

# The (Quantum ?) Physics of Electric Power Systems

Philippe Jacquod  
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UNIVERSITÉ  
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FACULTÉ DES SCIENCES

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School of Engineering  $\pi$

FNSNF

swissgrid

# Outline

- Electric power systems
- Operating steady-state : power flow equations
- Transient dynamics : swing equations

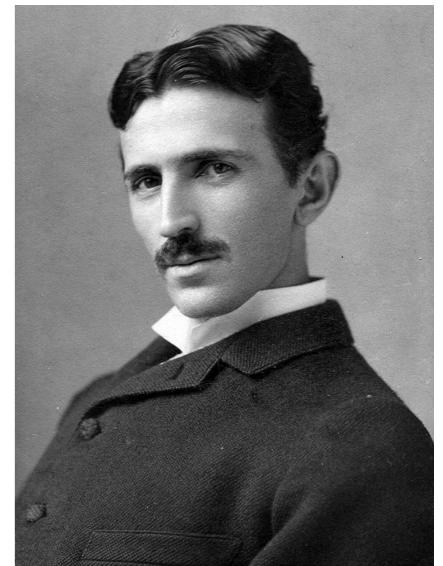
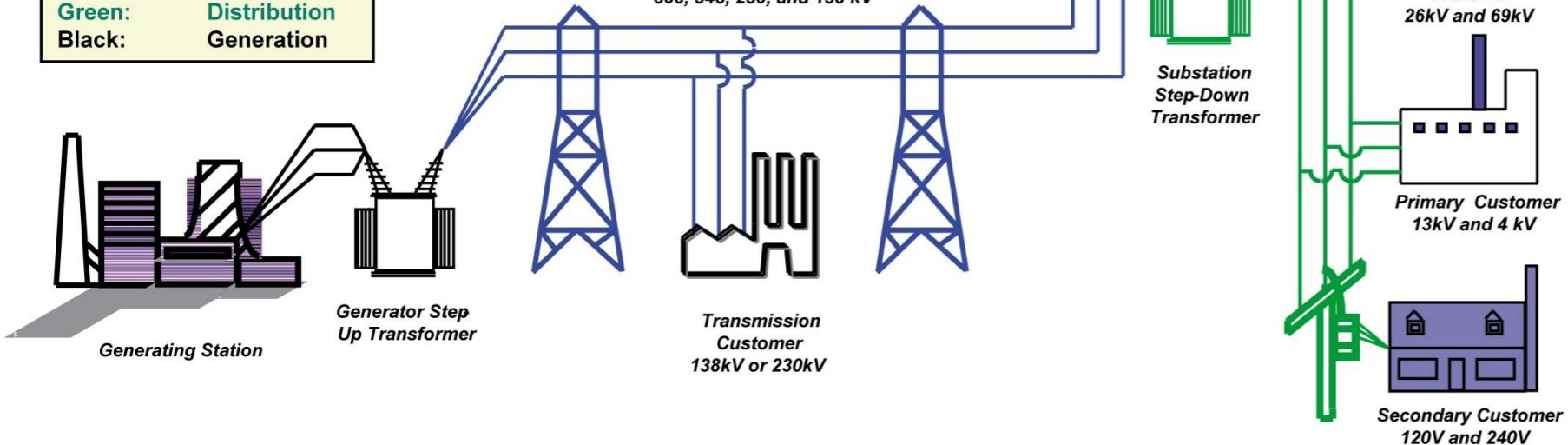
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# What are electric power systems ?

## Basic Structure of the Electric System

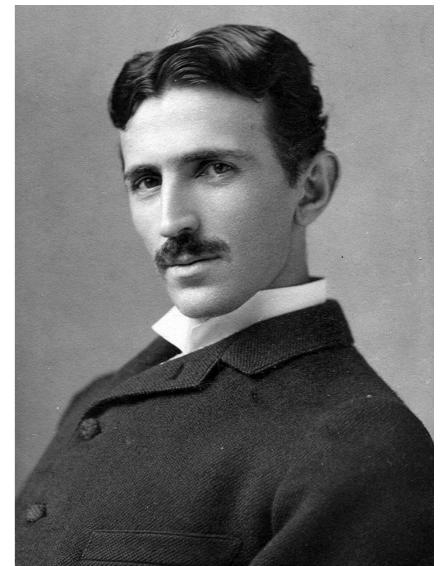
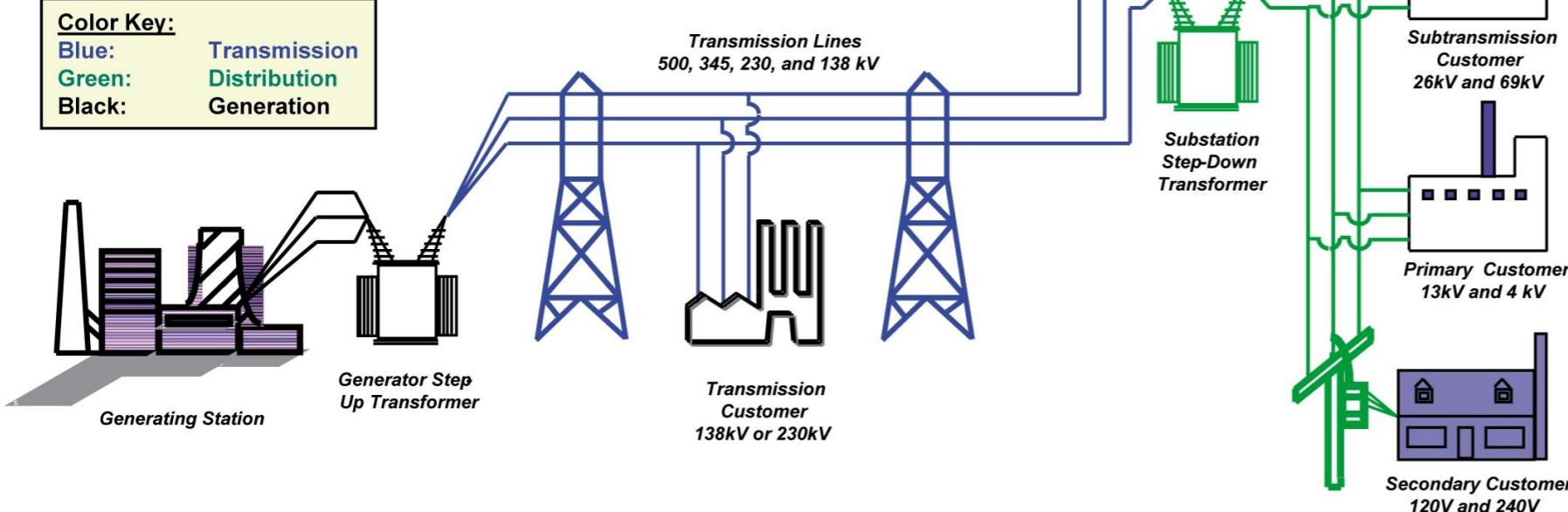
Color Key:	
Blue:	Transmission
Green:	Distribution
Black:	Generation



N Tesla 1856-1943

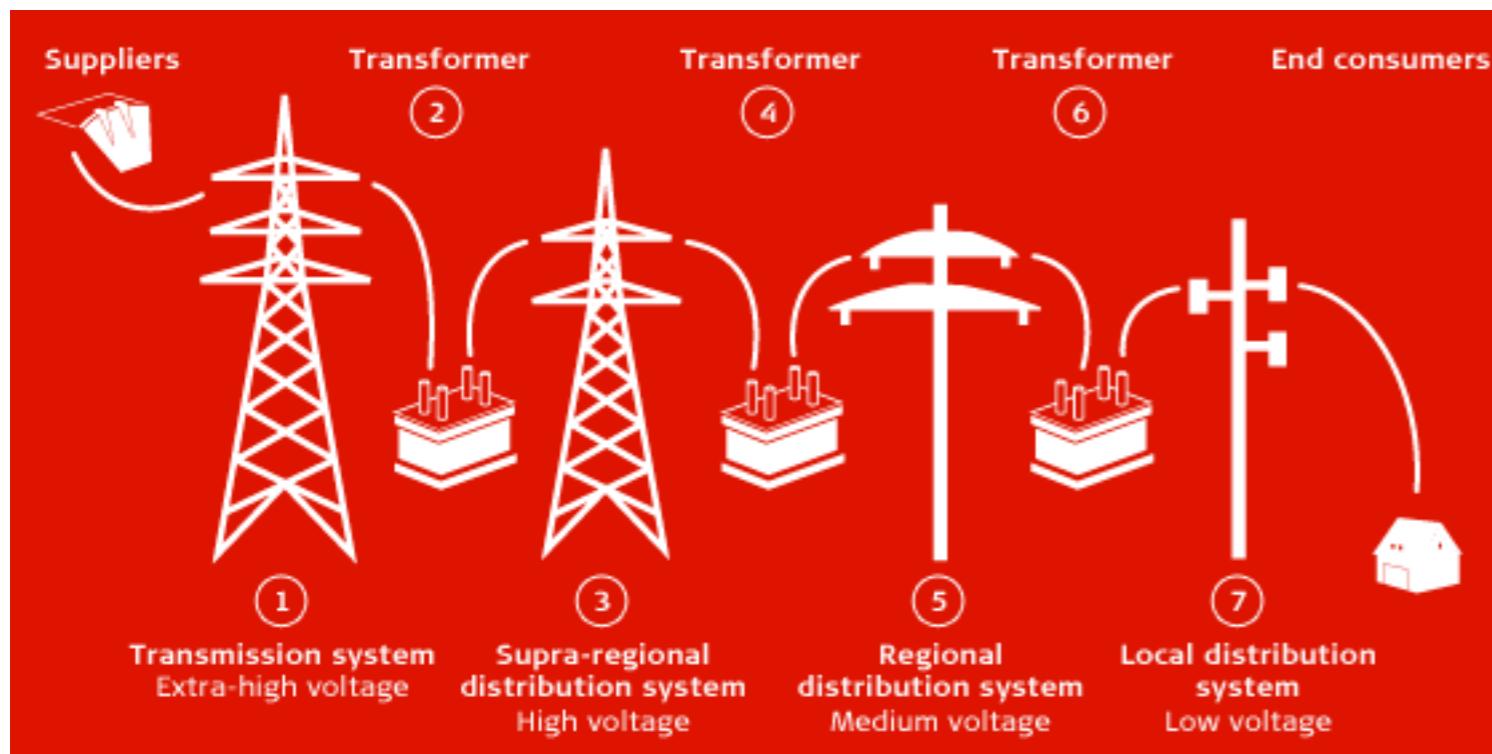
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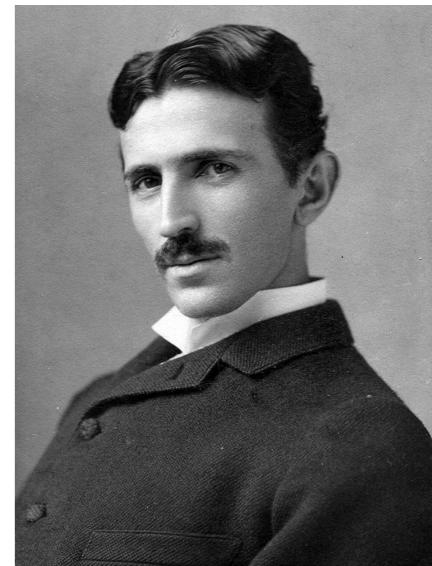
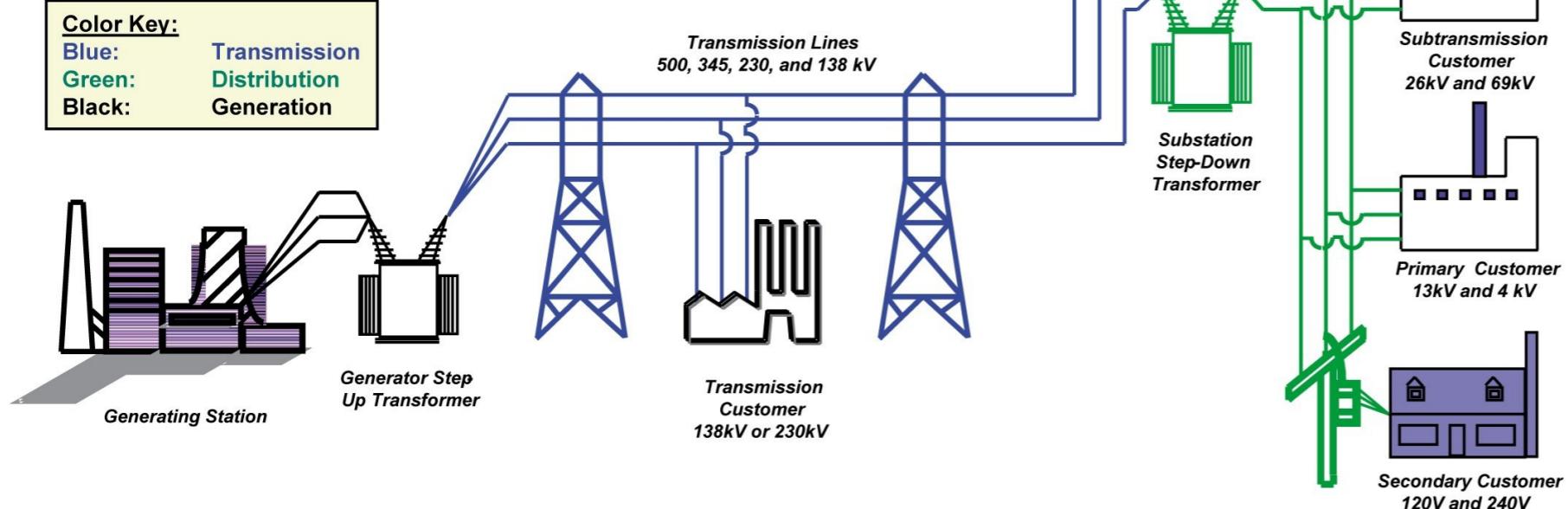
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## Seven levels of electric power systems



