作业说明:

完整推导了离散时间下的误差动力学,结果跟VINS代码中预积分部分,矩阵V中除了前四项噪声的系数符号相反,其余全部一致。这里解释下这个负号的成立:

- 1.由于零均值的高斯噪声,正负不影响。
- 2.另外从误差的协方差传递方式:

$$P_{i+1}^{15 \times 15} = F P_i F^T + V Q V^T \tag{1}$$

以及误差的雅各比:

$$J_{i+1}^{15 \times 15} = FJ_i \tag{2}$$

可以得出噪声传递矩阵的系数正负,不会影响最后结果。

1. 连续时间下的误差动力学

为简化起见,忽略了所有高阶项和重力的变化。参考《四元数数学基础》5.3节。

这里 $\delta p, \delta v, \delta \theta$ 对应IMU预积分中的 $\delta \alpha, \delta \beta, \delta \gamma$ 分别对应位置,速度,方向的变化量。其中方向的变化量用 $\delta \theta$ 来表示。可以写出:

2. 离散时间下的误差动力学

这里我们同样使用中值法积分处理离散情形。根据上一节的内容,我们可以知道方向误差的导数连续形式为:

$$\delta \dot{ heta}_t^{b_k} = -[\hat{w}_t - b_{w_t}]_{\times} \delta heta_t - \delta b_{w_t} - n_w$$
 (5)

则中值法离散形式为:

$$\delta \dot{ heta}_i = -[rac{\hat{w}_i + \hat{w}_{i+1}}{2} - b_{w_i}]_ imes \delta heta_i - rac{n_{w_i} + n_{w_{i+1}}}{2} - \delta b_{w_i}$$
 (6)

由此根据导数定义可得:

$$\delta\theta_{i+1} = [I - [\frac{\hat{w}_i + \hat{w}_{i+1}}{2} - b_{w_i}]_{\times} \delta t] \delta\theta_i - \delta t \frac{n_{w_i} + n_{w_{i+1}}}{2} - \delta t \delta b_{w_i}$$
 (7)

令:

$$egin{aligned} f_{11} &= I - [rac{\hat{w}_i + \hat{w}_{i+1}}{2} - b_{w_i}]_ imes \delta t \ v_{11} &= v_{13} = -rac{\delta t}{2} \ f_{14} &= -\delta t \end{aligned}$$

速度误差的导数连续形式为:

$$\delta \dot{eta}_{t}^{b_{k}} = -R_{t}^{b_{k}} [\hat{a}_{t} - b_{a_{t}}]_{\times} \delta \theta_{t} - R_{t}^{b_{k}} \delta b_{a_{t}} - R_{t}^{b_{k}} n_{a}$$
 (8)

则中值法离散形式为:

$$\delta \dot{eta}_i = -rac{1}{2} R_i [\hat{a}_i - b_{a_i}]_{ imes} \delta heta_i - rac{1}{2} R_{i+1} [\hat{a}_{i+1} - b_{a_i}]_{ imes} \delta heta_{i+1} - rac{1}{2} (R_i + R_{i+1}) \delta b_{a_i} - rac{1}{2} R_i n_{a_i} - rac{1}{2} R_{i+1} n_{a_{i+1}}$$

将式(32)代入上式可得:

$$egin{aligned} \delta \dot{eta}_i &= -rac{1}{2} R_i [\hat{a}_i - b_{a_i}]_ imes \delta heta_i - rac{1}{2} R_{i+1} [\hat{a}_{i+1} - b_{a_i}]_ imes \ \{ [I - [rac{\hat{w}_i + \hat{w}_{i+1}}{2} - b_{w_i}]_ imes \delta t] \delta heta_i - rac{n_{w_i} + n_{w_{i+1}}}{2} \delta t - \delta b_{w_i} \delta t \} \ &- rac{1}{2} (R_i + R_{i+1}) \delta b_{a_i} - rac{1}{2} R_i n_{a_i} - rac{1}{2} R_{i+1} n_{a_{i+1}} \end{aligned}$$

继续整理:

$$\delta \dot{eta}_i = \{ -rac{1}{2} R_i [\hat{a}_i - b_{a_i}]_ imes - rac{1}{2} R_{i+1} [\hat{a}_{i+1} - b_{a_i}]_ imes [I - [rac{\hat{w}_i + \hat{w}_{i+1}}{2} - b_{w_i}]_ imes \delta t] \} \delta heta$$

$$egin{aligned} &+rac{1}{4}R_{i+1}[\hat{a}_{i+1}-b_{a_i}]_ imes (n_{w_i}+n_{w_{i+1}})\delta t +rac{1}{2}R_{i+1}[\hat{a}_{i+1}-b_{a_i}]_ imes \delta b_{w_i}\delta t \ &-rac{1}{2}(R_i+R_{i+1})\delta b_{a_i} -rac{1}{2}R_in_{a_i} -rac{1}{2}R_{i+1}n_{a_{i+1}} \end{aligned}$$

