

## Improvement of the Mechanical Properties of Titania stabilized Alumina Ceramic Cutting tool.

Abu Naser Rashid Reza<sup>1,a</sup>, Tashneem Ara Islam<sup>2,b</sup>, Arman Hussain<sup>3,c</sup>  
Md. Fakhru Islam<sup>4,d</sup>, Md. Mohar Ali Bepari<sup>5,e</sup>.

<sup>1</sup> Research Assistant, Department of Materials Science and Engineering, GIST, Korea.

<sup>2</sup> Post Graduate Student, Department of Bionics, Rhine-Waal University of Applied Science, Germany.

<sup>3</sup> Lecturer, Department of Glass and Ceramic Engineering, BUET, Dhaka.

<sup>4</sup> Professor, Department of Glass and Ceramic Engineering, BUET, Dhaka.

<sup>5</sup> Professor, Department of Materials and Metallurgical Engineering, BUET, Dhaka

<sup>a</sup> amit\_buet@yahoo.com, <sup>b</sup> nipun32@yahoo.com, <sup>c</sup> ahussain@gce.buet.ac.bd

<sup>d</sup> fislam@gce.buet.ac.bd, <sup>e</sup> mohar@mme.buet.ac.bd

### Abstract

*In this work an attempt was taken to improve the mechanical properties of the  $Al_2O_3$  ceramic cutting tool which is continuation of the previous work. In this work,  $(100-x)\% TiO_2 - x\% Al_2O_3$  ( $x=98, 95$  and  $92$ ) were prepared using solid state route and pressed into pallets under 175-180MPa load and sintered at three different sintering temperatures 1350°C, 1400°C and 1450°C for 2 hours. Then hardness, wear rate and cutting properties were measured and analyzed with previously measured results of microstructure and densities. It was found that with the increase of %  $TiO_2$  the hardness of the ceramic cutting tools were increased, the wear rate decreased and cutting property got improved. The maximum hardness was found 22 GPa and the minimum weight loss  $0.06 \times 10^{-4}$  gm/min was found at 8%  $TiO_2$  stabilized  $Al_2O_3$  ceramic cutting tool. It was also found that 8%  $TiO_2$  stabilized  $Al_2O_3$  showed the best cutting property.*

Keywords: Hardness, Wear, Cutting property, Ceramic tools

### 1. Introduction

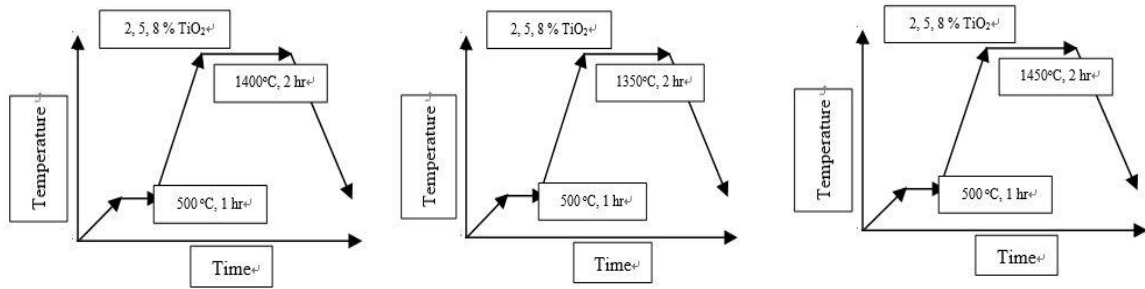
For many years, people are searching for a suitable material to produce cutting tools that can sustain higher temperature. There were many pathways taken to select specific materials as cutting tool which can survive at higher temperature. Ceramic materials, due to their better mechanical properties and higher chemical stabilities at high temperature, outperformed other materials and found as the best suited cutting tools materials for high temperature applications. Carbides are one of the most popular choices in making ceramic cutting tool in the industries. However, in recent days, Alumina ceramics has become a prominent material for cutting tools because of their high hardness, chemical inertness and wear resistance [1]. This ceramic is also retaining a high hardness at high temperature when compared to other cutting tools materials. Major limitations on using Alumina ceramic for cutting tools are its low toughness and low thermal shock resistance. Mechanical properties of  $Al_2O_3$  based ceramics have been improved by incorporating reinforcing phases such as TiC, TiN,  $ZrO_2$ , WC,  $TiO_2$  etc [2]. In this research work, addition of  $TiO_2$  in  $Al_2O_3$  ceramic has thoroughly investigated.

