

MCEN 4173/5173

Chapter 4

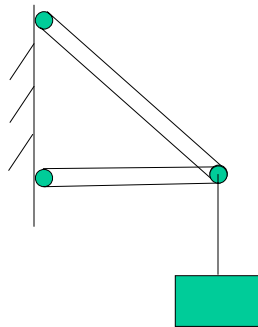
## 2D and 3D Truss Elements

Fall, 2006

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### Truss

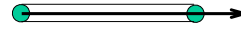
Truss is one of the simplest, yet very commonly used structural elements.



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## Truss

Features of a truss



- Forces can only be transmitted along the axial direction. Or a truss can only be subjected to axial load.
- The deformation is along the axial direction.
- A truss cannot sustain shear and moment.
- The load can only be applied at the two ends.

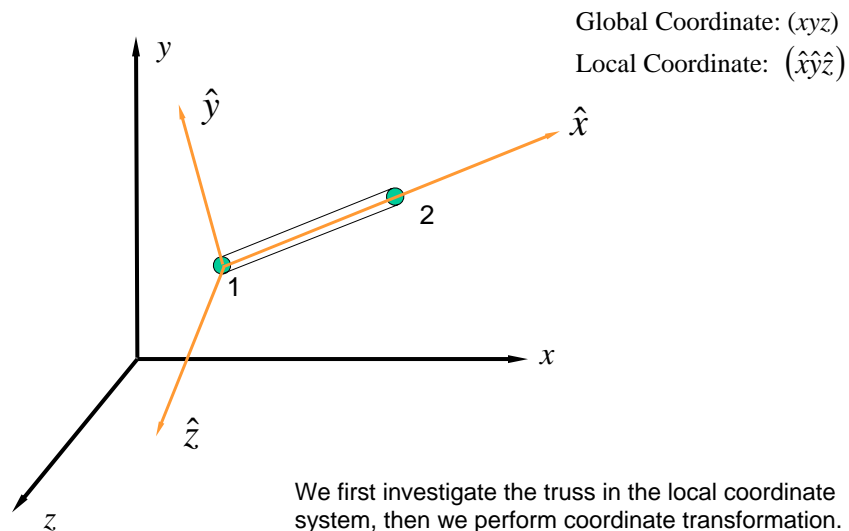
Learning points:

**Shape Functions**  
**Rotation of Coordinate System**

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## Truss

Mechanics of a truss

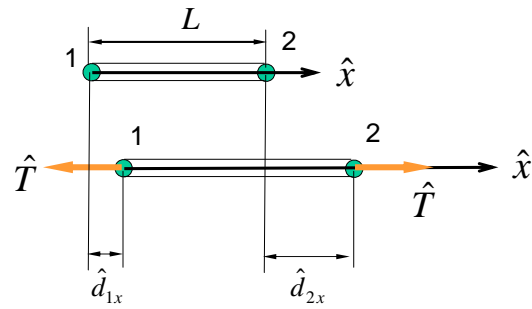


We first investigate the truss in the local coordinate system, then we perform coordinate transformation.

(Note: The procedure is different from lecture 3)

## Truss

Mechanics of a truss

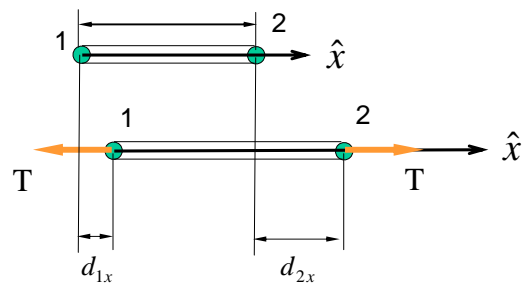


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## Truss

Shape Function

$$\varepsilon = \frac{du}{dx} \quad u = ?$$



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## Truss

Shape Function

$$\hat{u} = \left(1 - \frac{\hat{x}}{L}\right) \hat{d}_{1x} + \frac{\hat{x}}{L} \hat{d}_{2x}$$

$$\Rightarrow \hat{u} = \begin{bmatrix} 1 - \frac{\hat{x}}{L} & \frac{\hat{x}}{L} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \Rightarrow \hat{u} = \begin{bmatrix} N_1 & N_2 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

$N_1$  and  $N_2$  are called SHAPE FUNCTIONS, or Interpolation functions.

