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Q. Three isotropic sources, with spacing  $d$  between them, are placed along the z-axis. The excitation coefficient of each outside element is unity while that of the center element is 2. For a spacing of  $d = \lambda/4$  between the elements, find the

- (a) array factor
- (b) angles (in degrees) where the nulls of the pattern occur ( $0^\circ \leq \theta \leq 180^\circ$ )
- (c) angles (in degrees) where the maxima of the pattern occur ( $0^\circ \leq \theta \leq 180^\circ$ )

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a.  $E_t = E_1 + E_2 + E_3 = 2E_0 \frac{e^{jkr}}{r} + E_0 \frac{e^{jkr_1}}{r_1} + E_0 \frac{e^{jkr_2}}{r_2}$

where the center element is placed at the origin. For far-field observations

$$r_1 \approx r - d \cos\theta$$

$$r_2 \approx r + d \cos\theta$$

$$r_1 \approx r_2 \approx r \quad \text{for amplitude variations}$$

and

$$E_t \approx E_0 \frac{e^{jkr}}{r} \left\{ 2 + e^{jkd \cos\theta} + e^{-jkd \cos\theta} \right\}$$

$$\approx E_0 \frac{e^{jkr}}{r} \left\{ 2 \left[ 1 + \frac{1}{2} (e^{jkd \cos\theta} + e^{-jkd \cos\theta}) \right] \right\}$$

$$= E_0 \frac{e^{jkr}}{r} \left\{ 2 [1 + \cos(kd \cos\theta)] \right\}$$

Computer Program

Directivity

$$U = \cos^4\left(\frac{\pi}{4} \cos\theta\right)$$

$$At. d = \lambda/4$$

$$Prad = 8.7119$$

$$D_0 = 1.44244 \\ = 1.5910 \text{ dB}$$

$$Rd = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4} = \frac{\pi}{2}$$

$$AF(\theta) = 4 \cos^2\left(\frac{\pi}{4} \cos\theta\right)$$

Thus the array factor is equal to

$$AF(\theta) = 2[1 + \cos(kd \cos\theta)] = 4 \cos^2\left(\frac{kd}{2} \cos\theta\right)$$



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b. The nulls of the pattern can be found using either of the above forms for the array factor. For example.

One Form

$$AF(\theta) = 1 + \cos(kd \cos \theta_n) = 0$$

$$\cos(kd \cos \theta_n) = -1$$

$$kd \cos \theta_n = \cos^{-1}(-1) = n\pi, n = \pm 1, \pm 3, \dots$$

$$\theta_n = \cos^{-1}(n\lambda/2d), n = \pm 1, \pm 3, \pm 5, \dots$$

the other Form

$$2 \cos^2\left(\frac{kd}{2} \cos \theta_n\right) = 0$$

$$\frac{kd}{2} \cos \theta_n = \cos^{-1}(0) = \frac{n\pi}{2}, n = \pm 1, \pm 3, \dots$$

$$\theta_n = \cos^{-1}(n\lambda/(2d)), n = \pm 1, \pm 3, \dots$$

which are of identical form. Therefore both forms yield the same results. Thus for  $d = \lambda/4$

$$\theta_n = \cos^{-1}\left(\frac{n\lambda}{2d}\right)_{d=\lambda/4} = \cos^{-1}(2n), n = \pm 1, \pm 3, \dots \Rightarrow \text{No nulls exist.}$$



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C. Similarly the maxima of the pattern can be found using either of the two forms for the array factor. For example

6-1(Cont'd) One Form

$$AF(\theta) = 1 + \cos(kd \cos\theta_m) = 2$$

$$\cos(kd \cos\theta_m) = 1$$

Other Form

$$AF(\theta) = 2 \cos^2\left(\frac{kd}{2} \cos\theta_m\right) = 2$$

$$\cos\left(\frac{kd}{2} \cos\theta_m\right) = \pm 1$$

$$kd \cos\theta_m = \cos^{-1}(1) = 2m\pi, m=0, \pm 1, \dots, \quad \frac{kd}{2} \cos\theta_m = \cos^{-1}(\pm 1) = m\pi, m=0, \pm 1, \dots$$

$$\theta_m = \cos^{-1}\left(\frac{m\lambda}{d}\right), m=0, \pm 1, \pm 2, \dots, \quad \theta_m = \cos^{-1}\left(\frac{m\lambda}{d}\right), m=0, \pm 1, \pm 2, \dots$$

which are of identical form. Therefore both yield the same results.