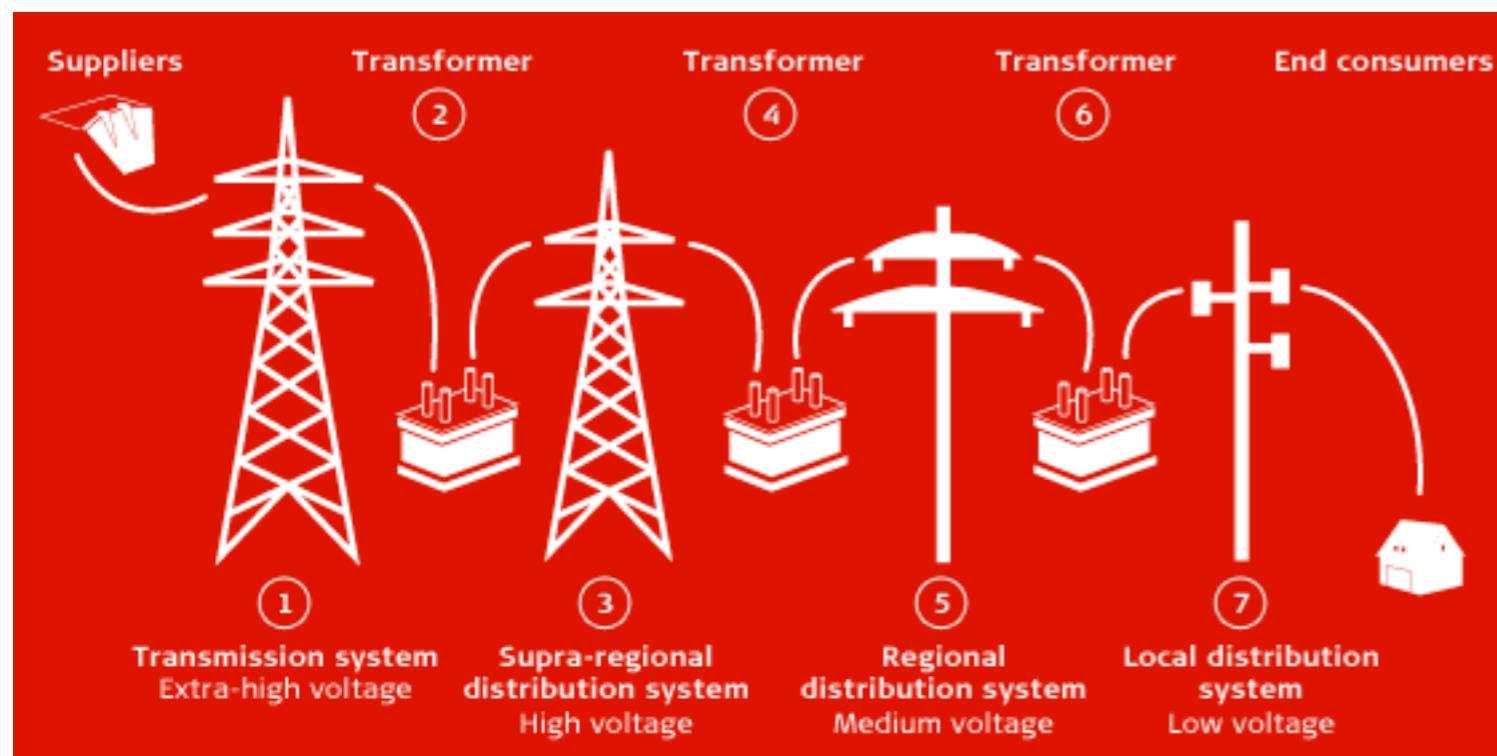
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N Tesla 1856-1943

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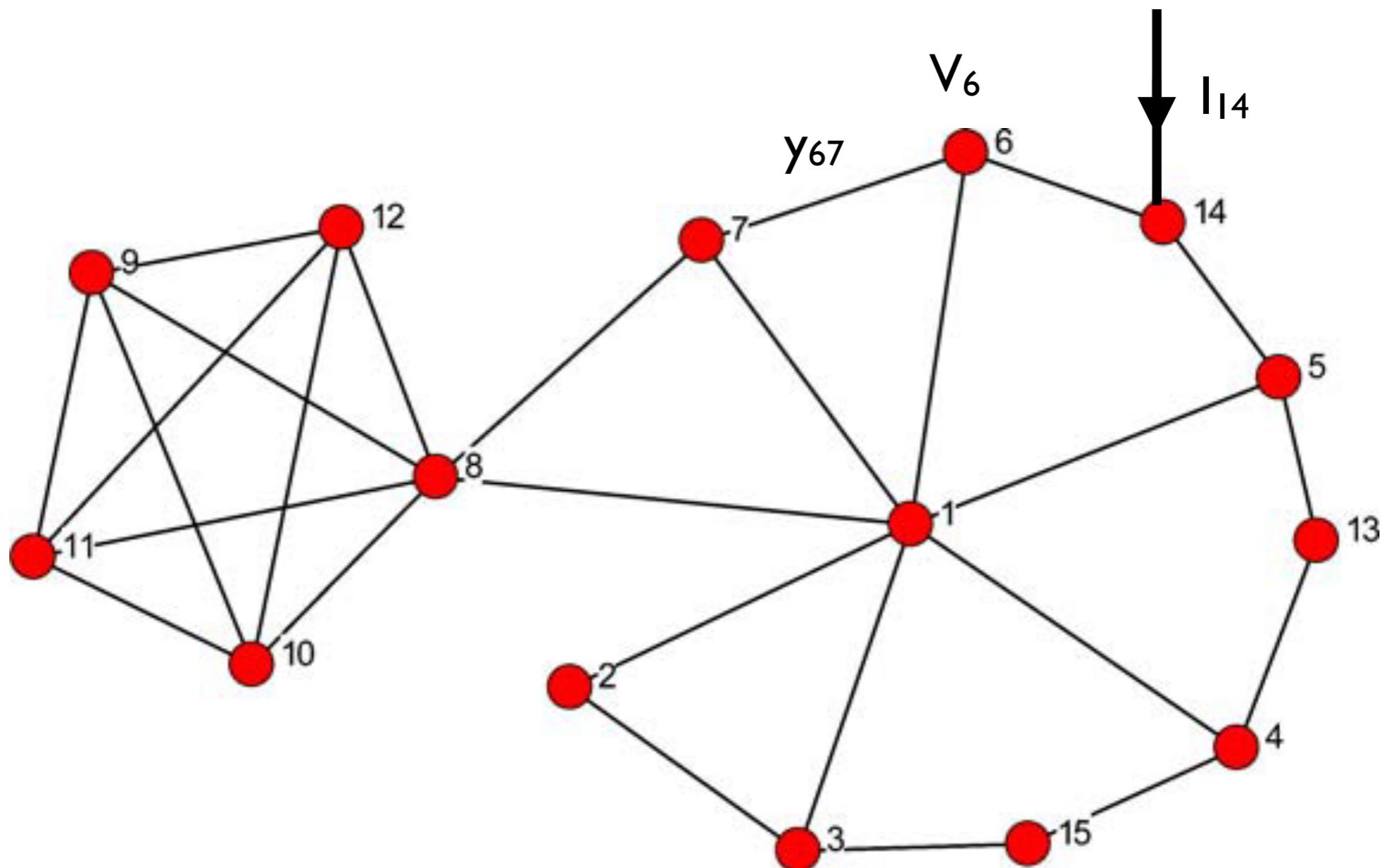
**Power :**  
\*conserved (~)  
\*control parameter  
“write Eq. for power”

# Operating steady-state of AC power grids

- Ohm's law

$$I_i = \sum_j Y_{ij} V_j$$

$I_i$  : current injected/collected at node i  
 $V_i$  : voltage at node i  
 $Y_{ij}$  : admittance matrix



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- Active power  
 $P = \text{Re}(S)$

finite time-average  
“truly transmitted”  
(injected and consumed)

vs.

reactive power  
 $Q = \text{Im}(S)$

zero time-average  
“oscillating in the circuit”

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## Power flow equations

$$P_i = \sum_j |V_i V_j| [G_{ij} \cos(\theta_i - \theta_j) + B_{ij} \sin(\theta_i - \theta_j)]$$
$$Q_i = \sum_j |V_i V_j| [G_{ij} \sin(\theta_i - \theta_j) - B_{ij} \cos(\theta_i - \theta_j)]$$

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Voltages at buses i and j      Conductance matrix      Voltage angles at buses i and j      Susceptance matrix

# Approximated power flow equations : very high voltage

- Admittance dominated by its imaginary part  
for large conductors  $\sim$  high voltage  
 $G/B < 0.1$  for 200kV and more

***neglect conductance*** →

$$P_i \simeq \sum_j |V_i V_j| B_{ij} \sin(\theta_i - \theta_j)$$

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- No conductance  $\sim$  no voltage drop

***consider constant voltage***

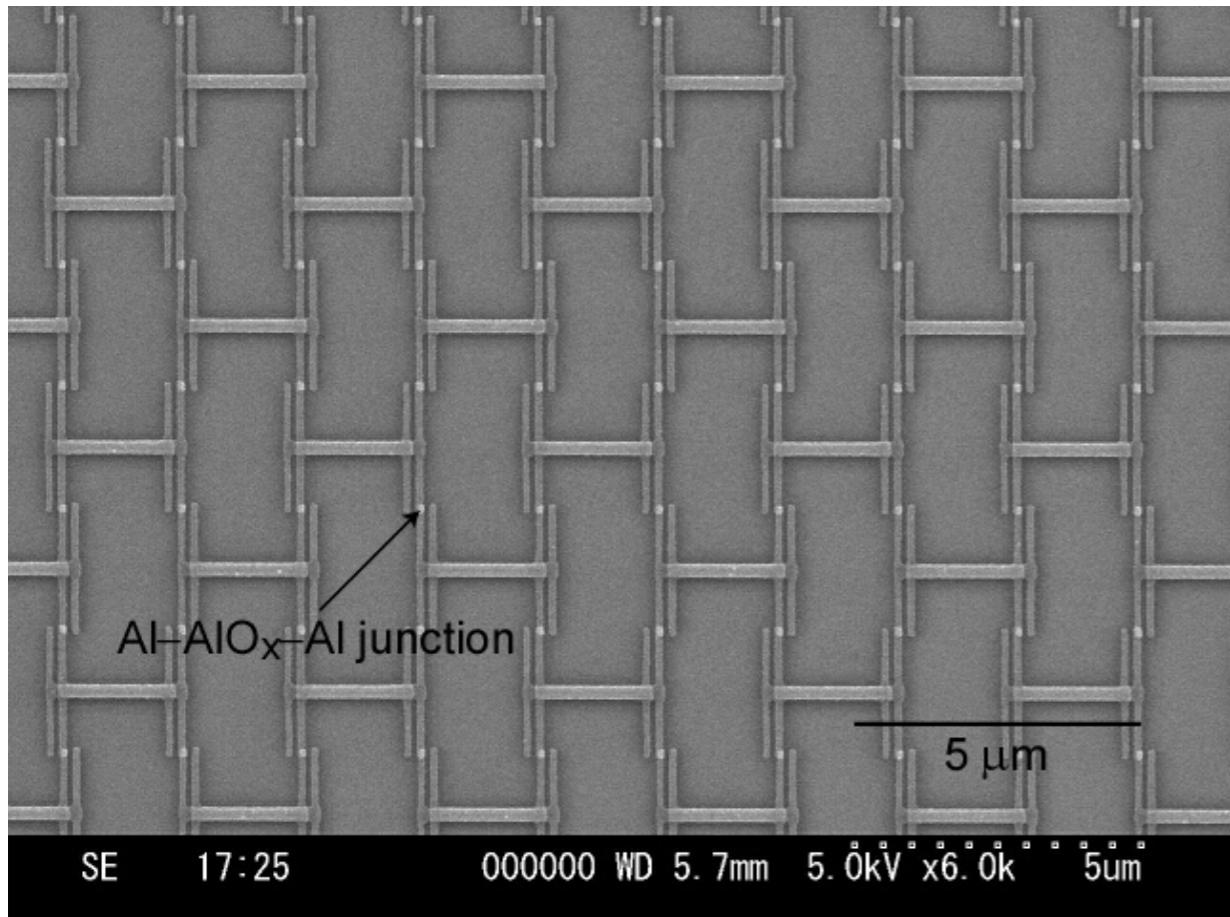
\*decoupling between P and Q

\*consider P only

(a.k.a. lossless line approx.) →

$$P_i = \sum_j B_{ij} \sin(\theta_i - \theta_j)$$

# Synchronous fixed points vs. Josephson junctions



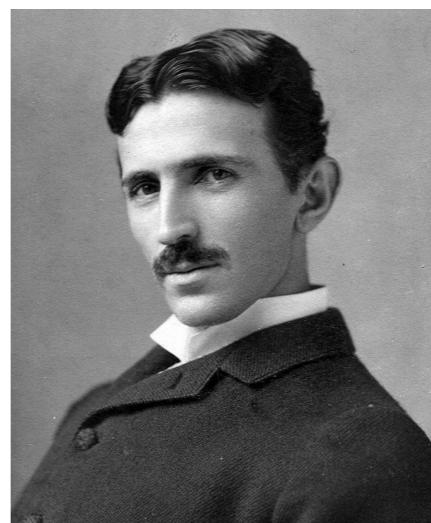
Josephson current

$$I_{ij} = I_c \sin(\theta_j - \theta_i)$$

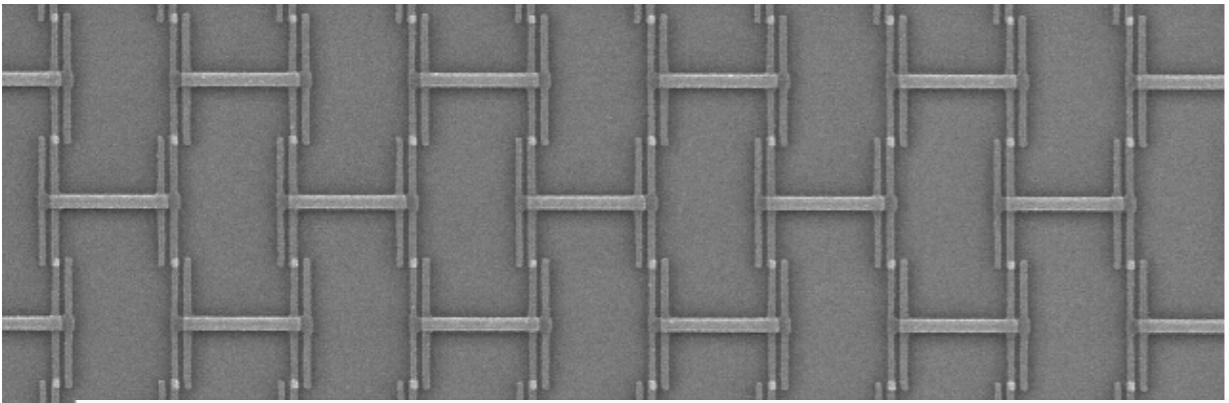


High voltage  
AC transmitted power

$$P_{ij} = B_{ij} \sin(\theta_i - \theta_j)$$



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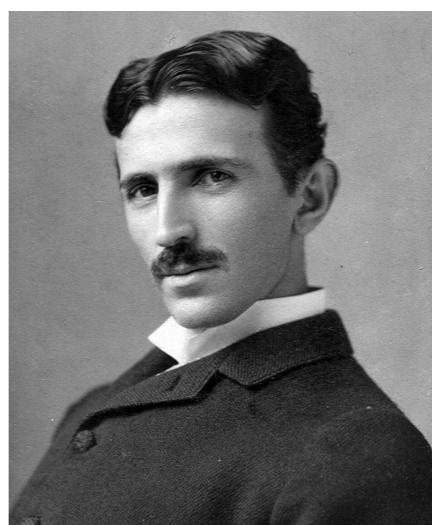
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# Circulating loop flows