根据导数定义可得:

$$\deltaeta_{i+1} = \deltaeta_i + f_{21}\delta heta_i - rac{1}{2}(R_i + R_{i+1})\delta t\delta b_{a_i} + f_{24}\delta b_{w_i} \ -rac{1}{2}R_i\delta t n_{a_i} - rac{1}{2}R_{i+1}\delta t n_{a_{i+1}} + v_{21}n_{w_i} + v_{23}n_{w_{i+1}}$$
 (10)

令:

$$egin{aligned} f_{21} &= -rac{1}{2}R_{i}[\hat{a}_{i}-b_{a_{i}}]_{ imes}\delta t -rac{1}{2}R_{i+1}[\hat{a}_{i+1}-b_{a_{i}}]_{ imes}[I-[rac{\hat{w}_{i}+\hat{w}_{i+1}}{2}-b_{w_{i}}]_{ imes}\delta t]\delta t \ f_{22} &= I \ f_{23} &= -rac{1}{2}(R_{i}+R_{i+1})\delta t \ f_{24} &= rac{1}{2}R_{i+1}[\hat{a}_{i+1}-b_{a_{i}}]_{ imes}\delta t^{2} \ v_{20} &= -rac{1}{2}R_{i}\delta t \ v_{21} &= v_{23} &= rac{1}{4}R_{i+1}[\hat{a}_{i+1}-b_{a_{i}}]_{ imes}\delta t^{2} \ v_{22} &= -rac{1}{2}R_{i+1}\delta t \end{aligned}$$

位置误差导数的连续形式:

$$\delta \dot{\alpha}_t^{b_k} = \delta \beta_t^{b_k} \tag{11}$$

则中值法离散形式为:

$$\delta \dot{\alpha}_i = \frac{1}{2} \delta \beta_i + \frac{1}{2} \delta \beta_{i+1} \tag{12}$$

将式(35)代入上式可得:

$$\delta \dot{\alpha}_{i} = \delta \beta_{i} + \frac{1}{2} f_{21} \delta \theta_{i} - \frac{1}{4} (R_{i} + R_{i+1}) \delta t \delta b_{a_{i}} + \frac{1}{2} f_{24} \delta b_{w_{i}}$$

$$- \frac{1}{4} R_{i} \delta t n_{a_{i}} - \frac{1}{4} R_{i+1} \delta t n_{a_{i+1}} + \frac{1}{2} v_{21} n_{w_{i}} + \frac{1}{2} v_{23} n_{w_{i+1}}$$

$$(13)$$

根据导数定义:

$$\deltalpha_{i+1} = \deltalpha_i + \delta t\deltaeta_i + rac{1}{2}f_{21}\delta t\delta heta_i - rac{1}{4}(R_i + R_{i+1})\delta t^2\delta b_{a_i} + rac{1}{2}f_{24}\delta t\delta b_{w_i}$$

令:

$$egin{align} v_{00} &= -rac{1}{4}R_i\delta t^2 \ v_{01} &= v_{03} = rac{\delta t}{2}v_{21} \ v_{02} &= -rac{1}{4}R_{i+1}\delta t^2 \ f_{00} &= I \ \end{pmatrix}$$

$$f_{01}=rac{\delta t}{2}f_{21} \ f_{02}=\delta t \ f_{03}=-rac{1}{4}(R_i+R_{i+1})\delta t^2 \ f_{04}=rac{\delta t}{2}f_{24}$$

根据式(7)可得:

$$egin{aligned} \delta b_{a_{k+1}} &= \delta b_{a_k} + \delta t n_{b_a} \ \delta b_{w_{k+1}} &= \delta b_{w_k} + \delta t n_{b_w} \end{aligned}$$

令:

$$f_{33} = f_{44} = I \ v_{34} = v_{45} = \delta t$$

由上可以写出离散时间下的误差动力学,这里交换了 β,θ :

+	$egin{array}{c} v_{00} \ 0 \ v_{20} \ 0 \ \end{array}$	$egin{array}{c} v_{01} \ v_{11} \ v_{21} \ 0 \ \end{array}$	$egin{array}{c} v_{02} \ 0 \ v_{22} \ 0 \ \end{array}$	$egin{array}{c} v_{03} \ v_{13} \ v_{23} \ 0 \ \end{array}$	$egin{array}{c} 0 \ 0 \ v_{34} \ \end{array}$	$\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$	$egin{bmatrix} n_{a_i} \ n_{w_i} \ n_{a_{i+1}} \ n_{w_{i+1}} \ n_{b_a} \ \end{pmatrix}$
	$\begin{vmatrix} 0 \\ 0 \end{vmatrix}$	0	0	0	034	$\left. egin{array}{c} v_{45} \end{array} ight $	$\left egin{array}{c} n_{b_a} \ n_{b_w} \end{array} ight $