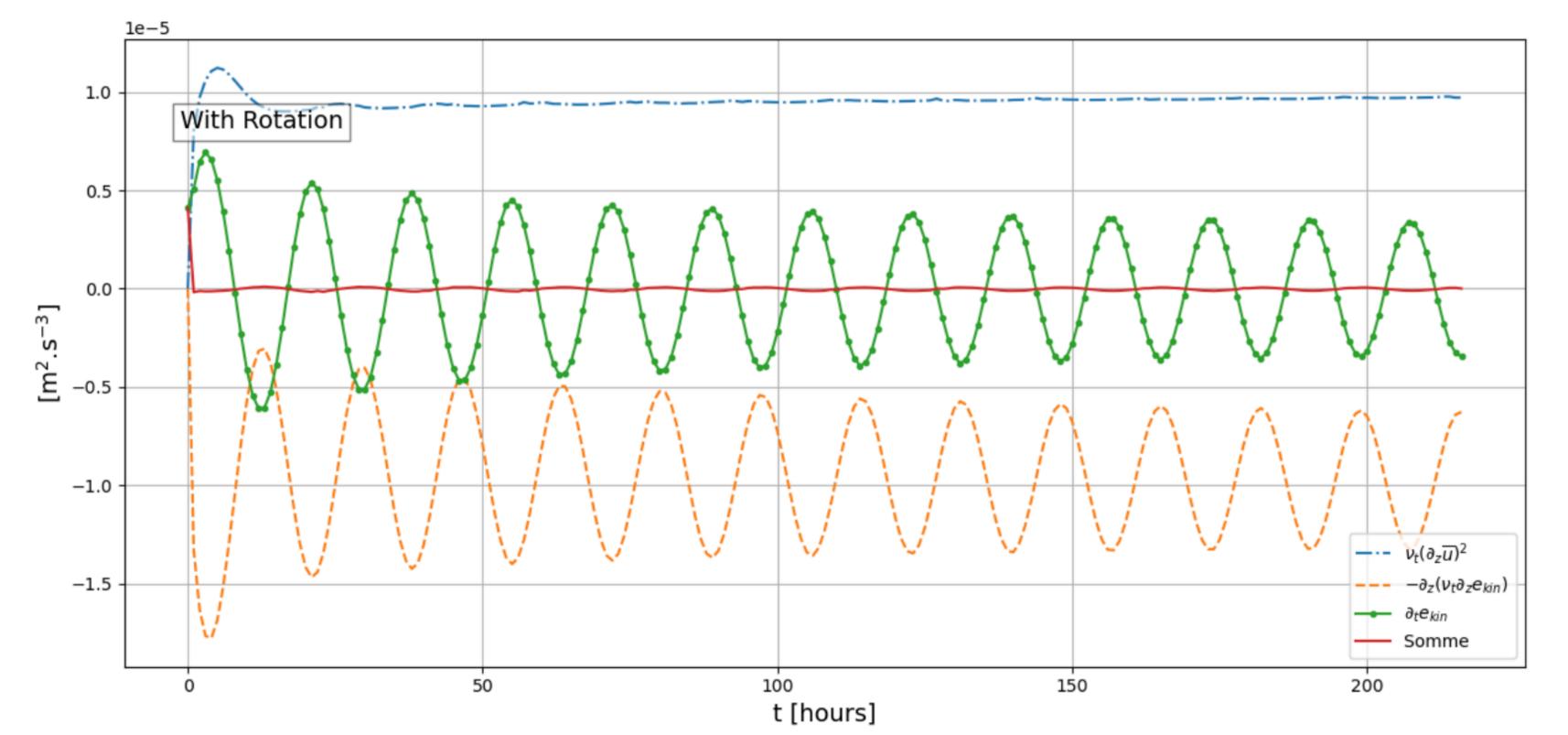


Bilan d'énergie cinétique

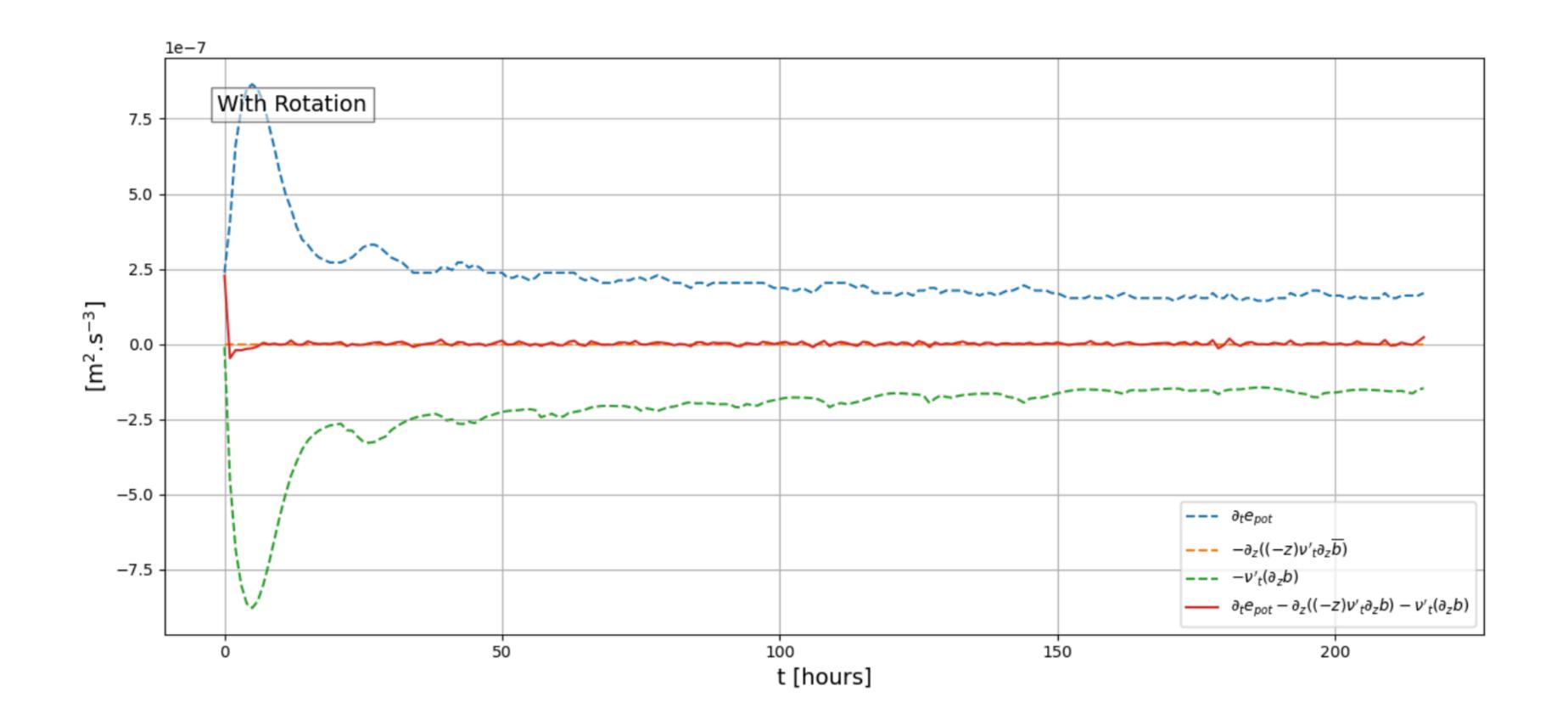
$$\begin{cases} \frac{\partial}{\partial t} (\frac{1}{2}u^2) - fuv - \frac{\partial}{\partial z} \left(\nu_t u \frac{\partial u}{\partial z} \right) = \nu_t (\frac{\partial u}{\partial z})^2 \\ \frac{\partial}{\partial t} (\frac{1}{2}v^2) + fuv - \frac{\partial}{\partial z} \left(\nu_t v \frac{\partial v}{\partial z} \right) = \nu_t (\frac{\partial v}{\partial z})^2 \end{cases}$$



$$\frac{\partial}{\partial t}(E_{kin}) - \langle \mathbf{U_{surf}}.\tau \rangle = -P$$