\*Thm: Different solutions to the simplified power-flow problem

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may differ only by circulating loop current(s) **in any network**

Dörfler, Chertkov, Bullo, PNAS '13; Delabays, Coletta and PJ, JMP '16

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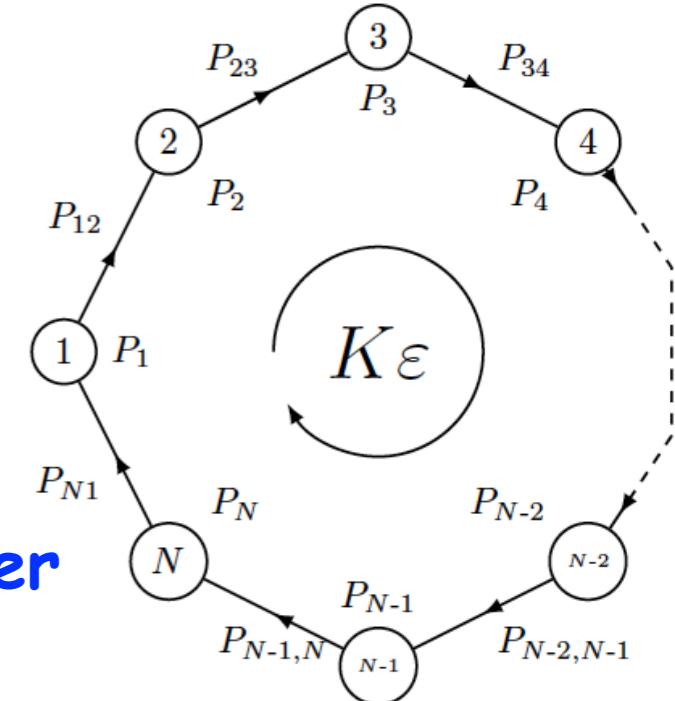
Dörfler, Chertkov, Bullo, PNAS '13; Delabays, Coletta and PJ, JMP '16

\*Voltage angle.  $V_i = |V_i|e^{i\theta_i}$  uniquely defined

→  $q = \sum_i |\theta_{i+1} - \theta_i|_{2\pi} / 2\pi \in \mathbb{Z}$  ~topological winding number

→ discretization of these loop currents ~vortex flows

Janssens and Kamagate '03; Delabays, Coletta and PJ, JMP '16; JMP '17



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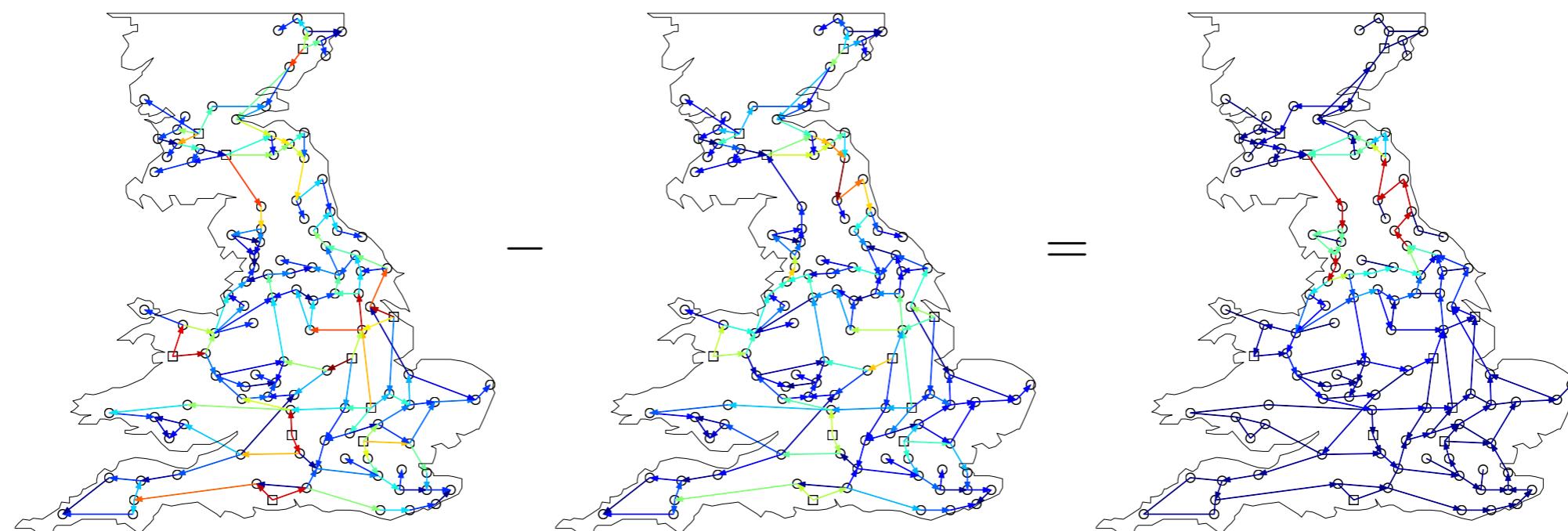
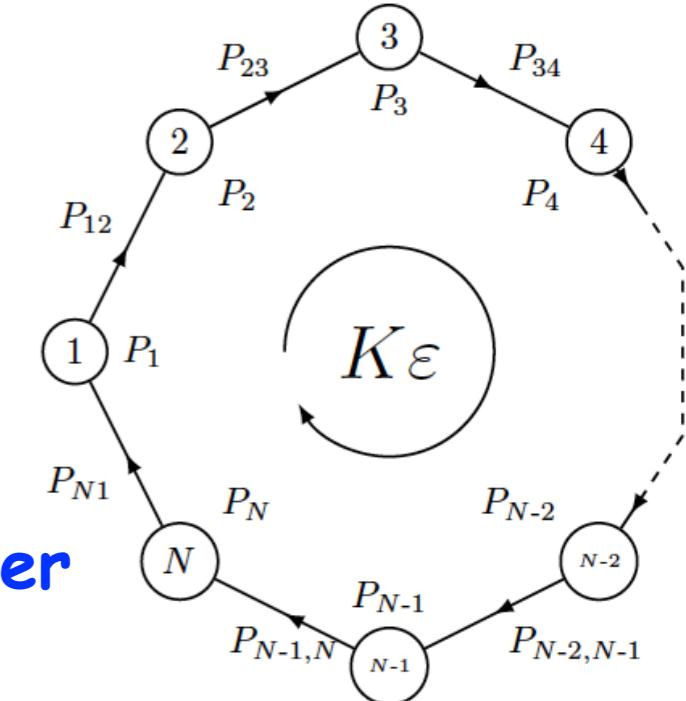
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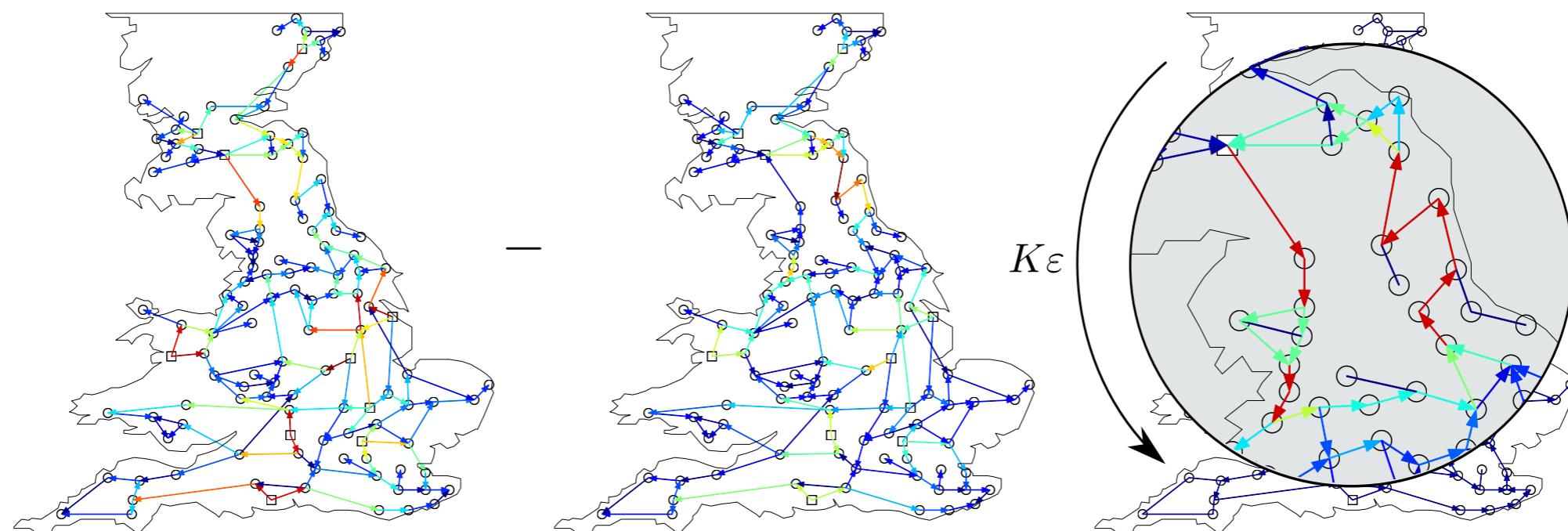
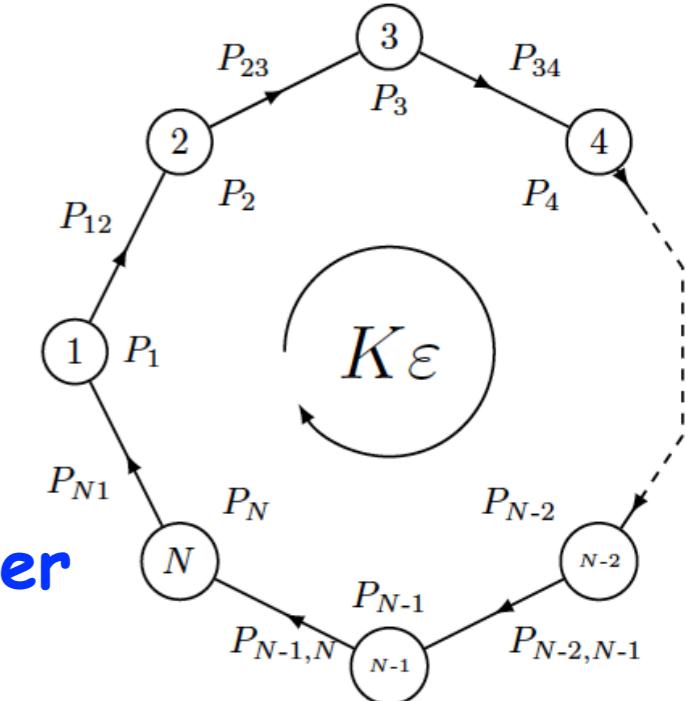
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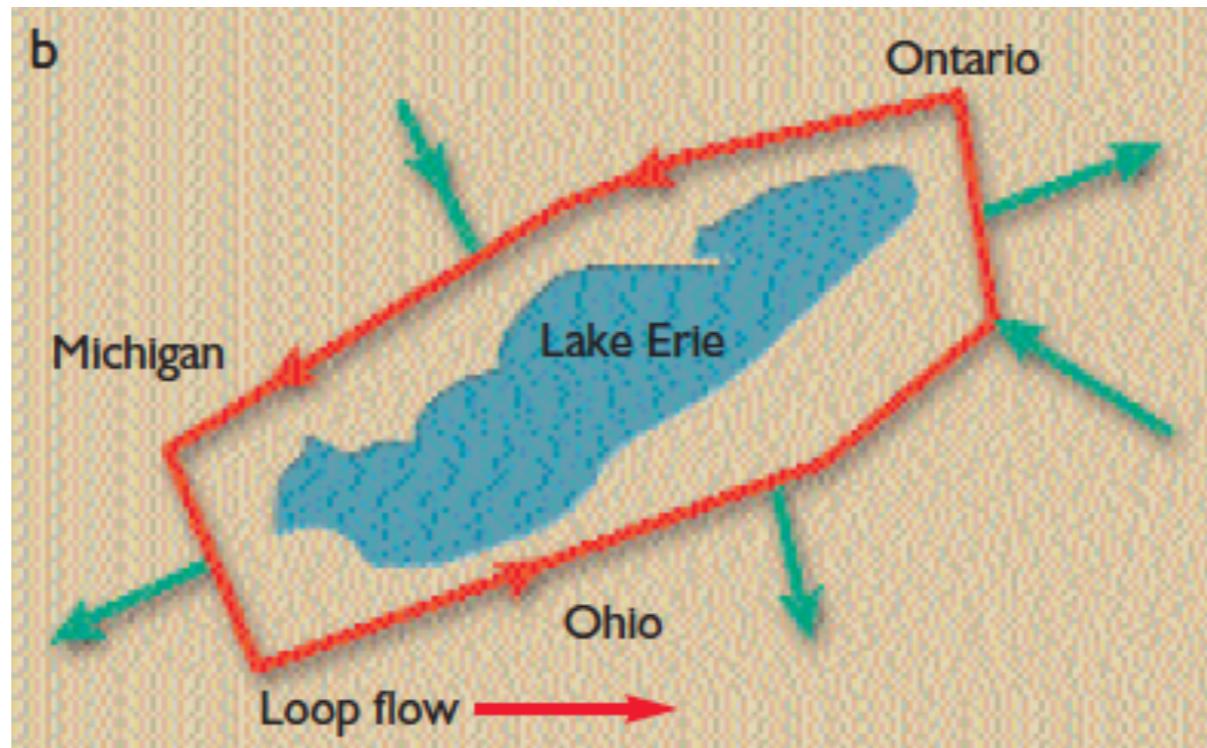
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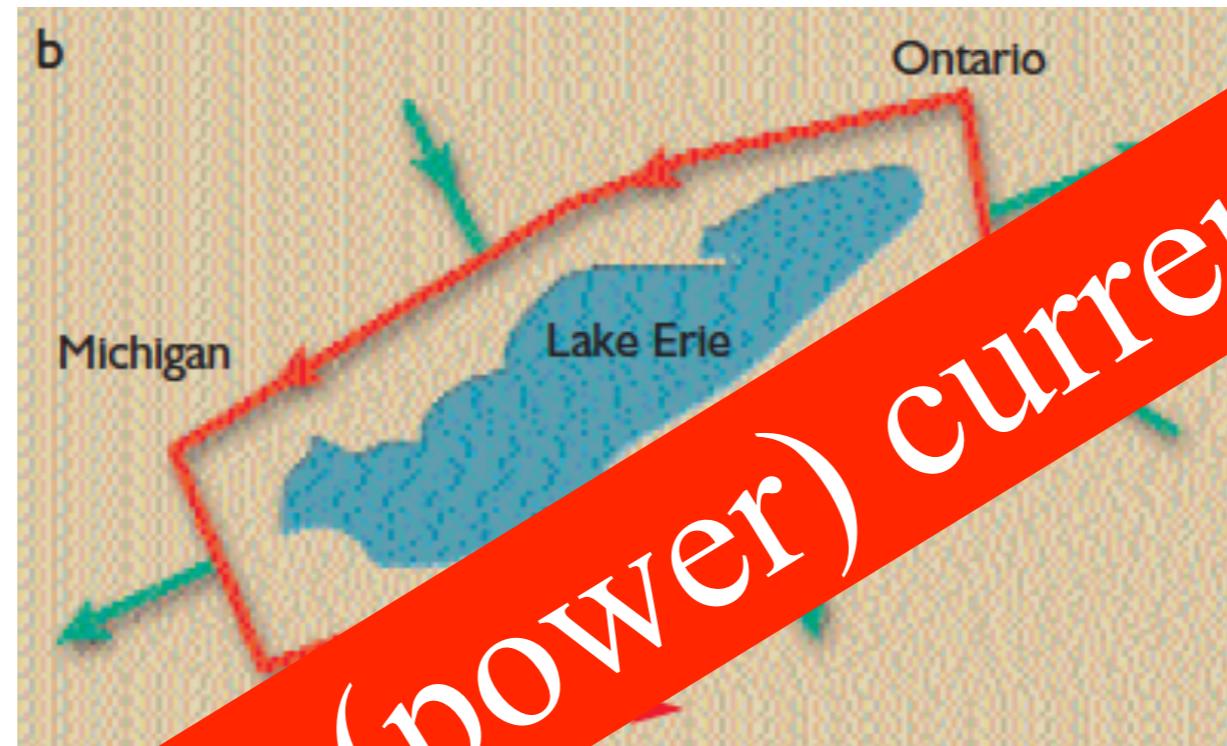