Shape functions describe the shape of displacement field and are one of the determinant factors in governing the efficiency and accuracy of FEA.

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## Truss

Shape Functions in general

In FEA, we hope

$$u(x, y, z) = a_0 + a_1x + b_1y + c_1z + \dots$$

$f_1, f_2, f_3, \dots$  are shape functions

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## Truss

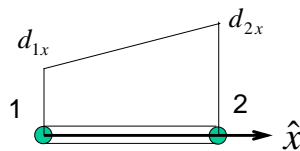
Shape Functions in general

$$N_1 = 1 - \frac{\hat{x}}{L} \quad N_2 = \frac{\hat{x}}{L}$$

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## Truss

Shape Function



Here, the shape functions are linear functions

Do linear functions make sense here? Or can we use quadratic functions?

Linear function:

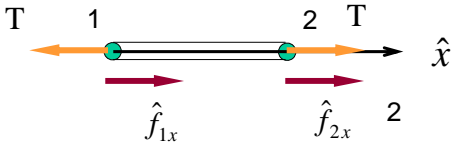
Since

Quadratic function:

Since

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### Truss Element

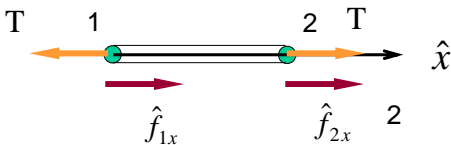


$$\hat{T} = EA\hat{\epsilon} = EA \frac{\hat{d}_{2x} - \hat{d}_{1x}}{L} \Rightarrow \begin{aligned} \hat{f}_{1x} &= -\hat{T} = \frac{EA}{L}(\hat{d}_{1x} - \hat{d}_{2x}) \\ \hat{f}_{2x} &= \hat{T} = \frac{EA}{L}(-\hat{d}_{1x} + \hat{d}_{2x}) \end{aligned}$$

$$\Rightarrow \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

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### Truss Element

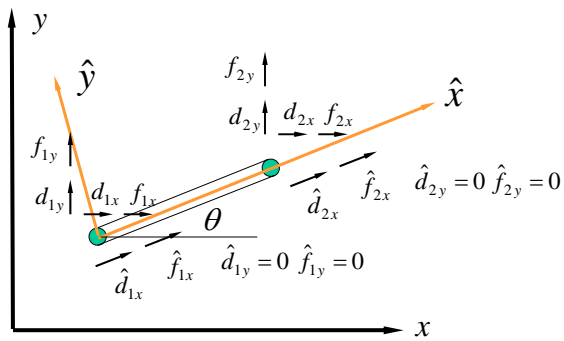


$$\hat{T} = EA\hat{\epsilon} = EA \frac{d\hat{u}}{d\hat{x}} \quad \hat{u} = \begin{bmatrix} N_1 & N_2 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \Rightarrow \begin{aligned} \hat{f}_{1x} &= -\hat{T} = EA \begin{bmatrix} -\frac{dN_1}{d\hat{x}} & -\frac{dN_2}{d\hat{x}} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \\ \hat{f}_{2x} &= \hat{T} = EA \begin{bmatrix} \frac{dN_1}{d\hat{x}} & \frac{dN_2}{d\hat{x}} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \end{aligned}$$

$$\Rightarrow \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = EA \begin{bmatrix} -\frac{dN_1}{d\hat{x}} & -\frac{dN_2}{d\hat{x}} \\ \frac{dN_1}{d\hat{x}} & \frac{dN_2}{d\hat{x}} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

$$\frac{dN_1}{d\hat{x}} = -\frac{1}{L} \quad \frac{dN_2}{d\hat{x}} = \frac{1}{L} \Rightarrow \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \quad 12$$