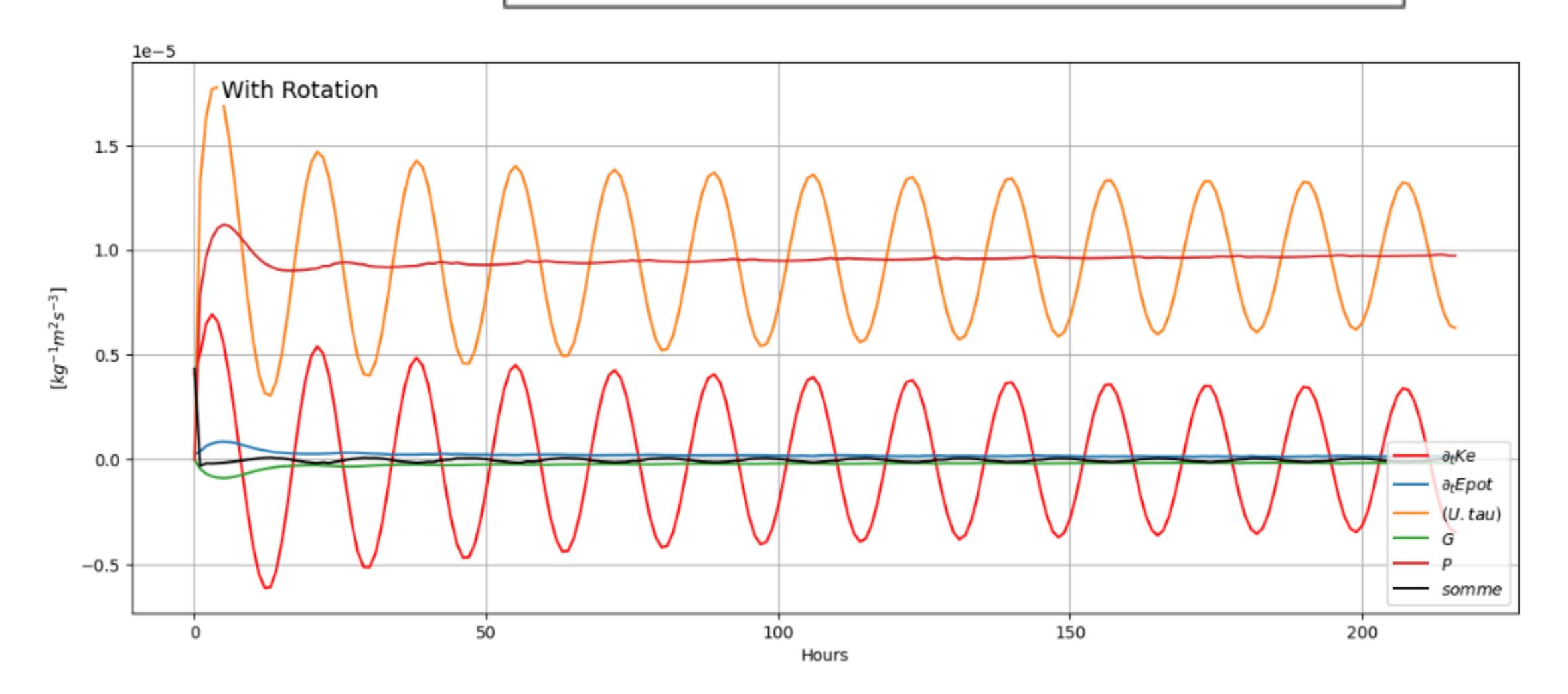


Bilan d'énergie Potentiel



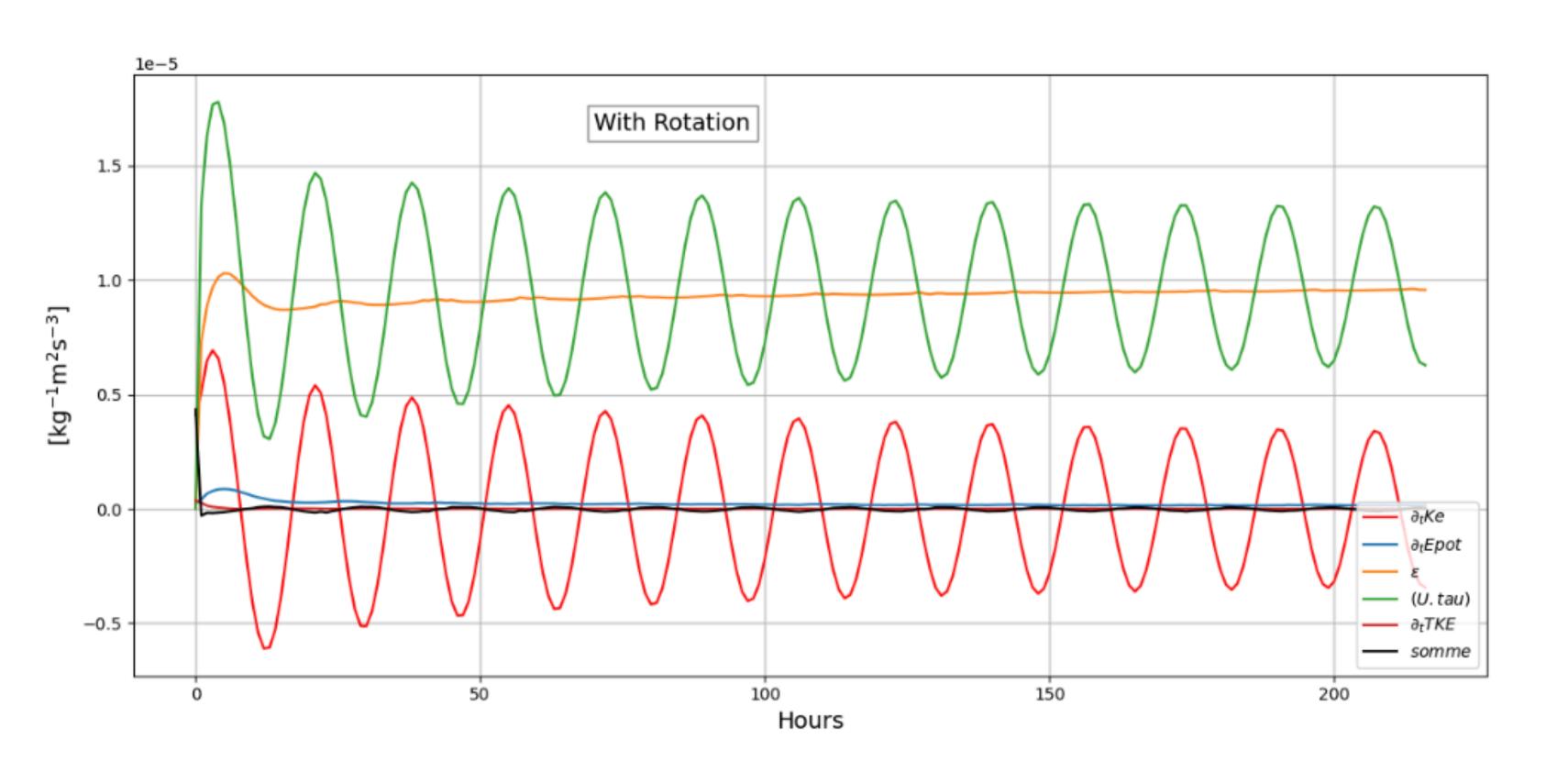
Bilan TKE

$$\frac{\partial}{\partial t}(TKE) = P + B - \int_{-H}^{0} \epsilon dz$$

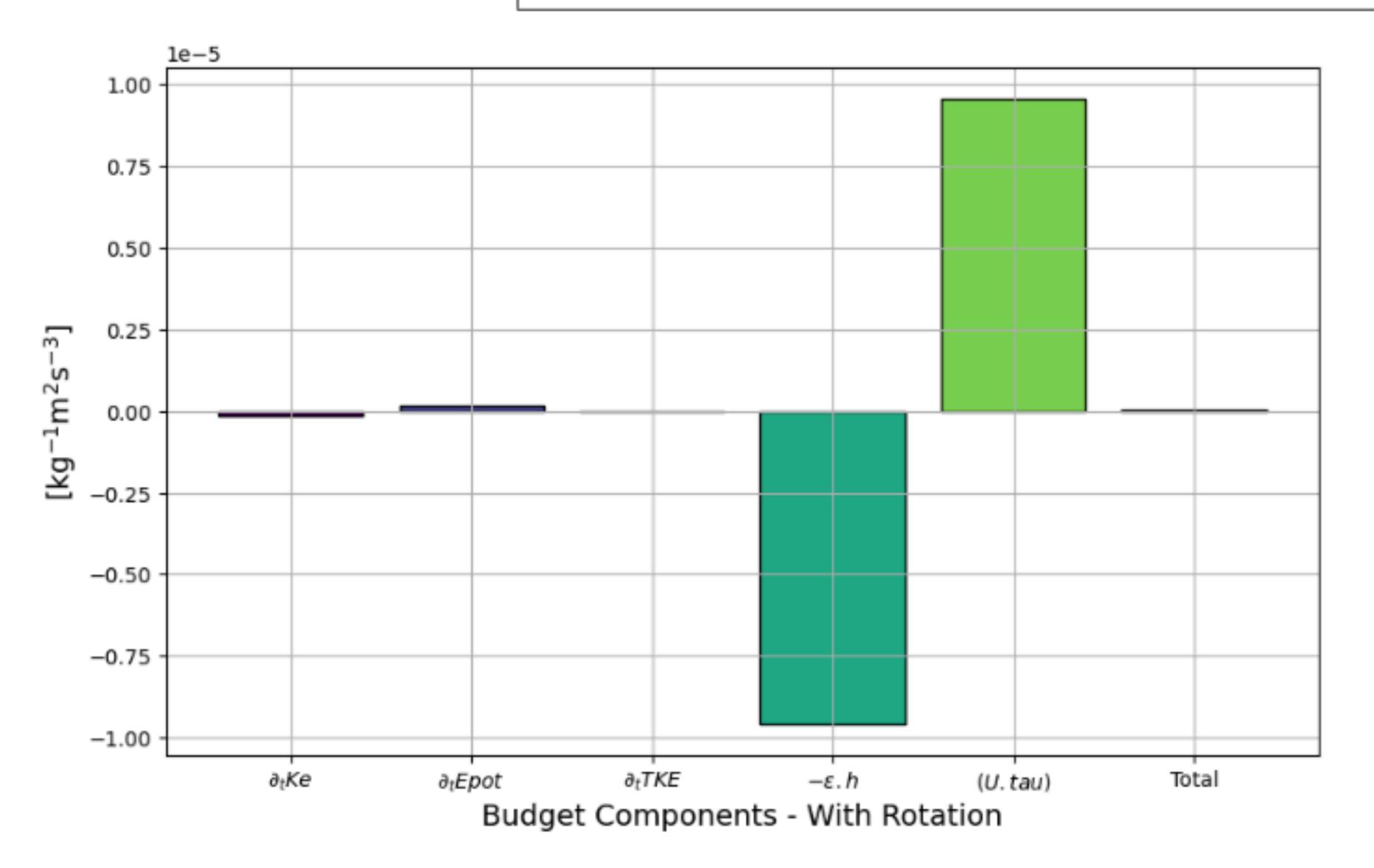


Bilan d'énergie

$$\left| \frac{\partial}{\partial t} (E_{kin}) + \frac{\partial}{\partial t} (E_{pot}) + \frac{\partial}{\partial t} (TKE) \right| = +\langle \mathbf{U_{surf}}.\tau \rangle - \int_{-H}^{0} \epsilon dz$$



Bilan d'énergie
$$\left| \frac{\partial}{\partial t} (E_{kin}) + \frac{\partial}{\partial t} (E_{pot}) + \frac{\partial}{\partial t} (TKE) = + \langle \mathbf{U_{surf}}.\tau \rangle - \int_{-H}^{0} \epsilon dz \right|$$