# Circulating loop flows



“Where the network jogs around large geographical obstacles, such as the Rocky Mountains in the West or the Great Lakes in the East, loop flows around the obstacle are set up that can drive as much as 1 GW of power in a circle, *taking up transmission line capacity without delivering power to consumers.*”

# Circulating loop flows



“Where the network is interconnected and large geographical obstacles, such as the Rocky Mountains in the West or the Great Lakes in the East, loop flows around the obstacle. Such loops can take power that can drive as much as 1 GW of power in a circle, *taking up transmission capacity without delivering power to consumers.*”

Persistent (power) current !

# Circulating loop flows

Different power flow solutions  
with different loop flows exist, but...

How do they appear ? how are they generated ?

# Circulating loop flows

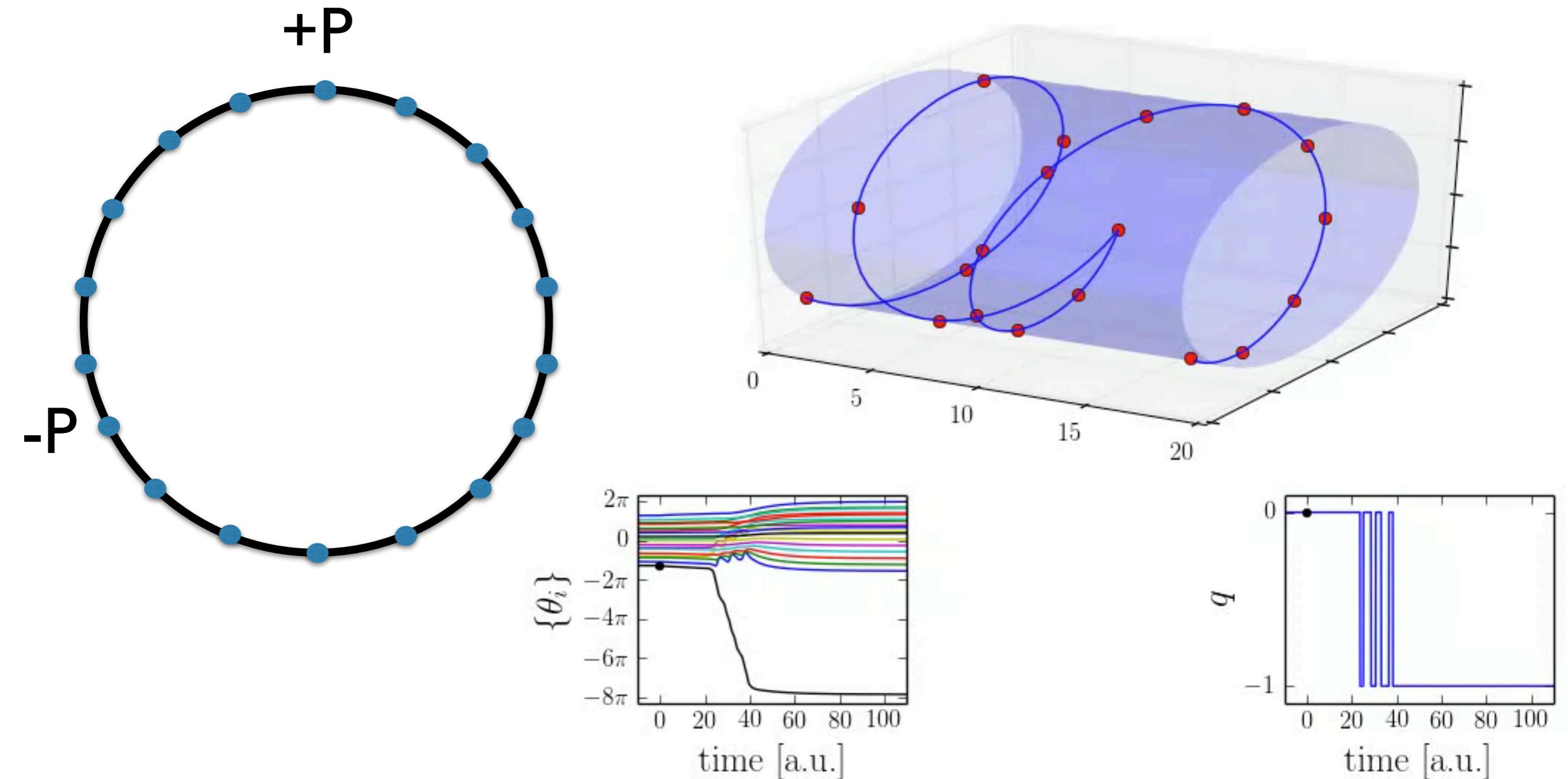
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Solution :

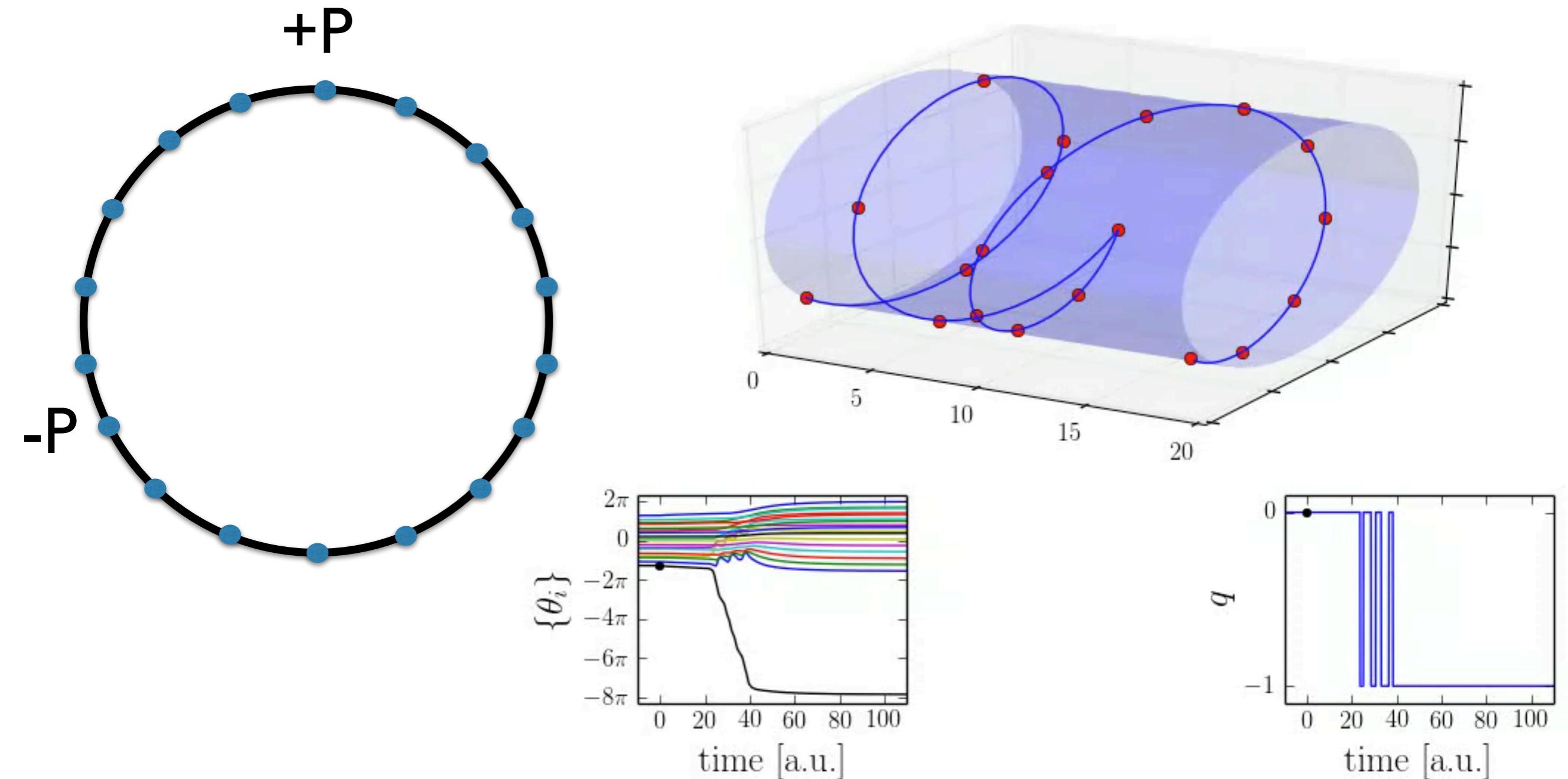
- (i) line tripping
- (ii) line tripping and reclosing
- (iii) dynamical phase slip
- (iv) fluctuating power injections

