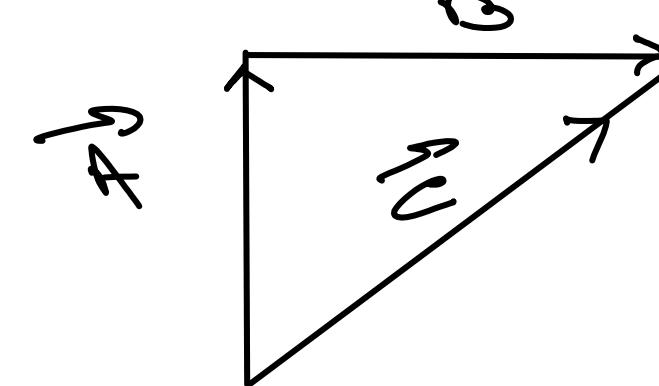


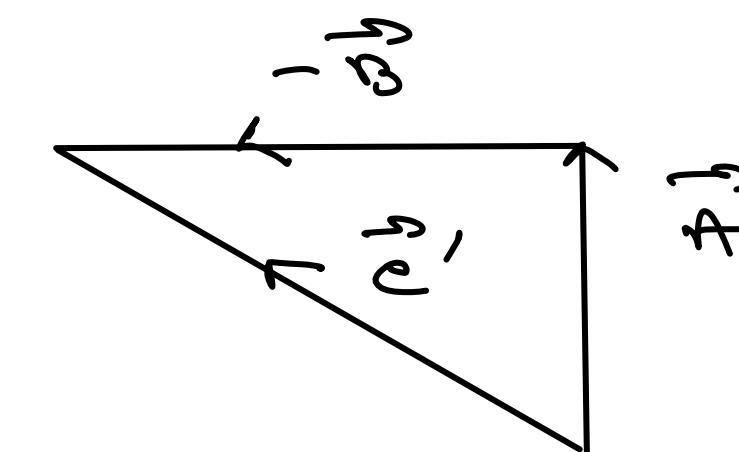
Vector Operations

(1) Addition



vector \vec{C} = $\vec{A} + \vec{B}$

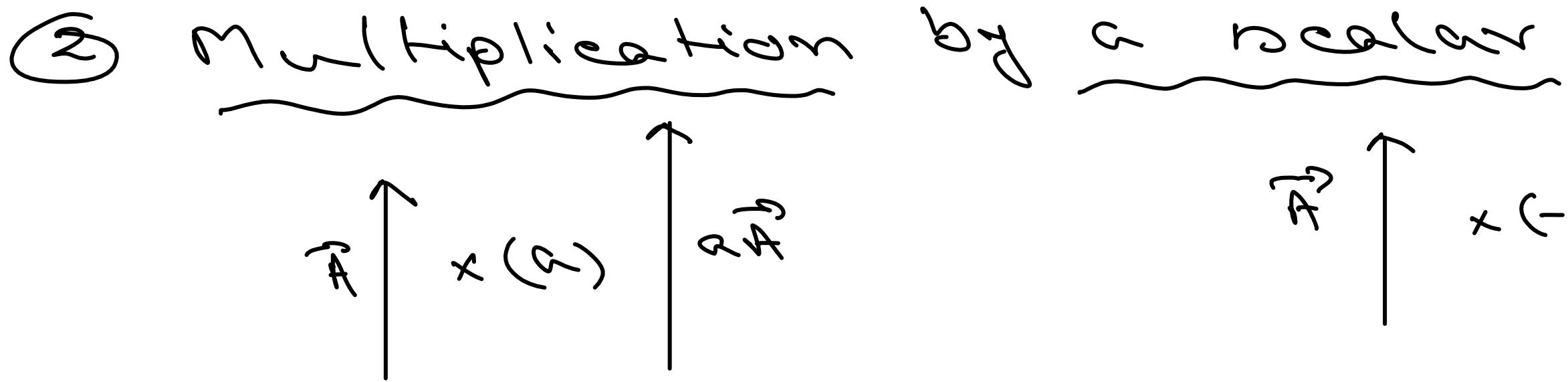
Subtraction



$$\vec{C}' = \vec{A} - \vec{B}$$

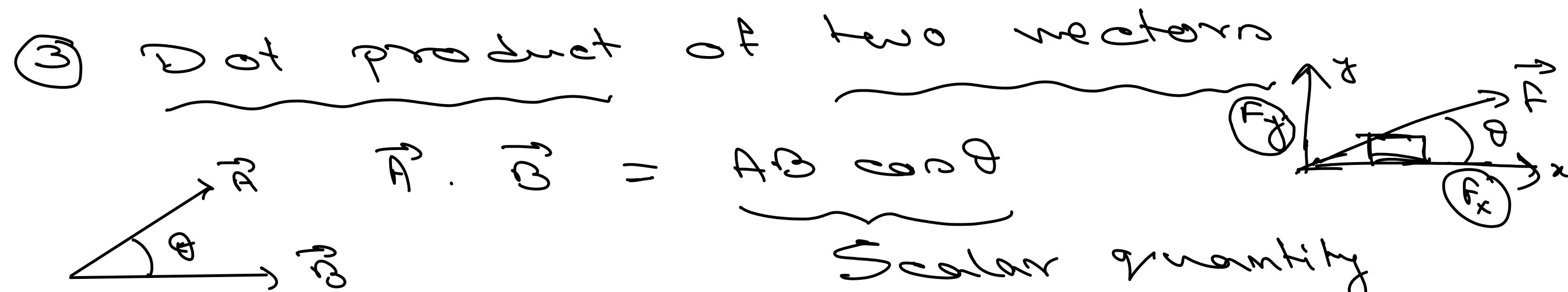
(+) Addition is associative

$$(\vec{A} + \vec{B}) + \vec{C} = \vec{A} + (\vec{B} + \vec{C})$$



(2) Multiplication by a scalar is distributive

$$q(F_A + F_B) = qF_A + qF_B$$



$$F_{AB} = \vec{F}_A \cdot \vec{F}_B$$

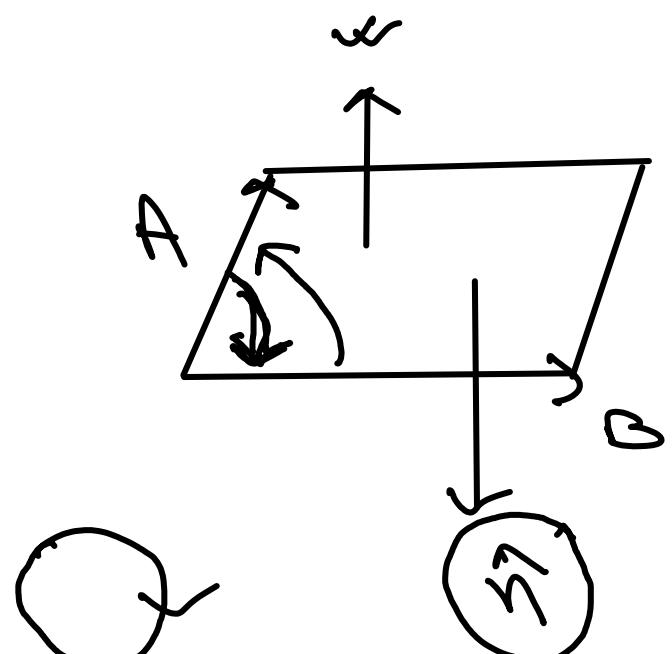
$$F_{AB} = F_A \cos \theta$$

⑦ $\vec{D} \cdot \vec{Q} + \vec{P} \cdot \vec{R} = \vec{D} \cdot \vec{Q} + \vec{P} \cdot \vec{R}$ is Commutative

⑧ $\vec{D} \cdot \vec{Q} + \vec{P} \cdot \vec{R} = \vec{D} \cdot (\vec{Q} + \vec{R}) = \vec{D} \cdot \vec{S}$ is Distributive

Geometrically, $\vec{D} \cdot \vec{Q}$ is simply product of length times the projection of \vec{Q} along \vec{D} or vice versa.

⑨ If the two vectors \vec{D}, \vec{Q} are parallel:
they are perpendicular;
 $\vec{D} \cdot \vec{Q} = \vec{D} \cdot \vec{Q} \uparrow$
 $= 0$

- (5) Cross product betw. two vectors
- $$\vec{A} \times \vec{B} = \vec{n}$$
- 
- \vec{n} = unit vector
perpendicular to the plane formed by \vec{A} and \vec{B}
- $\vec{A} \times \vec{B}$ = points into the page
- $\vec{A} \times \vec{B}$ = points out of the page.

- (6) Cross product is distributive
- $$(\vec{A} + \vec{B}) \times \vec{C} = \vec{A} \times \vec{C} + \vec{B} \times \vec{C}$$
- $\vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times \vec{B} + \vec{A} \times \vec{C}$
- commutative

To geometrically,
the parallelogram $\{A' \times B'\}$ generated by

- (+)
1) If the vectors $\vec{P} \times \vec{Q} = 0$ are parallel,
2) if the perpendicular $\vec{P} \times \vec{Q} = PB_3$

3) Component form

1) Cartesian co-ordinate system

2) Basis vectors $= x_1, x_2$

$$\vec{P} = P_1 x_1 + P_2 x_2$$

Component

\mathcal{P}_X is the orthogonal projection onto the line through x_0 perpendicular to $\mathcal{A}x_0$.
 $\mathcal{P}_{\mathcal{A}x_0}$ is the orthogonal projection onto the line $\mathcal{A}x_0$.

(+) Definition

$$\mathcal{P}_X x = (A_{xx} + B_x) x + (A_{xy} + B_y) y + (A_{xz} + B_z) z$$

(+) Multiplication by scalar

$$\mathcal{P}_X (c \mathcal{P}_X x) = (c A_{xx}) x + (c A_{xy}) y + (c A_{xz}) z$$

(+) Product rule

$$\mathcal{P}_X (\mathcal{P}_X x) = \mathcal{P}_X B_x + \mathcal{P}_X A_{xy} y + \mathcal{P}_X A_{xz} z$$

$$x = B_x + A_{xy} y + A_{xz} z$$

$$\begin{aligned} \mathcal{P}_X^2 &= -\mathcal{P}_X^\perp \\ \mathcal{P}_X^\perp &= -\mathcal{P}_X \cdot \mathcal{P}_X = -\mathcal{P}_X \cdot \mathcal{P}_X^\perp = -\mathcal{P}_X^\perp \cdot \mathcal{P}_X = 0 \end{aligned}$$

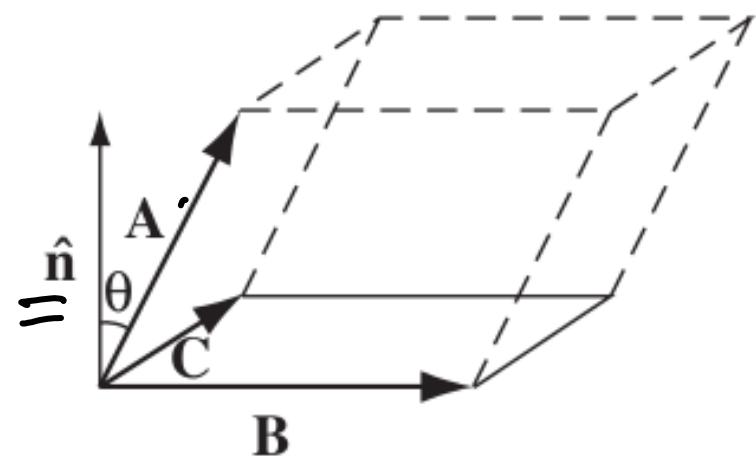
Triple Product

$$\# \text{ scalar triple product} = D^3 \cdot (\underbrace{\beta_1 + \beta_2}_{\beta})$$

→ Geometrically, $\vec{F} \cdot (\vec{a} \times \vec{c})$ is the volume of a parallelopiped.

$|\vec{a} \times \vec{c}| = \text{Area of the base}$

$|\vec{F}| \cos \theta = \text{Altitude}$



$$\vec{F} \cdot (\vec{a} \times \vec{c}) = \vec{a} \cdot (\vec{c} \times \vec{F}) = \vec{c} \cdot (\vec{F} \times \vec{a})$$

Link to the Recording:

$$\begin{aligned}
 A \cdot P_j &= P_j = \beta_1 \beta_2 \dots \beta_n \\
 P_j \cdot P_j &= (A + \beta_1 \beta_2 \dots \beta_n) P_j = \beta_1 \beta_2 \dots \beta_n P_j + A P_j \\
 P_j \cdot \beta_j &= (A + \beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n) \beta_j = \beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n \beta_j + A \beta_j \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n \beta_j + \beta_1 \beta_2 \dots \beta_{j-1} \beta_j \beta_{j+1} \dots \beta_n + A \beta_j \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n (\beta_j + \beta_{j+1} \beta_j \beta_{j+2} \dots \beta_n) + A \beta_j \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n (\beta_j + \beta_{j+1} \beta_{j+2} \dots \beta_n \beta_j) \cdot (\beta_1 \beta_2 \dots \beta_{j-1} \beta_{j+1} \dots \beta_n \beta_j) \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} (\beta_j \beta_{j+1} \dots \beta_n \beta_j + \beta_{j+1} \beta_{j+2} \dots \beta_n \beta_j \beta_{j+1}) \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} (\beta_j \beta_{j+1} \dots \beta_n \beta_j + \beta_{j+1} \beta_{j+2} \dots \beta_n \beta_j \beta_{j+1}) \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} (\beta_j \beta_{j+1} \dots \beta_n \beta_j + \beta_{j+1} \beta_{j+2} \dots \beta_n \beta_j \beta_{j+1}) \\
 P_j \cdot \beta_j &= \beta_1 \beta_2 \dots \beta_{j-1} (\beta_j \beta_{j+1} \dots \beta_n \beta_j + \beta_{j+1} \beta_{j+2} \dots \beta_n \beta_j \beta_{j+1})
 \end{aligned}$$

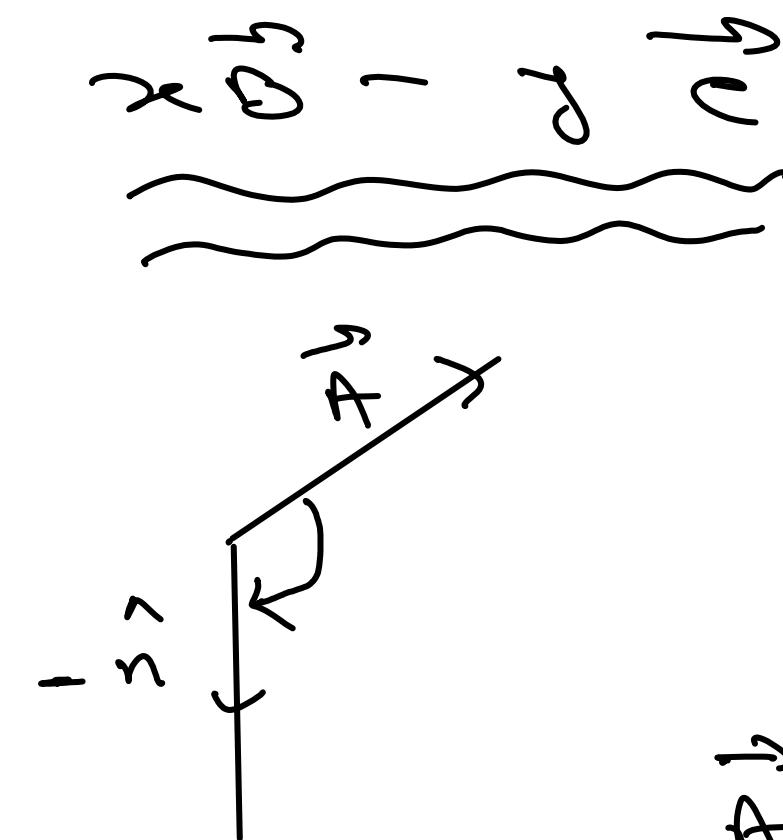
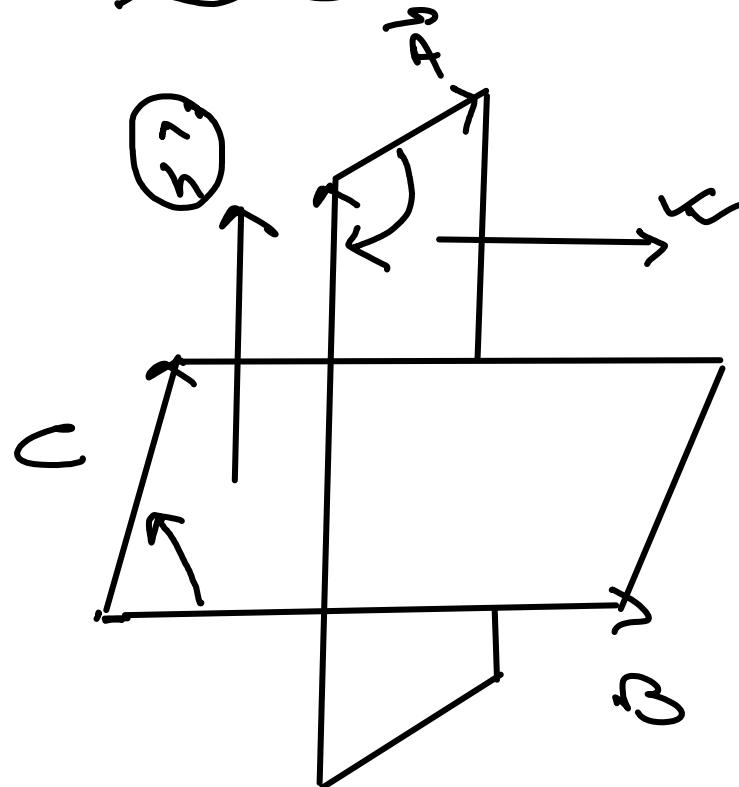
Triple product

Scalar product

$$\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A}) = \vec{C} \cdot (\vec{A} \times \vec{B})$$

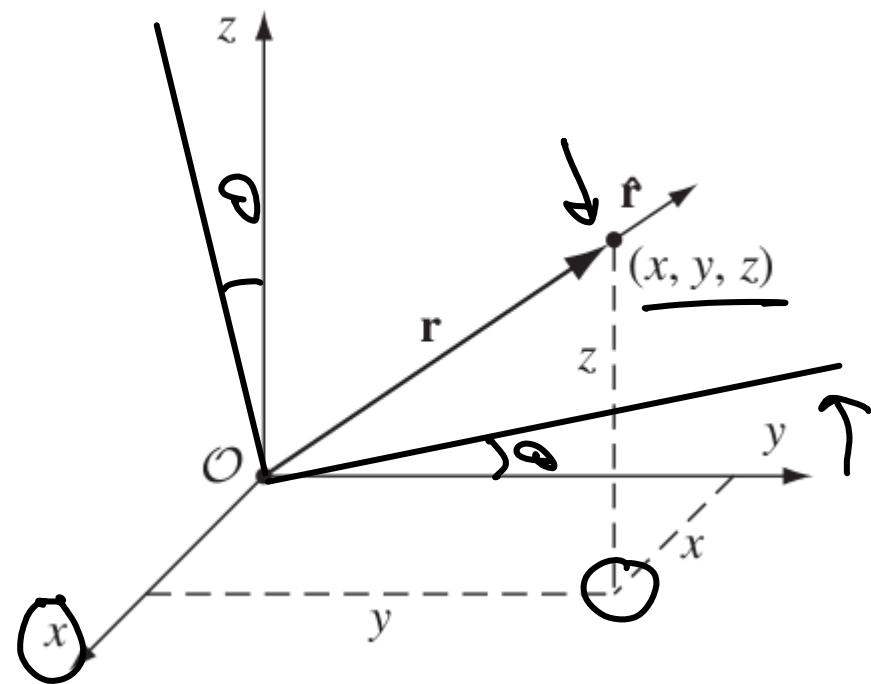
vector triple product

$$\vec{A} \times (\vec{B} \times \vec{C}) = \vec{B} (\vec{A} \cdot \vec{C}) - \vec{C} (\vec{A} \cdot \vec{B})$$

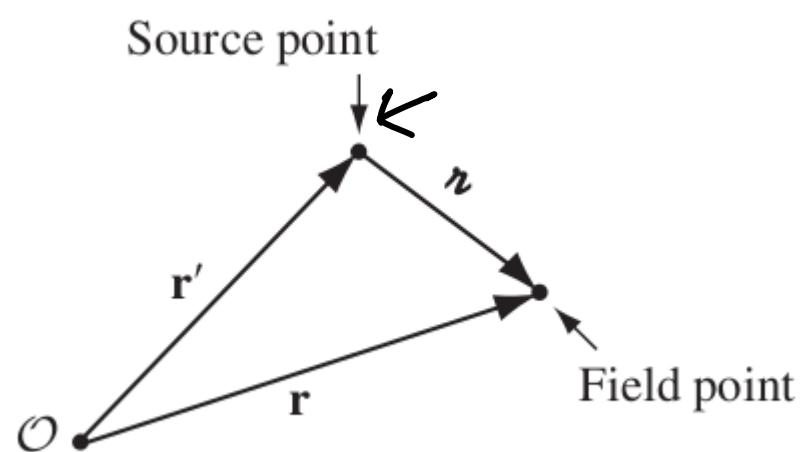


$\vec{A} \times (\vec{B} \times \vec{C}) = \text{on } BC \text{ plane}$
(Pointed towards right)

Position vector



Separation vector



$\mathbf{r}' = \mathbf{r} - \mathbf{r}'$ = Position vector of which
we wish to calculate the

$\mathbf{r}' = \mathbf{r}'$ = Position vector of the
source

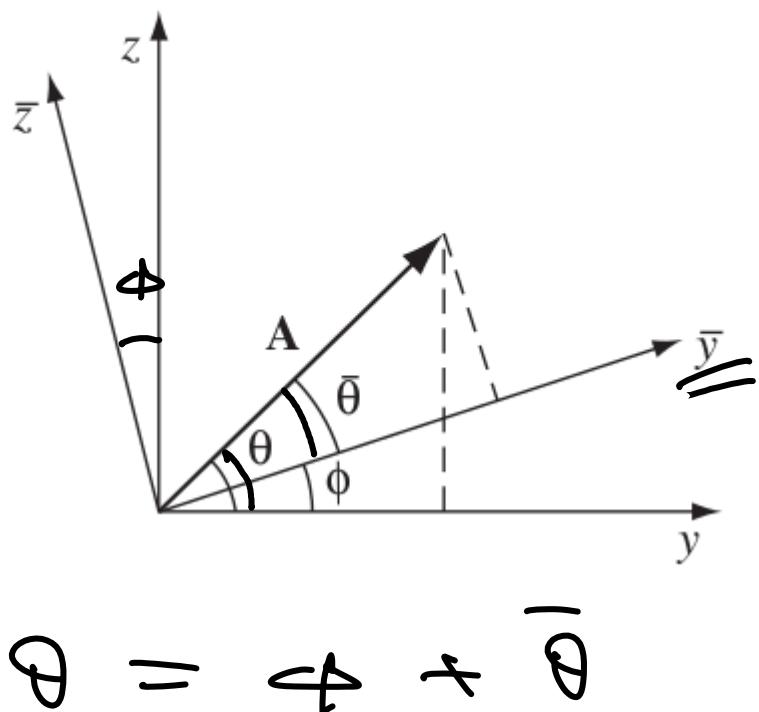
$\mathbf{r}' = \mathbf{r}'$ = Separation vector.
 $= \mathbf{r}' - \mathbf{r}$

$$\begin{aligned}\mathbf{r}' &= \mathbf{x} + \mathbf{y} + \mathbf{z} \\ \mathbf{r} &= |\mathbf{r}'| = \sqrt{x^2 + y^2 + z^2} \\ \mathbf{r}' &= \frac{\mathbf{r}'}{|\mathbf{r}'|} = \frac{x}{\sqrt{x^2 + y^2 + z^2}} \mathbf{i} + \frac{y}{\sqrt{x^2 + y^2 + z^2}} \mathbf{j} + \frac{z}{\sqrt{x^2 + y^2 + z^2}} \mathbf{k}\end{aligned}$$