When alumina is doped with  $TiO_2$  to a certain level, the densifications temperature reduces and makes the mechanical properties like hardness, wear resistance and cutting property much more prominent. It has already been found that the addition of  $TiO_2$  in  $Al_2O_3$  reduces the sintering temperature and retards the grain growth [3]. The working paper aims to highlight some improved mechanical properties like hardness, wear and cutting rate of  $TiO_2$  stabilized  $Al_2O_3$  Ceramic Cutting tools and to evaluate the structure-property relationship.

### 2. Experimental

In this research work, conventional solid state ceramic processing technique was followed. Samples were prepared from commercial alpha  $Al_2O_3$  with the addition of 2, 5 & 8 wt % of  $TiO_2$ . The alumina powders used in

this work were of 99.87% purity with particle size of around 40nm while, the TiO<sub>2</sub> powders were of 99.9% purity with particle size around 40nm. First, the raw materials were ball-milled at 150 rpm for 18~20 hours in acetone medium. After proper mixing, the powders were extracted with the help of acetone. Then the wet powders were dried at 110-120°C for 24 hours. After drying, 5~8% PVA (Polyvinyl alcohol) binder was mixed with the powder before compaction. Then, the samples were prepared by using 175-180MPa pressure for 2 minutes holding with a uniaxial hydraulic press. The prepared samples were around 13 mm in diameter and 2 mm thick. These green samples were then dried for one day at 110°C. Finally, the samples were sintered at different sintering temperature. Single stage sintering were carried out for all the sintering cycles where at the first step of sintering the binder was removed by holding the samples at temperature 500°C for 1 hr. After binder removal, at the second step of sintering the samples were fired at 1350°C, 1400°C and at 1450°C for 2 hours (Fig. 1, 2 and 3). With 3 composition and 3 temperature variations, total 9 sets of samples were prepared. The final sintered samples were around 11 mm in diameter and 1.5 mm thick. Finally after sintering, percent theoretical density, grain size, mechanical properties such as hardness, wear and cutting properties were measured and compared with the help of the microstructure of the respected samples, obtained from Scanning Electron Microscope (SEM).



**Fig. 1.** Single stage sintering cycle for different composition of TiO<sub>2</sub> in Al<sub>2</sub>O<sub>3</sub> with increasing temperature

The hardness values of the samples were measured using Vickers Micro hardness Testing Machine (**Fig.2.**) The indentations were made on the specimens using 1 kg load for 30 seconds. The diagonal of the indentations were measured in SEM.

The hardness was calculated using the following formula:

$$H.V. = \frac{1.854Pg}{d} \quad (1)$$

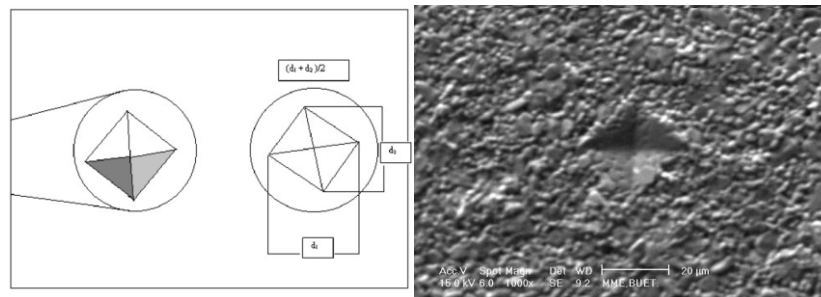
Where,

P = Applied load, kg

d = Mean diagonal of indentation, (m)

g = gravitational acceleration, (9.8m/s<sup>2</sup>)

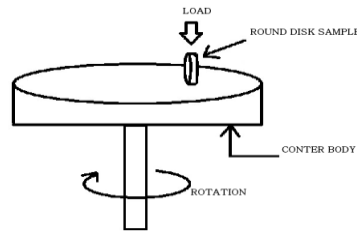
H.V. = Vickers hardness, (GPa)



**Fig. 2.** Indentation of the pyramid cone of Vickers hardness test

Wears of the samples were measured by a wear-testing machine where the samples were placed on a moving disc (Pin and Disk Method). The discs used in the test were made of hardened steel. First the weights of the ceramic sample tools were measured and marked accordingly. Then the samples were placed in the holder and set in the machine (**Fig. 3.**). After the test the weight of the tools were again taken for the data calculation and result.