# Dynamical generation of vortex flows



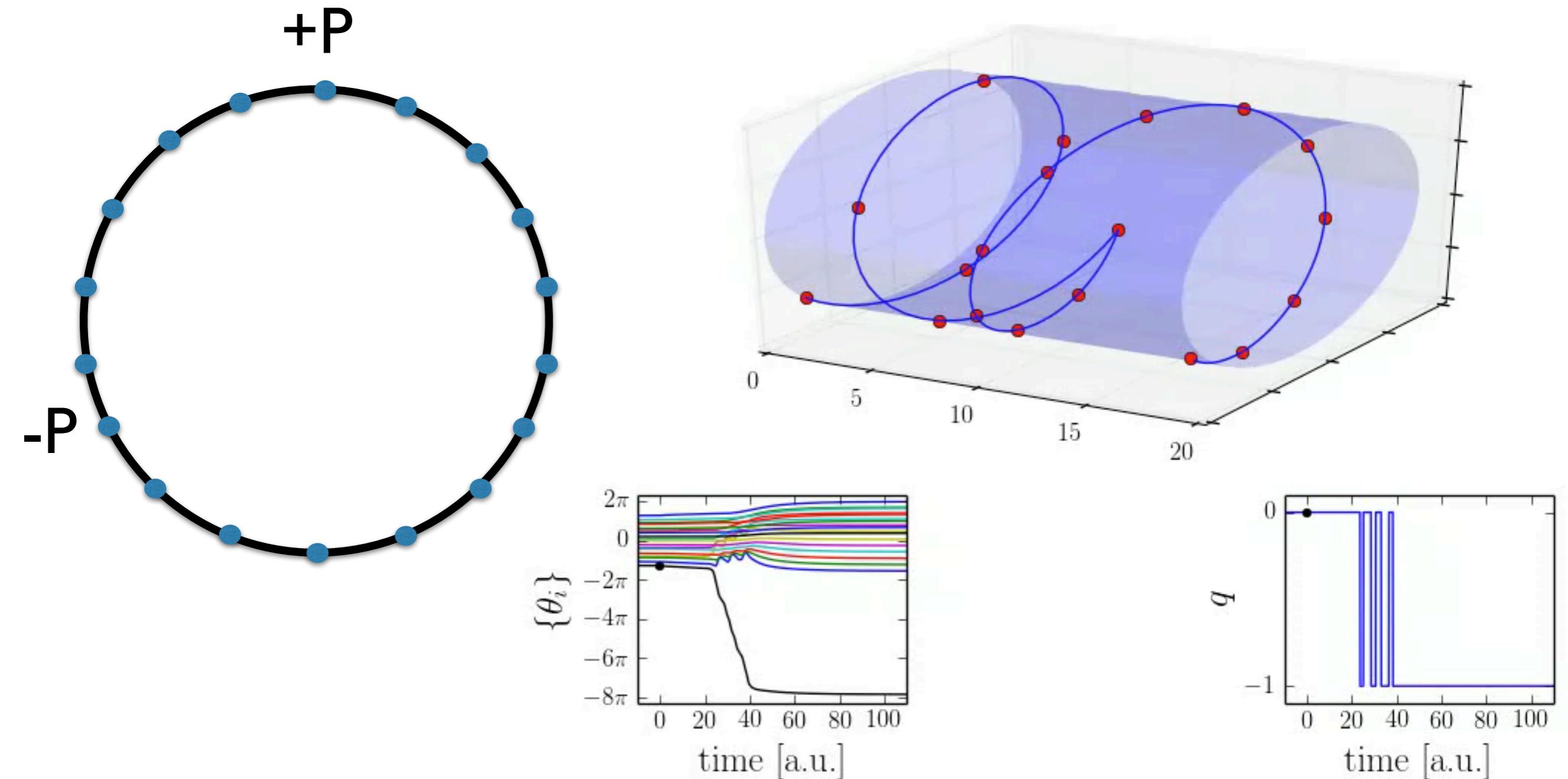
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Coletta, Delabays, Adagideli and PJ, New J Phys. '16

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Coletta, Delabays, Adagideli and PJ, New J Phys. '16

Similarity with quantum phase slips in small SC and JJ arrays

D. S. Golubev and A. D. Zaikin, '01

Lau, Markovic, Bockrath, Bezryadin and Tinkham '01

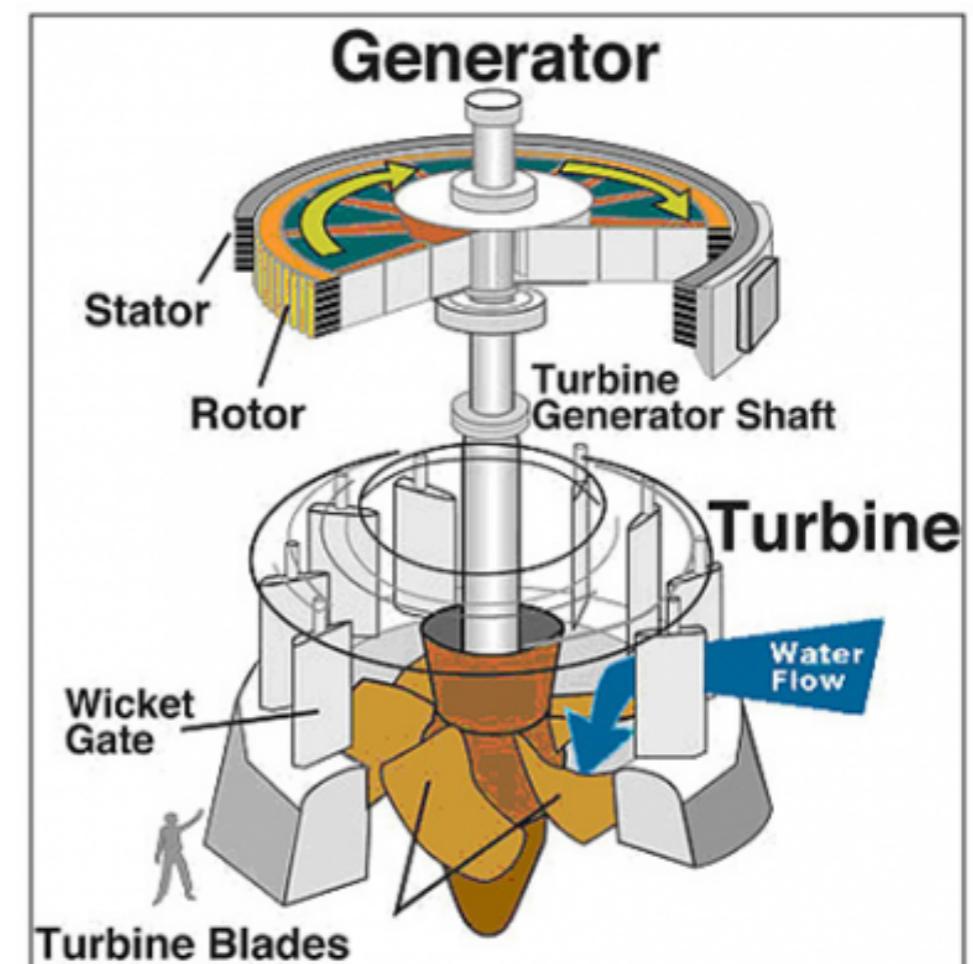
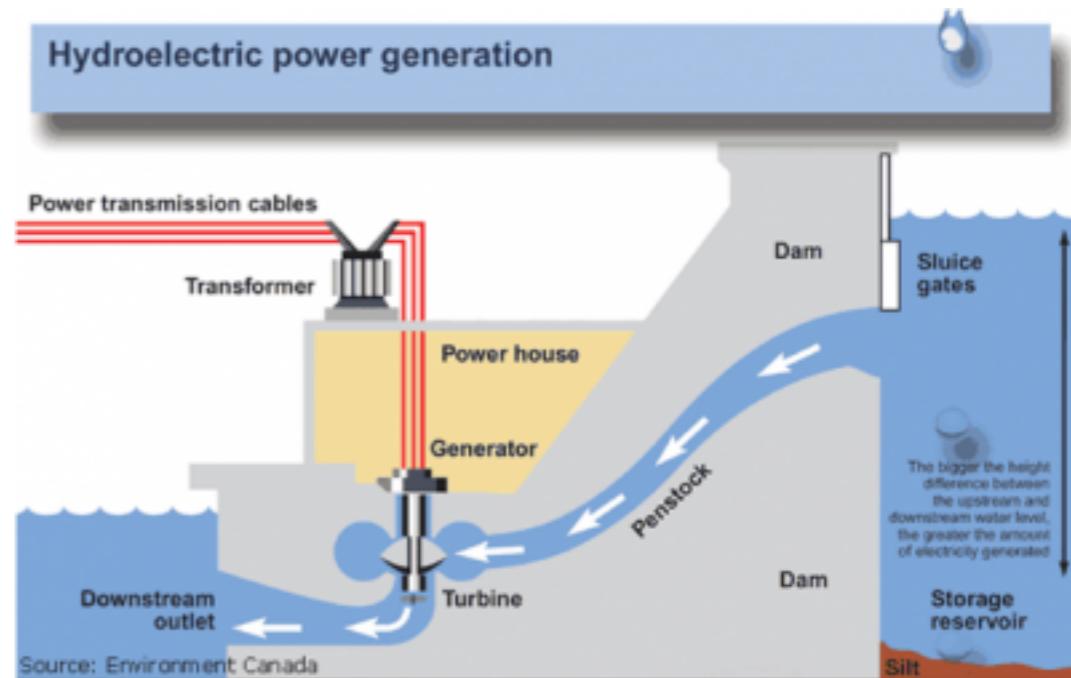
Matveev, Larkin and Glazman '02

# Outline

- Electric power systems
- Operating steady-state : power flow equations
- Transient dynamics : swing equations

# Dynamics of AC power grids

- Electricity production with rotating machines
- Potential, chemical, nuclear or thermal energy converted into mechanical energy (rotation)
- Mechanical energy converted into electric energy
- Time-dependence : think power instead of energy
- Balance between power in, power out and energy change in rotator : **SWING EQUATIONS**



# Today's (and yesterday's) AC power grids

Dynamics: Swing Equations.

- from few AC cycles to ~10-20 secs.
- In rotating frame @ 50/60 Hz

$$I_i \ddot{\theta}_i + D_i \dot{\theta}_i = P_i - \sum B_{ij} \sin(\theta_i - \theta_j)$$

- I : inertia ~ rot. kinetic energy
- D : damping from primary control

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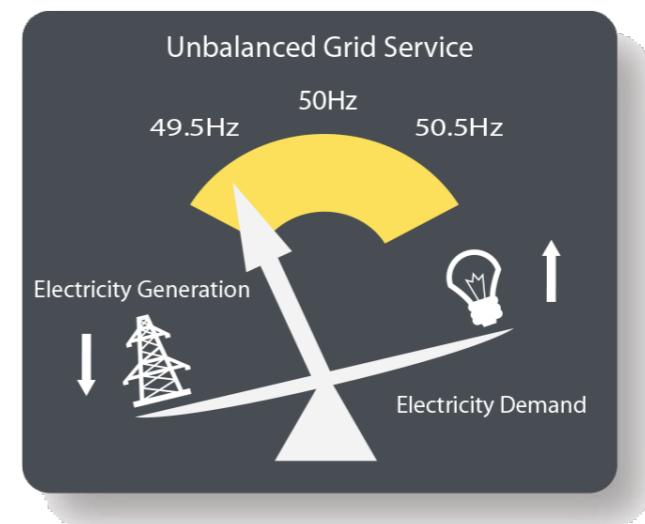
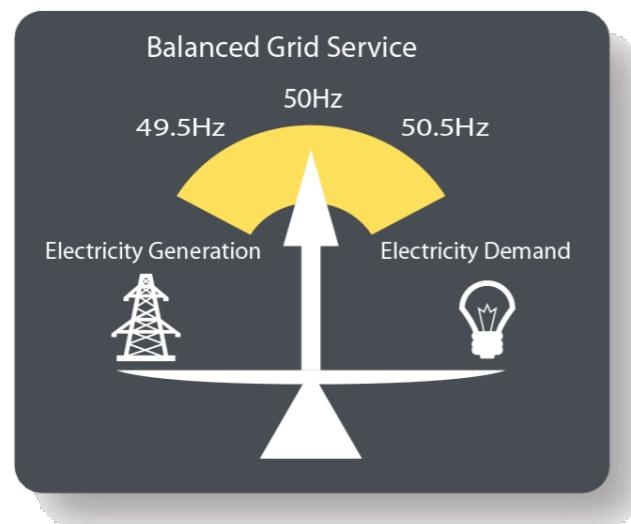
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- Coupling between power balance and frequency



figs. Taken from <http://northernutilities.co.uk>

**Change in kinetic energy = balance of power**

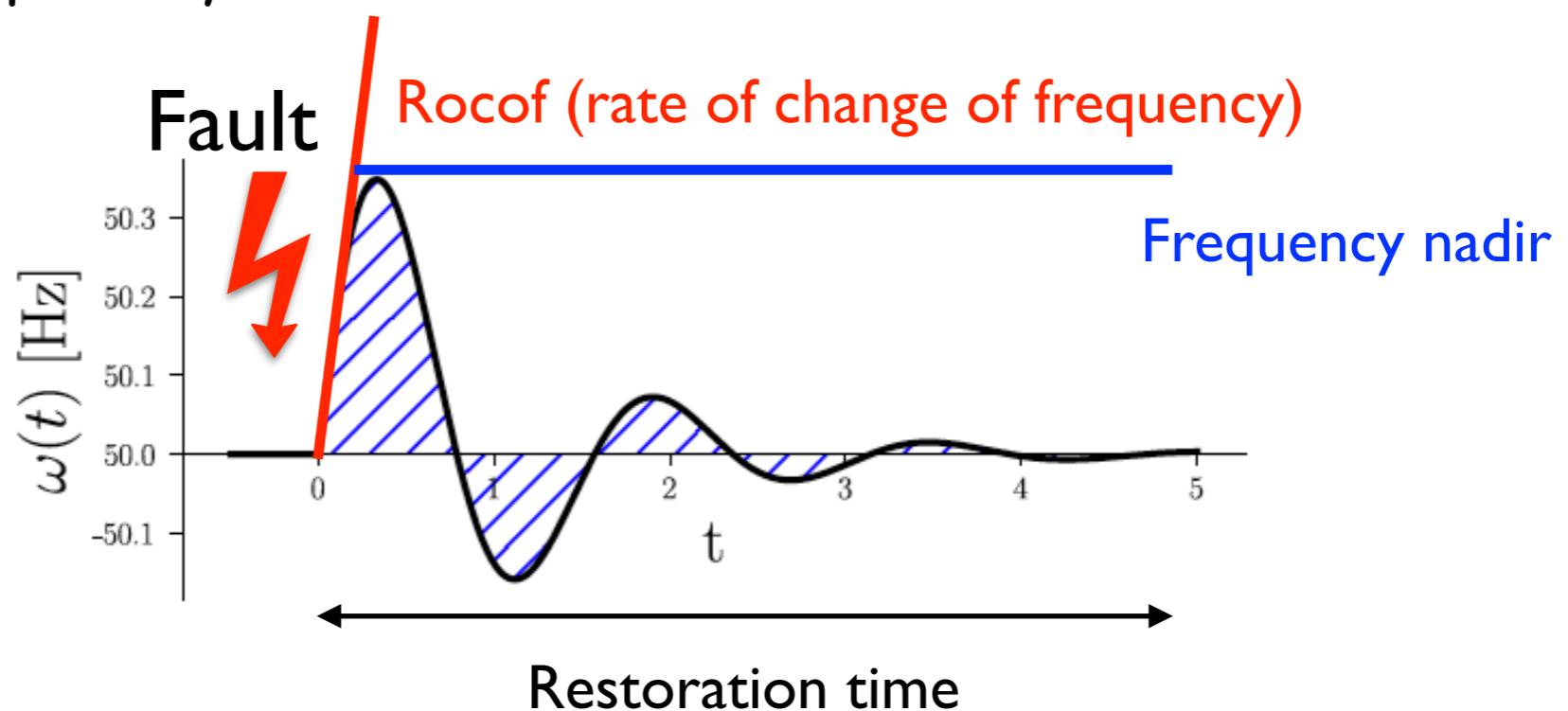
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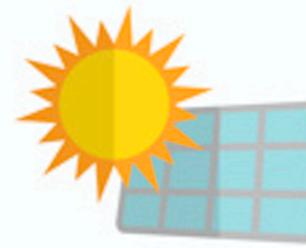
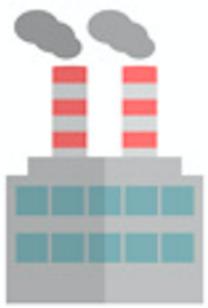
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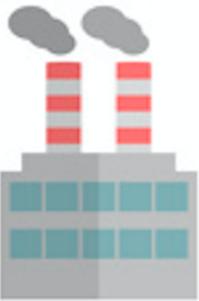


- Frequency transient as indicator of fault magnitude
- Frequency fluctuations need to be minimized... but how ?