Transformation of Vectors

If \vec{r}' or \vec{r} for "like a vector" to transform "like a vector"

say, we're going from (x, y, z) to (x', y', z')
 ↴ Rotation of \vec{r} & relative \vec{r} to (x, y, z)
 about $\vec{x} = \vec{x}'$



$$\vartheta = \phi + \bar{\alpha}$$

$$\begin{aligned}
 \vec{r}' &= \vec{r} \vec{y} \vec{y} \vec{y} \vec{y} \vec{y} \vec{y} \\
 &= \vec{r} (\cos \vartheta \vec{i} + \sin \vartheta \vec{j}) \\
 &= \vec{r} \cos \vartheta \vec{i} + \vec{r} \sin \vartheta \vec{j}
 \end{aligned}$$

$$\vec{P}_x^1 = P \cos \theta = P \cos(\theta - \phi)$$

$$= P (\sin \cos \phi - \cos \sin \phi)$$

$$= P_x \cos \phi - P_y \sin \phi$$

$$\vec{P}_y^1 = P$$

This is $\vec{P}_y^1 = P_1 \vec{P}_y^1 + P_2 \vec{P}_y^2$ written as

$$= \begin{pmatrix} \cos \phi & \sin \phi \\ -\sin \phi & \cos \phi \end{pmatrix} \begin{pmatrix} P_1 \\ P_2 \end{pmatrix}$$

and generally, $y =$

\begin{pmatrix} P_1 \\ P_2 \end{pmatrix} = \begin{pmatrix} R_{xx} & R_{xy} \\ R_{yx} & R_{yy} \end{pmatrix} \begin{pmatrix} P_x \\ P_y \end{pmatrix}

$$R_{yy} = 0$$

$$R_{xx} = 0$$

$$\begin{pmatrix} R_{xx} & R_{xy} \\ R_{yx} & R_{yy} \end{pmatrix} \begin{pmatrix} P_x \\ P_y \end{pmatrix}$$

$$= \begin{pmatrix} R_{xx} & 0 \\ R_{yx} & R_{yy} \end{pmatrix} \begin{pmatrix} P_x \\ P_y \end{pmatrix}$$

$$\begin{pmatrix} P_x \\ P_y \end{pmatrix} = \begin{pmatrix} R_{xx} & 0 \\ R_{yx} & R_{yy} \end{pmatrix}^{-1} \begin{pmatrix} P_x \\ P_y \end{pmatrix}$$

$$F_i = \sum_{j=1}^3 R_{ij} F_j$$

$\left\{ \begin{array}{l} j=1 = x \\ j=2 = y \\ j=3 = z \end{array} \right.$

Link to the Recording:

https://bennettu.sharepoint.com/sites/EPHY105L-Odd2021/Shared%20Documents/General/Recordings/Meeting%20in%20_General_-20210930_134250-Meeting%20Recording.mp4

Transformation of vectors

For rotation about an arbitrary axis in 3-D

$$\begin{pmatrix} \vec{A}'_x \\ \vec{A}'_y \\ \vec{A}'_z \end{pmatrix} = \begin{pmatrix} R_{xx} & R_{xy} & R_{xz} \\ R_{yx} & R_{yy} & R_{yz} \\ R_{zx} & R_{zy} & R_{zz} \end{pmatrix} \begin{pmatrix} \vec{A}_x \\ \vec{A}_y \\ \vec{A}_z \end{pmatrix}$$

\vec{A}'_i component

$$\vec{A}'_i = \sum_{j=1}^3 R_{ij} \vec{A}_j$$

$$\begin{cases} i = 1 = x \\ i = 2 = y \\ i = 3 = z \end{cases}$$

For rotation along x-axis by an angle ϕ :

$$R_{xx} = 1, \quad R_{xy} = 0, \quad R_{xz} = 0$$

$$R_{yx} = 0, \quad R_{yy} = \cos \phi, \quad R_{yz} = \sin \phi$$

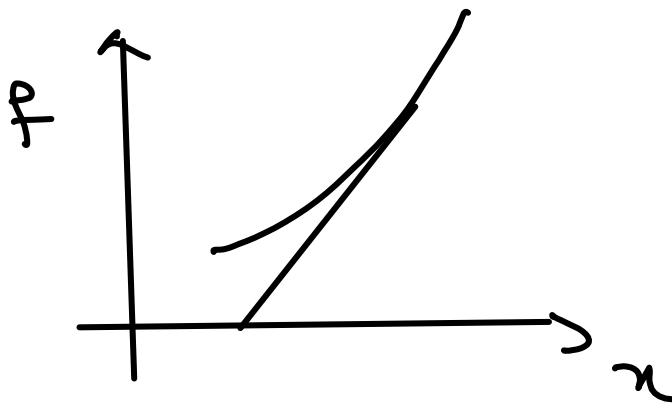
$$R_{zx} = 0, \quad R_{zy} = -\sin \phi, \quad R_{zz} = \cos \phi$$

\vec{A}
 θ
 ϕ
 \vec{A}'
 x
 y

$$\begin{aligned}
 \vec{A}' &= \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} \vec{A}_x \\ \vec{A}_y \end{pmatrix} \\
 &= \begin{pmatrix} \vec{A}_x \cos \theta + \vec{A}_y \sin \theta \\ -\vec{A}_x \sin \theta + \vec{A}_y \cos \theta \end{pmatrix}
 \end{aligned}$$

Gradient

To get the derivative of f_T we have to vary T with respect to its respective coordinate.



$$\frac{\partial f_T}{\partial T} = \left(\frac{\partial f_T}{\partial x} \right)_x \text{ Slope of the graph.}$$

$$\Rightarrow \Delta f_T = T = T(x, y, z)$$

$$\Rightarrow \Delta f_T = \left(\frac{\partial f_T}{\partial x} \right) \Delta x + \left(\frac{\partial f_T}{\partial y} \right) \Delta y + \left(\frac{\partial f_T}{\partial z} \right) \Delta z$$

This tells us how T varies when we alter f_T after infinitesimal variations of variables by $\Delta x, \Delta y, \Delta z$.

Rewrite Δf_T as:

$$g_1 = \left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} + \frac{\partial}{\partial z} \right) \cdot \underbrace{\left(\frac{\partial f}{\partial x} \right)}_{\text{Gradient of } f}.$$

Now write,

$$g_1 = \left| \frac{\partial f}{\partial x} \right| \cos \theta \quad \begin{matrix} \uparrow \\ \theta \end{matrix} \quad \begin{matrix} \downarrow \\ f \end{matrix}$$

Then for fixed $\left| \frac{\partial f}{\partial x} \right|$, g_1 is maximum when

$$\theta = 0 \text{ or } \cos \theta = 1$$

\Rightarrow the magnitude $\left| \frac{\partial f}{\partial x} \right|$ gives the slope along the maxima direction.

\downarrow $\frac{\partial f}{\partial x}$ is directed along the direction of maximum increase of f .

Link to the Recording:

https://bennettu.sharepoint.com/sites/EPHY105L-Odd2021/Shared%20Documents/General/Recordings/Meeting%20in%20_General_-20211004_154403-Meeting%20Recording.mp4?web=1

Del Operator

$$\vec{\nabla} = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$$

→ Operator, only has meaning when it operates on something.

Operations

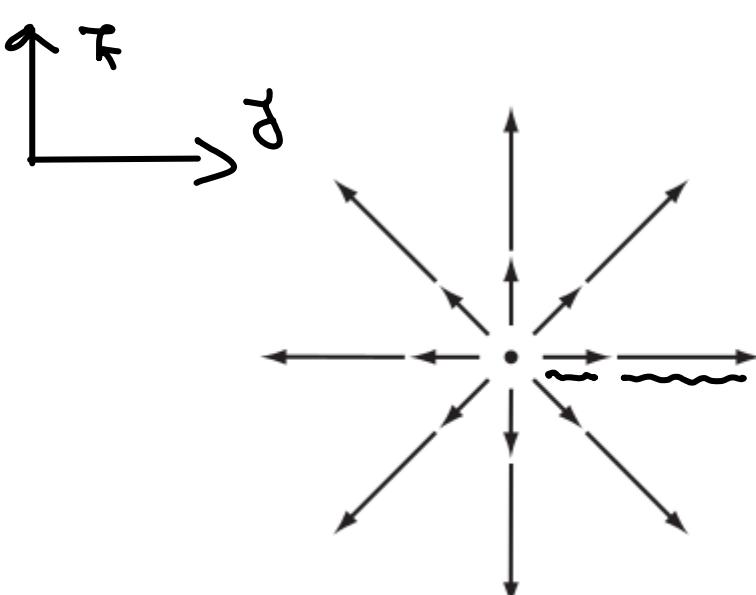
$$\vec{\nabla} F \equiv \text{Gradient}$$

$$\vec{\nabla} \cdot \vec{F} \equiv \text{Divergence}$$

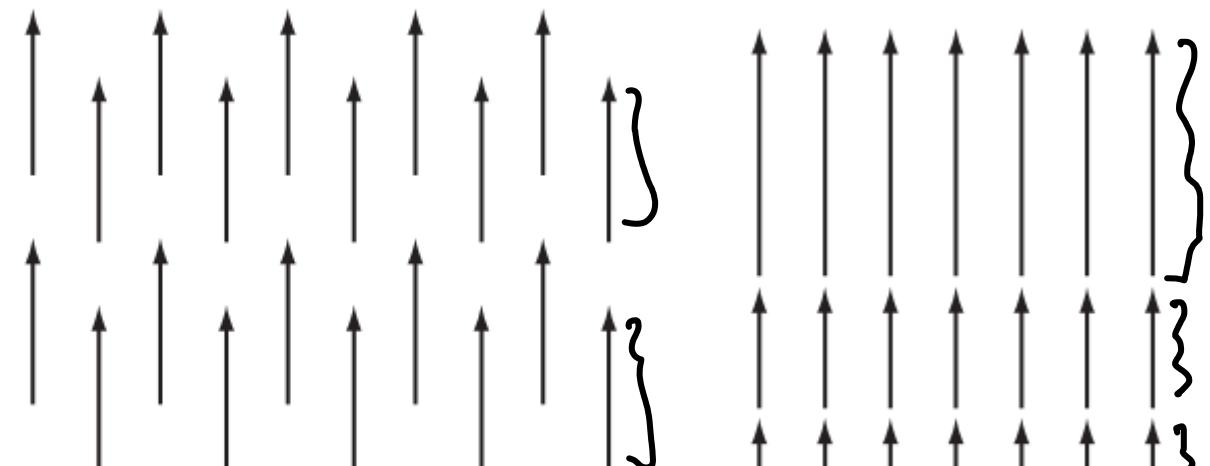
$$\vec{\nabla} \times \vec{F} \equiv \text{Curl}$$

Divergence

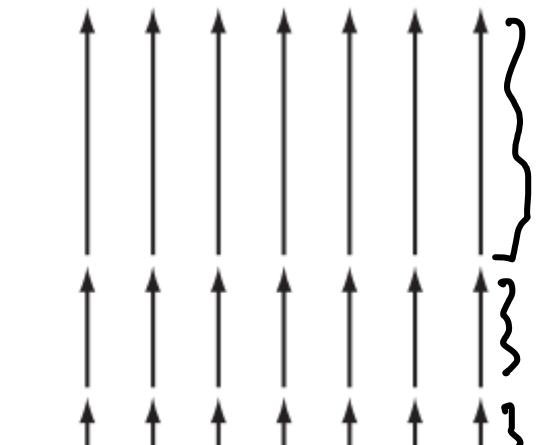
$\vec{\nabla} \cdot \vec{F} \equiv$ measurement of how the vector spreads out



(a)



(b)



(c)

$$\nabla \cdot \vec{P} = \frac{\partial P_x}{\partial x} + \frac{\partial P_y}{\partial y} + \frac{\partial P_z}{\partial z}$$

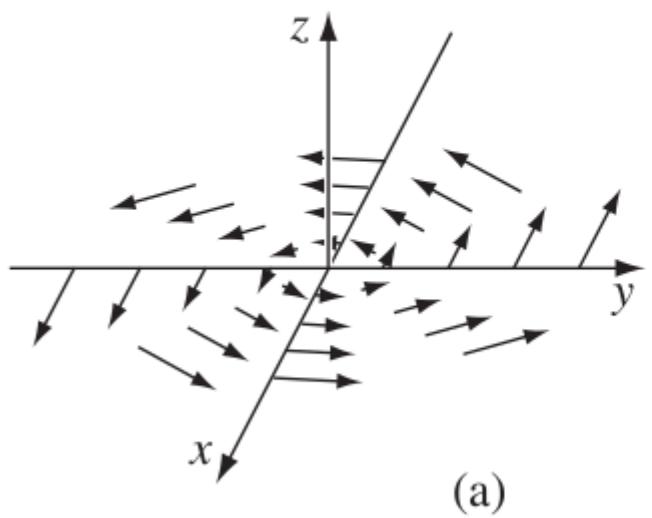
$$\nabla \cdot \vec{P} = 0$$

$$\nabla \cdot \vec{P} \neq 0$$

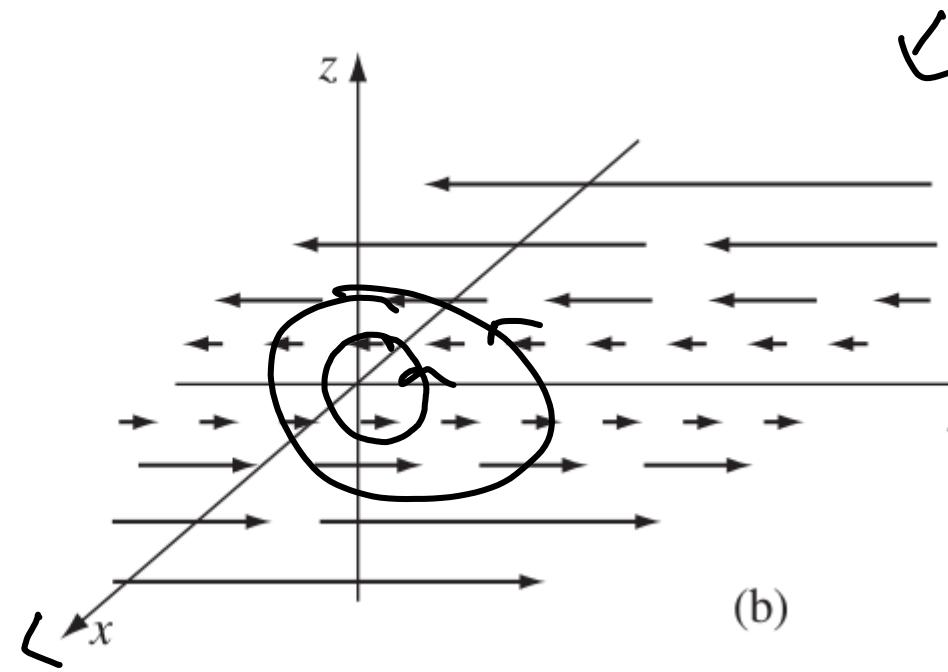
$\int \nabla \cdot \vec{D} = \oint \frac{\partial}{\partial r} D_r$ quantity.

$$\begin{aligned} \nabla \times \vec{P} &= \left| \begin{array}{ccc} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & P_x & P_y \\ 0 & P_y & P_z \end{array} \right| \\ &= \left(\frac{\partial P_z}{\partial y} - \frac{\partial P_y}{\partial z} \right) \hat{x} + \left(\frac{\partial P_x}{\partial z} - \frac{\partial P_z}{\partial x} \right) \hat{y} + \left(\frac{\partial P_y}{\partial x} - \frac{\partial P_x}{\partial y} \right) \hat{z} \end{aligned}$$

→ 3 ways to represent a point
) either ground or how much the vector



(a)



(b)

$$\vec{P} = \vec{P}_g + \vec{d}$$

$$\vec{P} = \vec{P}_g + \frac{\vec{P}_g - \vec{P}_g}{\|\vec{P}_g - \vec{P}_g\|}$$

$$\begin{aligned} \vec{d} &= \vec{P} - (\vec{P}_g + \vec{d}) \\ &= (\vec{P} - \vec{P}_g) + \vec{d} \\ &= \vec{v} + \vec{d} \end{aligned}$$

$$\begin{aligned} \rightarrow \quad \nabla \cdot (\kappa \vec{f}) &= \kappa \nabla \cdot \vec{f} + \vec{f} \cdot \nabla \kappa \\ \rightarrow \quad \nabla \cdot (\kappa \vec{A}) &= \kappa (\vec{A} \cdot \vec{\nabla}) + \vec{A} \cdot (\nabla \kappa) \\ \nabla \times (\kappa \vec{A}) &= \kappa (\vec{\nabla} \times \vec{A}) - \vec{A} \times (\nabla \kappa) \end{aligned}$$

Accordingly, there are *six* product rules, two for gradients:

$$(i) \quad \nabla(fg) = f\nabla g + g\nabla f,$$

$$(ii) \quad \nabla(\mathbf{A} \cdot \mathbf{B}) = \mathbf{A} \times (\nabla \times \mathbf{B}) + \mathbf{B} \times (\nabla \times \mathbf{A}) + (\mathbf{A} \cdot \nabla)\mathbf{B} + (\mathbf{B} \cdot \nabla)\mathbf{A},$$

two for divergences:

$$(iii) \quad \nabla \cdot (f\mathbf{A}) = f(\nabla \cdot \mathbf{A}) + \mathbf{A} \cdot (\nabla f),$$

$$(iv) \quad \nabla \cdot (\underline{\mathbf{A} \times \mathbf{B}}) = \mathbf{B} \cdot (\nabla \times \mathbf{A}) - \mathbf{A} \cdot (\nabla \times \mathbf{B}), \quad \leftarrow$$

and two for curls:

$$(v) \quad \nabla \times (f\mathbf{A}) = f(\nabla \times \mathbf{A}) - \mathbf{A} \times (\nabla f),$$

$$(vi) \quad \nabla \times (\mathbf{A} \times \mathbf{B}) = (\mathbf{B} \cdot \nabla)\mathbf{A} - (\mathbf{A} \cdot \nabla)\mathbf{B} + \mathbf{A}(\nabla \cdot \mathbf{B}) - \mathbf{B}(\nabla \cdot \mathbf{A}).$$

Second Derivative

① $\nabla \cdot (\nabla T) = \text{Divergence of gradient}$

② ~~$\nabla \times (\nabla T)$~~ $\nabla \times (\nabla T) = \text{Curl of gradient}$

③ $\nabla \times (\nabla \cdot \vec{A}) = \text{Gauge curl of divergence}$

④ $\nabla \cdot (\nabla \times \vec{A}) = \text{Divergence of curl}$

⑤ $\nabla \times (\nabla \times \vec{A}) = \text{Curl of curl}$

$$⑥ \nabla \cdot (\nabla^2 T) = \nabla^2 \nabla T$$

$$= \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2}$$

Sum of second derivatives is scalar.

$$⑦ \nabla \times (\nabla^2 T) = 0$$

(3)

$$H = \frac{\partial}{\partial x} + \frac{\partial}{\partial y}$$

Since H is a vector field, we can write:

$$H = H^1 \frac{\partial}{\partial x} + H^2 \frac{\partial}{\partial y}$$

$\frac{\partial}{\partial x} = \frac{\partial}{\partial x} + \frac{\partial}{\partial y}$

$\frac{\partial}{\partial y} = \frac{\partial}{\partial x} + \frac{\partial}{\partial y}$

$\frac{\partial}{\partial x} + \frac{\partial}{\partial y} = \left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} \right) + \left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} \right)$

$\frac{\partial}{\partial x} + \frac{\partial}{\partial y} = \frac{\partial}{\partial x} + \frac{\partial}{\partial y} - \frac{\partial}{\partial x} - \frac{\partial}{\partial y}$

$\frac{\partial}{\partial x} + \frac{\partial}{\partial y} = \frac{\cancel{\partial}}{\cancel{\partial}} + \frac{\cancel{\partial}}{\cancel{\partial}} - \frac{\cancel{\partial}}{\cancel{\partial}} - \frac{\cancel{\partial}}{\cancel{\partial}}$

$\frac{\partial}{\partial x} + \frac{\partial}{\partial y} = 0$

5

Δ)

$$\Delta \cdot (D_1 \times D_2) =$$

$$= + \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) - \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) - \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) - \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right)$$
$$= 0$$

$$\Delta \cdot (D_1 \times D_2) =$$
$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$
$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$

$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$
$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$
$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$
$$+ \frac{\partial | \partial}{\partial z} \left(\begin{array}{c} \cancel{\frac{\partial | \partial}{\partial z}} \\ \cancel{\frac{\partial | \partial}{\partial z}} \end{array} \right) =$$

$$\begin{aligned}
 ⑤ \quad \nabla^j \times (\nabla^k \times \vec{F}) &= \nabla^j (\nabla^k \cdot \vec{F}) - \nabla^k (\nabla^j \cdot \vec{F}) \\
 &\equiv ③
 \end{aligned}$$

Link to the recording:

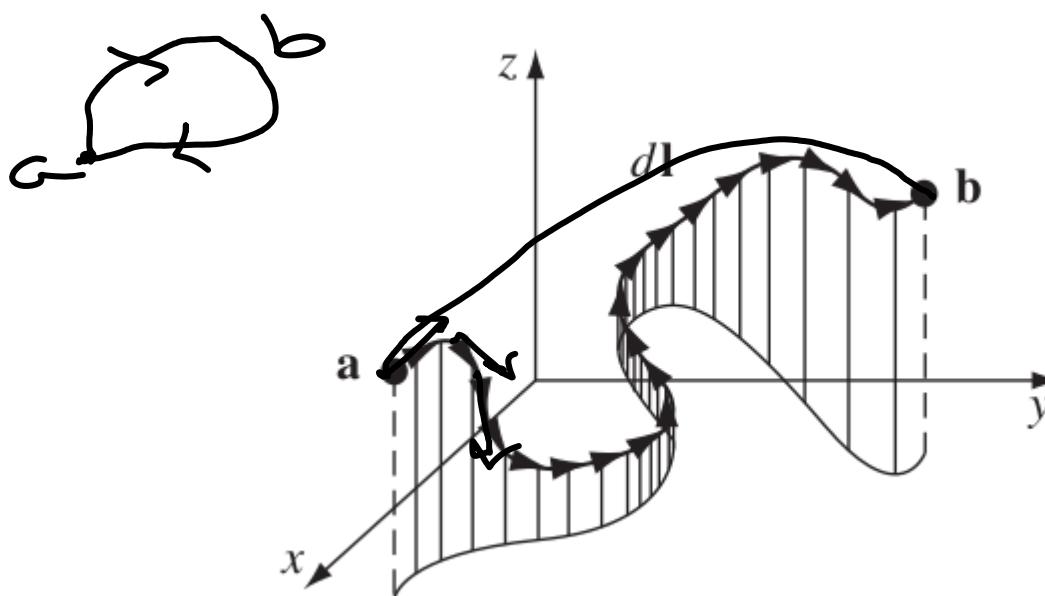
<https://bennettu.sharepoint.com/sites/EPHY105L-Odd2021/Shared%20Documents/Forms/AllItems.aspx?id=%2Fsites%2FPHY105L%2DOdd2021%2FShared%20Documents%2FGeneral%2FRecordings%2FPHY105L%20Theory%20Class%2D20211007%5F133314%2DMeeting%20Recording%2Emp4&parent=%2Fsites%2FPHY105L%2DOdd2021%2FShared%20Documents%2FGeneral%2FRecordings>

I) Integral Calculus

Line Integral

Integrals of form:

$$\int_a^b \mathbf{F} \cdot d\mathbf{l}$$



→ Integration is carried out along the shown path from α to β .