The cutting properties of the ceramic tools were tested by cutting a mild steel specimen in the lathe machine. The tools were used to cut mild steel back. Cutting was done for 2 minutes using cutting speed 465 rpm and depth of cut roughly 0.2 mm. First, the weights of the tools were taken. Then the metal removal was measured by weighing out the chips in every cut. The tools after cutting mild steel were weighed again and by the difference of its initial weight and final weight the cutting rate was determined.



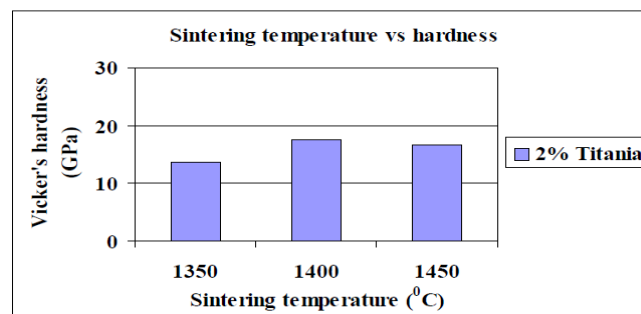
**Fig. 3.** Wear test (Pin on disk method)

### 3. Results and discussions

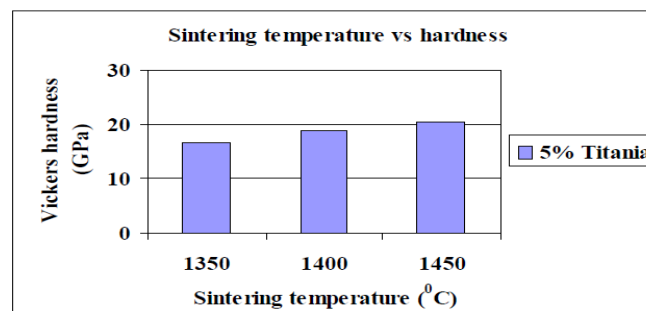
At higher sintering temperature and higher % of  $\text{TiO}_2$  content high degree of densification has been achieved. The maximum value of % theoretical density was achieved 95.18% for 8%  $\text{TiO}_2$  stabilized alumina cutting tool sintered at  $1450^\circ\text{C}$ <sup>[3]</sup>. The hardness, wear test and cutting properties were discussed in the following sections.

#### 3.1 Hardness

Theoretically, with increase of sintering temperature densification rate as well as the hardness also increases. This is because denser the samples, more difficult will be the penetration of indenter and higher will be the hardness<sup>[5]</sup>. From the **Fig. 4** it can be seen that with increase in sintering temperature for 2%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$ , the hardness of cutting tools increases from  $1350^\circ\text{C}$  to  $1400^\circ\text{C}$ . But at higher temperature of  $1450^\circ\text{C}$  the hardness drops. It is due to grain coarsening at elevated temperature, density drops<sup>[3]</sup> slightly and so does the hardness.



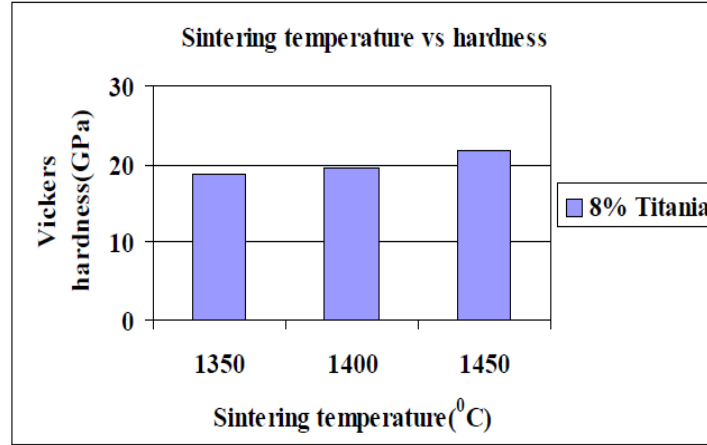
**Fig. 4.** Sintering temperature versus hardness of 2%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$