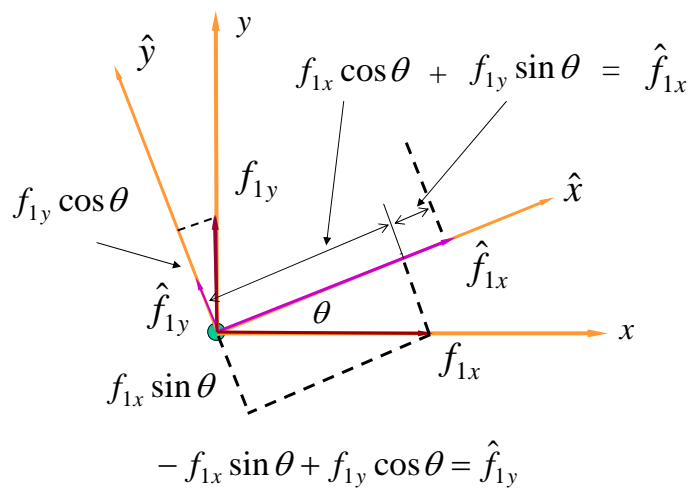
## Truss Element -2D



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## Truss Element -2D

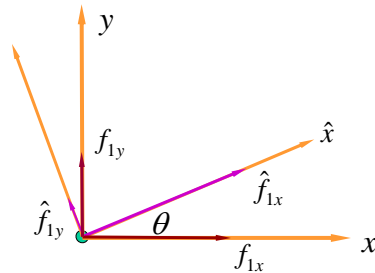
How are quantities in different coordinate systems related?



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## Truss Element -2D

How are quantities in different coordinate systems related?



$$\begin{aligned}\hat{f}_{1x} &= f_{1x} \cos \theta + f_{1y} \sin \theta \\ \hat{f}_{1y} &= -f_{1x} \sin \theta + f_{1y} \cos \theta\end{aligned}$$

$$\begin{aligned}\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} &= \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} \quad \text{or} \quad \begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} \\ \{\hat{f}\} &= [T]\{f\} \quad [T]^{-1} = [T]^T \quad \{f\} = [T]^{-1}\{\hat{f}\}\end{aligned}$$

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## Truss Element -2D

How are quantities in different coordinate systems related?

$$\begin{aligned}\begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} &= \begin{bmatrix} C & -S \\ S & C \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} \quad \begin{Bmatrix} d_{1x} \\ d_{1y} \end{Bmatrix} = \begin{bmatrix} C & -S \\ S & C \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \end{Bmatrix} \\ C &= \cos \theta \quad S = \sin \theta\end{aligned}$$

Now the question is:

$$\begin{aligned}\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} &= [??] \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} \quad \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} = [??] \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix}\end{aligned}$$

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## Truss Element -2D

How are quantities in different coordinate systems related?

$$\begin{aligned}
 \begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} &= \begin{bmatrix} C & -S \\ S & C \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} \quad \rightarrow \quad \begin{aligned} f_{1x} &= C\hat{f}_{1x} - S\hat{f}_{1y} \\ f_{1y} &= S\hat{f}_{1x} + C\hat{f}_{1y} \end{aligned} \quad \rightarrow \quad \begin{aligned} f_{1x} &= C\hat{f}_{1x} - S\hat{f}_{1y} + 0\hat{f}_{2x} + 0\hat{f}_{2y} \\ f_{1y} &= S\hat{f}_{1x} + C\hat{f}_{1y} + 0\hat{f}_{2x} + 0\hat{f}_{2y} \\ f_{2x} &= 0\hat{f}_{1x} + 0\hat{f}_{1y} + C\hat{f}_{2x} - S\hat{f}_{2y} \\ f_{2y} &= 0\hat{f}_{1x} + 0\hat{f}_{1y} + S\hat{f}_{2x} + C\hat{f}_{2y} \end{aligned} \\
 &\quad \downarrow \\
 \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} &= \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} \quad \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} = \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix}
 \end{aligned}$$

## Truss Element -2D

How are quantities in different coordinate systems related?