- (*) Closed integral: $\oint \mathbf{F} \cdot d\mathbf{l}$
- (*) One simple example: $W = \int \mathbf{F} \cdot d\mathbf{l} = \int_a^b (\mathbf{F} \cdot \mathbf{dl}) + \int_b^a (\mathbf{F} \cdot \mathbf{dl})$ ($= \text{work done}$)

* Usually the line integral depends on the path taken, but for a class of vectors the integral only depends on the end points.

is \rightarrow A force that has this property is called "conservative force".

for such vectors,

$$\begin{aligned} &= \int_{\gamma^0}^{\gamma^1} (\vec{F} \cdot d\vec{r}) + \int_{\gamma^1}^{\gamma^2} (\vec{F} \cdot d\vec{r}) \\ &= \int_{\gamma^0}^{\gamma^2} (\vec{F} \cdot d\vec{r}) - \int_{\gamma^0}^{\gamma^1} (\vec{F} \cdot d\vec{r}) = 0 \end{aligned}$$

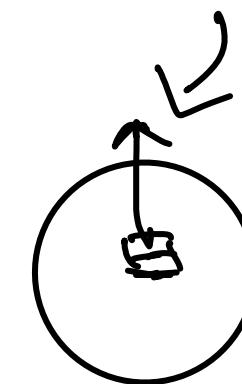
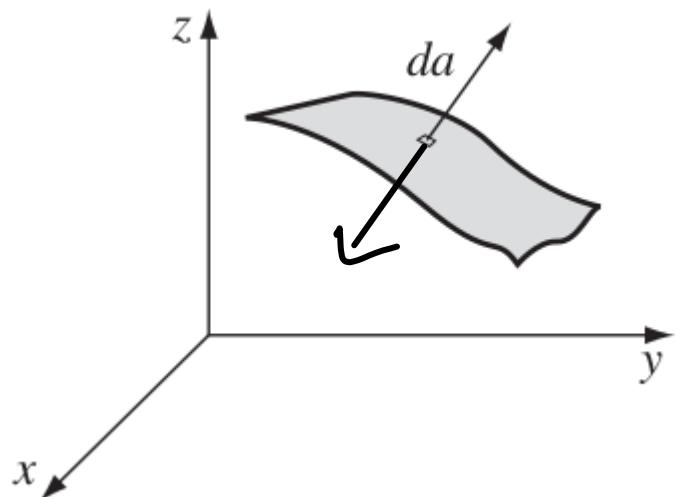
Surface Integral

1) Integral is of form:

$$\int \int_{\Sigma} = f \cdot d\sigma$$

Closed surface = $\int \int_{\Sigma} f \cdot d\sigma$

$d\sigma$ = infinitesimal
surface area
element



→ integral is taken over
a specified surface area.

② There are two directions perpendicular
to any surface.

→ if surface is closed $d\sigma$ is
always outward.

$\text{Flux}:$ (4) describes flow of a fluid.

Then $\int \vec{q} \cdot \vec{n} ds = \int q^x dx$ \Rightarrow total mass passes through unit surface.

$$\Rightarrow \frac{\text{Flux}}{\text{Volume}}.$$

Volume integral

Integral is of the form:

$dV = \text{infinitesimal volume}$

$dV = \text{element}$

$dV = \text{any scalar.}$

Cartesian coordinates system

Def.
 if $\vec{A} = \text{Density}$ of some substance,
 $\int \vec{A} d\vec{r} = \text{Total mass}.$

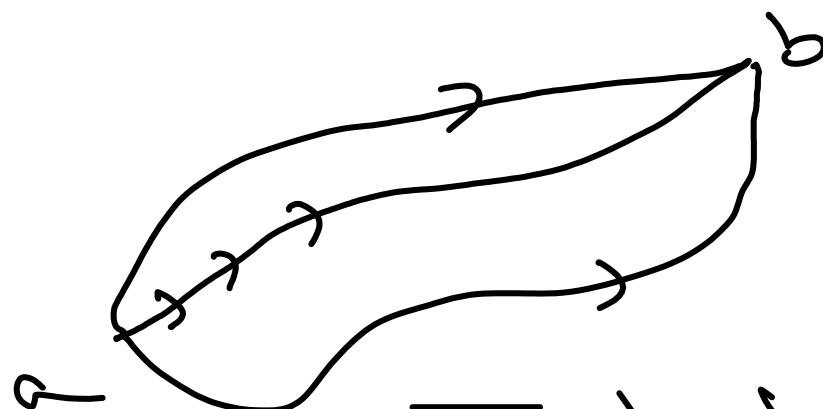
Fundamental theorem for gradients

Let us consider a line integral.

Here the vector, $\vec{A} = (\nabla \phi)$.

Then

$$\int_C \vec{A} \cdot d\vec{r} = \int_C (\nabla \phi) \cdot d\vec{r}$$



→ many taken from infinitesimal steps

Total charge is,

$$\int_a^b (\nabla \phi) \cdot d\vec{r} = \phi_b - \phi_a$$

(independent path)

Corollary

(1) $\oint_C (\nabla \phi) \cdot d\vec{r} = 0$ if ϕ is independent of path

(2) $\oint_C (\nabla \phi) \cdot d\vec{r} = 0$

Link to the recording:

<https://bennettu.sharepoint.com/sites/EPHY105L-Odd2021/Shared%20Documents/Forms/AllItems.aspx?id=%2Fsites%2FEPHY105L%2DOdd2021%2FShared%20Documents%2FGeneral%2FRecordings%2FEPHY105L%20theory%20Class%2D20211011%5F154532%2DMeeting%20Recording%2Emp4&parent=%2Fsites%2FEPHY105L%2DOdd2021%2FShared%20Documents%2FGeneral%2FRecordings>

Fundamental Theorem states that the integral of a derivative over a region is equal to the value of the function at the boundary.

④ Fundamental theorem of gradient

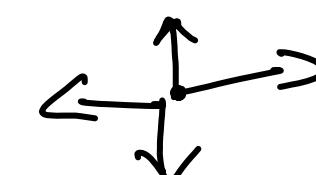
$$\nabla \int_a^b (\nabla T) \cdot d\vec{r} = T(b) - T(a)$$

$$\nabla \cdot \oint (\nabla T) \cdot d\vec{r} = 0$$

④ Fundamental theorem of Divergence

Statement : $\int_V (\nabla \cdot \vec{v}) dV = \oint_S \vec{v} \cdot d\vec{A}$

≡ Gauss' theorem / Divergence theorem.

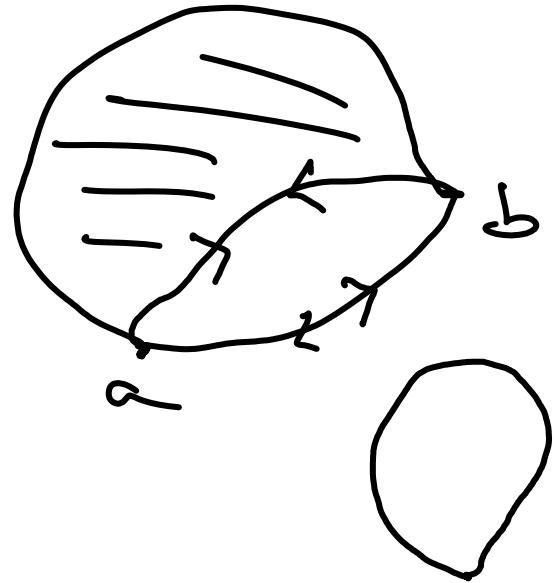
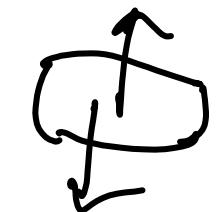
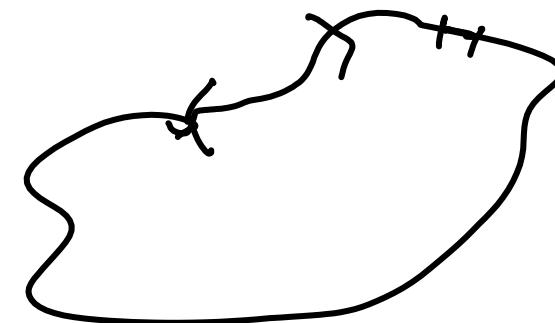


(*) Fundamental theorem for curv's

Statement:

$$\int_S (\vec{A} \times \vec{B}) \cdot d\vec{a} = \oint_C \vec{B} \cdot d\vec{r}$$

\Rightarrow Stoke's theorem.



\rightarrow The given consistency of Stoke's Theorem with the right-hand rule.

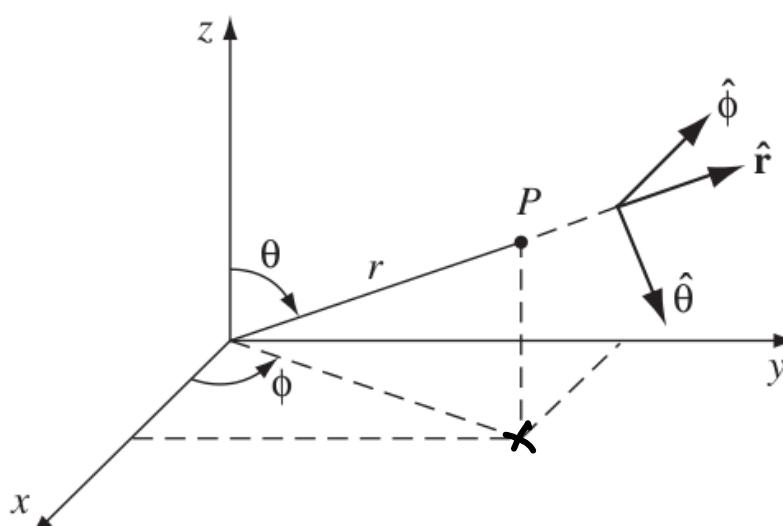
(*) Stoke's theorem states that $\int_S (\vec{A} \times \vec{B}) \cdot d\vec{a}$ is equal to the line integral $\oint_C \vec{B} \cdot d\vec{r}$ around the boundary.

Corollary: $\oint_S (\nabla \times \vec{A}) \cdot d\vec{A}$ depends only on the boundary line, but on the particular surface chosen.

* $\oint_S (\nabla \times \vec{A}) \cdot d\vec{A} = 0$ for any closed surface since since shrinking a single point boundary integral vanishes.

Cylindrical Coordinates

* Spherical-Polar coordinates



Three coordinates =

$$(r, \theta, \phi)$$

$r \rightarrow$ Distance from origin

$\theta \rightarrow$ Polar angle \equiv angle measured from x_1 -axis.

$\phi \rightarrow$ Azimuthal angle \equiv angle around from x_1 -axis.

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

(*) Unit vectors $\hat{i}_1, \hat{o}, \hat{\phi}$ constitute a
orthogonal basis just like x_1, x_2, x_3

Any vector can be written as
 $\vec{A} = A_r \hat{i}_1 + A_\theta \hat{o} + A_\phi \hat{\phi}$
radial polar azimuthal

The unit vectors:

$$\hat{r} = \sin\theta \cos\phi \hat{i} + \sin\theta \sin\phi \hat{j} + \cos\theta \hat{k}$$

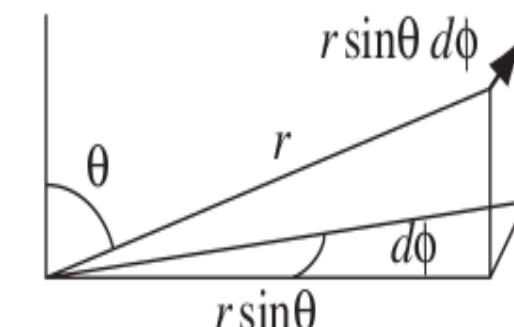
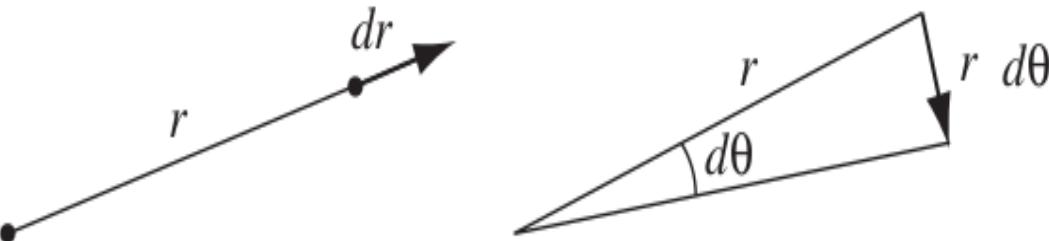
$$\hat{\theta} = \cos\theta \cos\phi \hat{i} + \cos\theta \sin\phi \hat{j} - \sin\theta \hat{k}$$
$$\hat{\phi} = -\sin\phi \hat{i} + \cos\phi \hat{j}$$

Let:

$$\hat{r} = \sin\theta \cos\phi \hat{i} + \sin\theta \sin\phi \hat{j} + \cos\theta \hat{k}$$

$$d\hat{r} = \frac{\partial \hat{r}}{\partial r} dr, \quad \hat{\theta} = \frac{\partial \hat{r}}{\partial \theta}, \quad \hat{\phi} = \frac{\partial \hat{r}}{\partial \phi}$$

④) Finite displacement along \hat{r} , $\hat{\theta}$, $\hat{\phi}$



$$\partial_{\theta} r_1 = r_2$$

$$\partial_{\theta} r_0 = r_0$$

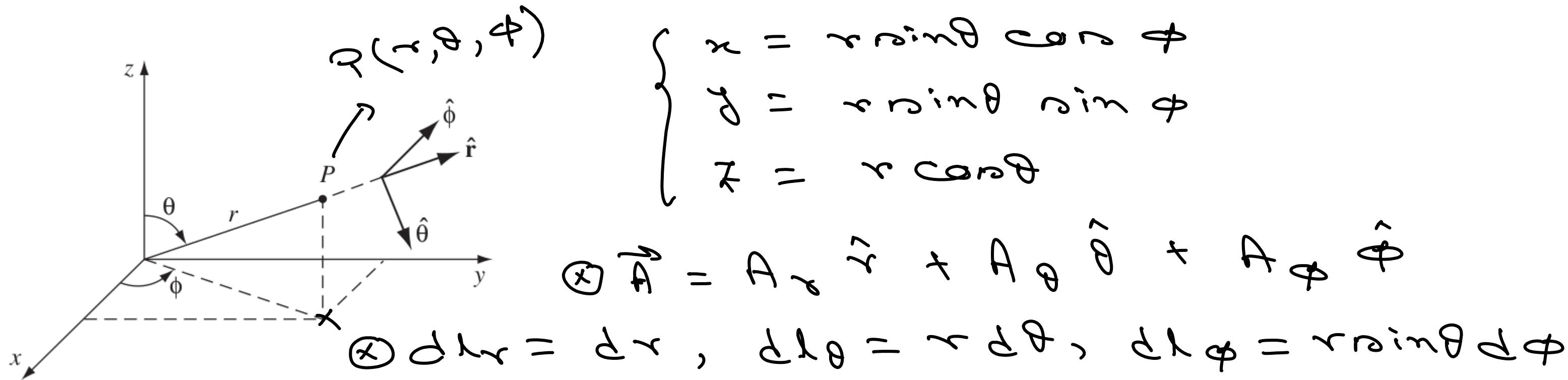
$$\partial_{\theta} \phi = \sin \theta \partial \phi$$

$$\downarrow \quad \text{From initial place } \{b\}$$
$$\partial_{\theta} r_0 = r_2 \hat{x} + r_0 \hat{y} + \sin \theta \hat{\phi}$$

$$\begin{aligned} \partial_{\theta} &= \partial_{\theta} r_0 \partial_{\theta} \phi \\ &= h^2 \sin \theta \partial_{\theta} \phi \end{aligned}$$

$$= h^2 \sin \theta \partial_{\theta} \phi$$

Spherical Polar Coordinates



→ \rightarrow infinitesimal displacement:

$$d\vec{r} = dr \hat{r} + r d\theta \hat{\theta} + r \sin\theta d\phi \hat{\phi}$$

→ \rightarrow infinitesimal volume:

$$dV = dr \, d\theta \, d\phi \, d\phi'$$

$$V = \iiint dV = \int_0^R \int_0^\pi \int_0^{2\pi} r^2 \sin\theta \, dr \, d\theta \, d\phi =$$

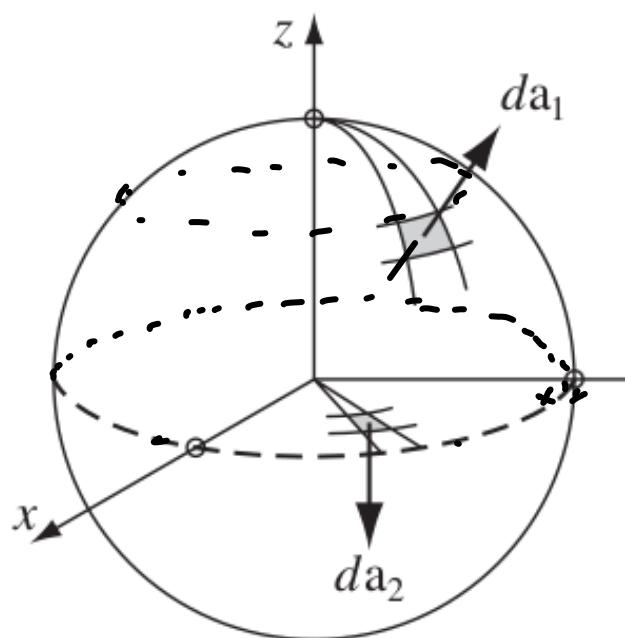
$$\frac{4}{3} \pi R^3$$

Limits

$$\begin{array}{ll} r = \text{Ranging from} & 0 \quad 0 \quad t \quad s \\ \theta = \text{Ranging from} & 0 \quad t \quad \theta \quad \pi \\ \phi = \text{Ranging from} & 0 \quad t \quad 2\pi \end{array}$$

→ Infinitesimal surface

→ Depends on geometry.



⊕ A surface element on the outer surface:

$$dA_s = \frac{r^2}{\rho} d\Omega \quad \text{if } \rho = \text{const.}$$

$$= r^2 \sin\theta d\theta d\phi$$

⊕ Surface lies on the xy plane.

$$\rightarrow \theta = \text{const.}$$

$$dA_s = r dr d\theta = r dr d\phi$$

④ Now, we can write vector derivatives:

$$\begin{aligned}\vec{\nabla} T &= \frac{\partial T}{\partial r} \hat{r} + \frac{\partial T}{\partial \theta} \hat{\theta} + \frac{\partial T}{\partial \phi} \hat{\phi} \\ \frac{\partial T}{\partial r} &= \frac{\partial T}{\partial r} \left(\frac{\partial r}{\partial x} \right) + \frac{\partial T}{\partial \theta} \left(\frac{\partial r}{\partial y} \right) \\ &\quad + \frac{\partial T}{\partial \phi} \left(\frac{\partial r}{\partial z} \right) \\ \vdots &\quad \vdots \\ \vdots &\quad \vdots\end{aligned}$$

Gradient:

$$\underline{\nabla} T = \frac{\partial T}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial T}{\partial \phi} \hat{\phi}. \quad (1.70)$$

Divergence:

$$\nabla \cdot \mathbf{v} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 v_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta v_\theta) + \frac{1}{r \sin \theta} \frac{\partial v_\phi}{\partial \phi}. \quad (1.71)$$

Curl:

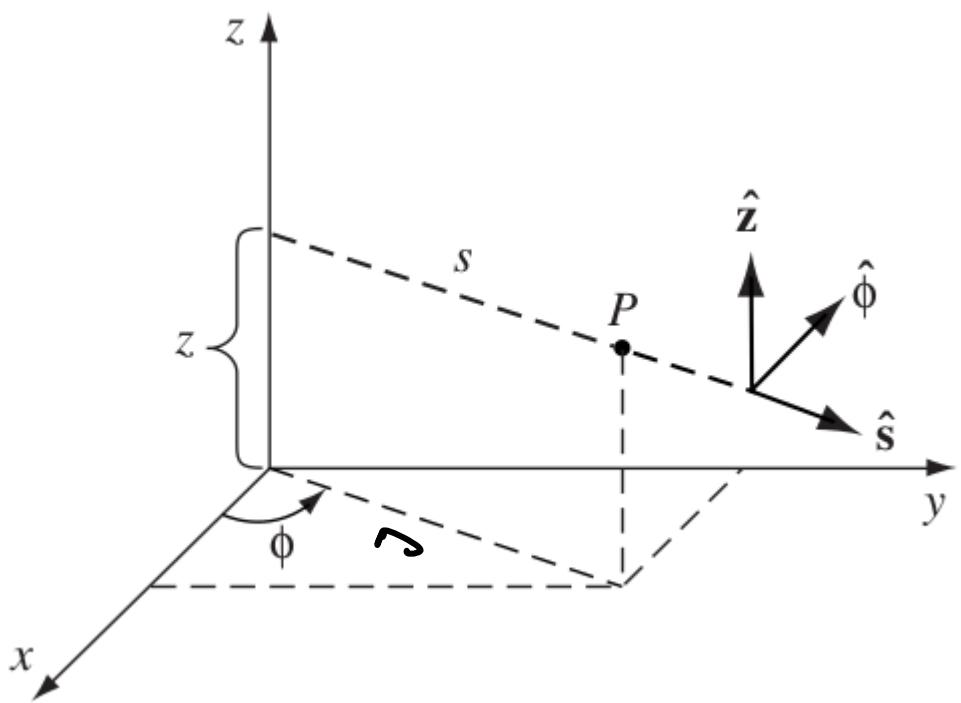
$$\begin{aligned}\nabla \times \mathbf{v} &= \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial \theta} (\sin \theta v_\phi) - \frac{\partial v_\theta}{\partial \phi} \right] \hat{r} + \frac{1}{r} \left[\frac{1}{\sin \theta} \frac{\partial v_r}{\partial \phi} - \frac{\partial}{\partial r} (r v_\phi) \right] \hat{\theta} \\ &\quad + \frac{1}{r} \left[\frac{\partial}{\partial r} (r v_\theta) - \frac{\partial v_r}{\partial \theta} \right] \hat{\phi}.\end{aligned} \quad (1.72)$$

Laplacian:

$$\nabla^2 T = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2}. \quad (1.73)$$

Cylindrical Coordinates

$$P = P(r, \theta, z)$$



θ = Same as spherical
 r = Same as Cartesian
 z = Distance from π -axis.

$$\left. \begin{aligned} x &= r \cos \theta \\ y &= r \sin \theta \\ z &= z \end{aligned} \right\}$$

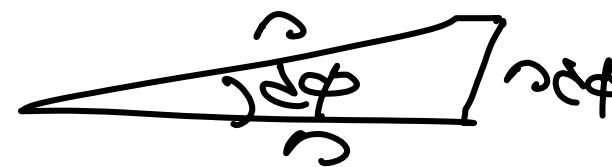
$$\left. \begin{aligned} r &= \sqrt{x^2 + y^2} \\ \theta &= \tan^{-1} \frac{y}{x} \\ z &= z \end{aligned} \right\}$$

(+) If infinitesimal displacement:

$$dr =$$

$$dr_\theta = \partial r / \partial \theta$$

$$, dr_z = dz$$



$$\Rightarrow \vec{dr} = r_s \hat{s} + r_\phi \hat{\phi} + r_\pi \hat{z}$$

(*) Volume element, $dV = r_s dr_\phi dr_\pi$

Ranges:

- $r =$ Ranging from 0 to ∞
- $\phi =$ Ranging from 0 to 2π
- $\pi =$ Ranging from $-\infty$ to $+\infty$

Gradient:

$$\nabla T = \frac{\partial T}{\partial s} \hat{s} + \frac{1}{s} \frac{\partial T}{\partial \phi} \hat{\phi} + \frac{\partial T}{\partial z} \hat{z}. \quad (1.79)$$

Divergence:

$$\nabla \cdot \mathbf{v} = \frac{1}{s} \frac{\partial}{\partial s} (s v_s) + \frac{1}{s} \frac{\partial v_\phi}{\partial \phi} + \frac{\partial v_z}{\partial z}. \quad (1.80)$$