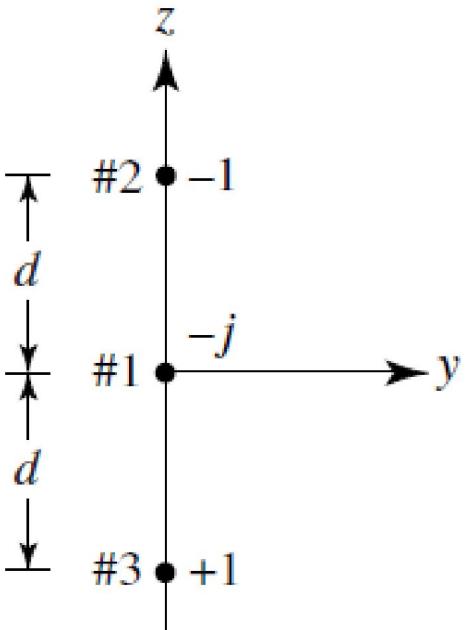
Thus for  $d = \lambda/4$ .

$$A_m = \cos^{-1}(4m), m=0, \pm 1, \pm 2, \rightarrow \begin{cases} m=0: \theta_0 = \cos^{-1}(0) = 90^\circ \\ m=\pm 1: \theta_1 = \cos^{-1}(4) \Rightarrow \text{Does not exist.} \end{cases}$$

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Q. A three-element array of isotropic sources has the phase and magnitude relationships shown. The spacing between the elements is  $d = \lambda/2$ .

(a) Find the array factor. (b) Find all the nulls.





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a. Derive the array factor;

$$AF = -e^{jkd\cos\theta} - j + e^{-jkd\cos\theta} = -2j\sin(kd\cos\theta) - j$$

$$AF = 2\sin(kd\cos\theta) + 1$$

$$AF = 2\sin(\pi\cos\theta) + 1$$

b.  $2\sin(\pi\cos\theta) = -1$

$$kd\cos\theta = \sin^{-1}(-\frac{1}{2}) = -\frac{\pi}{6}, -\frac{5\pi}{6}, -\frac{13\pi}{6}, \dots, \frac{7\pi}{6}, \frac{11\pi}{6}, \frac{19\pi}{6}$$

$$\theta_n = \cos^{-1}\left(\frac{x}{\pi}\right)$$

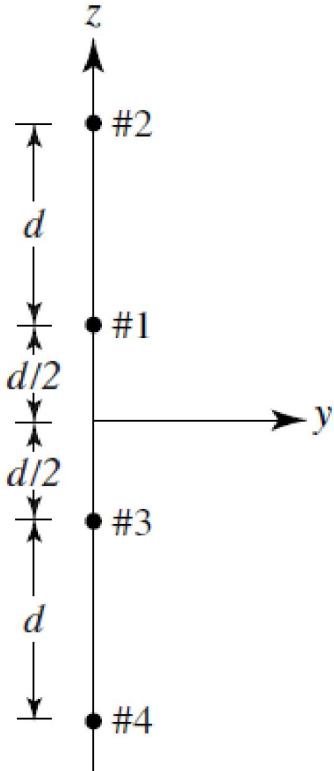
$$-\frac{\pi}{6} \rightarrow \theta_1 = 99.59^\circ$$

$$-\frac{5\pi}{6} \rightarrow \theta_2 = 146.44^\circ$$

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Q. Four isotropic sources are placed along the z-axis as shown. Assuming that the amplitudes of elements #1 and #2 are +1 and the amplitudes of elements #3 and #4 are -1 (or 180 degrees out of phase with #1 and #2), find