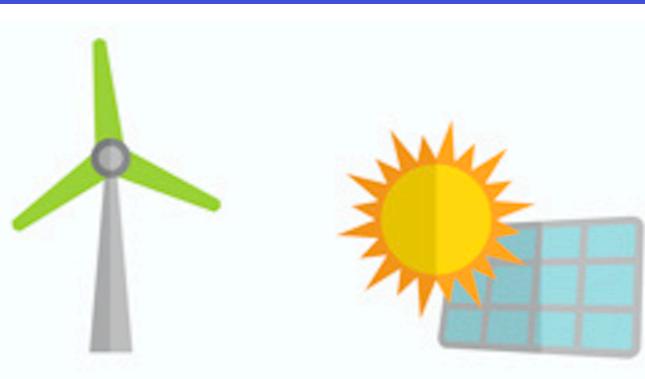
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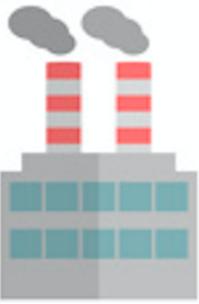


- Centralized

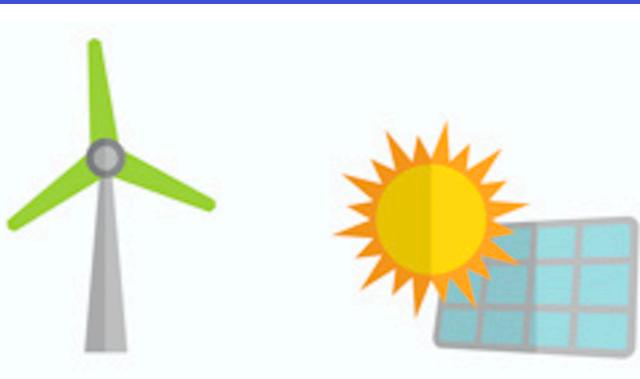


- Decentralized
  - issues at distribution level
  - easier at transmission level  
(=reduction in load) up to some level...

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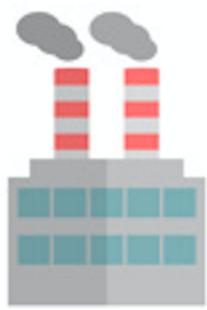


- Centralized
- Dispatchable/predictable



- Decentralized
  - issues at distribution level
  - easier at transmission level  
(=reduction in load) up to some level...
- Uncertain
  - power / energy reserve

Tomorrow



• Centra

• Dispatc



Aaron Rupar

@atrupar

Suivre

TRUMP: "If Hillary got in... you'd be doing wind. Windmills. Weeeee. And if it doesn't blow, you can forget about television for that night. 'Darling, I want to watch television.' 'I'm sorry! The wind isn't blowing.' I know a lot about wind."

Traduire le Tweet

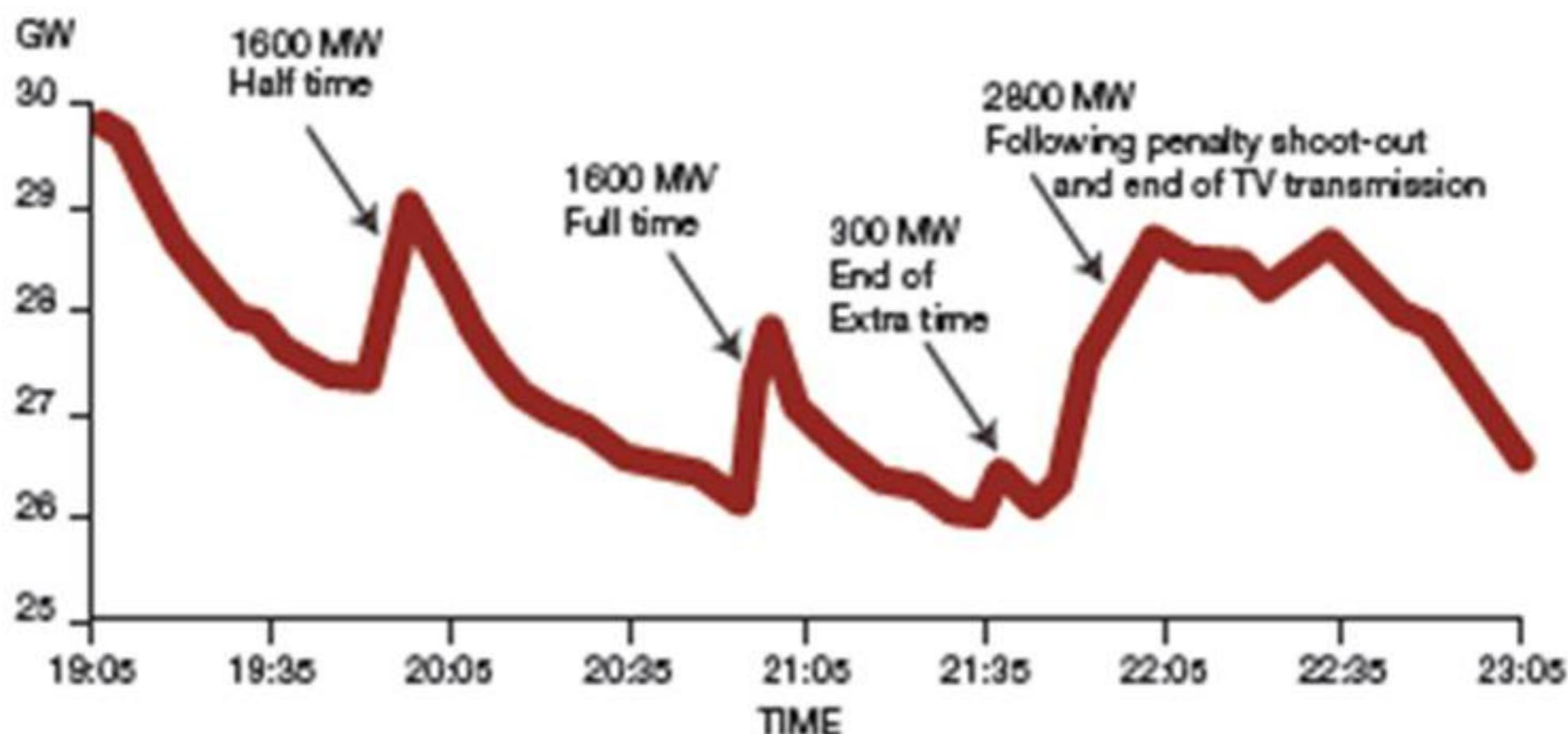


level  
level  
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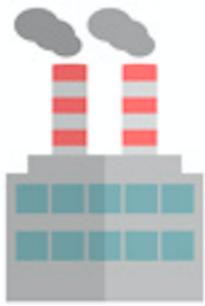
've

# Variability and uncertainty are nothing new for grid operators

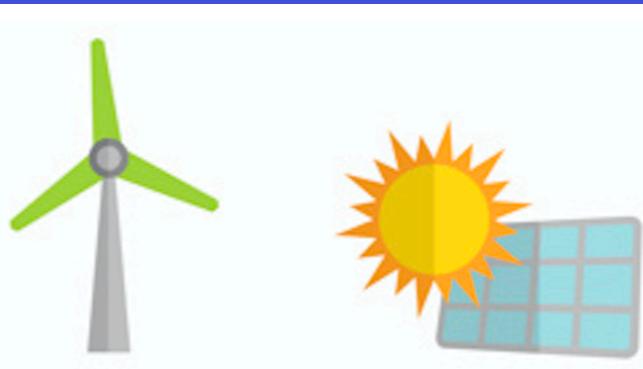
England Vs Germany 1990, World Cup Semi-Final, Kick Off 19:00



# Old vs. new productions

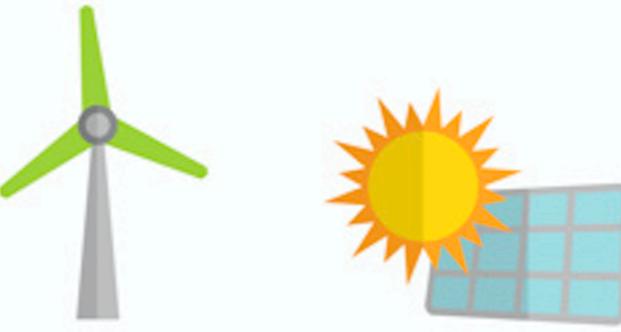
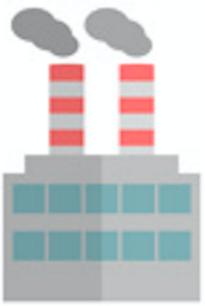


- Rotating machine with inertia
  - frequency definition
  - grid stability :
    - \*energy reserve
    - \*droop control



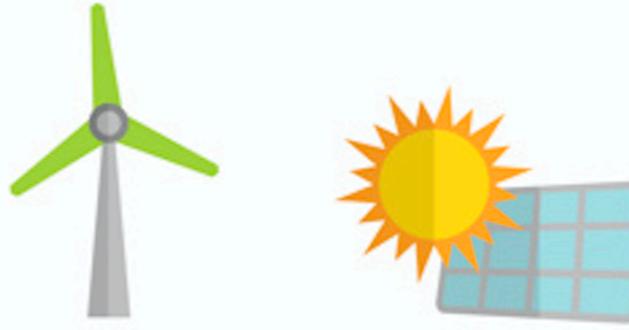
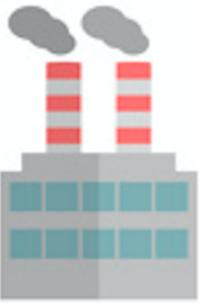
- No inertia

# Old vs. new productions



- ?? Where is it problematic to substitute  
• Old productions with new renewables ??
- inertia
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    - inertia
    - frequency definition
    - grid stability
    - \*energy reserve
    - \*droop control
- ?? Where is it not ??

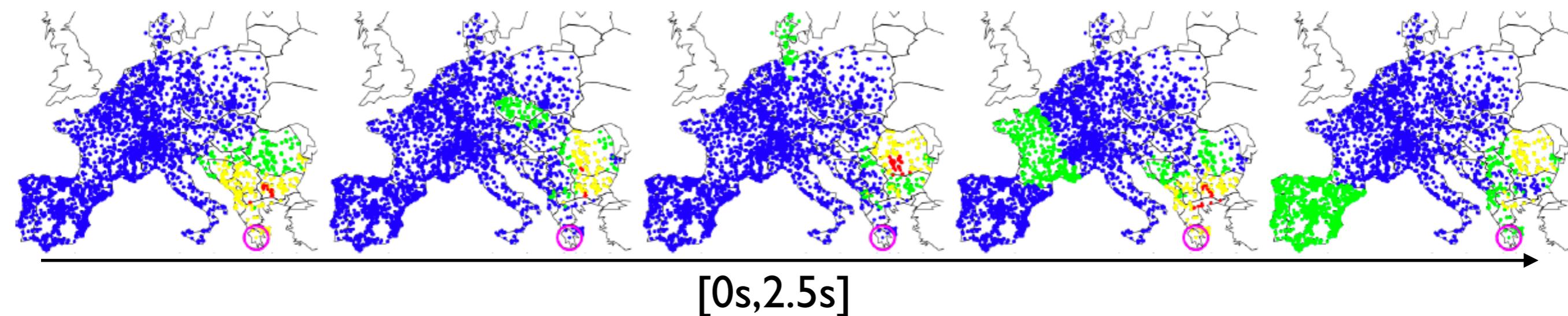
# Disturbance propagation

Fault : sudden power loss



$$P_b = P_b^{(0)} - \Delta P$$

- RoCoF < 0.04 Hz/s
- 0.04 Hz/s ≤ RoCoF < 0.1 Hz/s
- 0.1 Hz/s ≤ RoCoF < 0.2 Hz/s
- 0.2 Hz/s ≤ RoCoF < 0.5 Hz/s