Curl:

$$\nabla \times \mathbf{v} = \left(\frac{1}{s} \frac{\partial v_z}{\partial \phi} - \frac{\partial v_\phi}{\partial z} \right) \hat{s} + \left(\frac{\partial v_s}{\partial z} - \frac{\partial v_z}{\partial s} \right) \hat{\phi} + \frac{1}{s} \left[\frac{\partial}{\partial s} (s v_\phi) - \frac{\partial v_s}{\partial \phi} \right] \hat{z}. \quad (1.81)$$

Laplacian:

$$\nabla^2 T = \frac{1}{s} \frac{\partial}{\partial s} \left(s \frac{\partial T}{\partial s} \right) + \frac{1}{s^2} \frac{\partial^2 T}{\partial \phi^2} + \frac{\partial^2 T}{\partial z^2}. \quad (1.82)$$

Volume integral

Volume integral:

$$\int \int \int V dV$$

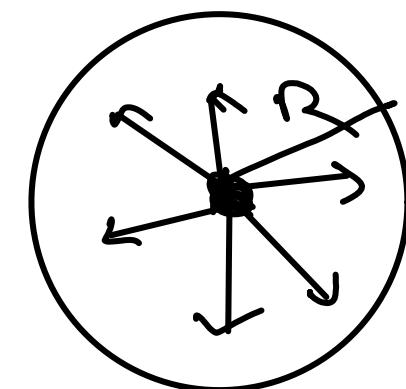
Fundamental / π :

$$\int \int (\rho \cdot \phi) dV = \int \int \rho \cdot \phi$$

$$\int \rho \cdot \phi = \int \rho$$

$$\int \rho = \int r^2 = \int_0^r \int_0^\pi \int_0^{2\pi}$$

$$r^2 \sin\theta \cdot r^2 \sin\theta \cdot r^2 \phi = r^5 \sin\theta \sin\theta \phi = r^5 \sin^2\theta \phi$$



Line integral

$$\int (P dx + Q dy) = \int_{x_1}^{x_2} P(x, y) dx + \int_{y_1}^{y_2} Q(x, y) dy$$

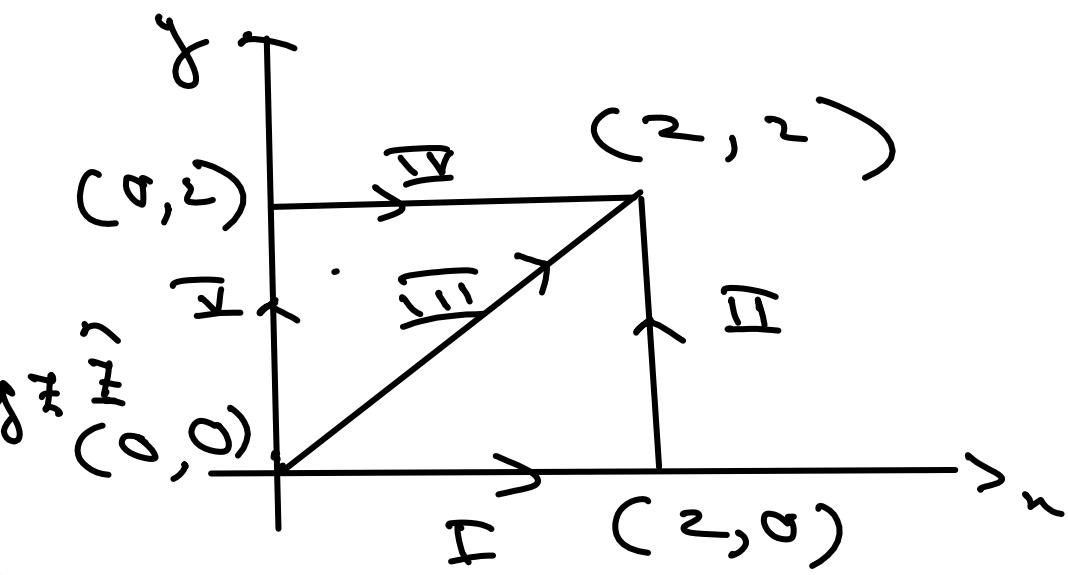
$$\text{along } \Gamma: \quad \int_{x_1}^{x_2} P(x, y) dx + \int_{y_1}^{y_2} Q(x, y) dy = \int_{x_1}^{x_2} x^2 dx + \int_{y_1}^{y_2} y^2 dy = \int_{x_1}^{x_2} x^2 dx + \int_{y_1}^{y_2} y^2 dy$$

$$\text{along } \Gamma: \quad \int_{x_1}^{x_2} x^2 dx = x^3 \Big|_{x_1}^{x_2} = x_2^3 - x_1^3$$

$$\text{along } \Gamma: \quad \int_{y_1}^{y_2} y^2 dy = y^3 \Big|_{y_1}^{y_2} = y_2^3 - y_1^3 = \frac{x^3}{3} - \frac{y^3}{3} = \frac{x^3 - y^3}{3}$$

$$\text{along } \Gamma: \quad \int_{x_1}^{x_2} x^2 dx = x^3 \Big|_{x_1}^{x_2} = x_2^3 - x_1^3$$

$$\text{along } \Gamma: \quad \int_{y_1}^{y_2} y^2 dy = y^3 \Big|_{y_1}^{y_2} = y_2^3 - y_1^3 = \frac{x^3 - y^3}{3}$$



$$\text{---} + \text{---} = \frac{24}{3} = 8$$

$$\text{III} \quad \frac{\partial f}{\partial x} = \frac{\partial f}{\partial x} + \frac{\partial f}{\partial y}$$

$$x^4 - 2x^3 = \underline{x^4 - 2x^3 + x^2 - x}$$

$$\int_0^1 (x^2 dx + x^3 dx) = \left[\frac{x^3}{3} \right]_0^1 + \left[\frac{x^4}{4} \right]_0^1$$

$$= \frac{8}{3} + \frac{16}{4}$$

$$= \frac{8}{3} + 5$$

$$\frac{2}{3} = \underline{\underline{8}}$$

$$\frac{d^2x}{dy^2}$$

— July —

~~+ x 3~~

$$y = x$$

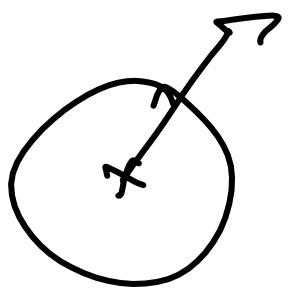
$$y = y$$

$$j = m + \frac{1}{2}$$

$$= \frac{y_2 - y_1}{x_2 - x_1} \cdot x$$

— x

Surface integral



On the surface of a sphere,

$$d\mathbf{q} = d\theta \, d\phi \, r^2$$

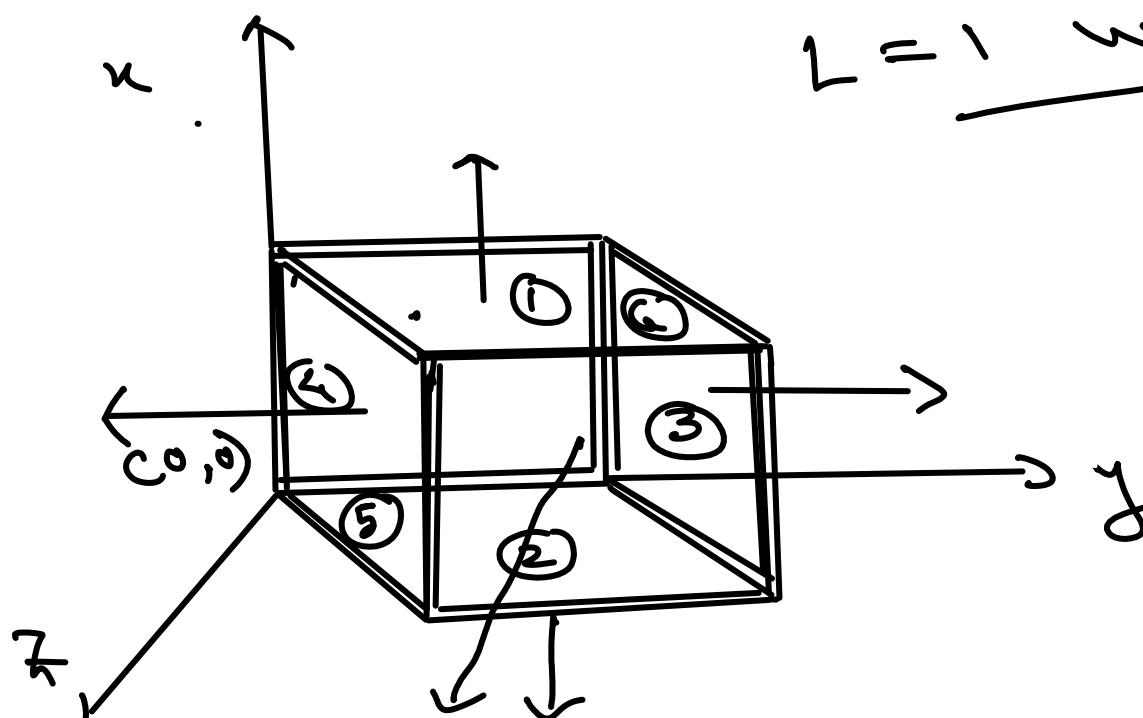
using $d\mathbf{q}$

$$\mathbf{F} \cdot d\mathbf{q} = \mathbf{F} \cdot d\mathbf{q}$$



$$\int d\mathbf{q} \cdot \mathbf{F} =$$

$$\int d\mathbf{q} \cdot \mathbf{F} = r^2 \sin \theta \, d\theta \, d\phi$$



$$r = \text{unit}$$

$$\mathbf{F} = x^1 \hat{x} + x^2 \hat{y} + x^3 \hat{z}$$

$$d\mathbf{q}_1 \cdot d\mathbf{q}_2 =$$

$$dx_1 dx_2$$

$$dx_1 dx_2$$

$$dx_1 dx_2$$

$$dx_1 dx_2$$

$$(x^1 = 0)$$

$$(x^2 = 0)$$

$$(x^3 = 0)$$

$$(x^1 = 0)$$

$$(x^2 = 0)$$

$$\begin{aligned} \text{curl } F &= \text{curl } (\nabla \times A) \\ F &= \nabla \times A \end{aligned}$$

$$\begin{aligned} \text{curl } F &= \int_A \partial_x \partial_y \partial_z F = 0 \\ \text{curl } F &= \int_A \partial_x \partial_y \partial_z (\nabla \times A) = \int_A \partial_x \partial_y \partial_z (\partial_x A_1 + \partial_y A_2 + \partial_z A_3) \\ &= \int_A \partial_x^2 A_1 + \partial_y^2 A_1 + \partial_z^2 A_1 \\ &= \int_A \partial_x^2 A_1 = 0 \end{aligned}$$

$$\begin{aligned} \text{curl } F &= \int_A \partial_x \partial_y \partial_z F = 0 \\ \text{curl } F &= \int_A \partial_x \partial_y \partial_z (\nabla \times A) = \int_A \partial_x \partial_y \partial_z (\partial_x A_1 + \partial_y A_2 + \partial_z A_3) \\ &= \int_A \partial_x \partial_y \partial_z \partial_x A_1 + \int_A \partial_x \partial_y \partial_z \partial_y A_1 + \int_A \partial_x \partial_y \partial_z \partial_z A_1 \\ &= \int_A \partial_x^2 A_1 + \int_A \partial_y^2 A_1 + \int_A \partial_z^2 A_1 \\ &= \int_A \partial_x^2 A_1 = 0 \end{aligned}$$

$$\begin{aligned}
 \left\{ \begin{array}{l} \mathcal{D}_1 = x^2 y^5 + x y^2 z^5 \\ \mathcal{D}_2 = \left(\frac{\partial}{\partial x} \right)^2 + \left(\frac{\partial}{\partial y} \right)^2 + \left(\frac{\partial}{\partial z} \right)^2 \\ \mathcal{D}_3 = \frac{\partial}{\partial x} (x^2) + \frac{\partial}{\partial y} (y^2) + \frac{\partial}{\partial z} (z^2) \end{array} \right. \\
 \begin{aligned}
 \mathcal{D}_1 &= \left(\frac{\partial}{\partial x} \right)^2 + \left(\frac{\partial}{\partial y} \right)^2 + \left(\frac{\partial}{\partial z} \right)^2 \cdot (x^2 y^5 + x y^2 z^5) \\
 &= 2x + 2y^2 + z^2
 \end{aligned}
 \end{aligned}$$

The Electric field

Electric charge is quantized. Charge of any system can be written as $Q = ne$ carried by one electron.

n = A multiple, "almost always" an integer (exception: quarks)

Electrostatics = Study of electric charges which are stationary.

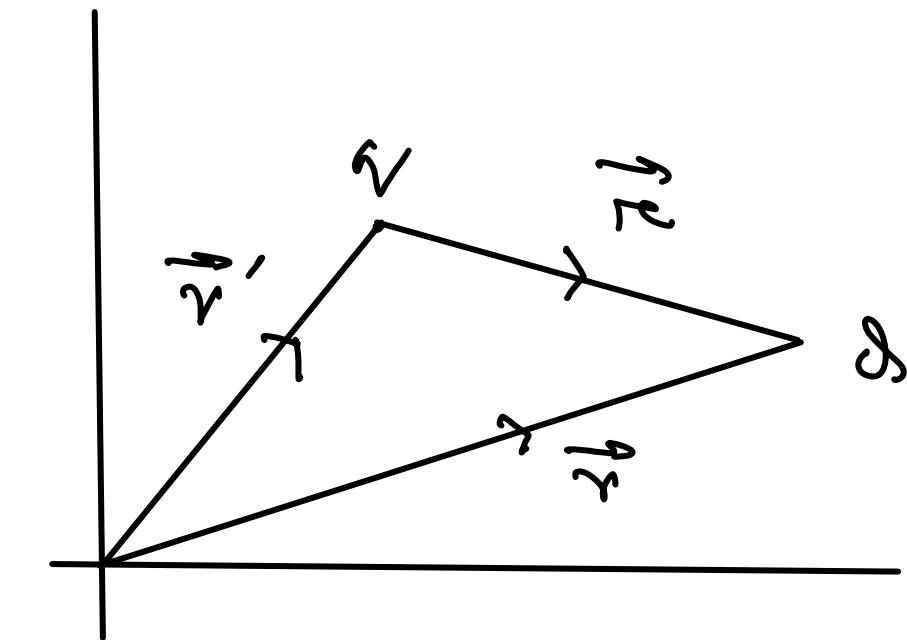
Coulomb's law

Force on a test Q due to a single

Point charge q at rest and distance r , try to say:

$$F_y = \frac{q\pi \epsilon_0}{r^2} - \frac{q\delta}{r^2} r_1$$

ϵ_0 = Permittivity
unit, $\epsilon_0 = 8.85 \times 10^{-12} \text{ C}^2 \text{ N}^{-1} \text{ J}^{-1}$



Electric Field

Using, we have several such point charges r_1, r_2, \dots, r_n at distances r_1, r_2, \dots, r_n from origin on \mathcal{S} :

$$\begin{aligned}
 \vec{E}_1 &= -\nabla V_1 + \left(\frac{q}{4\pi\epsilon_0} \frac{\partial}{\partial r} \left(\frac{q_1}{r_1^2} \vec{r}_1 + \frac{q_2}{r_2^2} \vec{r}_2 + \dots + \frac{q_n}{r_n^2} \vec{r}_n \right) \right) \\
 &= \frac{q}{4\pi\epsilon_0} \frac{\partial}{\partial r} \left(\frac{q_1}{r_1^2} \vec{r}_1 + \frac{q_2}{r_2^2} \vec{r}_2 + \dots + \frac{q_n}{r_n^2} \vec{r}_n \right)
 \end{aligned}$$

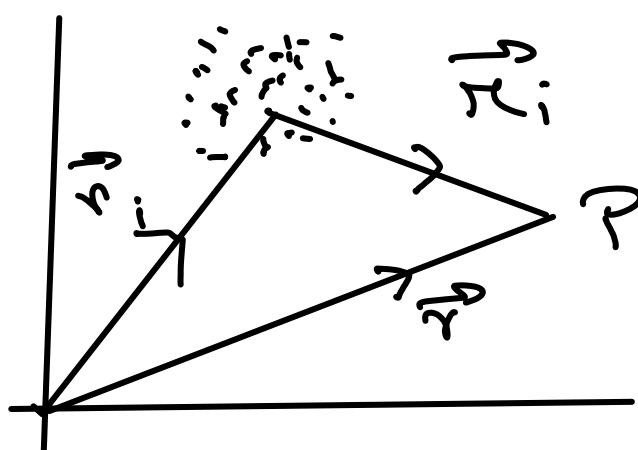
$$\vec{E}_1 = q \frac{\partial V}{\partial r}$$

\rightarrow electric field

Here,

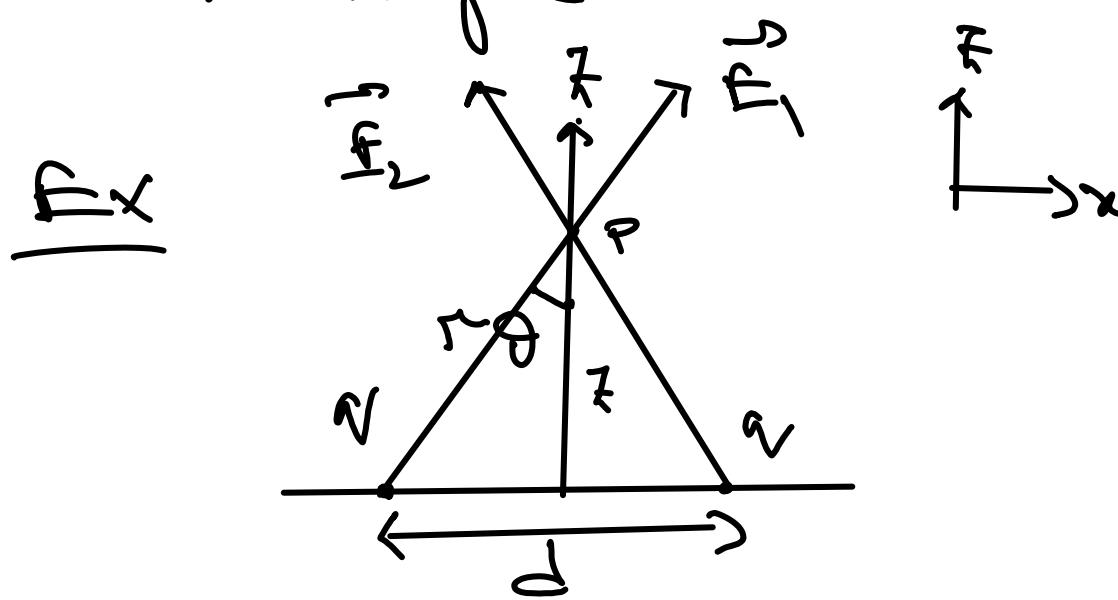
$$\vec{E}_1(r) = \frac{1}{4\pi\epsilon_0} \sum_i \frac{q_i}{r_i^2} \vec{r}_i$$

\rightarrow Electric field due to source charges.



Physically, $\vec{F}(2)$ is force per unit charge.

Charge.



$$\vec{F} = \vec{E}_x + \vec{E}_r$$

(i) x-components cancel
and z-components add up.

$$F_x = 2 \frac{1}{4\pi\epsilon_0} \frac{q^2}{r^2} \cos\theta$$

$$r = \left[\pi^2 + \left(\frac{d}{2} \right)^2 \right]^{1/2}$$

$$\cos\theta = \frac{\pi}{r}$$

$$F_y = \frac{1}{4\pi\epsilon_0} \frac{2\pi\pi}{\left[\pi^2 + \left(\frac{d}{2} \right)^2 \right]^{3/2}} \text{ N/C}$$

E_{ext} away from charge, $\vec{r} \gg r$

$$E = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2}$$

Continuous Charge distribution

$$E(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho}{r^2} d\tau$$

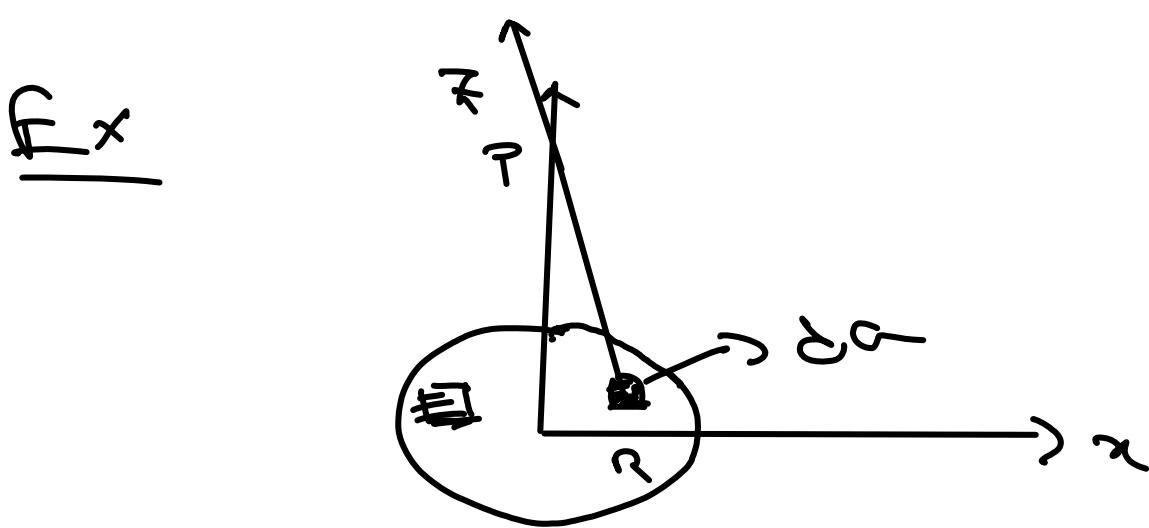
- Charge spread over a line

$d\tau = \lambda d\tau'$
small line element of source
charge per unit length

- Charge spread over a surface

$d\sigma = q d\sigma'$ infinitesimal surface
charge per unit surface

- (*) Charge ρ need over a volume
 $\rho_v = \rho$
 ↳ Given infinitesimal vol.
 ↳ Charge density.