**Fig. 5.** Sintering temperature versus hardness of 5%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$

From **Fig. 5** and **Fig. 6** a gradual increase in hardness with increase in sintering temperature can be found for

5%  $\text{TiO}_2$  and 8%  $\text{TiO}_2$  stabilized alumina in the temperature range  $1350^\circ\text{C}$  to  $1450^\circ\text{C}$ . Maximum value of Vickers's hardness of 22 GPa was obtained for 8%  $\text{TiO}_2$ -92%  $\text{Al}_2\text{O}_3$  composition, sintered at  $1450^\circ\text{C}$ . The reason behind this is that with higher percentage of  $\text{TiO}_2$  it can provide the pinning effect and retards the grain growth<sup>[3]</sup> of  $\text{Al}_2\text{O}_3$ . For 2%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$  the amount of  $\text{TiO}_2$  is very small, that's why it could not provide sufficient pinning effect<sup>[3]</sup> on  $\text{Al}_2\text{O}_3$  grains and at higher temperature exaggerated grain growth of  $\text{Al}_2\text{O}_3$  occurred which can also be seen from the microstructures<sup>[3]</sup>. For this reason, even at higher temperature we have obtained fine grain dense microstructure with high hardness.

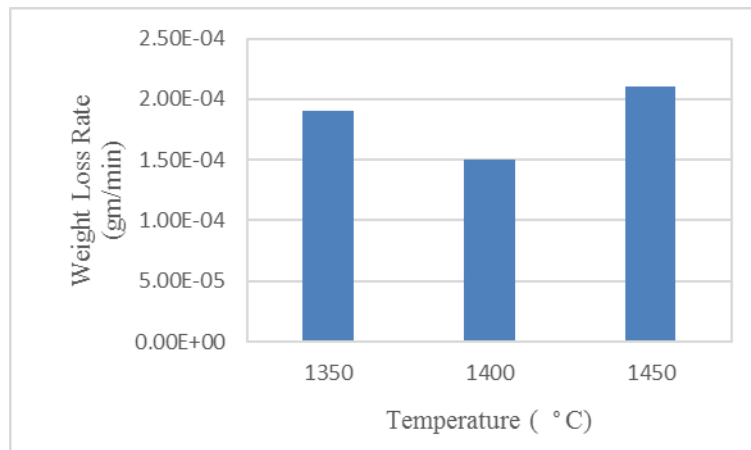


**Fig. 6.** Sintering temperature versus hardness of 8%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$

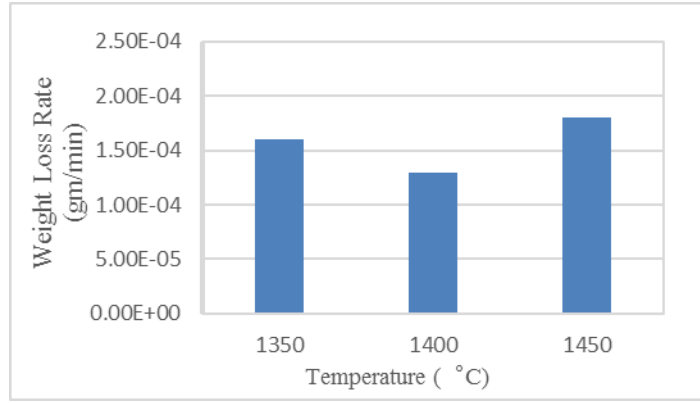
So the hardness can be increased at low temperature by increasing %  $\text{TiO}_2$  and higher hardness can be achieved with increasing both temperature along with %  $\text{TiO}_2$ .