- (a) the array factor in simplified form



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$$\begin{aligned}
 (a) \quad E &= \frac{e^{-jkr_2}}{r_2} + \frac{e^{-jkr_1}}{r_1} - \frac{e^{-jkr_3}}{r_3} - \frac{e^{-jkr_4}}{r_4} \\
 &= \frac{\bar{e}^{jkr}}{r} \left[ e^{jk\frac{3d}{2}\cos\theta} + e^{jk\frac{d}{2}\cos\theta} - e^{-jk\frac{d}{2}\cos\theta} - e^{-jk\frac{3d}{2}\cos\theta} \right]
 \end{aligned}$$

$$r_1 = r - \frac{d}{2}\cos\theta, \quad r_2 = r - \frac{3d}{2}\cos\theta, \quad r_3 = r + \frac{d}{2}\cos\theta, \quad r_4 = r + \frac{3d}{2}\cos\theta$$

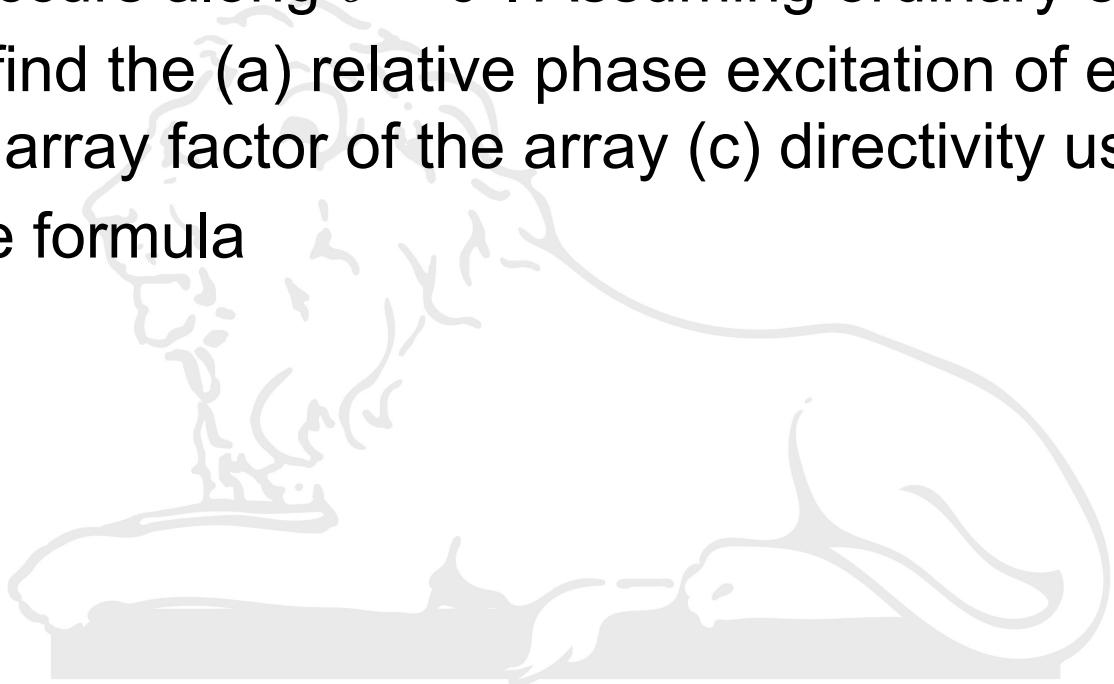
$$AF = 2j \left[ \sin\left(\frac{3kd}{2}\cos\theta\right) + \sin\left(\frac{kd}{2}\cos\theta\right) \right]$$





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Q. Design a two-element uniform array of isotropic sources, positioned along the z-axis a distance  $\lambda/4$  apart, so that its only maximum occurs along  $\theta = 0^\circ$ . Assuming ordinary end-fire conditions, find the (a) relative phase excitation of each element (b) array factor of the array (c) directivity using Kraus' approximate formula



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Placing one element at the origin and the other at  $d$  distance above it, the array factor is equal to

$$AF(\theta) = 1 + e^{j(kd\cos\theta + \beta)} = 2e^{j\frac{1}{2}(kd\cos\theta + \beta)} \left[ \frac{e^{j\frac{1}{2}(kd\cos\theta + \beta)}}{2} + e^{+j\frac{1}{2}(kd\cos\theta + \beta)} \right]$$

$$AF(\theta) = 2e^{j\frac{1}{2}(kd\cos\theta + \beta)} \cos[\frac{1}{2}(kd\cos\theta + \beta)]$$

which in normalized form can be written as

$$(AF)_n = \cos[\frac{1}{2}(kd\cos\theta + \beta)]$$

a.  $\beta = -kd = -\frac{2\pi}{\lambda} \left( \frac{\lambda}{4} \right) = -\frac{\pi}{2}$ .