$F_x = \frac{q}{\epsilon_0} \left(\frac{1}{\pi r^2} - \frac{1}{\sqrt{r^2 + z^2}} \right) z$

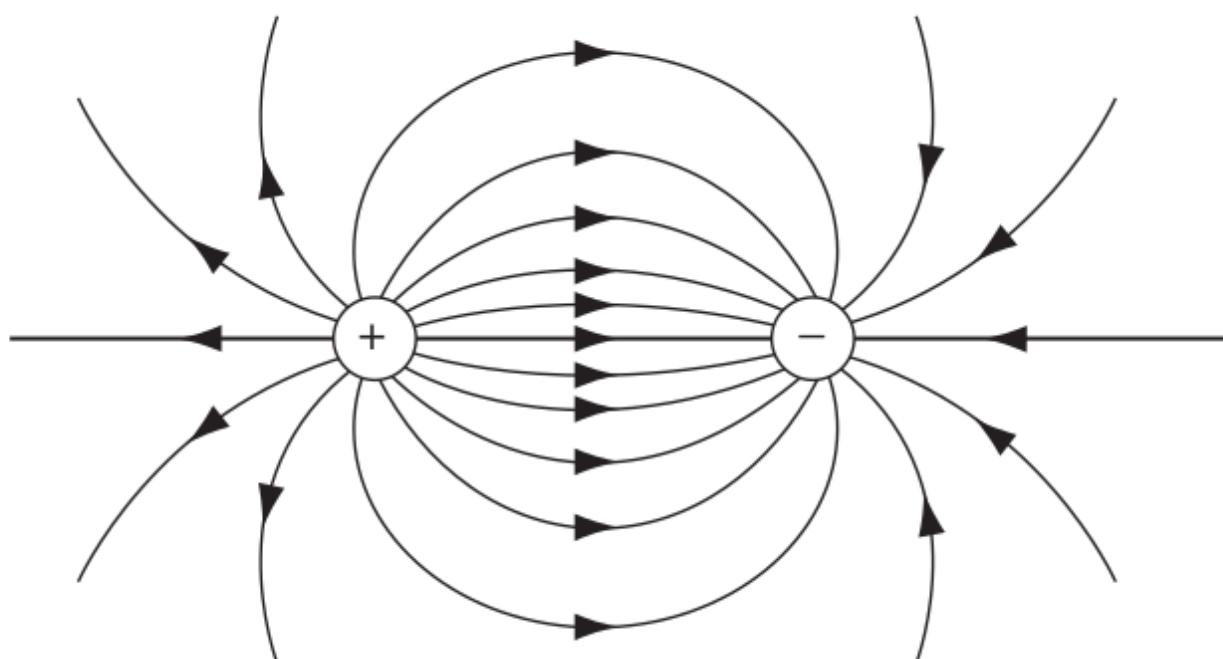
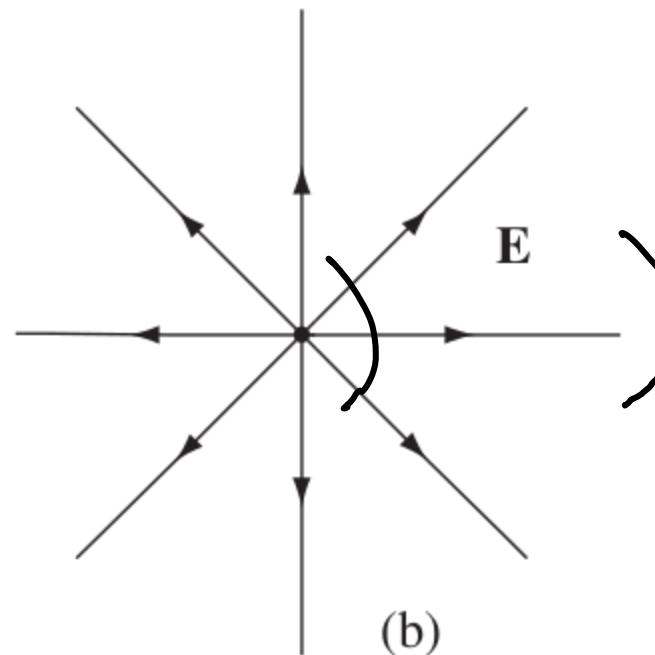
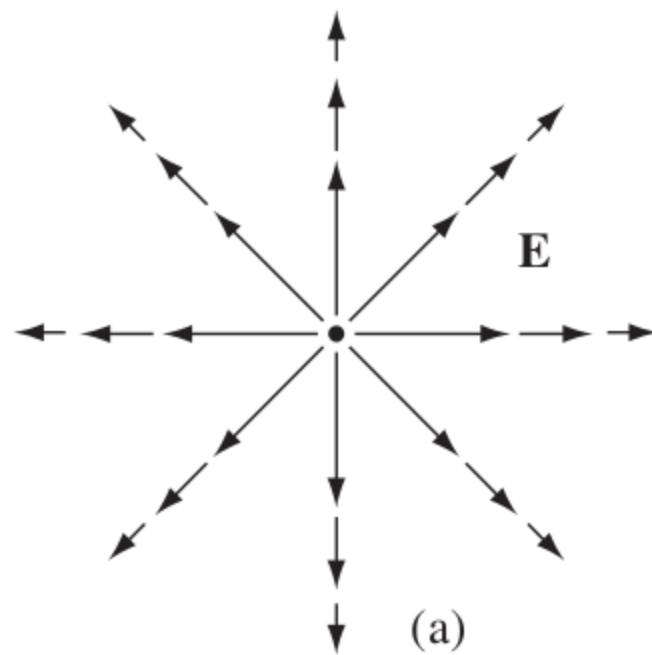
$$= \frac{q}{2\pi\epsilon_0} \int_0^R \int_0^{2\pi} \int_0^z \frac{r^2 dr dz d\theta}{(r^2 + z^2)^{3/2}}$$

$$= \frac{q}{2\pi\epsilon_0} \int_0^R \int_0^{2\pi} \frac{(2\pi r^2 dr) q}{(r^2 + z^2)^{3/2}}$$

$$= \frac{q}{2\pi\epsilon_0} \int_0^R \frac{2\pi r^2 dr}{(r^2 + z^2)^{1/2}}$$

- (*) Uniform surface charge dist. (σ)
- $dP = r dr d\theta$
- $= 2\pi r dr$

Divergence of Electric Field

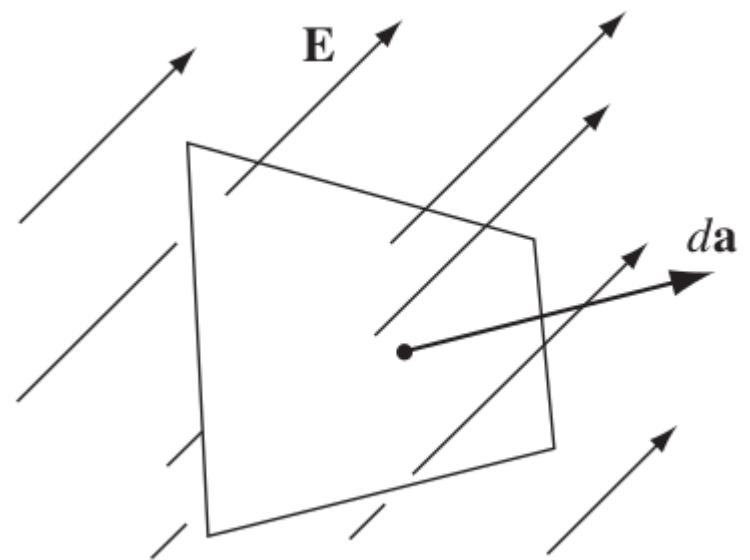


$$\vec{E}(r) = \frac{1}{4\pi\epsilon_0} \frac{k}{r^2} \hat{r}$$

→ The field strength falls as r increases

→ Field lines originate at positive charge and terminate at negative charge.

$\frac{\text{flux}}{\text{area}}$ or \vec{E}



Flux through a surface

$$\Phi_E = \int_S \vec{E} \cdot d\vec{a}$$

\int_S measures the "number
of field lines" crossing
through S .

↓ Flux through any closed surface
enclosing the charge is a measure
of the electric charge.

⇒ Essence of Gauss' law

* A charge outside does not contribute
since the field lines simply pass through
the surface.

(+) A point charge q sits at the origin.

enclosed by a spherical surface.

$$\oint \mathbf{E} \cdot d\mathbf{l} = \frac{1}{\epsilon_0} \int_{\text{inside}} q \quad (\text{L}) \text{ is } (\delta^2 \sin \theta) d\theta$$

$$= \frac{1}{\epsilon_0} \int_0^{2\pi} \int_0^\pi r^2 \sin \theta dr d\theta \quad \Rightarrow \text{independent}$$

$$= \frac{1}{\epsilon_0} r^2 \int_0^{2\pi} \int_0^\pi \sin \theta d\theta d\phi \quad \Rightarrow \text{independent}$$

→ The number of field lines crossing the surface does not depend on the radius of the sphere.

→ The surface can be of any shape.

(*) Flux through charge = $\frac{q}{\epsilon_0}$ by surface enclosing

→ If we have a collection of charges,

$$\vec{E} = \sum_{i=1}^n \vec{P}_i$$

Flux through a surface enclosing

charge of $\vec{E} \cdot \vec{dA}$ = $\sum_{i=1}^n \oint \vec{E}_i \cdot \vec{dA}_i$

$$= \frac{q}{\epsilon_0}$$

(*) Far away closed surface

(*)

if $\oint \vec{E} \cdot d\vec{l} = 0$ then \vec{E} is zero.

System = ρ volume charge density of the system.

$\rho_{\text{enc.}} = \frac{1}{V} \int \rho dV$

Σe

$$\vec{E} \cdot d\vec{l} = q_e$$

$$\oint \vec{E} \cdot d\vec{l} = \frac{q_e}{\epsilon_0} \quad \text{done.}$$

net electric field

Quantitative statement of \vec{E}

Gauss' law.

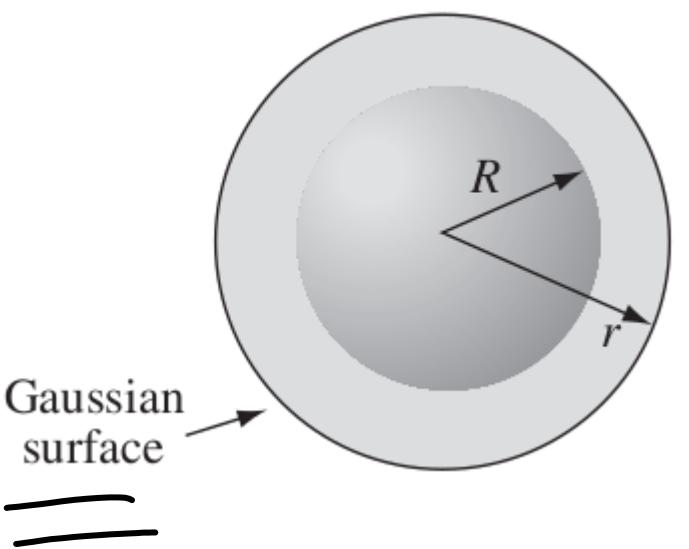
$\oint \vec{E} \cdot d\vec{l} = \frac{q_{\text{enc.}}}{\epsilon_0}$ charge enclosed

Hence,

$$\Rightarrow \vec{E} \cdot d\vec{l} = \frac{\epsilon_0}{\epsilon_0} \Rightarrow \text{Gauss' law differential form.}$$

④ When symmetry permits, this is a very simple way to calculate E .

Ex:



$$\text{Gauss law} \cdot d\vec{l} =$$

Electric field outside uniformly charged solid sphere of radius and total charge $= r$.

$\rightarrow \vec{E}$ points radially outward, so does

$d\vec{q}$

$$u(\vec{r}, t) = u(\vec{r})$$

The magnitude of $d\vec{q}$ is const. over the Gaussian surface.

Hence,

$$u(\vec{E}/d) = \vec{E}/d$$

$$= \vec{E}/(4\pi r^2)$$

$$\Rightarrow \vec{E} = \frac{\vec{E}}{4\pi r^2} = \frac{\vec{E}}{4\pi r_0^2}$$

$$\Rightarrow E = \frac{1}{4\pi \epsilon_0 r^2}$$

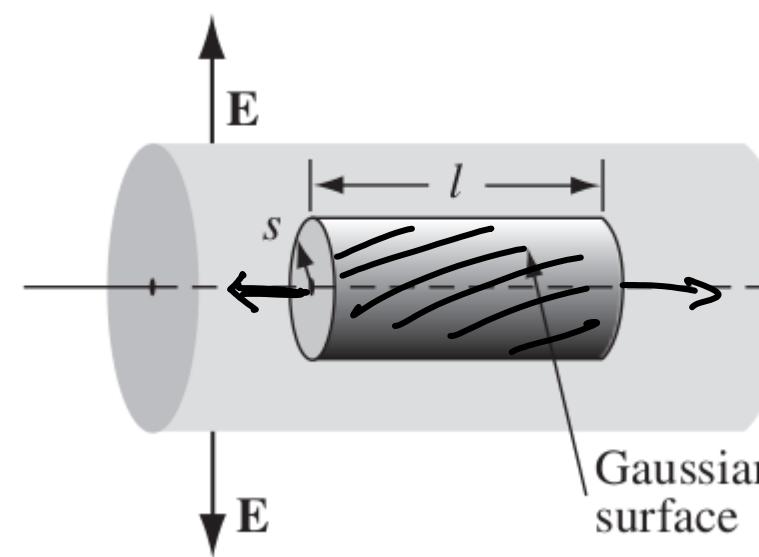
(*) Gauss' law is always true, but not always useful

→ lens has to be uniform
→ Gaussian surface has to
be symmetric.

- (+) Different kind of symmetry:
① Spherical
② Cylindrical
③ Planar

Examples of application of Gauss's law (contd.)

④ Cylindrical symmetry:



→ Long cylinder carrying charge density, $\rho = kr$.
 $E_{\text{inside}} = ?$

$$\oint \mathbf{E} \cdot d\mathbf{l} = \frac{\text{Q enc.}}{\epsilon_0}$$

The enclosed charge:

$$\begin{aligned} Q_{\text{enc.}} &= \int_S \rho dV = \int_0^l \int_0^{2\pi} \int_0^r (kr) (r' dr' d\theta' dz') \\ &= 2\pi k l \int_0^r r'^2 dr' \\ &= \frac{2}{3} \pi k l r^3 \end{aligned}$$

Looking at the symmetry:

$$\int \vec{E} \cdot d\vec{a} = \vec{E} \cdot \int d\vec{a} = \vec{E} / 2\pi r$$

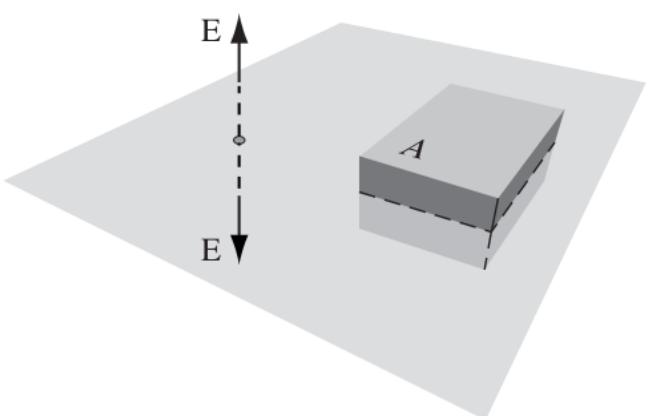
(*) The two ends contribute nothing since

$$\vec{E} \perp d\vec{a}$$

Hence,

$$\vec{E} / 2\pi r = \frac{1}{\epsilon_0} \frac{\rho}{3} \pi k t r^3$$
$$\Rightarrow \vec{E} = \frac{1}{3\epsilon_0} \kappa r^2 \hat{z}$$

(*) Infinite plane carrying uniform charge density ρ .



→ Gaussian pillbox

$$\oint \vec{E} \cdot d\vec{a} = \frac{\text{Dens.}}{\epsilon_0}$$

$$\text{Dens.} = \rho A$$

area of enclosed surface
(equal to the area of the lid)

\vec{m}_E points outward.
 From top and bottom surfaces,
 $\Rightarrow \vec{m}_E = N_A \vec{r}_E$
 $\Rightarrow N_A \vec{r}_E = \frac{q}{2\epsilon_0} \hat{n}$
 $\Rightarrow \vec{m}_E = \frac{q}{2\epsilon_0} \hat{n}$ unit vector pointing
outward from
surface.

Case of \vec{m}_E

Take a point charge at origin

$$\vec{m}_E = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r}$$

Calculate line integral from point 'a' to 'b'

\vec{E} in spherical coordinates: $\vec{E} = E_r \hat{r}_r + E_\theta \hat{r}_\theta + E_\phi \hat{r}_\phi$
 Polar coordinates: r, θ, ϕ

$$\Rightarrow \vec{E} \cdot \hat{r}_r = \frac{1}{4\pi\epsilon_0} \frac{r^2}{r^2} \vec{r}_r$$

Then

$$\vec{E} \cdot \hat{r}_r = \frac{1}{4\pi\epsilon_0} \left(\frac{r^2}{r_s} - \frac{r^2}{r_o} \right)$$

Plane part, $r = r$

$$\Rightarrow \vec{E} \cdot \hat{r}_r = C r^5$$

Apply Stoke's theorem: $\oint_C (\vec{A} \times \vec{E}) \cdot d\vec{l} = \oint_M \vec{E} \cdot d\vec{r}$

$\nabla \cdot (\nabla \times \vec{E}) = 0 \equiv$ True for only
electrostatics.

Electric Potential

∂_t : The time integral is independent of

Defining it is:

Electric potential $\nabla V(r)$ = - $\int_0^t \vec{E}(r) \cdot d\vec{r}$

(+) Potential difference

$$\nabla V(r_b) - \nabla V(r_a) = - \int_{r_a}^{r_b} \vec{E}(r) \cdot d\vec{r} = - \vec{E}_y \cdot (r_b - r_a)$$

dependence
point

$$\begin{aligned}
 & \text{Let } V(\vec{r}) - V(\vec{r}') = -\int_{\vec{r}'}^{\vec{r}} \vec{E} \cdot d\vec{r} \\
 & \Rightarrow V(\vec{r}) - V(\vec{r}') = -\int_{\vec{r}'}^{\vec{r}} (\nabla V) \cdot d\vec{r} = -\nabla V \cdot (\vec{r} - \vec{r}') \\
 & \quad \text{From the above equation, we can say that gradient} \\
 & \quad \text{arbitrary two points } \vec{r}' \text{ and } \vec{r}, \\
 & \Rightarrow V(\vec{r}) = -\nabla V
 \end{aligned}$$

✎ Changing the reference point can change
 $V(\vec{r}) = -\int_{\vec{r}'}^{\vec{r}} \vec{E} \cdot d\vec{r} = -\int_{\vec{r}_0}^{\vec{r}} \vec{E} \cdot d\vec{r} - \int_{\vec{r}_0}^{\vec{r}'} \vec{E} \cdot d\vec{r} = V + V(\vec{r}_0)$

$k = \text{const.}$ independent of r .

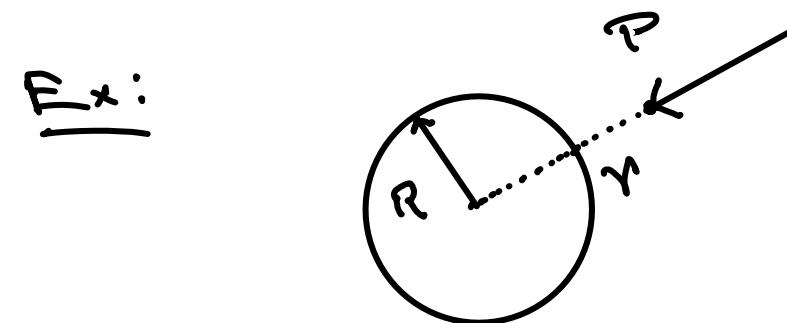
(*) Potential diff. being a physical quantity
should be independent of reference point.

$$V(b) - V(a) = V(b) - V(a)$$

(*) Obey's superposition law. $V_{\text{tot}} = V_1 + V_2 + \dots$
Correction due to charges,

$$V = V_1 + V_2 + \dots$$

(*) Unit : $\frac{\text{Coul}}{\text{m}^2}$ Coul N^{-1}A^2

Electric potential

Find potential inside and outside a σ spherical shell carrying a uniform charge density

$Q = \text{Total charge}$

→ Reference point (O) $\equiv \infty$

From Gauss' law, field outside,

$$\oint \mathbf{E} \cdot d\mathbf{l} = \frac{Q_{\text{enc}}}{4\pi\epsilon_0 r^2}$$

Field inside the sphere, $\oint \mathbf{E} \cdot d\mathbf{l} = 0$

→ For point outside the sphere ($r > R$)

$$V(r) = - \oint \mathbf{E} \cdot d\mathbf{l} = - \frac{1}{4\pi\epsilon_0} \int_{r_1}^{r_2} \frac{Q}{r^2} dr$$

$$= - \frac{1}{4\pi\epsilon_0} \frac{Q}{r_2}$$

For point inside the sphere ($r \leq R$)

$$\nabla \phi = -\sigma \hat{r}$$

$$= -\frac{4\pi \sigma}{3} r^2 \hat{r}$$

is non-zero although the electric field is zero.

(*) Points on & Laplace's eqn.

$$\nabla \cdot \vec{E} = \rho$$
$$= \frac{4\pi \rho}{3} r^2$$

Now do they go back into?

$$\Rightarrow \nabla^2 V = -\frac{1}{\epsilon_0} \rho$$

$$\Rightarrow \nabla^2 V = -\frac{1}{\epsilon_0} \rho \equiv \text{Poisson's eq.}$$

From there if $\nabla^2 V = 0$ charge distribution,
 $\nabla^2 V = 0 \equiv \text{Laplace's eq.}$

$$\times \nabla^2 \times \rho = \nabla^2 \times (-\nabla^2 V) = 0$$

Potential up to charge distribution

$$\rho = \frac{1}{4\pi\epsilon_0} \frac{\partial V}{\partial r}$$

$$V = V_0 + r_0 \theta + r_0 \sin \theta$$

$$\rho = \frac{1}{4\pi\epsilon_0} r_0^2 \theta$$

Setting the reference point at ∞ , the potential due to a point charge q at origin

$$\begin{aligned} V(r) &= - \int_{\infty}^r \frac{1}{4\pi\epsilon_0} \frac{q}{r'^2} dr' \\ &= \frac{1}{4\pi\epsilon_0} \frac{q}{r} \end{aligned}$$

r = distance between r and r' , then,

$$V(r) = \frac{1}{4\pi\epsilon_0} \frac{q}{r}$$

From superposition principle,

$$V(r) = \sum_{i=1}^n \frac{q_i}{4\pi\epsilon_0 r_i}$$

(for a collection of charges)

[Superposition: if there is
 a collection of charges: $\vec{E} = \vec{E}_1 + \vec{E}_2 + \dots + \vec{E}_n$
 \vec{v}^x

↓ If it's a continuous charge
 distribution,

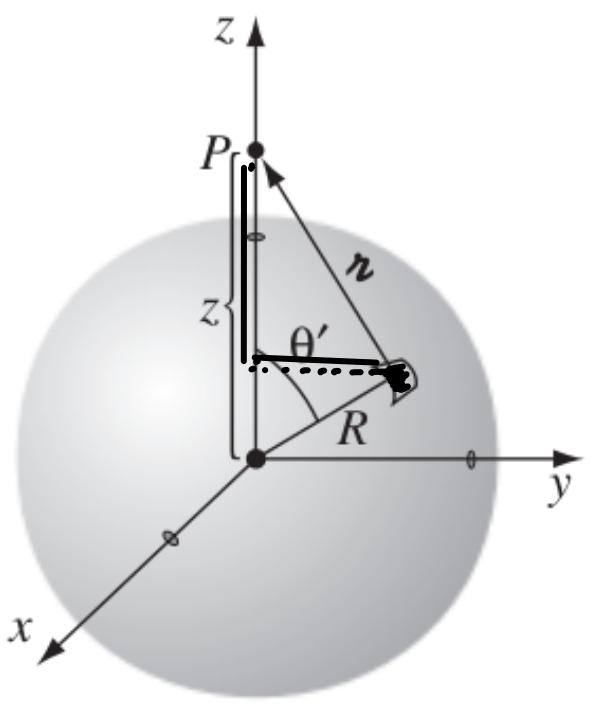
$$\vec{v}(z) = \int_{-\infty}^{\infty} \rho(z') dz'$$

⊕ Volume charge distribution: $\rho_v = \rho d\tau'$

⊕ Surface: $\sigma_s = q d\sigma'$

⊕ Line: $\sigma_l = q d\sigma'$

|Ex: Potential of a uniformly charged spherical shell with radius R .



$$V(\vec{r}) = \frac{1}{2\pi\sigma} \int \frac{q}{r'} d\omega'$$

$$r^2 = R^2 + r'^2 - 2Rr \cos\theta'$$

(Cosine law)

$$\begin{aligned} r^2 &= (R \sin\theta')^2 + (r - R \cos\theta')^2 \\ &= R^2 (\sin^2\theta' + \cos^2\theta') + r^2 - 2Rr \cos\theta' \\ &= R^2 + r^2 - 2Rr \cos\theta' \end{aligned}$$

On the surface of a sphere, element of surface area $dA = R^2 \sin\theta' d\theta' d\phi$

$$\Rightarrow 1\pi F_0 V(\vec{r}) = q \int_0^{2\pi} \frac{\int_{-\pi}^{\pi} R^2 \sin\theta' \cdot d\theta' d\phi}{\underbrace{[R^2 + r^2 - 2Rr \cos\theta']^{1/2}}_{\sim}}$$

$$R^2 + x^2 - 2Rx \cos\theta' = r$$

$$2.Rx \sin\theta' dx = dr$$

$$\Rightarrow \frac{1}{2} \pi \epsilon_0 \nu(x) = 2\pi R^2 q \left(\frac{1}{R} \left[R^2 + x^2 - 2Rx \cos\theta' \right]^{\frac{1}{2}} \right)$$

$$= \frac{R^2 q}{\pi} \left[\sqrt{(R+x)^2} - \sqrt{(R-x)^2} \right]$$

$$\Rightarrow \nu(x) = \frac{Rq}{2\epsilon_0 \pi} \left((R+x) - (x-R) \right)$$

For point outside, $(x > R)$, $\nu(x) = \frac{Rq}{\epsilon_0 \pi}$

For points inside, $x < R$

$$L(x) = \frac{2|P|q}{\pi x} \left[(R_+ x) - (R_- x) \right]$$

$$z = \frac{\pi n^2 q}{c}$$

for terms $\frac{q}{r}$ and z

$$L(r) = \frac{1}{\pi r_0} \frac{R}{r} \quad (r > R)$$

$$= \frac{1}{\pi r_0} \frac{R^2}{r} \quad (r \leq R)$$

Work done to move a charge

We have a stationary configuration of charges. We want to move a test charge 'q' from point 'r' to 's'.