$\hat{x}\hat{y}\hat{z} \Rightarrow xyz$

$$\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} = \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} \quad \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} = \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix}$$

$xyz \Rightarrow \hat{x}\hat{y}\hat{z}$

$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} = \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} \quad \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix} = \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix}$$

## Truss Element -2D

Element stiffness matrix in global coordinate

$$\begin{aligned} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} &= \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix} \Rightarrow \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix} \\ \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} &= \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{1y} \\ \hat{d}_{2x} \\ \hat{d}_{2y} \end{Bmatrix} \\ &= \frac{EA}{L} \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} \quad 19 \end{aligned}$$

## Truss Element -2D

Element stiffness matrix in global coordinate

$$\begin{aligned} \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} &= \frac{EA}{L} \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} \\ \Rightarrow \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} &= \frac{EA}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ -CS & -S^2 & CS & S^2 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix} \\ [T] &= \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \quad \begin{aligned} \{f\} &= [T^T] [\hat{K}]^e [T] \{d\} \\ [K] &= [T^T] [\hat{K}]^e [T] \end{aligned} \quad 20 \end{aligned}$$

## Truss Element -2D

### Global Stiffness Matrix

Using the direct stiffness method.

Note: This time, each node has 2 degrees of freedom.

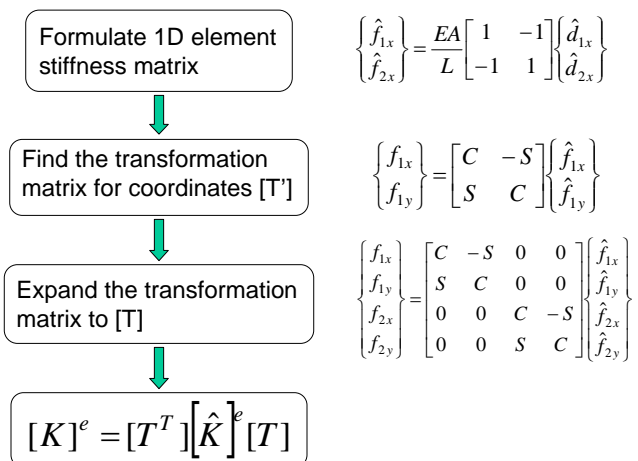
If we have N nodes in the model,

$$[K] = \begin{bmatrix} & & & \\ & & & \\ & & & \\ & & & \end{bmatrix}_{2N \times 2N}$$

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## Truss Element -3D

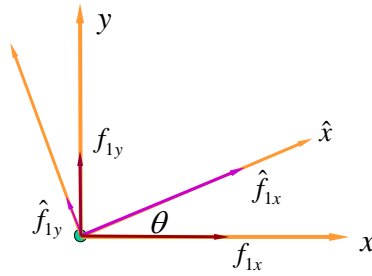
Review: what did we do when we move from 1D to 2D?



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### Truss Element -3D

Coordinate transformation matrix

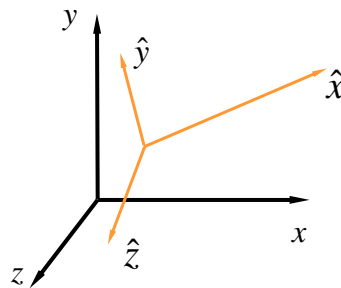


$$\begin{aligned} & \begin{matrix} x & y \\ \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) \end{matrix} \\ & \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} \begin{matrix} \hat{x} \\ \hat{y} \end{matrix} \\ & \begin{matrix} \hat{x} & \hat{y} \\ \cos(\langle x, \hat{x} \rangle) & \cos(\langle x, \hat{y} \rangle) \\ \cos(\langle y, \hat{x} \rangle) & \cos(\langle y, \hat{y} \rangle) \end{matrix} \\ & \begin{Bmatrix} f_{1x} \\ f_{1y} \end{Bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{Bmatrix} \begin{matrix} x \\ y \end{matrix} \end{aligned}$$

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### Truss Element -3D

Coordinate transformation matrix



$$\begin{aligned} & \begin{matrix} x & y & z \\ \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) & \cos(\langle \hat{x}, z \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) & \cos(\langle \hat{y}, z \rangle) \\ \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle) \end{matrix} \\ & \begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{1z} \end{Bmatrix} = \begin{bmatrix} \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) & \cos(\langle \hat{x}, z \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) & \cos(\langle \hat{y}, z \rangle) \\ \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle) \end{bmatrix} \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{1z} \end{Bmatrix} \begin{matrix} \hat{x} \\ \hat{y} \\ \hat{z} \end{matrix} \end{aligned}$$