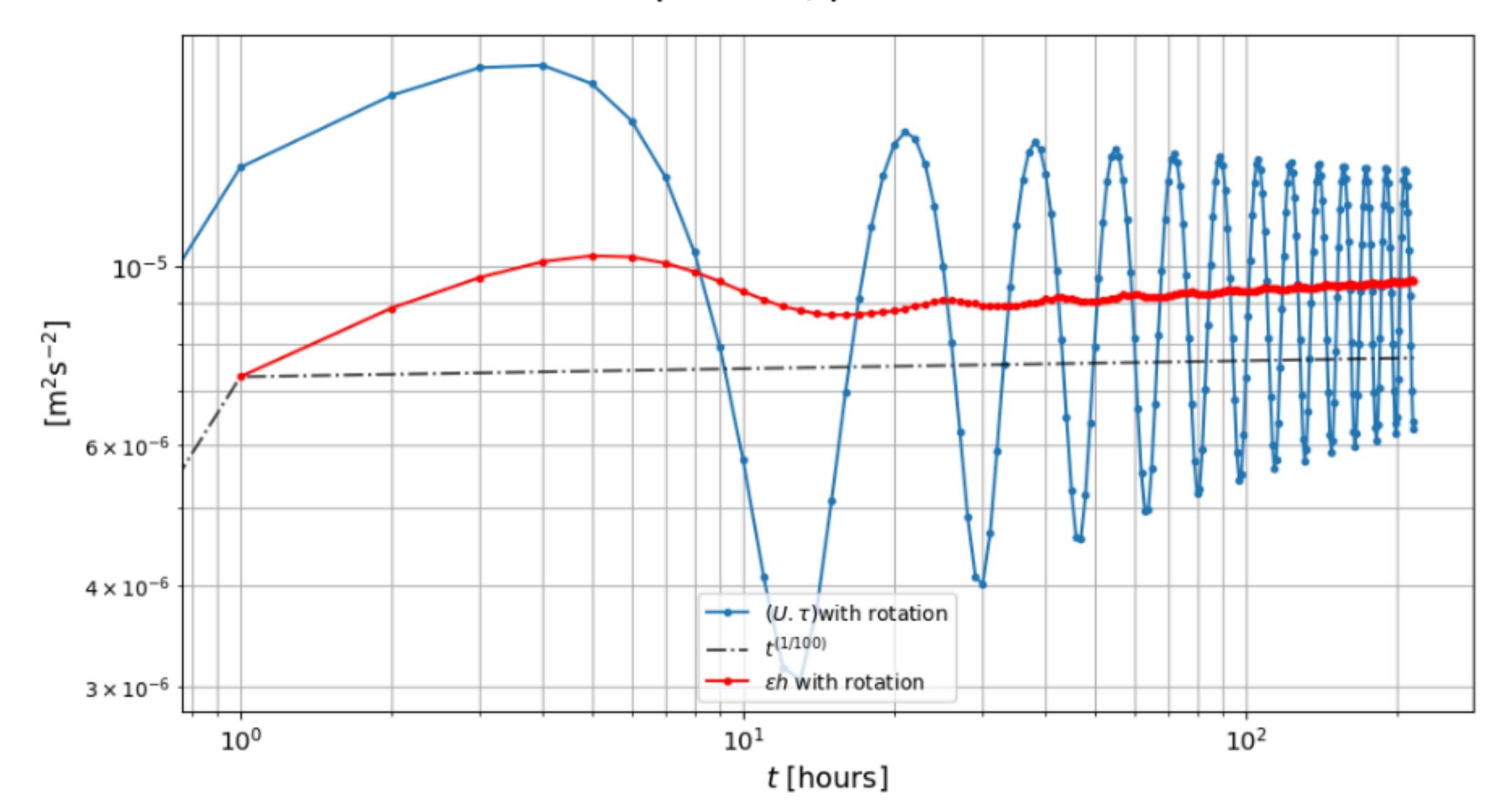
3 hypothese

Hypothèse 1 :
$$\langle U.u_*^2 \rangle \propto \epsilon h = c$$

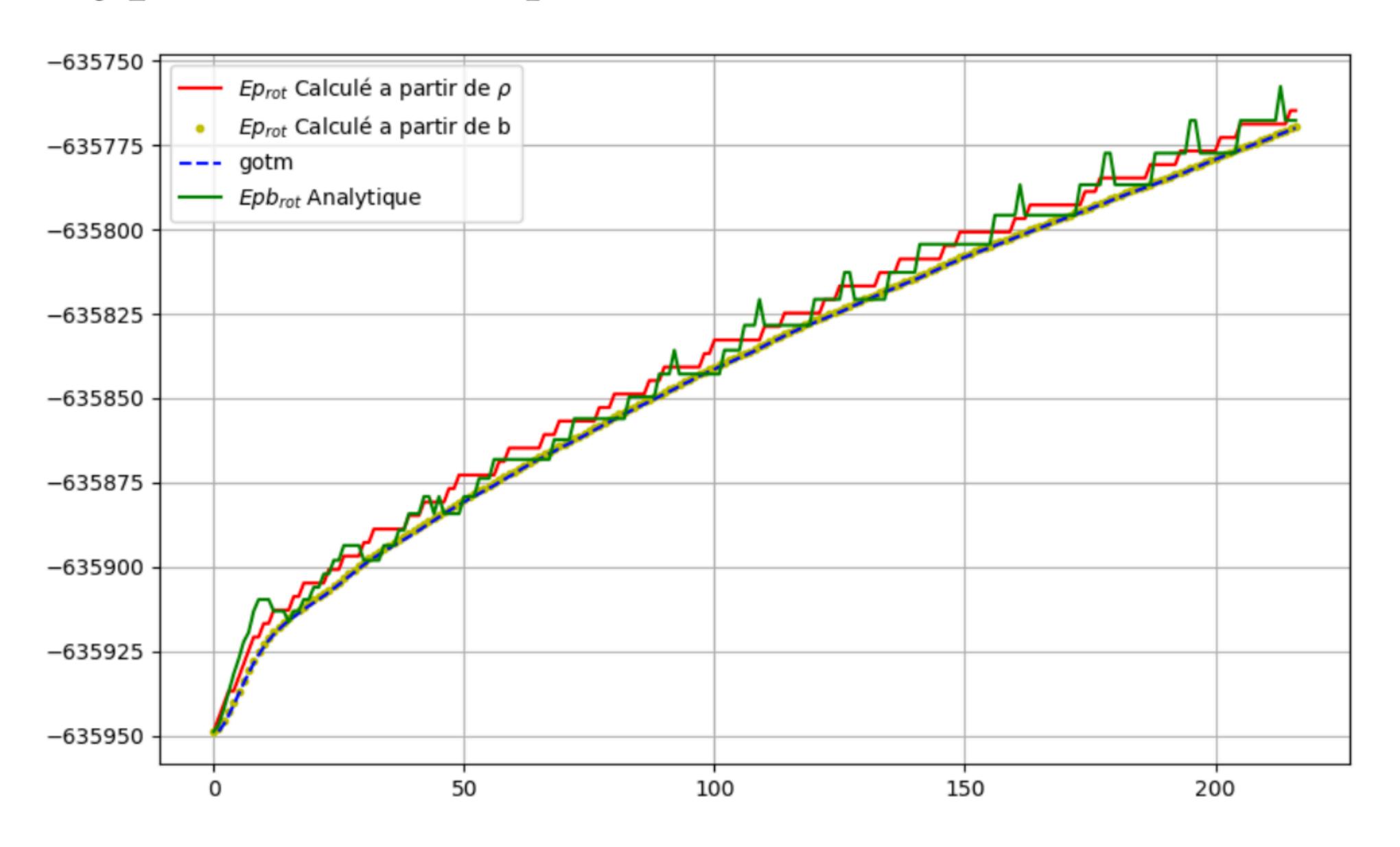
Hypothèse 2 :