Electric force on test charge q:

$$\vec{F} = q\vec{E}$$

→ The force we have to exert in opposition to this force = $-q\vec{E}$

$$\text{Work done, } W = \int_C q\vec{F} \cdot d\vec{r}$$

$$= -q \int_C \vec{E} \cdot d\vec{r}$$

$$= q (\psi(s) - \psi(r))$$

→ independent of the path taken.

\Rightarrow Electrostatic force is "conservative".

$$\Sigma = \delta [V(x) - V(\infty)] = \delta V(x)$$

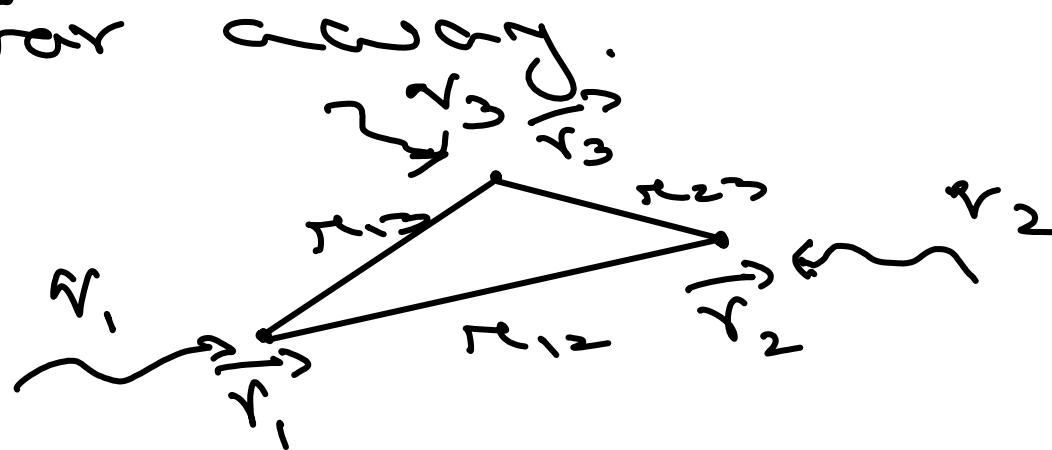
reference point = ∞

\rightarrow Potential difference betw. two points

$$V(b) - V(a) = \frac{k}{|b-a|}$$

Energy of a point charge distribution

\rightarrow To calculate how much work it takes to assemble a collection of point charges by one bringing the charges one by one from



\rightarrow For q , we have to do no work since there is no electric field beforehand.
 $\Rightarrow \Sigma = 0$

$$\rightarrow \text{in order to bring in } q_2, \quad \zeta_2 = \frac{1}{4\pi\epsilon_0} \frac{q_2}{r_{12}}$$

\rightarrow similarly, to bring in q_3 ,

$$\zeta_3 = \frac{1}{4\pi\epsilon_0} \frac{q_3}{r_{13}} + \frac{1}{4\pi\epsilon_0} \frac{q_3}{r_{23}}$$

$$\rightarrow \zeta_4 = \frac{1}{4\pi\epsilon_0} \frac{q_4}{r_{14}} + \frac{1}{4\pi\epsilon_0} \frac{q_4}{r_{24}} + \frac{1}{4\pi\epsilon_0} \frac{q_4}{r_{34}}$$

The total work done to complete the charge configuration:

$$\zeta = \frac{1}{4\pi\epsilon_0} \left(\frac{q_1 q_2}{r_{12}} + \frac{q_1 q_3}{r_{13}} + \frac{q_1 q_4}{r_{14}} + \frac{q_2 q_3}{r_{23}} + \frac{q_2 q_4}{r_{24}} + \frac{q_3 q_4}{r_{34}} \right)$$

$$\text{In general, for } n \text{ charges:}$$

$$\psi = \frac{1}{4\pi\epsilon_0} \sum_{i=1}^n \sum_{j>i} \frac{q_i q_j}{r_{ij}}$$

$$V_R = \frac{1}{8\pi\epsilon_0} \sum_{i=1}^n \sum_{j \neq i} \frac{q_i q_j}{r_{ij}}$$

$$\Rightarrow V = \frac{1}{n!} \sum_{i=1}^n q_i \left(\sum_{j \neq i} \frac{1}{4\pi\epsilon_0} \frac{q_j}{r_{ij}} \right)$$

\hookrightarrow Potential at point i
due to all other charges.

Hence,

$$V = \frac{1}{n!} \sum_{i=1}^n q_i V_i$$

\Rightarrow Represents the energy stored in

The system has potential energy.

Conductors

A perfect conductor contains unlimited number of free charges.

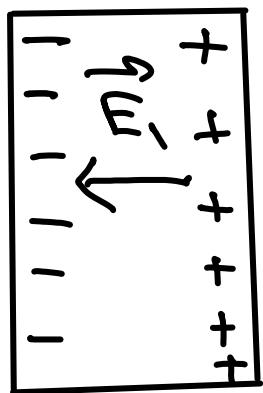
⊗ Basic electrostatic property:

→ $E = 0$ inside any conductor.

A conductor is put in an external electric field. The induced charges produce an electric field E , inside the conductor such that

E is oriented opposite to the direction of E_0 .

The continuous flow tends to cancel E_0 . The charges flow inside until an equilibrium



is reached when \vec{E}_i , inside the conductor, cancels \vec{E}_0 exactly.

Inside, $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$

$$\nabla \cdot \vec{E} = \rho \Rightarrow \rho = 0$$

→ Inside the conductor, charge density is zero → equal number of positive and negative charges.

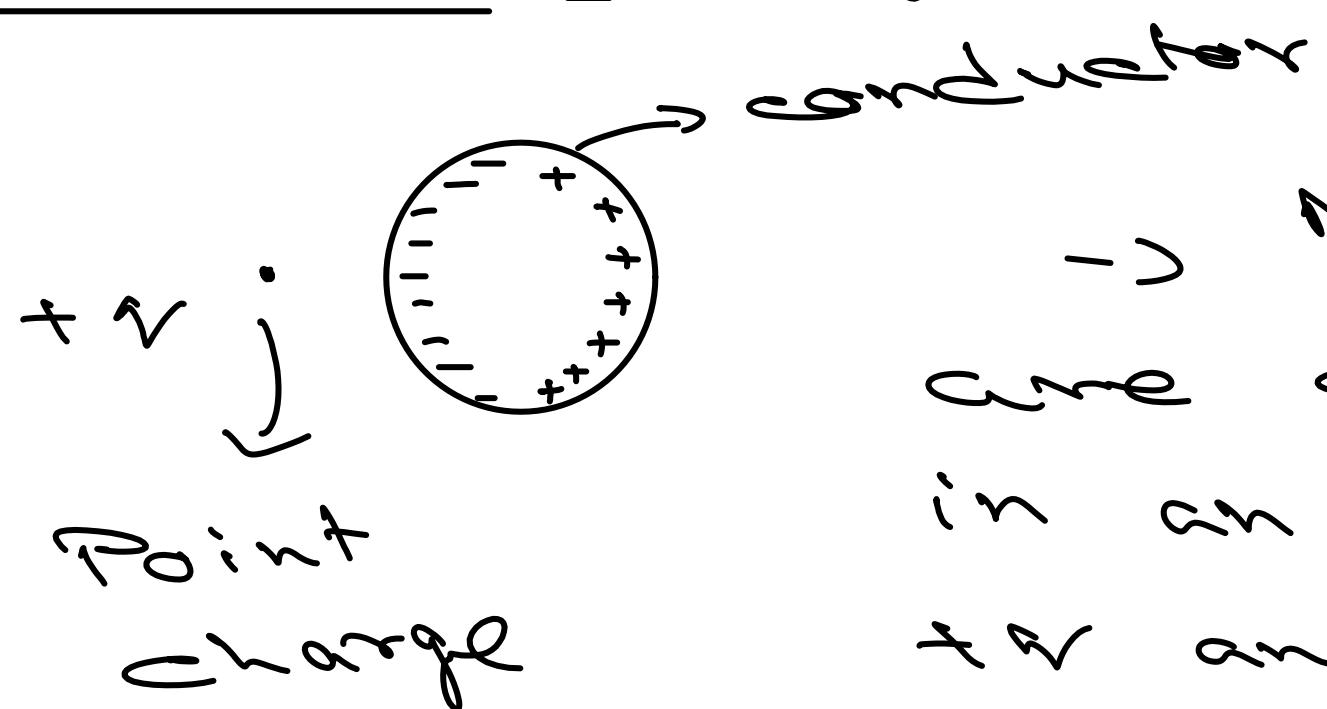
(*) Any net charge can only reside on the surface.

For conductors are equipotential. Consider two points on the surface of the conductor, $V(b) - V(a) = - \int_a^b \vec{E} \cdot d\vec{r} = 0$

$$\Rightarrow V(b) = V(a)$$

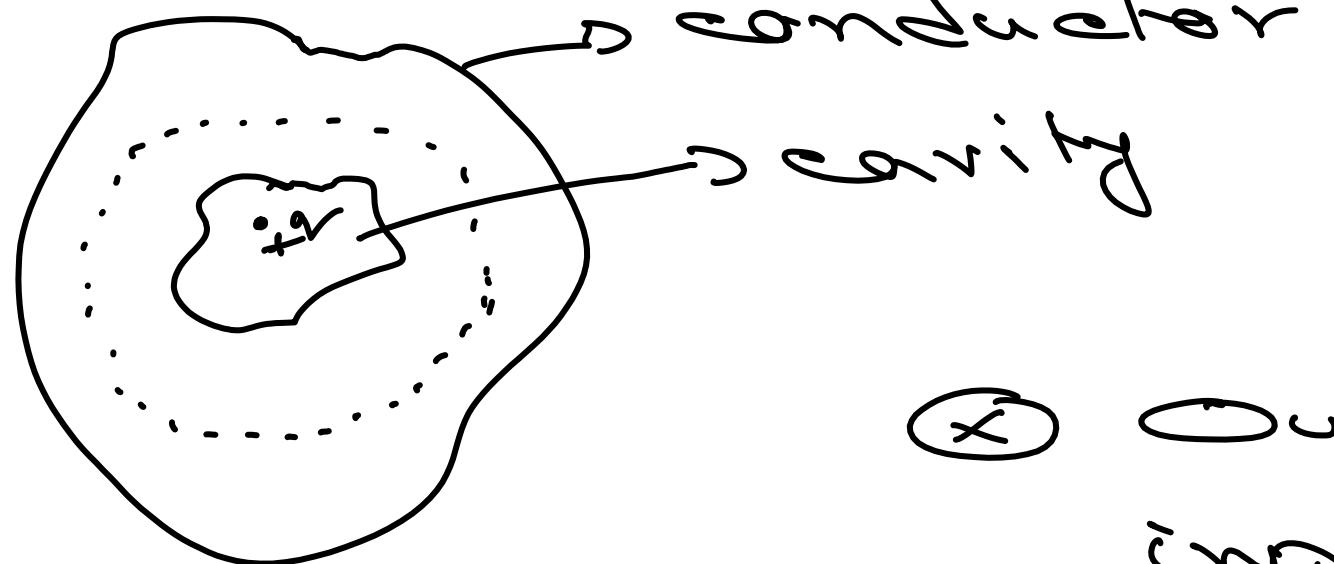
- (x) The electric field E is perpendicular to the surface.
- (x) The electro static energy is at its min. when the charge is spread over the surface.

Induced Charges



\rightarrow Negative induced charges are closer to $+q$ resulting in an attractive force betw $+q$ and the conductor.

- (x) $+q$ charge inside the cavity of a conductor

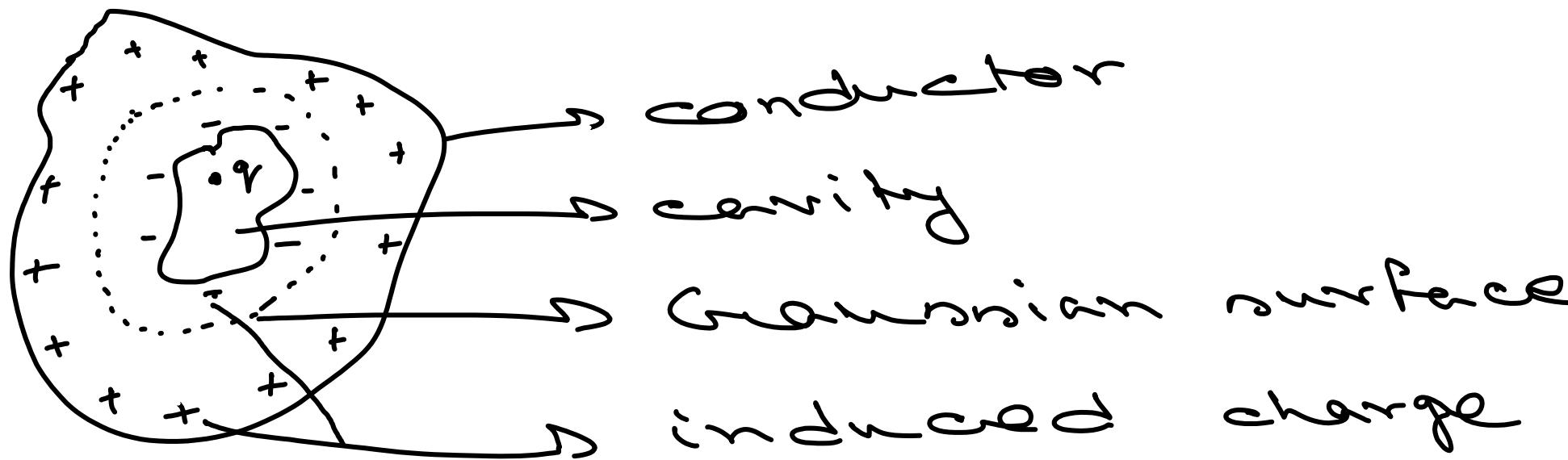


(x) Inside the cavity
 $E \neq 0$

(x) Outside the cavity, but
inside the conductor
 $E = 0$

(x) Outside the conductor,
 $E \neq 0$

Cavity inside a conductor



→ The total charge induced on the cavity wall is equal and opposite to the charge inside.

For the Gaussian surface,

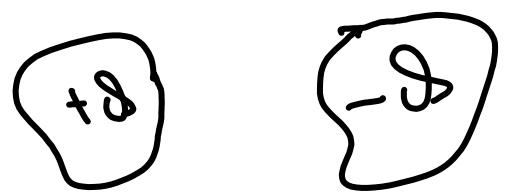
$$\oint \vec{E} \cdot d\vec{l} = 0 \Rightarrow \text{net enclosed charge} = 0$$

$$\Rightarrow V_{\text{induced}} = -q$$

- Field outside the conductor

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r}$$

Capacitor



→ Two conductors charged +δ and -δ with

The potential difference,

$$V = V_+ - V_- = - \int \vec{E} \cdot d\vec{r}$$

$$V \propto \delta$$

$$V = \frac{1}{4\pi\epsilon_0} \int r_2^{10} r_1^{12}$$

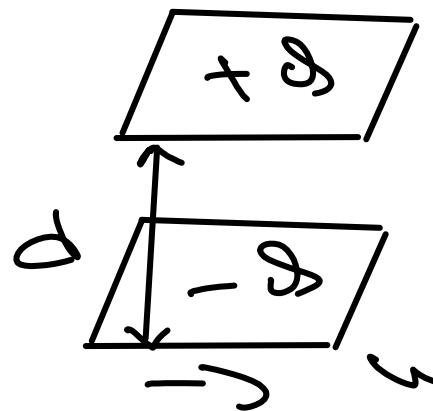
→ Increase δ ⇒ V increases

(x) V is also proportional to d .
 → The proportionality constant is called the capacitance.

$$C = \frac{Q}{V}$$

Determined by the sizes, shapes and separation betw. two conductors

Ex: Parallel plate capacitor



$A \rightarrow$ Area of the plates

$\sigma \rightarrow$ Charge density (surface)

Upper plate has charge $+q$ and lower

one has $-q$

$$E_f = \frac{\sigma}{\epsilon_0 A} \Rightarrow V = \frac{\sigma}{\epsilon_0 A} d$$

betw. the plates

$$\Rightarrow C = \frac{A\epsilon_0}{d}$$

(*) Work done to charge up a capacitor

To do:

→ At some point the charge on the plate = +q

$$\Rightarrow \text{Potential Diff.} = \frac{q}{C}$$

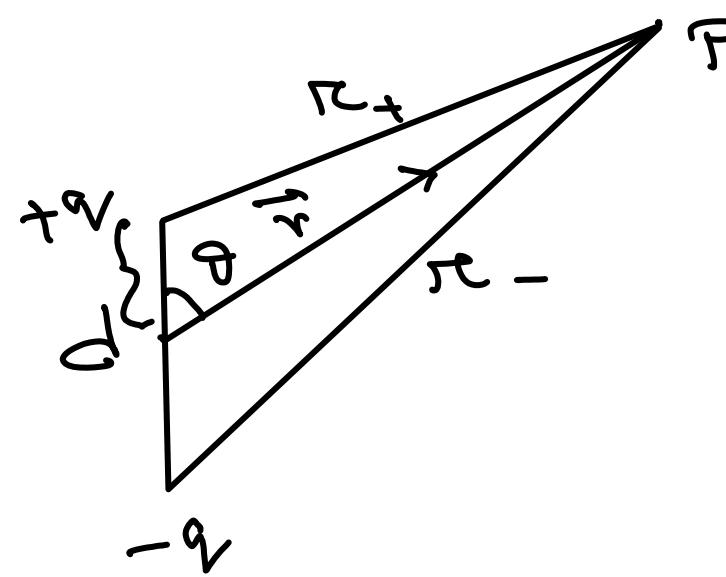
In order to bring dq (infinitesimal amount of charge) to the plate:

$$dV = \frac{q}{C} dr$$

The total work done

$$W = \int_0^q \frac{q}{C} dr = \frac{q^2}{2C} = \frac{1}{2} C V^2$$

Electric Dipole



An electric dipole with two equal and opposite charges ($\pm q$) separated by a distance ' d '.

Potential Due to the Dipole ?

r_- = distance of T from -v

$$r_+ \equiv \cdots \cdots \cdots + \sqrt{r}$$

\vec{r}_j = position vector of P_j .

$$\angle(21) = \frac{1}{4\pi\epsilon_0} \left(\frac{2}{r_+} - \frac{2}{r_-} \right)$$

$$\begin{aligned} x^2 + y^2 &= r^2 + \left(\frac{r}{\sin \theta}\right)^2 + 2r \cos \theta \\ &= r^2 \left(1 + \frac{1}{\sin^2 \theta}\right) + \frac{r^2 \cos^2 \theta}{\sin^2 \theta} \end{aligned}$$

$\frac{\sum q_i r_i^p}{r_p^p} \leq -$ (negligible) in the limit

$$\frac{1}{r_{1+}^{1-p}} = \frac{1}{r_1^p} \left(-1 + \frac{r_1^p}{2} \cos \theta \right)^{-1/p} \rightarrow 0 \quad (\text{neglecting higher order terms})$$

Then,

$$\Rightarrow V(\vec{r}) = \frac{1}{r_1} + \frac{r_1^p}{2} \cos \theta$$

The \sim the potential at point r_1 is $\sim r_1^{-1}$
 by the potential at point r_1 is $\sim r_1^{-1}$

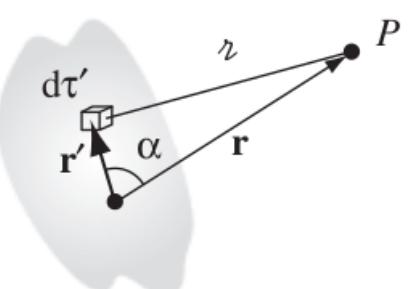
The Monopole and Dipole Terms

The most dominant contribution in the multipole expansion comes from the monopole term.

$$\nabla_{\text{mon}}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{\rho}{r^2} \hat{r}$$

→ If the total charge $\rho = 0$, then the most dominant contribution comes from the dipole term.

$$\nabla_{\text{dip.}}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \int r' \int d\tau' \cos\alpha S(r') d\tau'$$



$$\begin{aligned} \alpha &= \text{Angle between } \vec{r}' \text{ and } \vec{r} \\ \Rightarrow \nabla_{\text{dip.}}(\vec{r}) &= \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} \int r' \int d\tau' \cdot \int d\tau' \cos\alpha S(r') d\tau' \end{aligned}$$

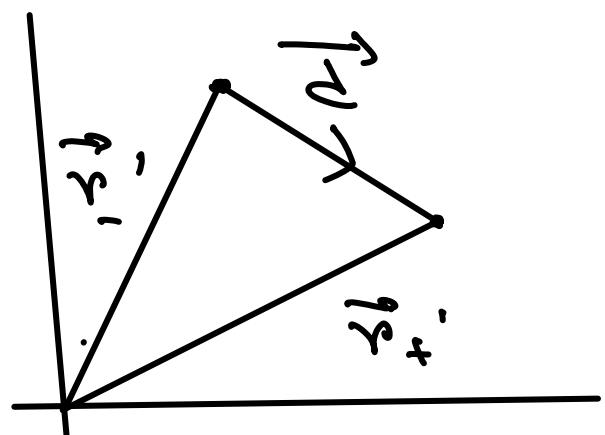
Call this the integral (is dependent on distribution of d_j)

$$= \frac{\text{Dipole moment}}{\rho} \int d\mathbf{r}' \rho(\mathbf{r}') d\mathbf{r}'$$

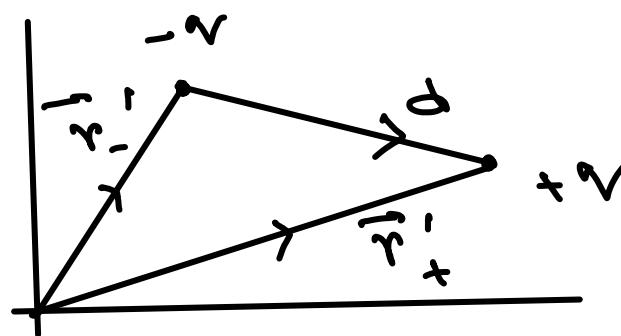
(x) $\tau_{ij} = q_i q_j \int \frac{1}{4\pi\epsilon_0 r^2} \rho(\mathbf{r}) \rho(\mathbf{r}')$

(x) $\tau_{ij} = \mu_{ij}$ μ_{ij} = dipole moment of point charges,

$$= 2 \left(\mathbf{r}_1 \cdot \mathbf{r}_2 - \frac{1}{r^2} \right) e^{-r/2}$$



Electric Dipole (Contd.)