### 3.2 Wear

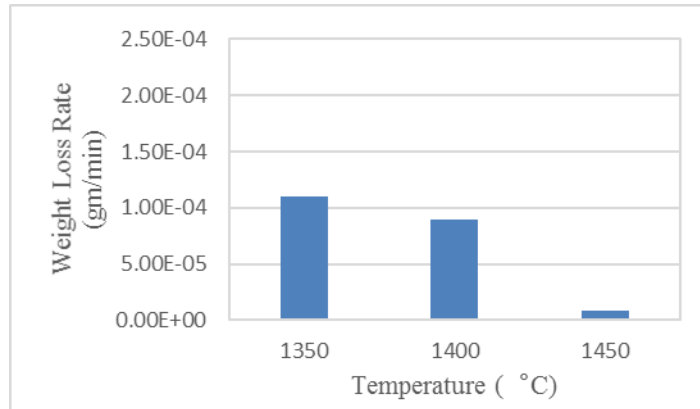
Theoretically, with increase in density and hardness, the wear rate decreases. From **Fig. 7**, **Fig. 8** and **Fig. 9** we can see that, for all the samples with increase of % $\text{TiO}_2$  in the compositions, wear rate gradually decreases. On the contrary, for the same composition, increasing temperature in the cases of 2%  $\text{TiO}_2$  and 5%  $\text{TiO}_2$  wear rate gradually decreased up to  $1400^\circ\text{C}$  and then slightly increased at  $1450^\circ\text{C}$ . This is due to the grain coarsening<sup>[3]</sup> occurs at higher temperature which reduces hardness. According to Hall-Patch relationship, we know that coarser the grain, inferior will be the mechanical properties like hardness, wear resistance etc.<sup>[4]</sup>. As the amount of  $\text{TiO}_2$  is very small it could not provide sufficient pinning effect to hinder grain growth of  $\text{Al}_2\text{O}_3$  grains. That is why excessive, grain growth has occurred at  $1450^\circ\text{C}$ , which is clearly visible in the microstructure<sup>[3]</sup>. Minimum wear rate of  $8 \times 10^{-6}$  gm/min was found for 8%  $\text{TiO}_2$  sintered at  $1450^\circ\text{C}$ . This is because the sample containing 8%  $\text{TiO}_2$  sintered at  $1450^\circ\text{C}$  has the highest density<sup>[3]</sup>, finer grain and high hardness<sup>[3]</sup> which is already told in the previous part of the paper.



**Fig. 7.** Sintering temperature vs wear rate of 2%  $\text{TiO}_2$  stabilized  $\text{Al}_2\text{O}_3$



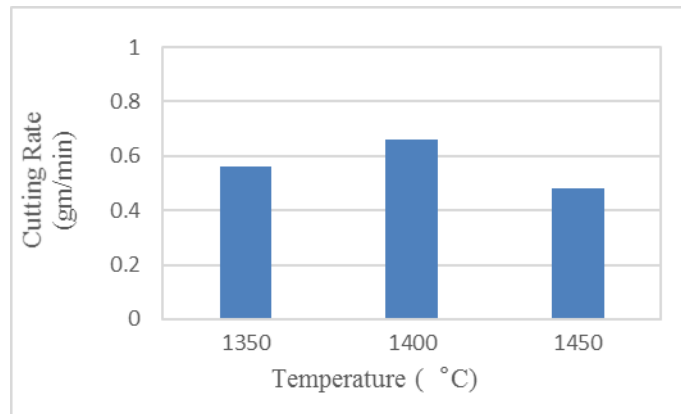
**Fig. 8.** Sintering temperature versus wear rate of 5% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub>



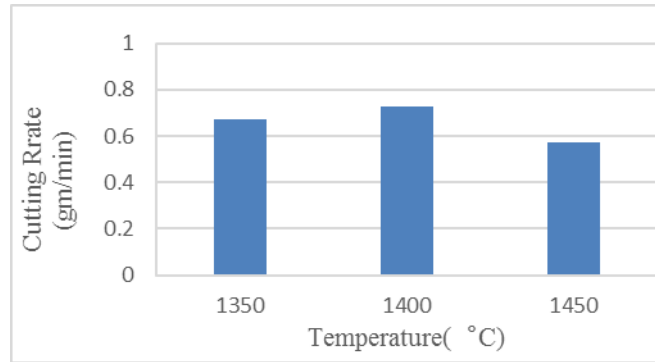
**Fig. 9.** Sintering temperature versus wear rate of 8% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub>