b. For  $d = \lambda/4$ ,  $(AF)_n = \cos[\frac{\pi}{4}(\cos\theta - 1)]$

c.  $(AF)_n|_{\max} = 1 = \cos[\frac{\pi}{4}(\cos\theta_m - 1)] \Rightarrow \theta_m = 0^\circ$

$$(AF)_n = 0.707 = \cos[\frac{\pi}{4}(\cos\theta_h - 1)] \Rightarrow \frac{\pi}{4}(\cos\theta_h - 1) = \cos^{-1}(0.707) = \begin{cases} +\frac{\pi}{4} \\ -\frac{\pi}{4} \end{cases}$$

For  $+\pi/4 \Rightarrow \cos\theta_h - 1 = 1 \Rightarrow \cos\theta_h = 2 \Rightarrow \theta_h = \cos^{-1}(2) \Rightarrow$  Does not exist

For  $-\pi/4 \Rightarrow \cos\theta_h - 1 = -1 \Rightarrow \cos\theta_h = 0 = \theta_h = \cos^{-1}(0) = 90^\circ = \frac{\pi}{2}$  radians

Therefore  $\theta_{1r} = \theta_{2r} = 2(\frac{\pi}{2} - \theta) = \pi$

$$\text{and } D_0 \simeq \frac{4\pi}{\theta_{1r}\theta_{2r}} = \frac{4\pi}{(\pi)^2} = \frac{4}{\pi} = 1.273 = 1.049 \text{ dB}$$



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Q. Repeat the design of above problem so that its only maximum occurs along  $\theta = 180$  degrees.

a.  $\beta = +kd = +\frac{\pi}{2}$

b.  $(AF)_n = \cos\left[\frac{\pi}{4}(\cos\theta + 1)\right]$

$$(AF)_n|_{\max} = 1 = \cos\left[\frac{\pi}{4}(\cos\theta_m + 1)\right] \Rightarrow \theta_m = 180^\circ = \pi \text{ radians}$$

$$(AF)_n = 0.707 = \cos\left(\frac{\pi}{4}(\cos\theta_h + 1)\right) \Rightarrow \theta_h = 90^\circ = \frac{\pi}{2} \text{ radians}$$

$$\Theta_{1r} = \Theta_{2r} = 2\left(\pi - \frac{\pi}{2}\right) = \pi$$

and

$$D_0 \simeq \frac{4\pi}{\pi^2} = \frac{4}{\pi} = 1.273 = 1.049 \text{ dB}$$



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- Q. Design a four-element ordinary end-fire array with the elements placed along the z-axis a distance  $d$  apart with a maximum array factor directed towards  $\theta = 0$  deg. For a spacing of  $d = \lambda/2$  between the elements find the
- (a) progressive phase excitation between the elements to accomplish this
  - (b) angles (in degrees) where the nulls of the array factor occur
  - (c) angles (in degrees) where the maximum of the array factor occur
  - (d) beamwidth (in degrees) between the first nulls of the array factor
  - (e) directivity (in dB) of the array factor



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a.  $\beta = -kd = -\frac{2\pi}{\lambda} \left(\frac{\lambda}{2}\right) = -\pi = -180^\circ$

b.  $\theta_n = \cos^{-1} \left[ 1 - \frac{n\lambda}{Nd} \right] = \cos^{-1} \left( 1 - \frac{n\lambda}{4\lambda_2} \right) = \cos^{-1} \left( 1 - \frac{n}{2} \right), n=1, 2, 3, \dots, n \neq 4, 8, \dots$

$n=1 : \theta_1 = \cos^{-1}(1/2) = 60^\circ$

$n=2 : \theta_2 = \cos^{-1}(0) = 90^\circ$

$n=3 : \theta_3 = \cos^{-1}(-1/2) = 120^\circ$

c.  $\theta_m = \cos^{-1} \left( 1 - m\lambda/d \right) = \cos^{-1} \left( 1 - m\lambda/\lambda_2 \right) = \cos^{-1} \left( 1 - 2m \right), m=0, 1, 2, \dots$