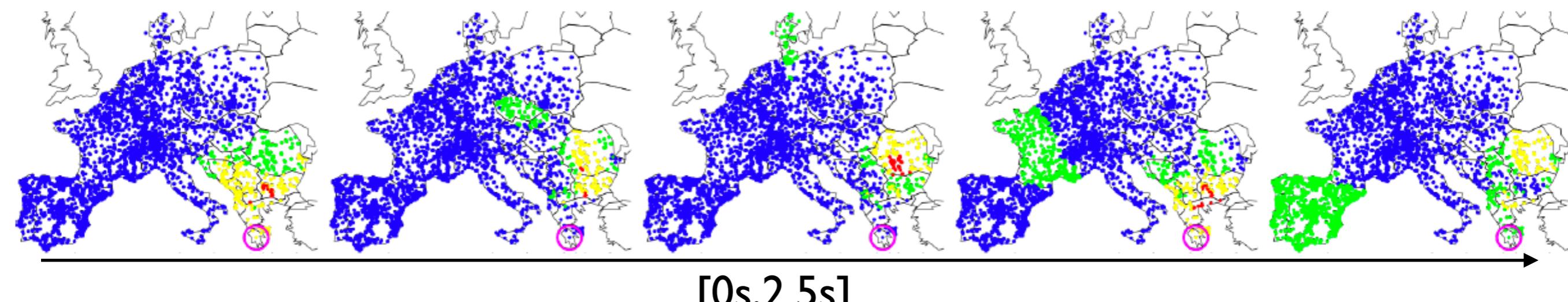
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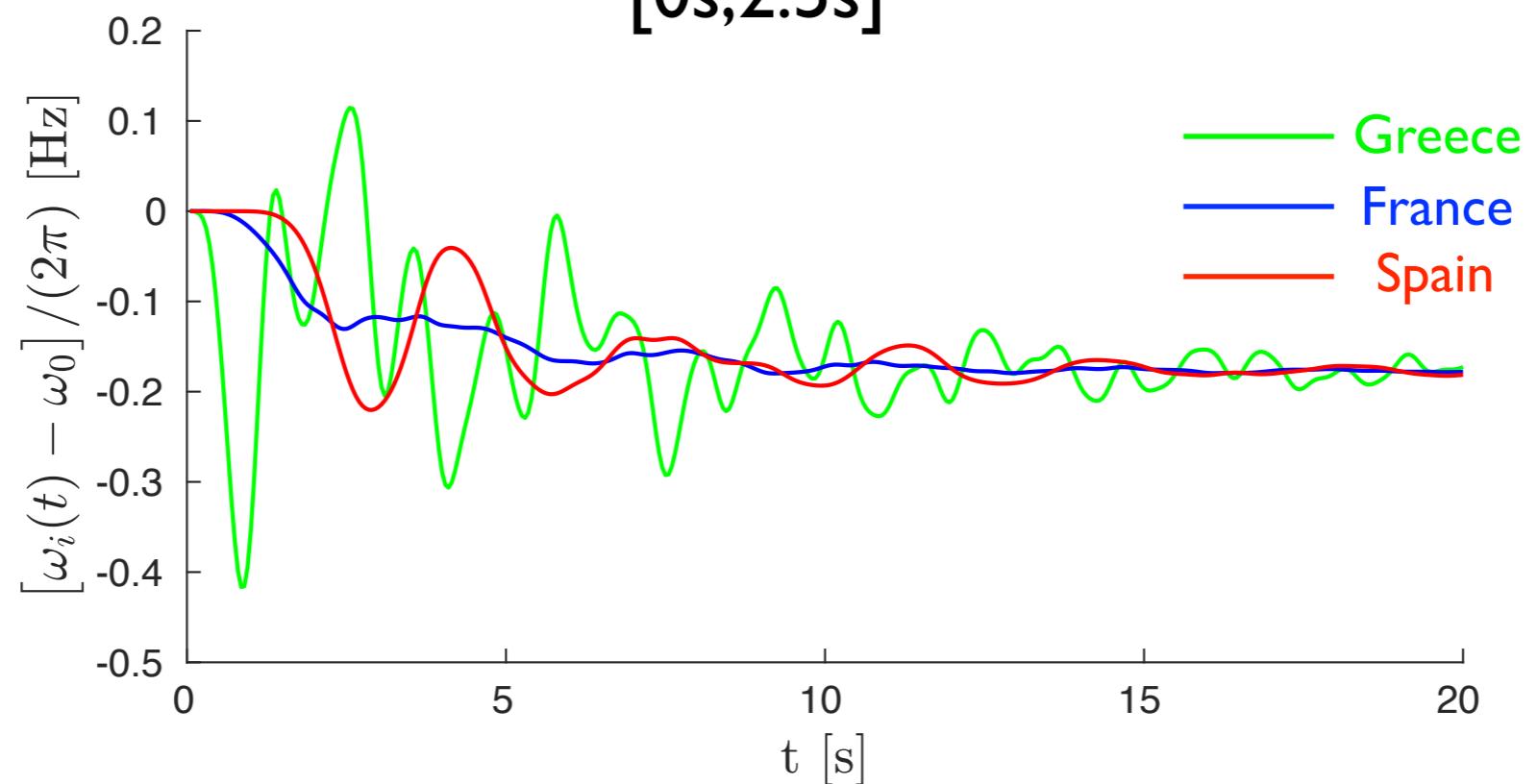


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[0s, 2.5s]



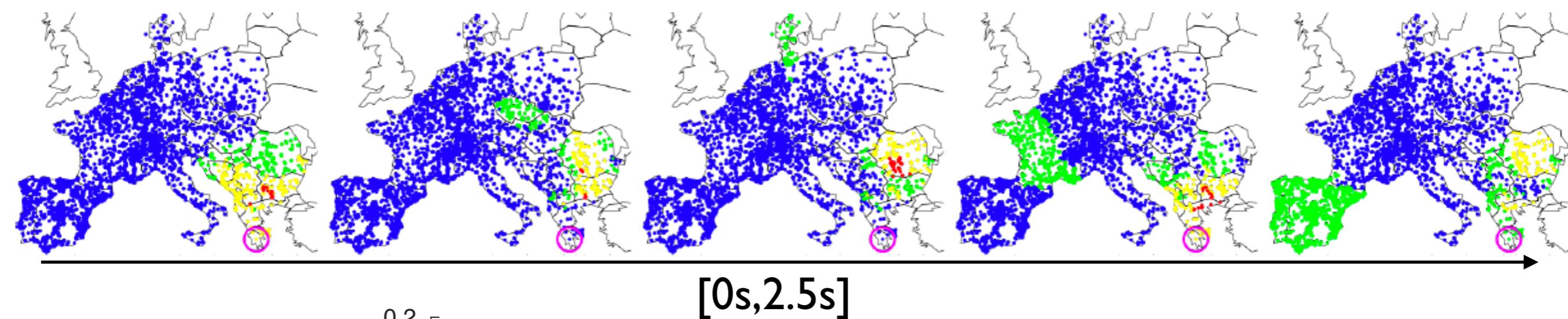
# Disturbance propagation

Fault : sudden power loss

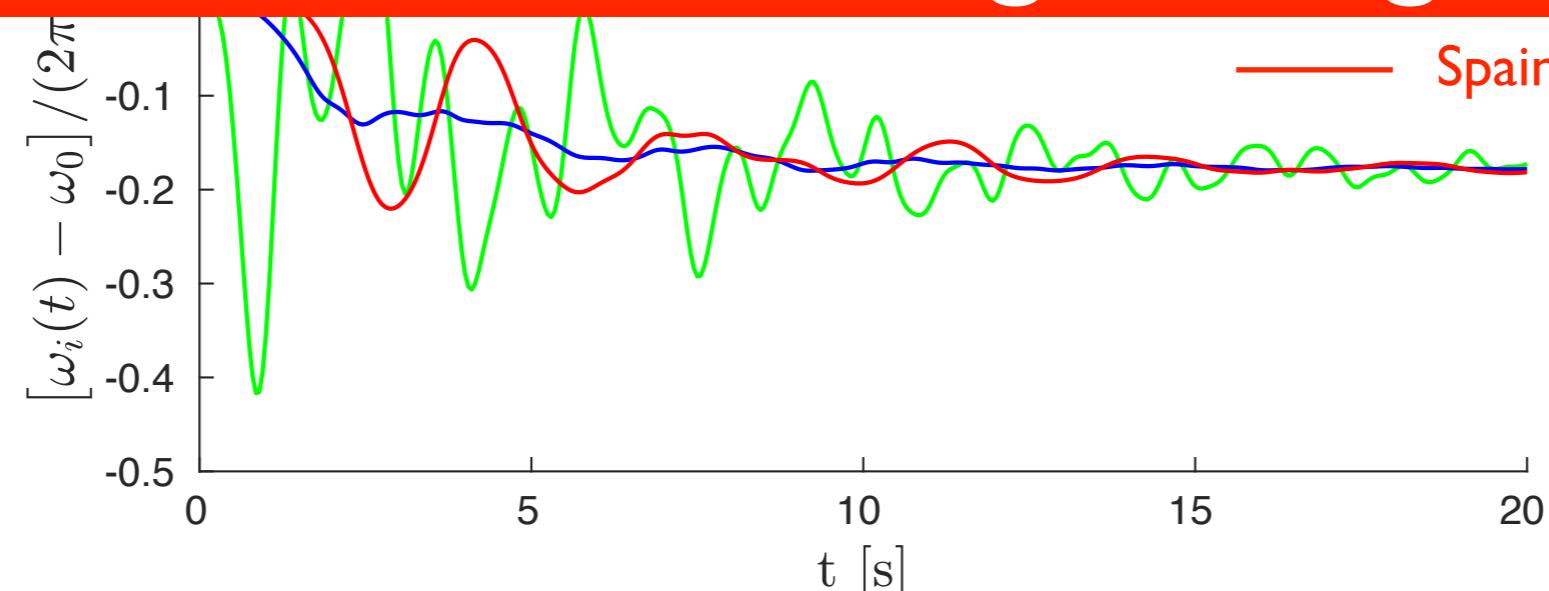


$$P_b = P_b^{(0)} - \Delta P$$

- RoCoF < 0.04 Hz/s
- 0.04 Hz/s ≤ RoCoF < 0.1 Hz/s
- 0.1 Hz/s ≤ RoCoF < 0.2 Hz/s
- 0.2 Hz/s ≤ RoCoF < 0.5 Hz/s

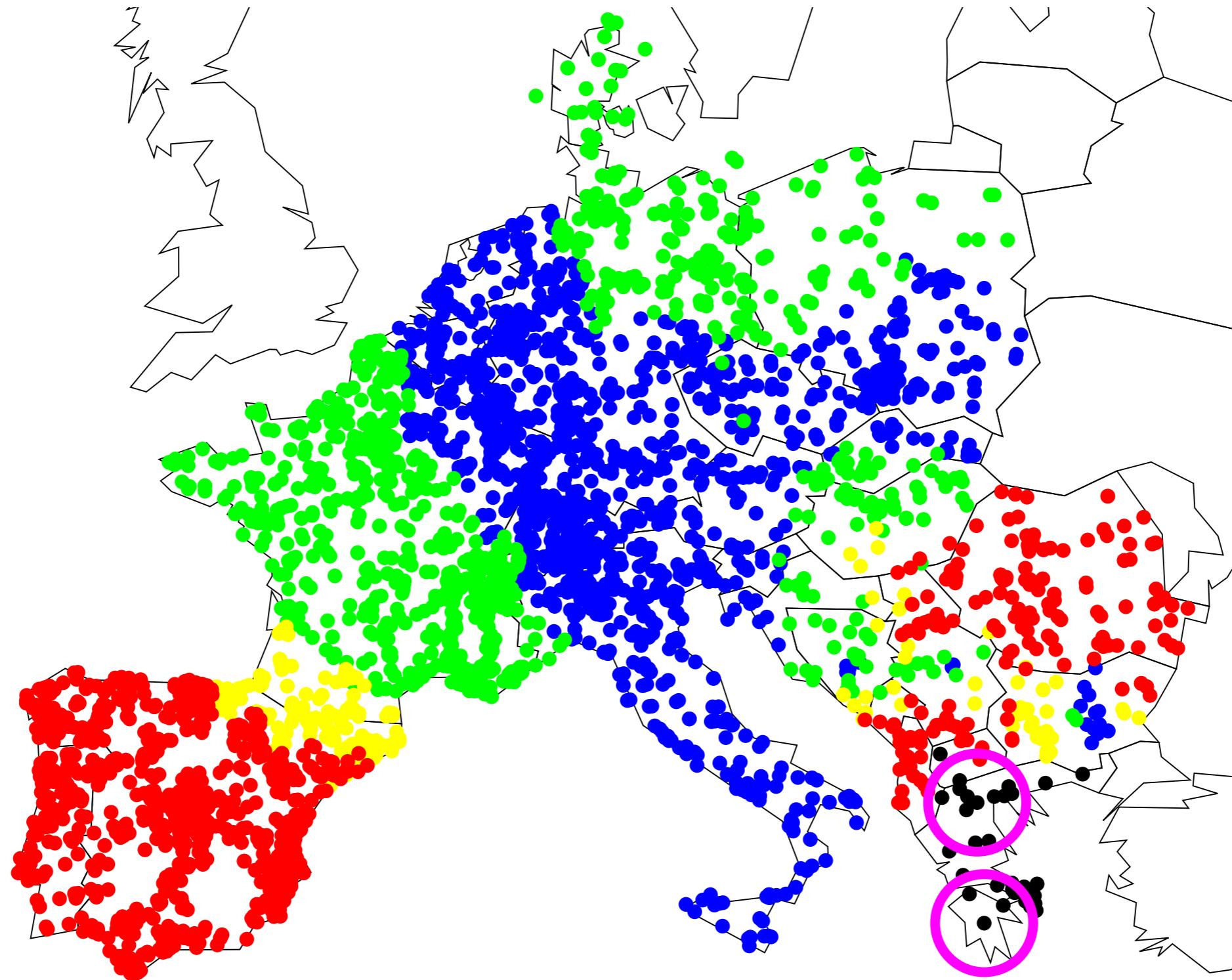


?? Perturbation tunneling through France ??