$$Ep_b \propto h^3 N^2$$

Hypothèse 3 :
$$\frac{dEpb}{dt} = \Gamma \epsilon_{interface} h$$

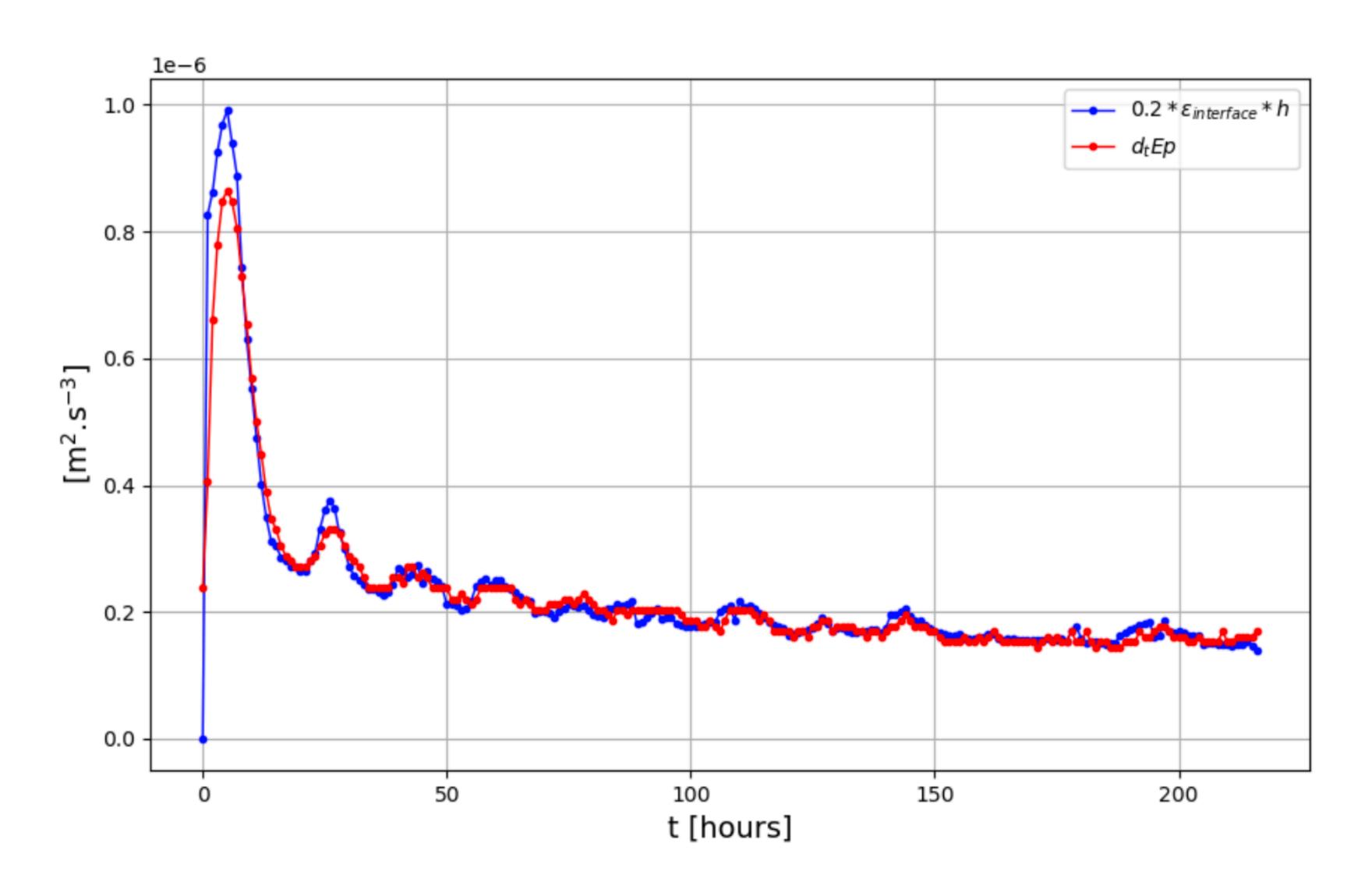
Hypothèse 1 : $\langle U.u_*^2 \rangle \propto \epsilon h = c$