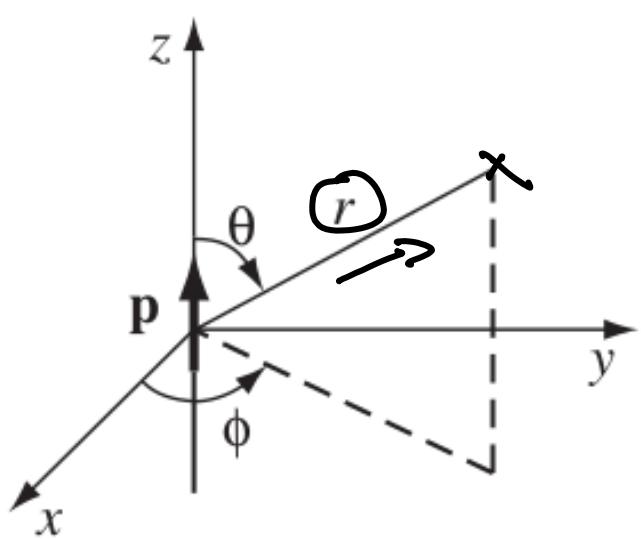
→ physical charges with equal and opposite charges
dipole moment, $\vec{p} = q \left(\frac{\vec{r}_1}{r_1} + \frac{\vec{r}_2}{r_2} \right)$

→ valid for the condition, $r \gg d$.

Dipole approximation = for a perfect dipole, $d \rightarrow 0 \Rightarrow$ then q simultaneously has to increase, $r \rightarrow \infty$.

⑥ A physical dipole becomes a pure dipole in the limit $d \rightarrow 0$ & $q \rightarrow \infty$ with the product $p = qr$ kept fixed and finite.

Electric field due to a dipole



Let's consider a dipole moment \vec{p} at the origin and a point r in the \hat{r} -direction.

$$\vec{d}_{ip} (r, \theta) = \frac{\vec{r} \cdot \vec{p}}{\epsilon_0 r^3}$$

$$\vec{E} = -\nabla V$$

For the electric field,

$$E_r = - \frac{\partial V}{\partial r} = \frac{N e \cos \theta}{\epsilon_0 r^3}$$

$$E_\theta = - \frac{\partial V}{\partial \theta} = \frac{N e \sin \theta}{\epsilon_0 r^3}$$

$$E_\phi = - \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} = \frac{N e \sin \theta}{\epsilon_0 r^3}$$

Then, the electric field is given by

$$M_j = R_{\theta}(\hat{h}, \theta) = \frac{\tau}{\sqrt{1 - \cos \theta}} (\gamma \cos \theta \hat{x} + \sin \theta \hat{y})$$

(*) $\hat{x}_j = M_j \theta$ \hat{g}_3 \Rightarrow M_j is

$$\hat{x}_j = (\hat{x}_j, \hat{d}) = \frac{\tau}{\sqrt{1 - \cos \theta}} \hat{x}_j + \begin{bmatrix} \gamma \\ \sin \theta \end{bmatrix}$$

$$\hat{x}_j = \hat{x}_j \cos \theta \hat{x} + \hat{x}_j \sin \theta \hat{y}$$

\hat{x}_j \Rightarrow $\hat{x}_j = \cos \theta \hat{x} + \sin \theta \hat{y}$

$$\hat{d} = (\hat{x}_j, \hat{d}) = \begin{bmatrix} \cos \theta & \sin \theta \\ 0 & 1 \end{bmatrix} \hat{d} - \begin{bmatrix} \gamma \\ \sin \theta \end{bmatrix}$$

$$= 3 \cos \theta \hat{z} - \cos \theta \hat{x} + \sin \theta \hat{y}$$

(x) Effective = $\mu \cos \theta \hat{z} + \sin \theta \hat{y}$

Thus off

Electric field due to a dipole

off $\sim r_{ij}^{-1}$

(f) The expression is valid for ideal dipoles and physical dipoles under approximation, $r \gg d$.



Dielectrics

Unlike conductors, in a dielectric material, electrons cannot move about freely. They can move about a bit within the atoms and (or) molecules.

⇒ if their movement is absolutely restricted \Rightarrow Insulators (small dielectric constant)

($\epsilon_r = 1$) if the charged particles can move a little bit \Rightarrow Dielectrics (large dielectric constants)

(+) Material is made up of neutral atoms (non-polar molecules) \rightarrow if a

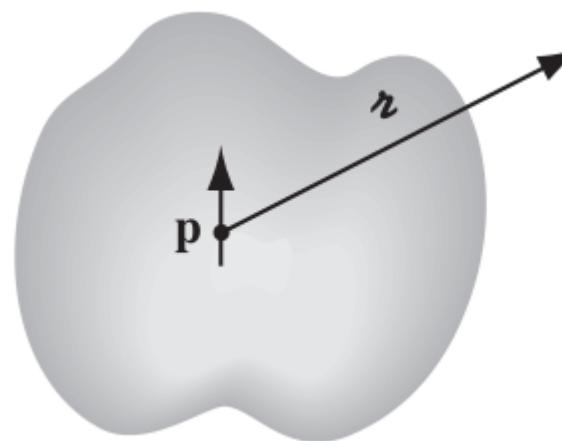
External electric field \rightarrow tiny dipoles
and induced dipoles pointing in the same
direction of the field.

- (x) If material is made of polar
molecules \rightarrow permanent dipoles in
the system \rightarrow external electric
field exerting torque on them \rightarrow
aligns them along the direction of the
electric field.
Y Polar effect is lot of tiny
polarising along the direction of the field
 $= \rightarrow$ Polarisation.

Polarization (\vec{P})

\vec{P} = Dipole moment per unit volume

Field due to a Polarized object



- ④ We have a polarized material.
- ⑤ All the dipoles are pointing in the same direction.

for a single dipole

$$\vec{E}(\vec{r}) = \frac{-}{4\pi\epsilon_0} \frac{\vec{p}}{r^2} \cdot \hat{r}$$

\vec{r} = vector from the dipole to the reference point.

Dipole moment: $\vec{p} = \frac{q}{l} \vec{d}$ for each

infinitesimal volume element $d\tau'$.

↳ The total potential,

$$\nabla = \frac{1}{4\pi\epsilon_0} \int_{\tau'} \frac{-\vec{\nabla}'(\vec{r}') \cdot \vec{r}'}{r'^2} d\tau'$$

$$= \frac{1}{4\pi\epsilon_0} \int_{\tau'} \vec{P} \cdot \vec{\nabla}' \left(\frac{1}{r'} \right) d\tau' \Big| = \frac{\vec{\nabla}' \left(\frac{1}{r'} \right)}{r'}$$

$$\Rightarrow \nabla = \frac{1}{4\pi\epsilon_0} \left[\int_{\tau'} \vec{\nabla}' \cdot \left(\frac{\vec{P}}{r'} \right) d\tau' - \int_{\tau'} \frac{1}{r'} (\vec{\nabla}' \cdot \vec{P}) d\tau' \right]$$

Using divergence theorem,

$$V = \frac{1}{\epsilon_0} \int_S \vec{r} \cdot \vec{P} \cdot d\vec{a}' - \frac{1}{\epsilon_0} \int_V (\nabla' \cdot \vec{P}) dV$$

Potential due to a surface charge distribution

$$\rho_s = \vec{P} \cdot \vec{n}$$

Potential due to a volume charge distribution

$$\rho_v = -\nabla' \cdot \vec{P}$$

Charge density:

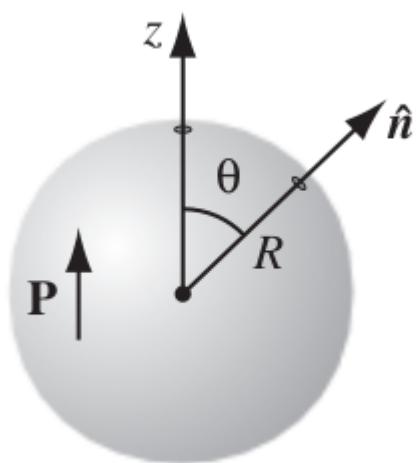
hence,

$$V(r) = \frac{1}{\epsilon_0} \int_S \frac{\rho_s}{r} d\vec{a}' + \frac{1}{\epsilon_0} \int_V \frac{\rho_v}{r} dV$$

→ Potential of a polarised object is the same as that produced by a volume and a surface charge densities.

These are called bound charge.

E_x :



Electric field produced by a uniformly polarized sphere of radius ' R '.

If \mathbf{P} is uniform, $\sigma_b = 0$

The surface bound charge density,

$$\sigma_b = \rho_s \cos \theta$$

We need to find the potential of a system with surface charge density ρ_{surf}

$$\nabla(\lambda, \theta) = \frac{\rho \epsilon_0 \cos \theta}{3 \epsilon_0 r^2}$$

$$\frac{\rho}{\epsilon_0} \rightarrow \frac{1}{r}$$

We know,

$$E = - \nabla \phi = \frac{\rho}{3 \epsilon_0 r^2}$$

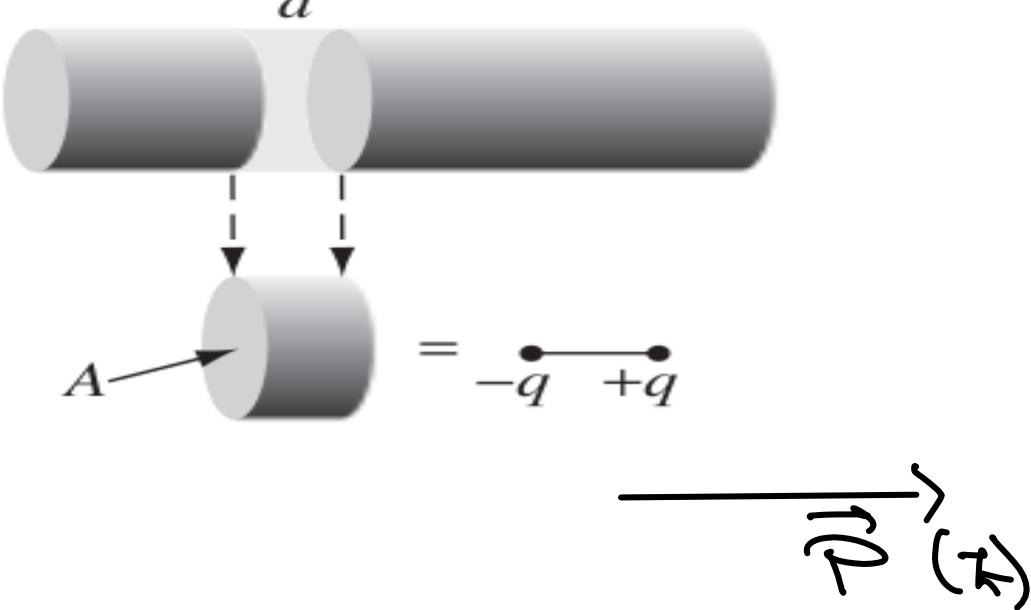
Physical interpretation of bound charge.

$$-\frac{++--++--++-+}{-+-+--+-+--+-+} = \frac{q}{r} \rightarrow \text{Bound charges.}$$

Above diagram showing effect of dipole made of positive and negative charges.

To calculate the amount of bound charges resulting from a polarization of dielectric parallel to \vec{P}

(+) A tube



On the small chunk,
the dipole moment

$$= \rho (A \sigma)$$

\rightarrow length of the
chunk
Cross-section
of the sides

In terms of charges at the
end, dipole moment = qd

from a



$$\tau = A_{\text{end}} \cos \theta$$

\rightarrow The charges
on the end are
still the same,

but

$$q_b = \frac{q}{A_{\text{end}}}$$

$$= \frac{q \cos \theta}{A}$$

$$= \tau \cos \theta$$

The net effect of polarization is to create a bound charge density over the surface of the material.

$$\text{Thus the bound charge} = \rho \cdot s$$

$$\Rightarrow \rho^2 = \frac{\rho^2}{\rho^2 - \rho} = \frac{\rho^2}{\rho} = \rho$$

$$\sigma_b = \frac{\rho}{d} = \rho = \rho \cdot s$$

The net effect of polarization is to create a bound charge density over the surface of the material.

$$\sigma_b = \rho \cdot s$$

Gauss's law in presence of Dielectrics

Polarisation \rightarrow accumulation of bound charges

$$\sigma_b = - \nabla \cdot P$$

$$\rho_b = \nabla \cdot P$$

\rightarrow These bound charges give rise to electric field.

Total field = field due to bound charges + field due to free charges

Within a dielectric,

$$\rho = \rho_b + \rho_f$$

\rightarrow free charge density

Using Gauss' law,

$$\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$
$$\Rightarrow \epsilon_0 (\nabla \cdot \vec{E}) = \rho = -\nabla \cdot \vec{D} + \rho_f$$

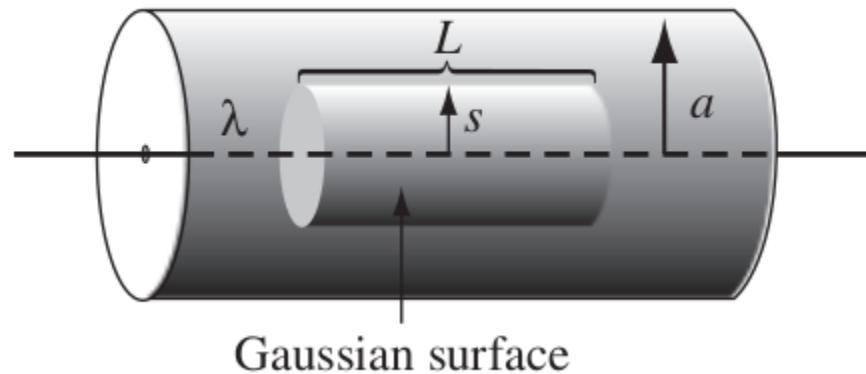
$$\nabla \cdot \vec{D} = \epsilon_0 \vec{E} + \vec{P} = \vec{D}_e + \vec{P}_f = \text{Electric displacement}$$

Hence, $\nabla \cdot \vec{D}_e = \int \rho_f dV$

For dielectrics,

$(\nabla \cdot \vec{D})_{\text{free}} = (\rho_f)_{\text{enc.}}$
(ρ_f free charge enclosed)

\vec{B}_x :



A long straight wire carrying uniform line charge density λ , surrounded by a dielectric medium of radius (a).

→ Gaussian surface has radius $\equiv 0$
length $\equiv L$

$$\oint \vec{B} \cdot d\vec{l} = (\partial_r)_{\text{enc.}}$$

$$\Rightarrow \partial (2\pi r l) = \rightarrow L$$

$$\Rightarrow \partial = \frac{\rightarrow L}{2\pi l}$$

$$\vec{B}_x = \frac{\lambda}{2\pi r}$$

Outside,
From,

$$\vec{P} = 0$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

$$\vec{D} = \epsilon_0 \vec{E}$$

$$\frac{\epsilon}{\epsilon_0} = \frac{\lambda}{2\pi \epsilon_0 s}$$

$$\epsilon = \frac{\lambda^2}{2\pi s}$$

Inside, $\vec{P} \neq 0$, we need the knowledge
of \vec{P} in order to calculate \vec{E} .

Linear Dielectrics

A class of dielectrics for which
the induced polarisation is proportional
to the electric field.

$$\vec{P} = \epsilon_0 \chi_e \vec{E}$$

$\chi_e = \text{Proportionality const. (Electric Susceptibility)}$

ϵ_0 is brought outside to makes χ_e dimensionless.

(+) Any material obeying $\vec{D} = \epsilon_0 \vec{E}$ is called a linear dielectric.

$$\begin{aligned}\vec{D} &= \epsilon_0 \vec{E} + \vec{P} \\ &= \epsilon_0 \vec{E} + \epsilon_c \chi_e \vec{E}\end{aligned}$$

$$= \epsilon_0 (1 + \chi_e) \vec{E}$$

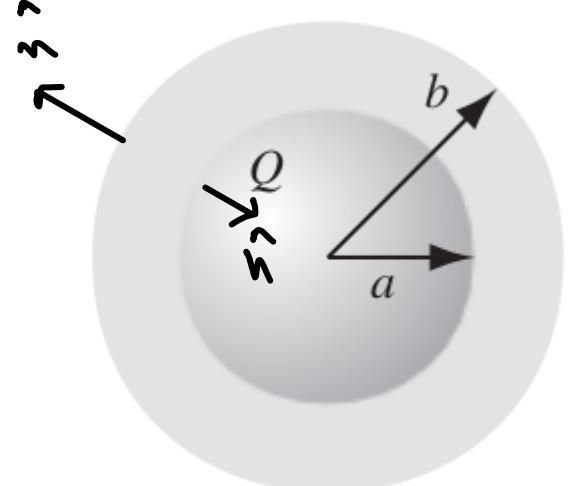
$$= \epsilon \vec{E}$$

$\rightarrow \epsilon = \epsilon_0 (1 + \chi_e)$ = Permittivity of a material

(*) $\chi_e = \infty$ & $\rho_e = 0$ $\Rightarrow \rho_e = \rho_0 = \rho_0$ material, there is no material, the space.

(*) $\epsilon_d = \epsilon_r \epsilon_0 = \text{Relative permittivity}$
 $\epsilon_r = \text{Dielectric const.}$

Q. If the center of a metal sphere of radius a carrying a total charge Q is surrounded by a dielectric material of relative permittivity ϵ_r . Calculate the potential at the center.



$$\rightarrow H_3 \text{ the beginning} \Leftrightarrow \frac{\partial^2 \phi}{\partial r^2} = h_3$$

$$F_3 \text{ inside the sphere} = 0 = F_3 = \rho$$

$$H_3 \text{ the beginning} , r \rightarrow r \\ F_3 = \frac{q}{4\pi \epsilon_0 r^2}$$

$$H_3 \text{ the beginning} , r \rightarrow b \\ F_3 = \frac{q}{4\pi \epsilon_0 b^2}$$

Potential at center,

$$V = - \frac{q}{4\pi\epsilon_0 r} \cdot \vec{r}$$

$$= - \frac{q}{4\pi\epsilon_0 r^2} \int_0^r \vec{r} \cdot d\vec{r} - \int_0^r \frac{\delta}{4\pi\epsilon_0 r'^2} \vec{r}' \cdot d\vec{r}'$$
$$= \frac{\delta}{4\pi\epsilon_0} \left(\frac{1}{r} + \frac{1}{a} - \frac{1}{b} \right)$$

Polarization,

$$\vec{D} = \epsilon_0 \chi_e \vec{E}$$

$$= \frac{\epsilon_0 \chi_e \delta}{4\pi\epsilon_0 r^2} dr$$

(ϵ_0 is the
dielectric)

Bound charges:

$$\sigma_1 = - \nabla \cdot \vec{D} = \frac{\epsilon_0 \chi}{4\pi r^2} \quad (r \text{ outer surface})$$

$$\sigma_2 = - \nabla \cdot \vec{D} = \frac{\epsilon_0 \chi}{4\pi r^2} \quad (r \text{ inner surface})$$

* \vec{n} points outward with respect to the dielectrics $\Rightarrow \vec{n} = \vec{r}$

$$\begin{aligned} \vec{n} &= \vec{r} \\ \vec{D} &= \epsilon_0 \vec{E} \\ r_1 &= b \\ r_2 &= a \end{aligned}$$

For a linear dielectric,

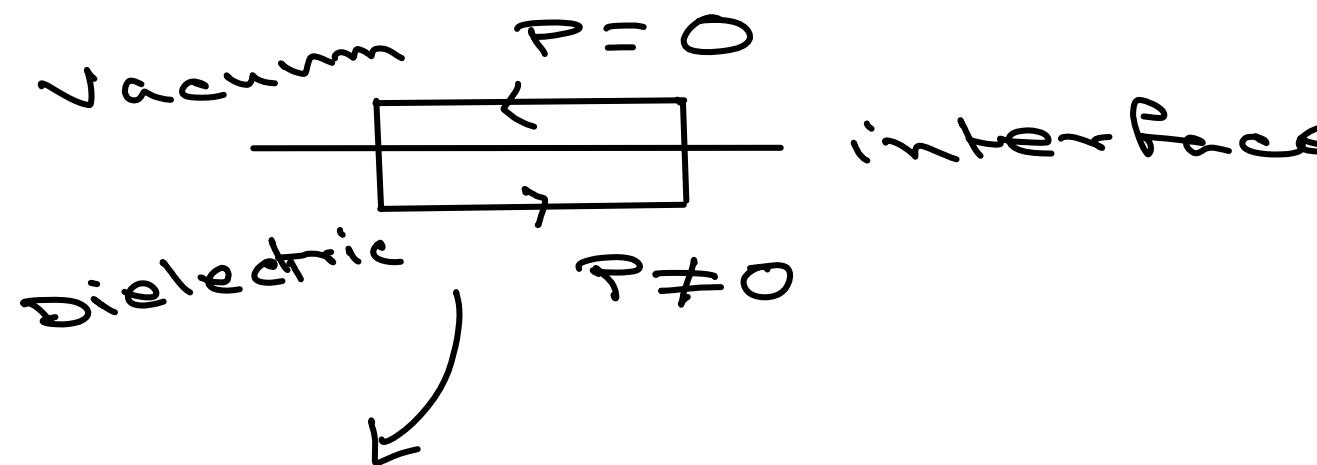
$$\vec{D} = \epsilon_0 \chi_e \vec{E}$$

$$\vec{D} = \epsilon \vec{E}$$

$$\epsilon = \epsilon_r \epsilon_0$$

ϵ_r \leftarrow
Dielectric
const.

(*) Does this mean



$$\vec{D} \times \vec{P} = 0$$

→ 1st order

$$\vec{D} \times \vec{P} = 0 \quad \text{we should} \\ \text{have } \vec{D} \cdot \vec{P} = 0$$

Around this gap

$$\vec{D} \cdot \vec{P} \neq 0 \quad \Rightarrow \quad \vec{D} \times \vec{P} \neq 0$$

→ If the space is completely filled with dielectrics, $\vec{D} \cdot \vec{P} = 0$ & $\vec{D} \times \vec{P} = 0$

\vec{D} can be obtained from free charge density

$$\vec{D} = \epsilon_0 \vec{E}$$

the field lines

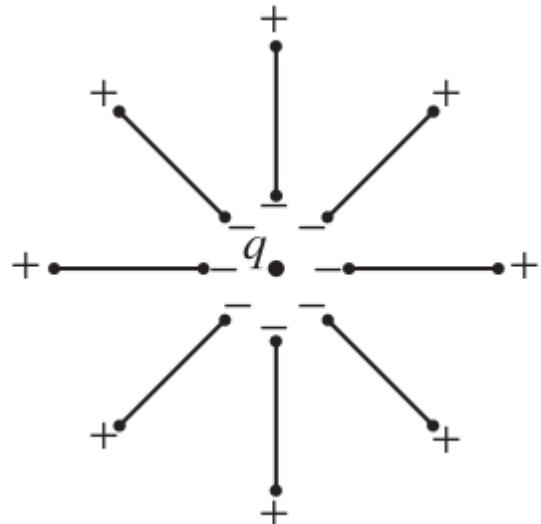
charge will produce in absence of dielectric.

$$\vec{E} = \frac{1}{\epsilon_r} \vec{D}$$

$$E_d = \frac{1}{\epsilon_0}$$

field is reduced by the factor by which the homogeneous linear dielectric.