$m=0 : \theta_0 = \cos^{-1}(1) = 0^\circ$

$m=1 : \theta_1 = \cos^{-1}(-1) = 180^\circ$

d.  $\Theta_0 = 2\cos^{-1} \left( 1 - \frac{\lambda}{Nd} \right) = 2\cos^{-1} \left( 1 - \frac{\lambda}{4\lambda_2} \right) = 2\cos^{-1} \left( 1 - \frac{1}{2} \right) = 2\cos^{-1} \left( \frac{1}{2} \right) = 2(60^\circ)$   
 $\Theta_0 = 120^\circ$

e.  $D_0 = 4N \left( \frac{d}{\lambda} \right) = 4(4) \left( \frac{\lambda/2}{\lambda} \right) = 8 = 9.03 \text{ dB}$



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- Q. Design an ordinary end-fire uniform linear array with only one maximum so that its directivity is 20 dB (above isotropic). The spacing between the elements is  $\lambda/4$ , and its length is much greater than the spacing. Determine the
- (a) number of elements
  - (b) overall length of the array (in wavelengths)
  - (c) approximate half-power beamwidth (in degrees)
  - (d) amplitude level (compared to the maximum of the major lobe) of the first minor lobe (in dB)
  - (e) progressive phase shift between the elements (in degrees).



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a.  $D_o = 4N \left(\frac{d}{\lambda}\right)$

$$20 = 10 \log_{10} D_o \text{ (dimensionless)} \Rightarrow D_o \text{ (dimensionless)} = 10^2 = 100$$

$$100 = 4N \left(\frac{\lambda}{4\lambda}\right) = N \Rightarrow N = 100$$

b.  $L = 99 \left(\frac{\lambda}{4}\right) = \frac{99}{4} \lambda = 24.75 \lambda$

$$\begin{aligned} c. \quad \Theta_{3dB} &= \Theta_h = 2 \cos^{-1} \left( 1 - \frac{1.391 \lambda}{Nd\pi} \right) \Big|_{n=100} = 2 \cos^{-1} \left( 1 - \frac{1.391 \lambda}{\pi \left(\frac{\lambda}{4}\right) 100} \right) \\ &= 2 \cos^{-1} \left( 1 - \frac{1.391 (4)}{100 \pi} \right) = 2 \cos^{-1} (1 - 0.01771) = 2 \cos^{-1} (0.98228) \end{aligned}$$

$$\Theta_h = 2(10.799) = 21.598^\circ \approx 21.6^\circ$$

d. Sidelobe (dB)  $\approx -13.5$  dB

e.  $\beta = \pm kd = \pm \frac{2\pi}{\lambda} \left(\frac{\lambda}{4}\right) = \pm \frac{\pi}{2} = \pm 90^\circ$



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- Q. Redesign the end-fire uniform array of above problem in order to increase its directivity while maintaining the same, as in the problem, uniformity, number of elements, spacing between them, and end-fire radiation.
- (a) What different from the design of the problem are you going to do to achieve this? Be very specific, and give values.
  - (b) By how many decibels (maximum) can you increase the directivity, compared to the design of the problem?
  - (c) Are you expecting the half-power beamwidth to increase or decrease? Why increase or decrease and by how much?
  - (d) What antenna figure of merit will be degraded by this design? Be very specific in naming it, and why is it degraded?

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a. Choose different phase excitation. That is

$$\beta = \pm \left( kd + \frac{2.94}{N} \right) \approx \pm \left( kd + \frac{\pi}{N} \right)$$

$$\beta = \pm \left( \frac{2\pi}{\lambda/4} + \frac{2.94}{100} \right) = \pm \left( \frac{\pi}{2} + 0.0294 \right) = \pm (1.570796 + 0.0294) = \pm (1.6) = \pm 91.684^\circ$$

b. Directivity increase by 1.789 factor = 2.526 dB

c. The HPBW will decrease because sidelobe level will increase.