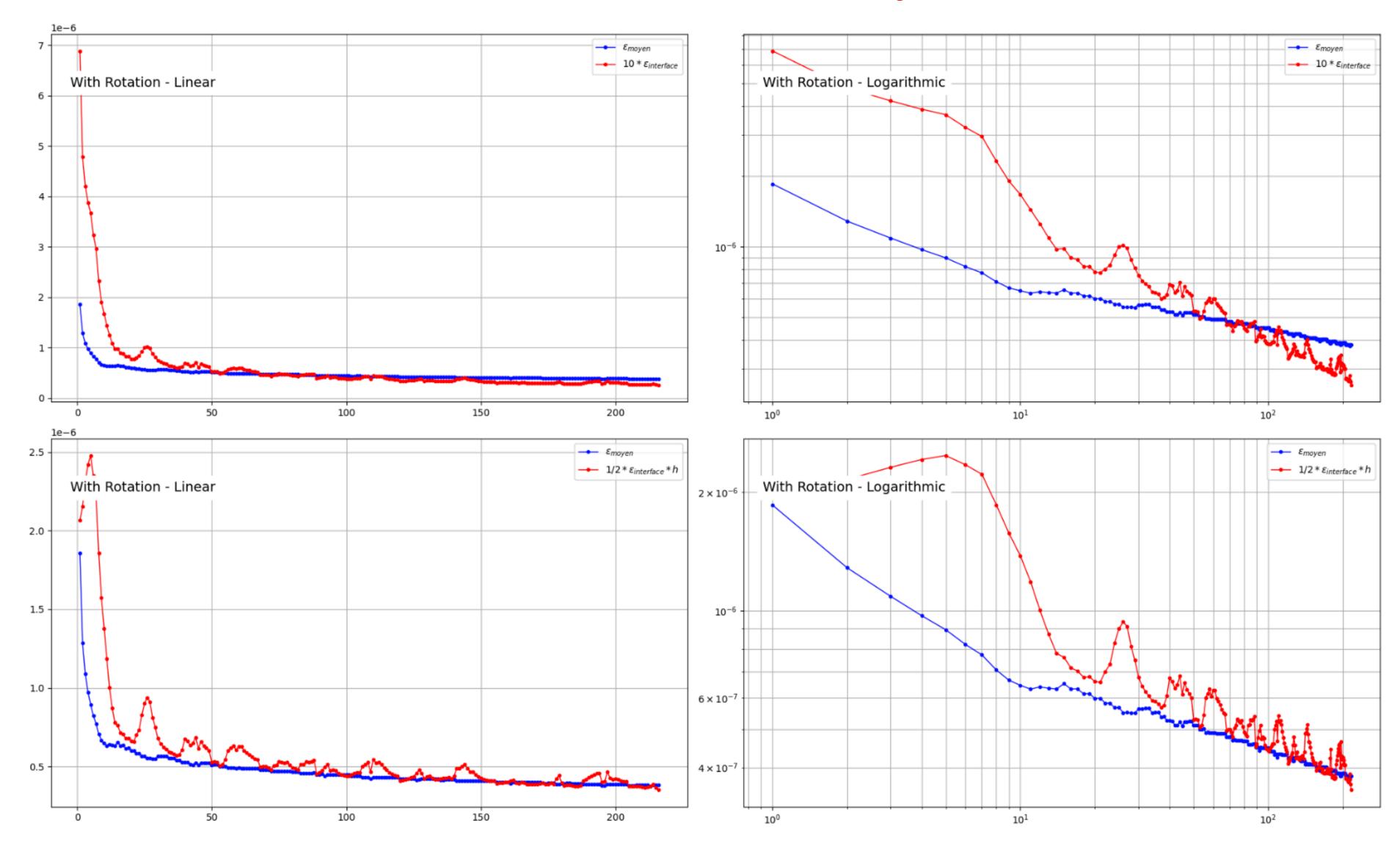
Hypothèse 2 : $Ep_b \propto h^3 N^2$



Hypothèse 3 :
$$\frac{dEpb}{dt} = \Gamma \epsilon_{interface} h$$



Relation qui relie sinterface et smoyen



Scaling à rediscuter

$$\begin{split} \epsilon h &= c \Leftrightarrow \Gamma \epsilon = \Gamma c h^{-1} \\ &\Leftrightarrow \frac{dEp_b}{dt} = \Gamma c h^{-1} \\ &\Leftrightarrow \frac{dh^3}{dt} = \frac{4}{\rho_0 N^2} \Gamma c h^{-1} \\ &\Leftrightarrow \frac{dh^4}{dt} = \frac{16}{\rho_0 N^2} \Gamma c \\ &\Leftrightarrow h = \left(\frac{16}{\rho_0 N^2} \Gamma c\right)^{1/4} t^{1/4} \end{split}$$