If free charge 'q' is embedded in dielectric,

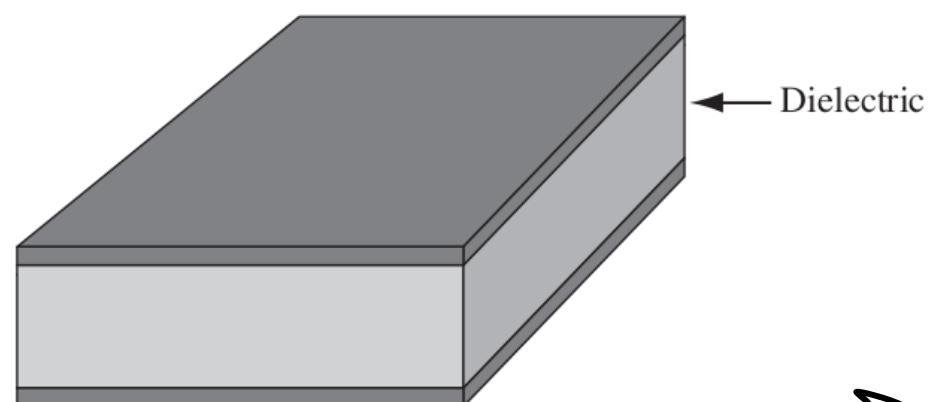


$$E = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2}$$

→ The free charge is shielded from all sides due to the polarisation.

⇒ This shielding effect reduces the electric field.

④ This property can be used to enhance capacitance of a system.

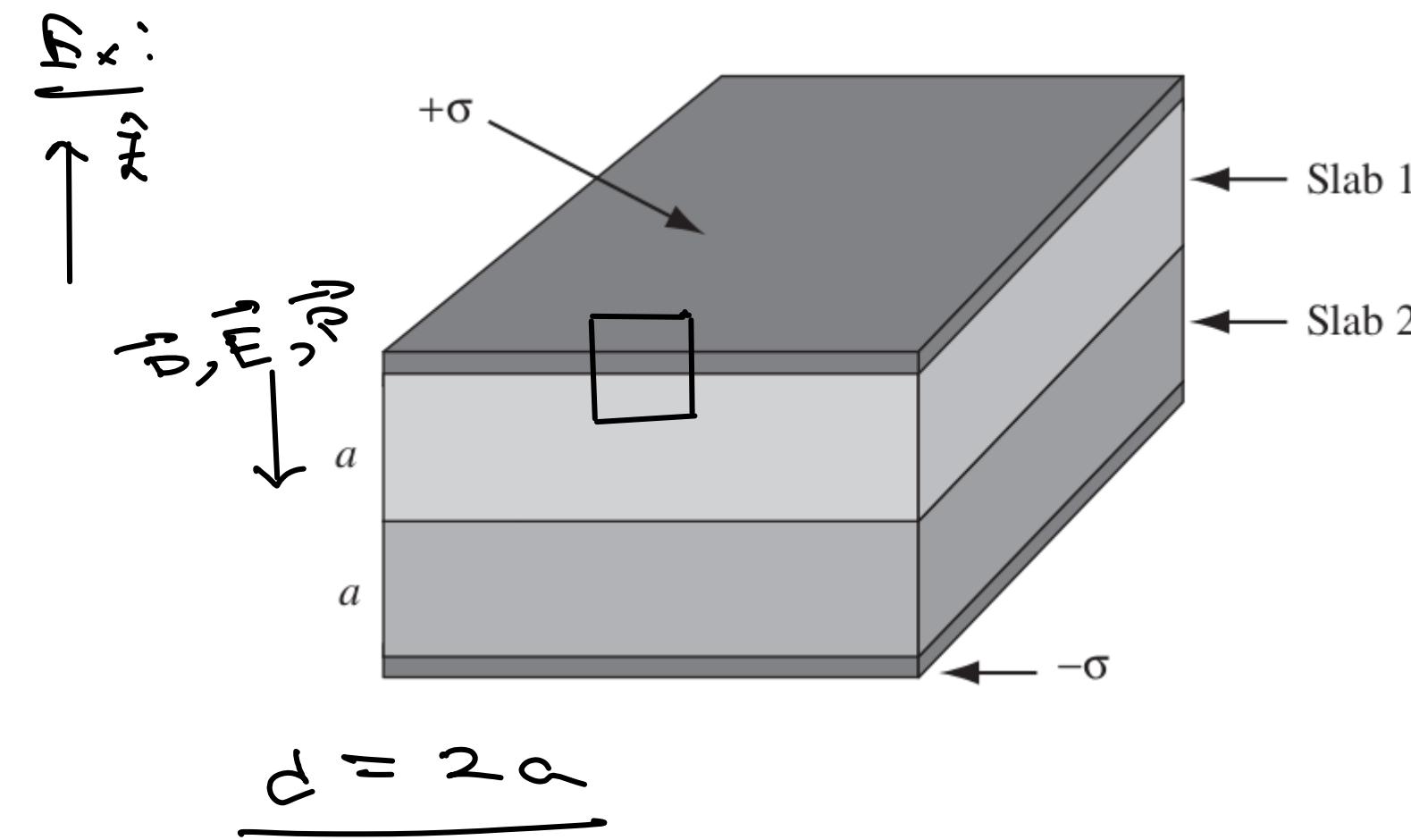


→ A parallel plate capacitor filled with dielectric material

⇒ The dielectric reduces E and ΔV (potential diff.) by a factor of ϵ_r .

The capacitance ($\frac{Q}{V}$) is increased by a factor,

$$C = \epsilon_r C_{\text{vac}}$$



$$a = 2a$$

Slab 1 has dielectric const = 2
Slab 2 - - - - - = 1.5

(*) σ is each slab:

We have a parallel plate capacitor with charge density $\pm \sigma$ on the plates.

The space between the plates is filled with two dielectric slabs with thickness a

$$\text{const} = 2$$

$$= 1.5$$

$$\text{of } \sigma_{xy} \cdot \sigma_{yy} = (\sigma_x)_{\text{enc.}}$$

$$\Rightarrow \sigma_{xx} = \sigma_{yy}$$

Then,

$$\sigma_{yy} = -q$$

$\sigma_{yy} = 0$ inside metal plates.

(i) E_y

$$\text{For } E_y \text{ in air: } \sigma_{yy} = q_b$$

For

$$-\bar{E}_1 = \frac{q}{\epsilon_1}$$

$$(2) \quad \Rightarrow \quad -\bar{E}_2 = \frac{q}{\epsilon_2}$$

$$\epsilon_1 = 2\epsilon_0$$

$$\epsilon_2 = 1.5\epsilon_0$$

$$\left. \begin{aligned} -\bar{E}_1 &= q/2\epsilon_0 \\ -\bar{E}_2 &= q/1.5\epsilon_0 = 2q/3\epsilon_0 \end{aligned} \right\}$$

④ Polarisation:

$$\Rightarrow \vec{P} = \epsilon_0 \chi_e \vec{E}$$
$$\vec{P}_1 = \frac{\epsilon_0 \chi_e q}{\epsilon_0 + \epsilon_s}$$

$$= \frac{\chi_e}{\epsilon_s} q$$

$$\chi_e = (\epsilon_s - 1)$$

$$\vec{P}_1 = \frac{\epsilon_s - 1}{\epsilon_s} q = (-\epsilon_s) q$$
$$\vec{P}_2 = \omega q$$

④ Potential difference,

$$\nabla \cdot \mathbf{E} = -\frac{q}{\epsilon_0 r^2} + \frac{q}{\epsilon_0 r^2} = \frac{q}{\epsilon_0 r^2} \left(\frac{1}{r^2} + \frac{1}{r^2} \right)$$

$$= \frac{+q}{6\pi r^2}$$

(+) Bound charges:

constant polarization $\Rightarrow \rho_b = 0$

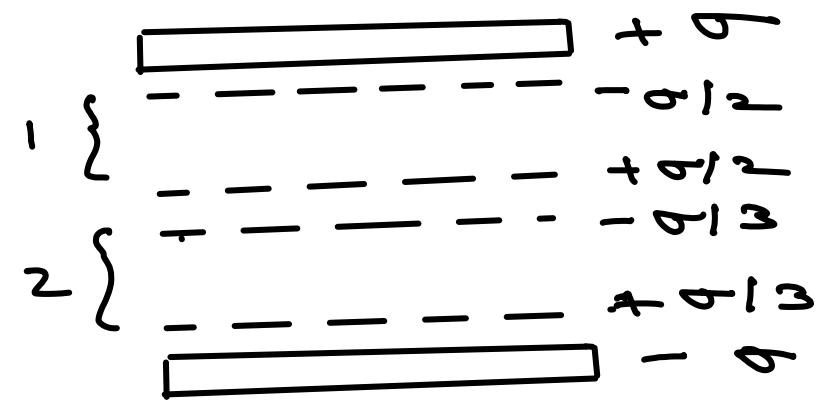
The bound surface charge density:

$$\rho_b = -\rho_s \quad (\text{top of slab})$$

$$= +\rho_s \quad (\text{bottom of slab})$$

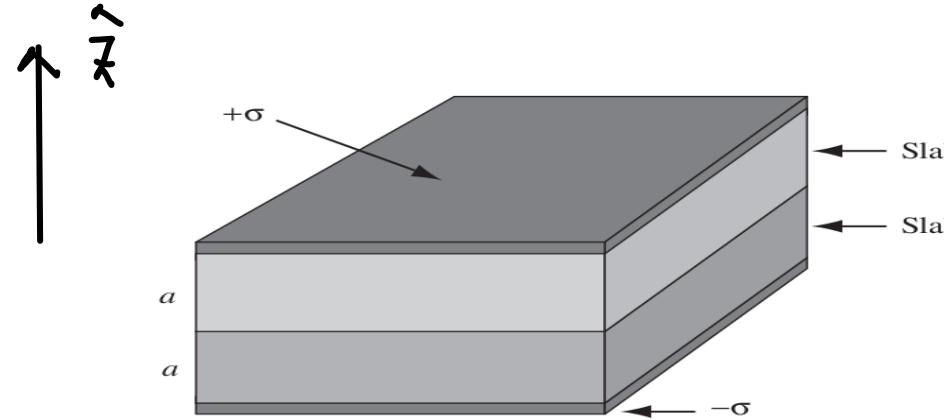
$$= -\rho_s \quad (\text{top of slab 2})$$

$$= +\rho_s \quad (\text{bottom of slab 2})$$



$$\begin{aligned} \rho_s &= \rho_s \cdot \delta(r) \\ &= \rho_s \delta(r) (-\delta(r)) \end{aligned}$$

Ex (contd)



Space betw. two capacitor plates filled with dielectric slab 1 and slab 2 with dielectric const = 2 and 1.5 respectively.

We found:

$$\begin{aligned}
 & \text{free charge} & \vec{D} = \sigma (-\hat{z}) \\
 & \left. \begin{array}{c} -\sigma/2 \\ +\sigma/2 \\ -\sigma/3 \\ +\sigma/3 \end{array} \right\} q_b & \vec{E}_1 = \frac{q}{2\epsilon_0} (-\hat{z}) ; \vec{P}_1 = \frac{q}{2} (-\hat{z}) \\
 & \text{free charge} & \vec{E}_2 = \frac{2\sigma}{3\epsilon_0} (-\hat{z}) ; \vec{P}_2 = \frac{q}{3} (-\hat{z}) \\
 & \text{Surface bound charge density } (\rho_b) & \textcircled{*} \text{ Volume bound charge density } f_b = 0
 \end{aligned}$$

$\textcircled{*}$ Potential difference, $\Delta V =$

$$q = \frac{\sigma}{A} \xrightarrow{\substack{\text{total charge} \\ \text{on plate}}} \frac{q}{A} \quad \text{Area of plate}$$

$$\begin{aligned}
 & \frac{q}{6\epsilon_0} \\
 & \frac{7\sigma a}{6A\epsilon_0}
 \end{aligned}$$

④ Capacitance, $C = \frac{Q}{V} = \frac{6A\epsilon_0}{7a}$

⑤ Check the electric fields from knowledge of bound and free charges:

Slab 1: Total surface charge above = $\sigma - \frac{\rho}{2}a = \frac{\rho}{2}a$

" " " below = $-\frac{\rho}{2}a$

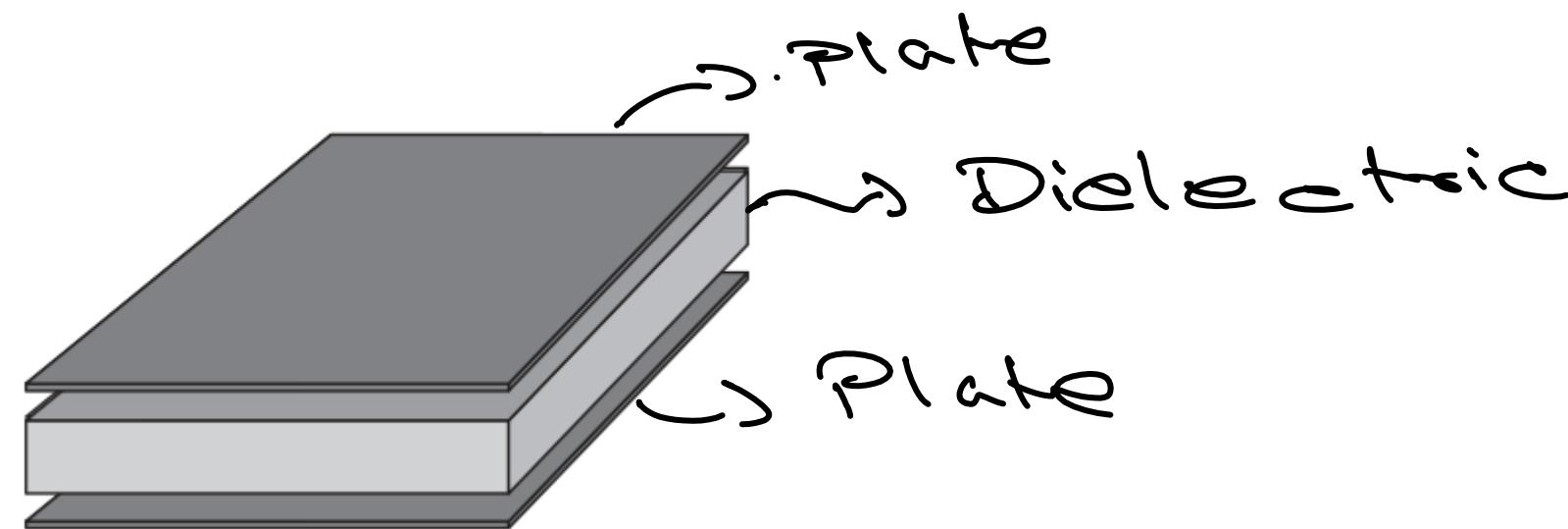
Slab 2: " " " above = $\frac{\rho}{3}a$

" " " below = $\frac{\rho}{3}a - \rho = -\frac{2\rho}{3}a$

Then, the electric fields:

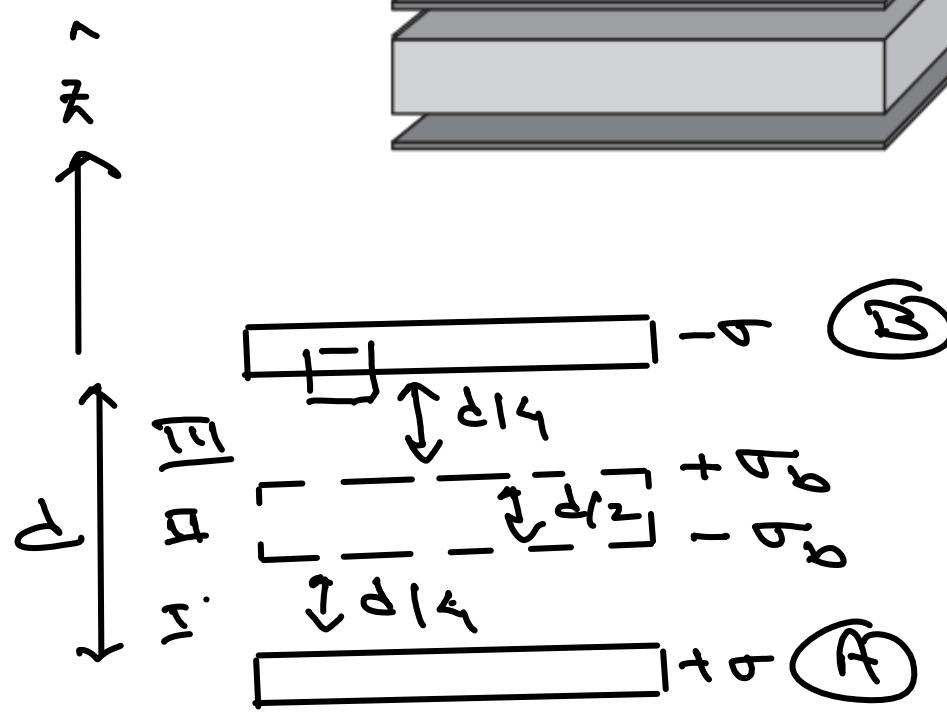
$$\left. \begin{aligned} \vec{E}_1 &= \frac{\rho}{2\epsilon_0} (-\hat{x}) \\ \vec{E}_2 &= \frac{\rho}{3\epsilon_0} (-\hat{x}) \end{aligned} \right\}$$

Ex:



(*) The space betw. the two plates is half filled with a dielectric slab.

→ Spacing betw. two plates = d
 \Rightarrow thickness of the dielectric slab = $\frac{d}{2}$



(*) Electric Displacement
 $\oint \vec{D} \cdot d\vec{l} = (D_p)_{enc.}$

$$\Rightarrow \vec{D}_1 \cdot \vec{l} = q_A$$

$$\Rightarrow \vec{D} = q \hat{x} \quad (\text{in all regions})$$

(x)

$$E_{\parallel} = \epsilon_0 \frac{q}{d} \hat{x}$$

(I)

$$H_{\parallel} = 0$$

(II)

$$\mu_{\parallel} = 1$$

(III)

⑥ Polarization:

in region F:

$$P_{\parallel} = \epsilon_0 \chi_e \hat{E}_{\parallel}$$

$$= \frac{\epsilon_0 \chi_e}{1 + \chi_e} q \hat{x}$$

$$= \frac{\epsilon_0 \chi_e}{1 + \chi_e} \hat{x}$$

$$= \frac{\chi_e}{1 + \chi_e} \hat{x}$$

(*) Bound charge densities:

$$\sigma_b = 0$$

(Polarisation is uniform)

$$\sigma_b = \rho \cdot \hat{z} = \frac{\chi_e \sigma}{(\chi + \chi_e)} \hat{z} \cdot \hat{z}$$

(Top plane dielectric)

$$= \frac{\chi_e \sigma}{(\chi + \chi_e)}$$

$$\sigma_b = -\frac{\chi_e \sigma}{(\chi + \chi_e)} \hat{z} \cdot (-\hat{z})$$

(Bottom plane dielectric)

$$= -\frac{\chi_e \sigma}{(\chi + \chi_e)}$$

$$\nabla \cdot \vec{D}_c = - \int_0^A \vec{E} \cdot \vec{d}x = \int_A^0 \vec{E} \cdot \vec{d}x$$

$$\begin{aligned}
 &= \int \frac{\sigma}{\epsilon_0} dx + \int \frac{\sigma}{\epsilon} dx + \int \frac{\sigma}{\epsilon_c} dx \\
 &= \frac{q}{\epsilon_0} \times \frac{A}{d} + \frac{q}{\epsilon} \times \frac{N}{d} + \frac{q}{\epsilon_c} \times \frac{r}{d} \\
 &= \frac{q}{\epsilon_0} \left(\frac{A}{d} + \frac{N}{d} \right) \\
 &= \frac{q(A + Nd)}{\epsilon_0 d} \\
 &= \frac{q}{\epsilon_0 A} (A + Nd)
 \end{aligned}$$

$q = \text{Total charge}$
 in plate

$A = \text{Total area}$
 of plate

$$q = Q/A$$

(*) Capacitance, $C = \frac{Q}{V}$

$$\Phi_d = \frac{\epsilon}{\epsilon_0} A$$

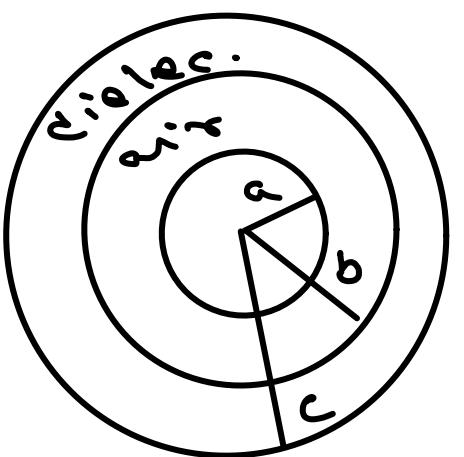
$$= \frac{2 \pi A \epsilon_0}{2 \left(r + \frac{\epsilon}{\epsilon_0} \right)}$$

$$= \frac{2 \pi \epsilon_0 A}{2} \frac{1}{1 + \frac{\epsilon}{\epsilon_0}}$$

$$= \frac{2 \epsilon_0 A}{2} \left(\frac{1}{1 + \frac{\epsilon}{\epsilon_0}} \right)$$

→ Capacitance in absence of ϵ

$$\text{dielectric} = \frac{\epsilon_0 A}{d}$$



$\rightarrow D_x:$

Space in betw. ($\epsilon_{\text{const}} = \epsilon_d$)

Coxial cable consisting of
Copper core (radius = a) surrounded by copper
Tubes (radius = b). The
(Partially from b to c)

δ = charge on a length 'l' on the copper
wires,

$$\oint \vec{v}_j \cdot d\vec{l} = \delta$$

$$\Rightarrow \vec{v}_j = \frac{\delta}{2\pi r_1} \hat{r}$$

Here, $r_j \equiv$ arbitrary radial distance
 $\hat{r}_j \equiv$ radial unit vector.

$$F_{jj}^{\parallel} = \frac{e \vec{v}_j}{2\pi r_0 \epsilon_0} \quad (c < r_b)$$

$$m_j = \frac{\delta}{2\pi r_1 \epsilon} \hat{r} \quad (b < r_c)$$

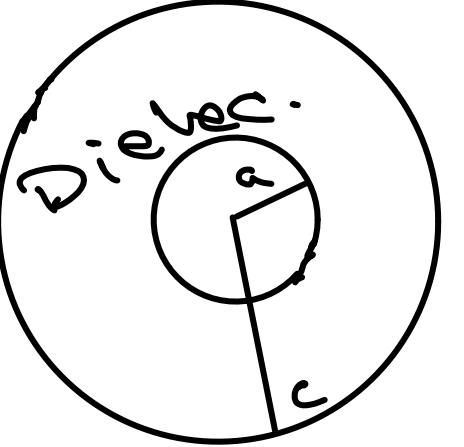
$$\Delta V = - \int_C \vec{E} \cdot d\vec{s} = \int_a^b \frac{\delta}{2\pi \epsilon_0 l} ds + \int_0^a \frac{\delta}{2\pi \epsilon_0 l} ds$$

$$= \frac{\delta}{2\pi \epsilon_0 l} \left[\ln\left(\frac{b}{a}\right) + \frac{\epsilon_0}{\epsilon} \ln\left(\frac{c}{b}\right) \right]$$

Capacitance per unit length:

$$\Rightarrow \frac{C}{l} = \frac{\delta}{2\pi \epsilon_0} = \frac{2\pi \epsilon_0}{\ln\left(\frac{b}{a}\right) + \left(\frac{1}{\epsilon_0}\right) \ln\left(\frac{c}{b}\right)}$$

Ex:



Linear charge density on wire = λ

$$Q = \lambda l$$

$$\Delta V = \int_a^b E \cdot dr$$

The space betw. is fully filled with dielectric.

$$E = \frac{2\pi\lambda r}{2\pi\epsilon_0}$$

($a < r < c$)

$$\Delta V = \int_a^b \frac{\lambda}{2\pi\epsilon_0} r dr$$

$$\Delta V = \frac{2\pi\lambda}{2\pi\epsilon_0} \ln \left(\frac{b}{a} \right)$$

Capacitance,

$$C = \frac{\Delta Q}{\Delta V} = \frac{2\pi\epsilon_0}{\ln(b/a)}$$