$$\theta_h = 2 \cos^{-1} \left( 1 - \frac{0.1398 \lambda}{Nd} \right) = 2 \cos^{-1} \left( 1 - \frac{0.1398 \lambda}{100 \lambda/4} \right) = 2 \cos^{-1} \left( 1 - \frac{0.1398(4)}{100} \right)$$

$$= 2 \cos^{-1} (1 - 0.005592) = 2 \cos^{-1} (0.9944) = 2 (6.066^\circ) = 12.13^\circ$$

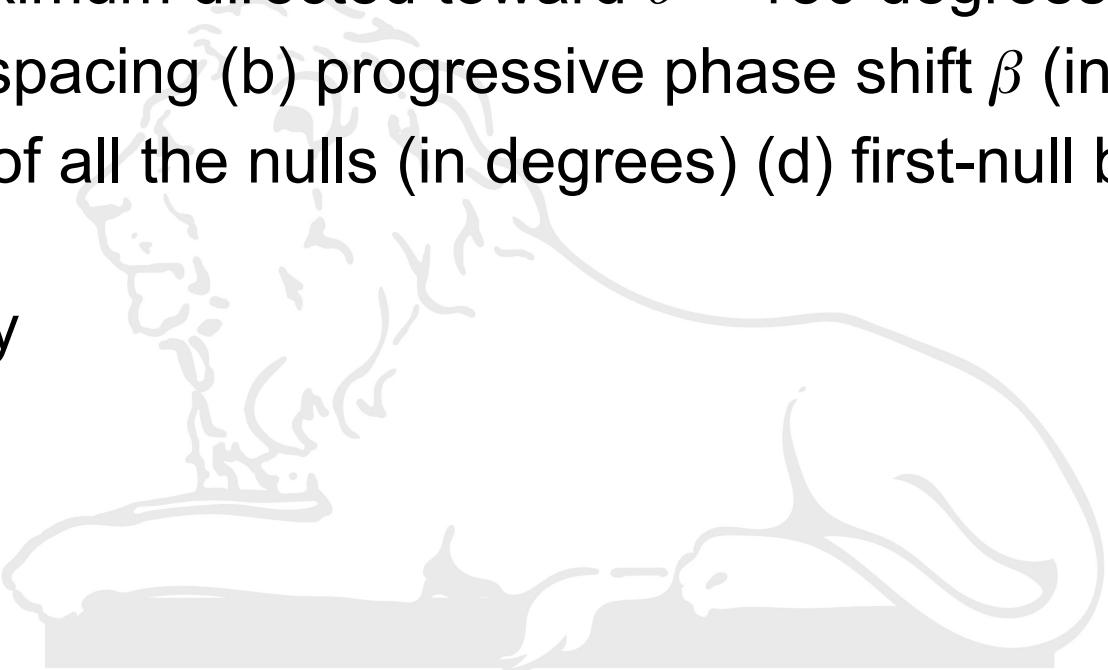
decreased by  $9.47^\circ$

d. Sidelobe level will increase. It will be higher than  $-13.5 \text{ dB}$

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Q. Ten isotropic elements are placed along the z-axis. Design a Hansen-Woodyard end-fire array with the maximum directed toward  $\theta = 180$  degrees. Find the:

- (a) desired spacing (b) progressive phase shift  $\beta$  (in radians)
- (c) location of all the nulls (in degrees) (d) first-null beamwidth (in degrees)
- (e) directivity



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a.  $d = \left(\frac{N-1}{N}\right) \frac{\lambda}{4} = 0.225 \lambda$

b.  $\beta = kd + \frac{2.94}{10} = 2\pi(0.225) + 0.294 = 1.7077 \text{ rad}$

c.  $\theta_n = \cos^{-1}(1 + (1-2n) \frac{\lambda}{2dN})$

$$\theta_n = \cos^{-1}(1 + (1-2n) \frac{1}{4.5})$$

$$\theta_1 = \cos^{-1}(0.777) = 38.9^\circ, \quad \theta_2 = \cos^{-1}(0.333) = 70.53^\circ,$$

$$\theta_3 = \cos^{-1}(-0.111) = 96.38^\circ, \quad \theta_4 = \cos^{-1}(-0.555) = 123.7^\circ.$$

d. First null Beamwidth

$$\theta_n = 2 \cos^{-1}\left(1 - \frac{\lambda}{2dN}\right) = 2 \cos^{-1}\left(1 - \frac{1}{2(0.225) \cdot 10}\right) = 77.88^\circ$$

e.  $D_o = 1.789 \left[ 4N \cdot \left( \frac{d}{\lambda} \right) \right] = 1.789 [4 \cdot 10 \cdot (0.225)] = 16.101 = 12.068 \text{ dB}$