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### Truss Element -3D

$$[T'] = \begin{bmatrix} \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) & \cos(\langle \hat{x}, z \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) & \cos(\langle \hat{y}, z \rangle) \\ \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle) \end{bmatrix}$$

$$[T] = \begin{bmatrix} [T'] & 0 \\ 0 & [T'] \end{bmatrix} \quad [\hat{K}]^e = \frac{EA}{L} \begin{bmatrix} 1 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$[K]^e = [T^T] [\hat{K}]^e [T]$$

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### Summary of Lecture 3 and 4

So far, we learned the following important concepts:

➤ Element stiffness matrix

➤ Shape function

**Element specific**

➤ Rotation of coordinate systems

**Not element specific**

➤ Global stiffness matrix

➤ Features of global stiffness matrix

➤ Physical meaning of elements in global stiffness matrix

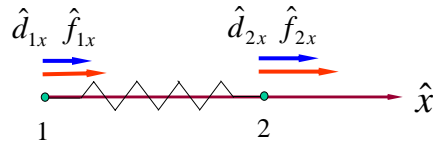
➤ Boundary conditions

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## Summary of Lecture 3 and 4

### Element stiffness matrix

- It represents the deformation (displacement) response of a node in an element to a nodal force.
- At element level.



$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

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## Summary of Lecture 3 and 4

### Element stiffness matrix

#### Shape function:

- A shape function describes the shape of displacement field (not the shape of an element).
- It also describes the contribution of displacement of a node to the displacement field of an element.

$$d = a_0 + a_1x + a_2x^2 + \dots \quad a_0=?, a_1=?, a_2=? \dots$$

Using conditions of  $d=d^{(1)}$ ,  $d=d^{(2)}$ ,  $d=d^{(3)}$ , ...

$$\rightarrow a_0 = a_0(d^{(1)}, d^{(2)}, d^{(3)}, \dots) \quad a_1 = a_1(d^{(1)}, d^{(2)}, d^{(3)}, \dots)$$

$$d = a_0(d^{(1)}, d^{(2)}, d^{(3)}, \dots) + a_1(d^{(1)}, d^{(2)}, d^{(3)}, \dots)x + a_2(d^{(1)}, d^{(2)}, d^{(3)}, \dots)x^2 + \dots$$

$$\rightarrow d = N_1d^{(1)} + N_2d^{(2)} + N_3d^{(3)} + \dots$$

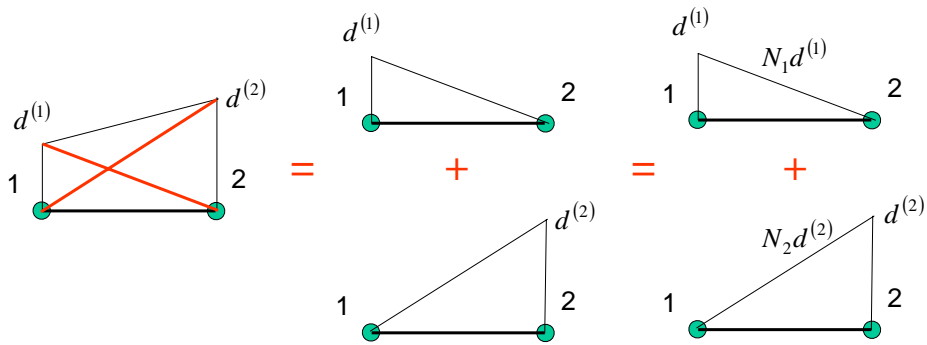
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### Summary of Lecture 3 and 4

Element stiffness matrix

Shape function:

$$d = N_1 d^{(1)} + N_2 d^{(2)} + N_3 d^{(3)} + \dots$$



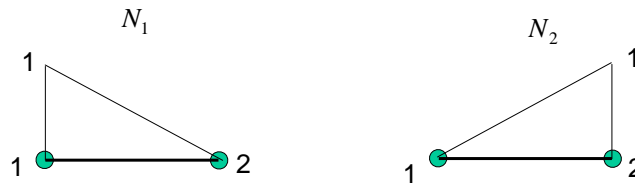
$N_1=1$ , at the coordinate of node 1,  $N_1=0$ , at the coordinate of node other than 1.