### 3.3 Cutting

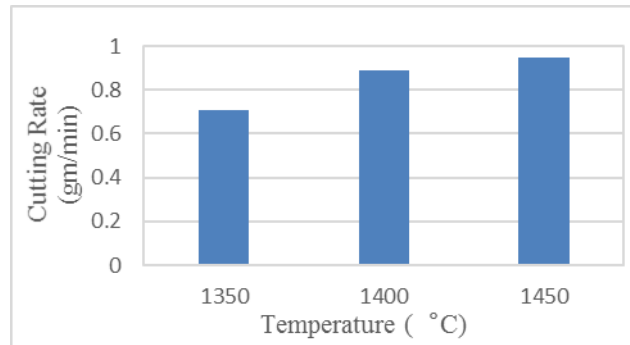
Theoretically with the increase of density and hardness cutting rate also increases. With the increase of TiO<sub>2</sub> in composition, for the same temperature, cutting property gradually improved, which is clearly visible from **Fig. 11** to **Fig. 12**. However, in the cases of 2% and 5% TiO<sub>2</sub> cutting property gradually improved up to 1400°C but then deteriorated at 1450°C and also samples had failed during cutting operation. This was happened due to grain coarsening occurred at higher temperature. So same thing can be said again with respect to pinning effect occurred at high % TiO<sub>2</sub> which inhibits the grain growth. And it was found that highest cutting rate of 0.95 gm/min was obtained in the sample containing 8% TiO<sub>2</sub> sintered at 1450°C. This is already discussed as we know the 8% TiO<sub>2</sub> sintered at 1450°C has the highest density<sup>[3]</sup>, finer grain and high hardness<sup>[3]</sup>.



**Fig. 10.** Sintering temperature versus cutting rate of 2% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub>



**Fig. 11.** Sintering temperature versus cutting rate of 5% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub>



**Fig. 12.** Sintering temperature versus cutting rate of 8% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub>

#### 4. Conclusion

The main focus of this research work was to find out the optimum conditions at which the mechanical properties of the Al<sub>2</sub>O<sub>3</sub> Ceramic Cutting tools begins to improve. In this research, it was found that 8% TiO<sub>2</sub> stabilized Al<sub>2</sub>O<sub>3</sub> sintered at 1450°C showed the maximum hardness. It was also found that, wear rate was also the minimum for the same condition, which is around  $8 \times 10^{-6}$  gm/min. Finally, it was observed that for the same condition the cutting rate was also maximum which 0.95 gm/min was. The reason behind the continuous improvement mechanical behavior was the addition of the TiO<sub>2</sub> in Al<sub>2</sub>O<sub>3</sub> to a certain extent. Lower % TiO<sub>2</sub> didn't not showed any prominent result at low temperatures. But at higher % of TiO<sub>2</sub> with higher temperature sintering showed better mechanical properties of the tools. This is because, lower TiO<sub>2</sub> addition does not provide any adequate pinning effect and with increasing of temperature densification occurred along with grain coarsening. As a result mechanical properties were not up to the mark. Moreover, when the % of TiO<sub>2</sub> increased from 2% to 8%, TiO<sub>2</sub> able to give sufficient pinning effect and inhibits grain coarsening and densification increases with smaller grains. As a result good mechanical properties were observed.

#### 5. Acknowledgement

Abu Naser Rashid Reza and Tashneem Ara Islam worked equally on this project under the supervision of Prof. Dr. Md. Mohar Ali Bepari.

#### 6. References

- [1] S. H. Avner, Introduction to Physical Metallurgy, McGraw-Hill Book Company, 2<sup>nd</sup> Edition, pp. 387-422, 1974.
- [2] M. Kitiwan and D. Atong, "Preparation of Al<sub>2</sub>O<sub>3</sub>-TiC Composites and Their Cutting Performances", *Journal of Solid Mechanics and Materials Engineering*, Vol. 1, No. 7, pp. 527-536, 2007
- [3] A. N. R. Reza, T. A. Islam, M. F. Islam and M. M. A. Bepari, "Effect of Composition and Sintering Temperature on the Microstructure and Theoretical Density of TiO<sub>2</sub> Stabilized Al<sub>2</sub>O<sub>3</sub> Cutting Tool", *International Conference on Mechanical, Industrial and Materials Engineering*, Paper No. MS-14, pp. 615-618, 2013.
- [4] F. Xiong, R. R. Manory, L. Ward, and M. Terheci, "Effect of Grain Size and Test Configuration on the Wear Behavior of Alumina", *Journal of American Ceramic Society*, Vol. 80, No. 5, pp. 1310-1312, 1997.
- [5] A. Krell, "Grain Size Dependence of Hardness in Dense Submicrometer Alumina," *Journal of American Ceramic Society*, Vol. 78, No. 4, pp. 1118-1120, 1995.