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Q. A uniform array of 20 isotropic elements is placed along the z-axis a distance  $\lambda/4$  apart with a progressive phase shift of  $\beta$  rad. Calculate  $\beta$  (give the answer in radians) for the following array designs:

- (a) broadside
- (b) end-fire with maximum at  $\theta = 0^\circ$
- (c) end-fire with maximum at  $\theta = 180^\circ$
- (d) phased array with maximum aimed at  $\theta = 30^\circ$
- (e) Hansen-Woodyard with maximum at  $\theta = 0^\circ$
- (f) Hansen-Woodyard with maximum at  $\theta = 180^\circ$



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$$kd = \frac{2\pi}{\lambda} \frac{\lambda}{4} = \frac{\pi}{2}$$

- a.  $\beta = 0$  radians
- b.  $\beta = -\pi/2$
- c.  $\beta = +\pi/2$
- d.  $\beta = -1.36 = -\frac{\sqrt{3}}{4}\pi = -0.433\pi$
- e.  $\beta = -(\frac{\pi}{2} + 0.147)$  or  $-(\frac{\pi}{2} + 0.157) = -\frac{11}{20}\pi = -1.72$
- f.  $\beta = +(\frac{\pi}{2} + 0.147)$  or  $+(\frac{\pi}{2} + 0.157) = \frac{11}{20}\pi = 1.72$



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Q. For a uniform broadside linear array of 10 isotropic elements, determine the approximate directivity (in dB) when the spacing between the elements is  
(a)  $\lambda/4$  (b)  $\lambda/2$  (c)  $3\lambda/4$  (d)  $\lambda$

$$D_o \approx 2N \left( \frac{d}{\lambda} \right)$$

a.  $d = \frac{\lambda}{4}$ ,  $D_o \approx 2 \cdot 10 \cdot \frac{1}{4} = 5 = 6.99 \text{ dB}$

Computer Program :  $D_o = 7.132 \text{ dB}$

b.  $d = \frac{\lambda}{2}$ ,  $D_o \approx 2 \cdot 10 \cdot \frac{1}{2} = 10 = 10 \text{ dB}$

Computer Program :  $D_o = 10.00 \text{ dB}$

c.  $d = \frac{3\lambda}{4}$ ,  $D_o \approx 2 \cdot 10 \cdot (0.75) = 15 = 11.76 \text{ dB}$

Computer Program :  $D_o = 11.624 \text{ dB}$

d.  $d = \lambda$ ,  $D_o \approx 2 \cdot 10 \cdot (1) = 20 = 13.0 \text{ dB}$

Computer Program :  $D_o = 10.011 \text{ dB}$

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Q. The maximum distance  $d$  between the elements in a linear scanning array to suppress grating lobes is

$$d_{\max} = \frac{\lambda}{1 + |\cos(\theta_0)|}$$

where  $\theta$  is the direction of the pattern maximum. What is the maximum distance between the elements, without introducing grating lobes, when the array is designed to scan to maximum angles of

- (a)  $\theta = 30^\circ$  (b)  $\theta = 45^\circ$  (c)  $\theta = 60^\circ$



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The recommended element spacing is

$$d = \frac{1}{1 + \cos\theta}, \text{ where } \theta \text{ is the scan angle in degrees}$$

a.  $\theta_0 = 30^\circ$

$$d = \frac{1}{1 + \cos 30^\circ} = 0.5359 \text{ wavelength}$$

b.  $\theta_0 = 45^\circ$

$$d = \frac{1}{1 + \cos 45^\circ} = \frac{1}{1 + 0.7071} = 0.58578 \text{ wavelength}$$

c.  $\theta_0 = 60^\circ$

$$d = \frac{1}{1 + \cos 60^\circ} = \frac{1}{1 + 0.5} = 0.6667 \text{ wavelength}$$

# **Thank You**

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## **Questions?**