$N_2=1$ , at the coordinate of node 2,  $N_2=0$ , at the coordinate of node other than 2. <sup>29</sup>

### Summary of Lecture 3 and 4

Element stiffness matrix

Shape function:

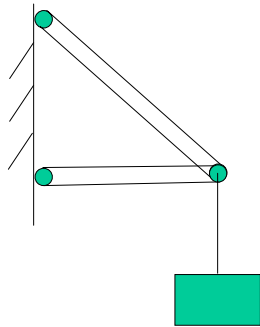


Such a feature of shape function is always true. We will use this feature to build a shape function later.

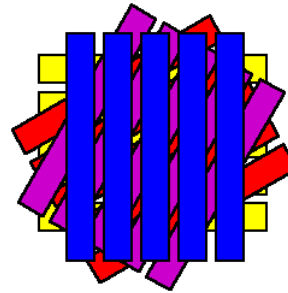
## Summary of Lecture 3 and 4

### Rotation of Coordinate Systems

The coordinate system used at element level might be different from the coordinate system used at global level.



Truss Structure



Top View of Rotated  
Fiber Layers

Composite Materials<sub>31</sub>

## Summary of Lecture 3 and 4

### Rotation of Coordinate Systems

$$\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} C & -S & 0 & 0 \\ S & C & 0 & 0 \\ 0 & 0 & C & -S \\ 0 & 0 & S & C \end{bmatrix} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix}$$

$$\Rightarrow \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ -CS & -S^2 & CS & S^2 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{1y} \\ d_{2x} \\ d_{2y} \end{Bmatrix}$$

$$[T] = \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix}$$

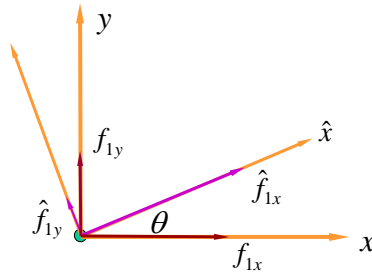
$$[K] = [T]^T [\hat{K}]^e [T]$$

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## Summary of Lecture 3 and 4

### Rotation of Coordinate Systems

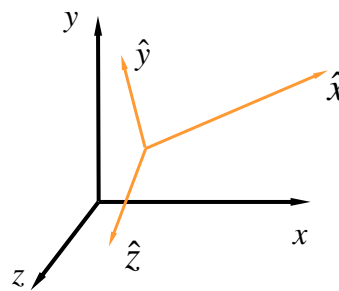


$$\begin{array}{c}
 \begin{array}{cc}
 x & y \\
 \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) \\
 \left\{ \begin{array}{c} \hat{f}_{1x} \\ \hat{f}_{1y} \end{array} \right\} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} f_{1x} \\ f_{1y} \end{bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{bmatrix} \\
 \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle)
 \end{array} \\
 \begin{array}{cc}
 \hat{x} & \hat{y} \\
 \cos(\langle x, \hat{x} \rangle) & \cos(\langle x, \hat{y} \rangle) \\
 \left\{ \begin{array}{c} f_{1x} \\ f_{1y} \end{array} \right\} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \end{bmatrix} \\
 \cos(\langle y, \hat{x} \rangle) & \cos(\langle y, \hat{y} \rangle)
 \end{array}
 \end{array}$$

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## Summary of Lecture 3 and 4

### Rotation of Coordinate Systems



$$\begin{array}{c}
 \begin{array}{ccc}
 x & y & z \\
 \left\{ \begin{array}{c} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{1z} \end{array} \right\} = \begin{bmatrix} \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) & \cos(\langle \hat{x}, z \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) & \cos(\langle \hat{y}, z \rangle) \\ \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle) \end{bmatrix} \begin{bmatrix} f_{1x} \\ f_{1y} \\ f_{1z} \end{bmatrix} = \begin{bmatrix} \cos(\langle \hat{x}, x \rangle) & \cos(\langle \hat{x}, y \rangle) & \cos(\langle \hat{x}, z \rangle) \\ \cos(\langle \hat{y}, x \rangle) & \cos(\langle \hat{y}, y \rangle) & \cos(\langle \hat{y}, z \rangle) \\ \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle) \end{bmatrix} \begin{bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{1z} \end{bmatrix} \\
 \cos(\langle \hat{z}, x \rangle) & \cos(\langle \hat{z}, y \rangle) & \cos(\langle \hat{z}, z \rangle)
 \end{array}
 \end{array}$$

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## Summary of Lecture 3 and 4

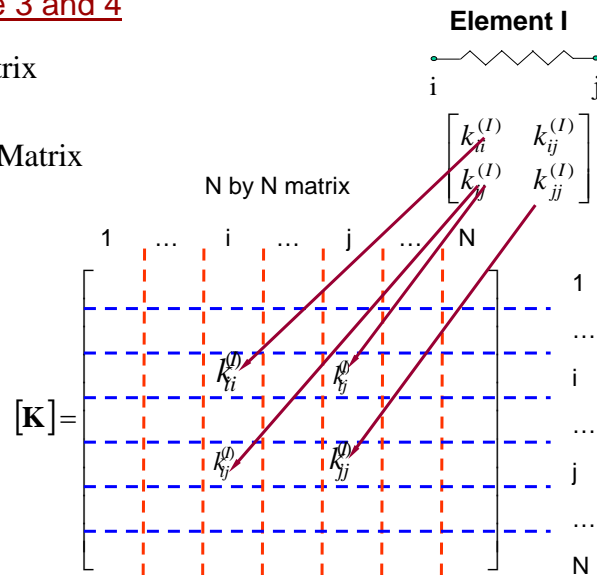
Global Stiffness Matrix

Element Stiffness Matrix

Direct  
Stiffness  
Method

Boeing  
Airplane

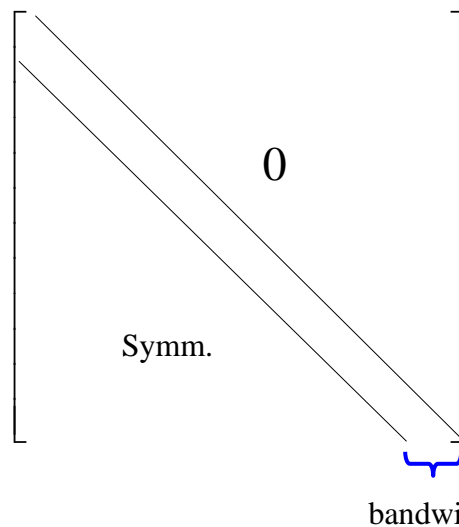
Global Stiffness Matrix



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## Summary of Lecture 3 and 4

Global Stiffness Matrix



**A large, symmetric,  
sparse matrix.**

**Memory requirement depends  
on the total DOF and bandwidth.**

- Total DOF depends on mesh and type of elements
- Bandwidth depends how nodes are numbered.

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### Summary of Lecture 3 and 4

#### Global Stiffness Matrix

#### Physical Meaning

$K_{ij}$  is equal to the reaction “force” on the  $i$ -th DOF due to a unit “displacement” on the  $j$ -th DOF whereas all the other DOFs are fixed.

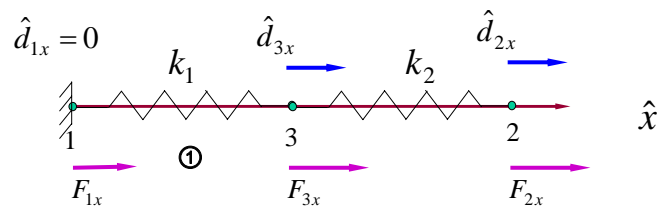
- Here, “force” can be a force, or a moment; “displacement” can be a displacement, or a rotation.
- $i$ -th DOF does NOT have to be in the same direction as  $j$ -th DOF.

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### Summary of Lecture 3 and 4

#### Boundary Conditions

For static analysis, boundary conditions should at least get rid of rigid body motion.



$$\begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix} = \begin{bmatrix} \text{X} & \text{X} & -\text{X}_1 \\ \text{X} & k_2 & -k_2 \\ -\text{X}_1 & -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} 0 \\ \hat{d}_{2x} \\ \hat{d}_{3x} \end{Bmatrix}$$

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