# Disturbance propagation

● RoCoF < 0.04 Hz/s   ● 0.04 Hz/s ≤ RoCoF < 0.1 Hz/s   ● 0.1 Hz/s ≤ RoCoF < 0.2 Hz/s   ● 0.2 Hz/s ≤ RoCoF < 0.5 Hz/s   ● 0.5 Hz/s ≤ RoCoF < 1 Hz/s



# Disturbance propagation vs. slow modes

Linearization of perturbation next to operating steady-state

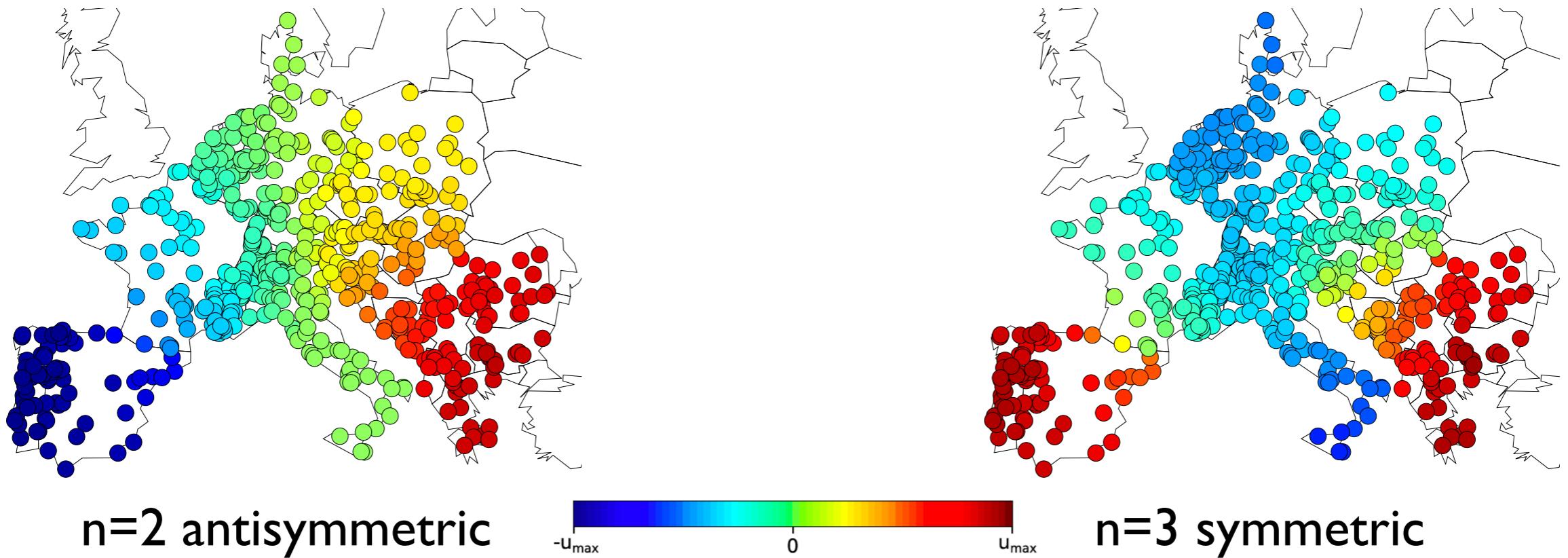
$$M\delta\ddot{\theta} + D\delta\dot{\theta} + L\delta\theta = \delta P$$

# Disturbance propagation vs. slow modes

Linearization of perturbation next to operating steady-state

$$M\delta\ddot{\theta} + D\delta\dot{\theta} + L\delta\theta = \delta P$$

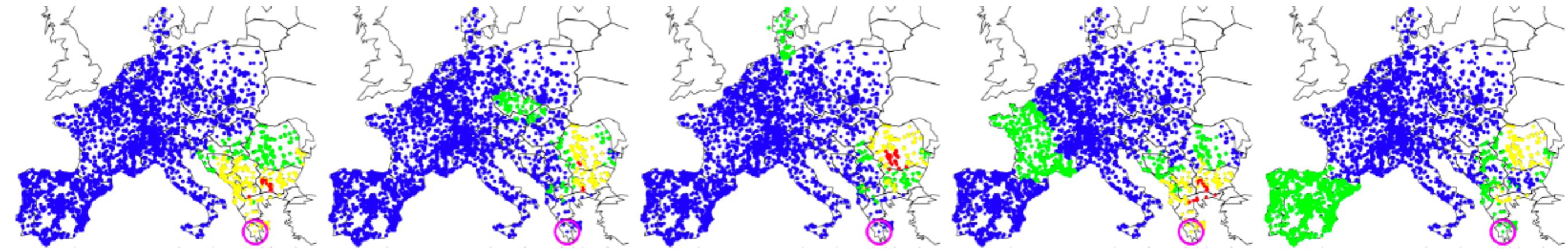
Two slowest, nonzero modes of the Laplacian matrix



...with the corresponding eigenvalues rather close  
~double-well potential vs. inter-area oscillations ?

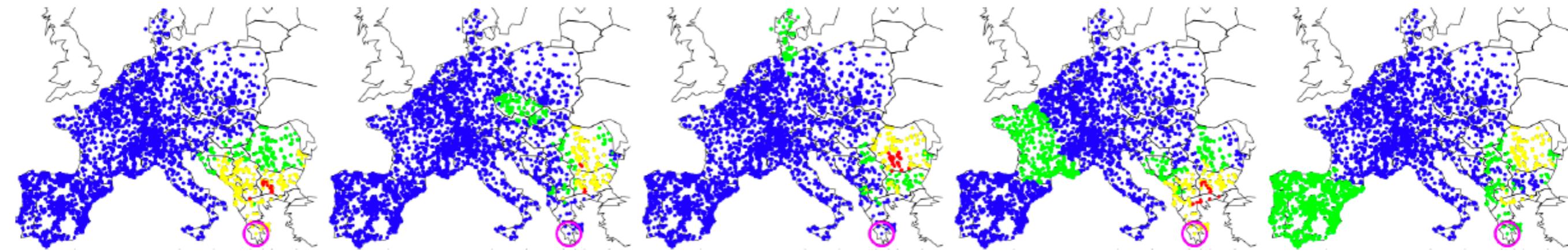
# Disturbance propagation vs. inertia

## Today's Europe

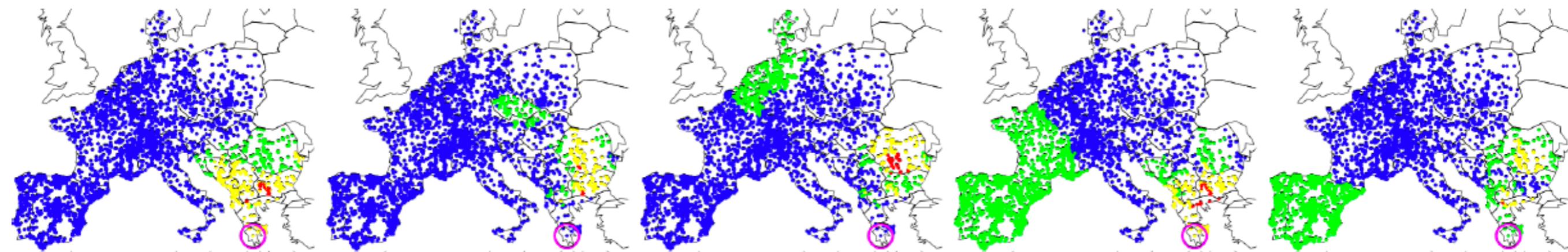


# Disturbance propagation vs. inertia

Today's Europe

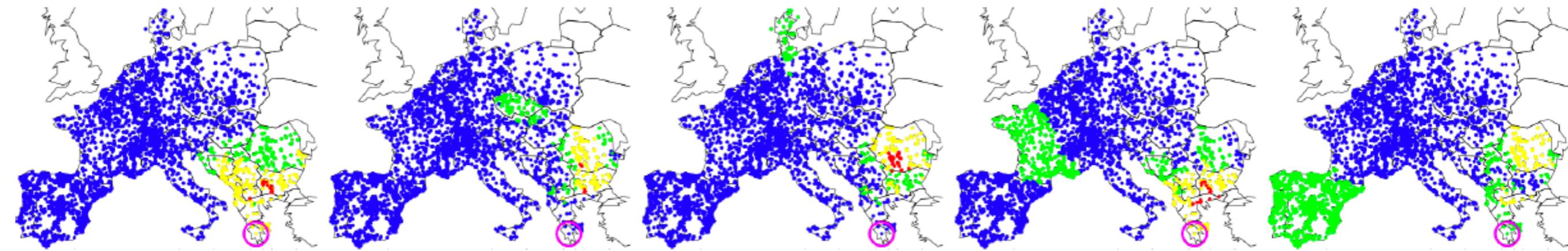


Inertia in France reduced to 50%

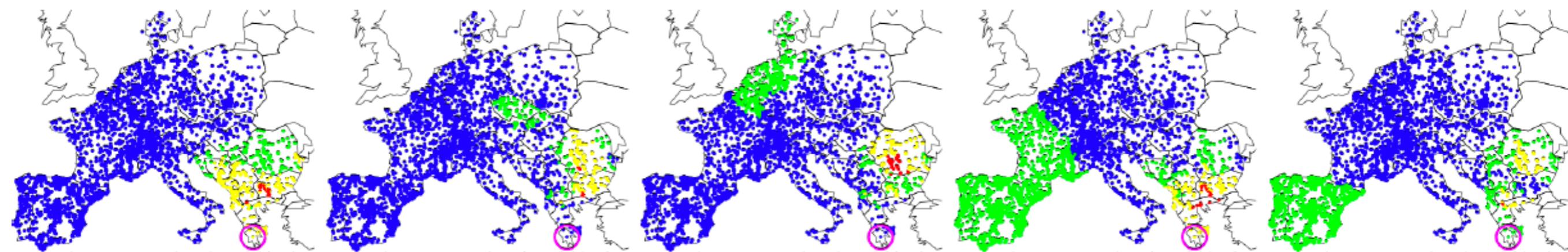


# Disturbance propagation vs. inertia

Today's Europe



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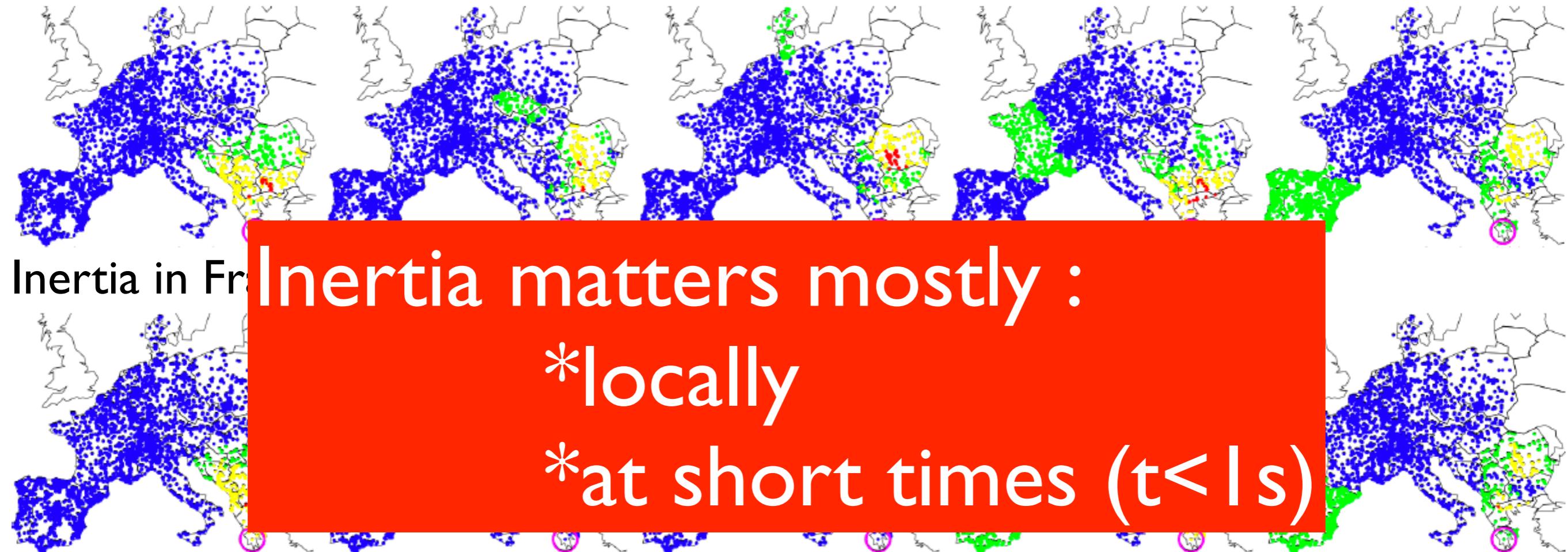


Inertia in Balkans doubled



# Disturbance propagation vs. inertia

## Today's Europe



# Disturbance propagation vs. inertia

**Optimal placement of inertia and primary control : a matrix perturbation theory approach**

# Disturbance propagation vs. inertia

## Optimal placement of inertia and primary control : a matrix perturbation theory approach

Matrix perturbation theory gives approximate expressions for the eigenvectors  $\mathbf{u}_\alpha$  and eigenvalues  $\lambda_\alpha$  of  $L_M$  in terms of those ( $\mathbf{u}_\alpha^{(0)}$  and  $\lambda_\alpha^{(0)}$ ) of  $L$  [10]. To leading order in  $\mu$  one has

$$\lambda_\alpha = m^{-1} [\lambda_\alpha^{(0)} + \mu \lambda_\alpha^{(1)} + \mathcal{O}(\mu^2)], \quad (27)$$

$$\mathbf{u}_\alpha = \mathbf{u}_\alpha^{(0)} + \mu \mathbf{u}_\alpha^{(1)} + \mathcal{O}(\mu^2), \quad (28)$$

with

$$\lambda_\alpha^{(1)} = \mathbf{u}_\alpha^{(0)\top} \mathbf{V}_1 \mathbf{u}_\alpha^{(0)}, \quad (29)$$

$$\mathbf{u}_\alpha^{(1)} = \sum_{\beta \neq \alpha} \frac{\mathbf{u}_\beta^{(0)\top} \mathbf{V}_1 \mathbf{u}_\alpha^{(0)}}{\lambda_\alpha^{(0)} - \lambda_\beta^{(0)}} \mathbf{u}_\beta^{(0)}. \quad (30)$$

# Disturbance propagation vs. inertia

**Optimal placement of inertia and primary control : a matrix perturbation theory approach**

# Disturbance propagation vs. inertia

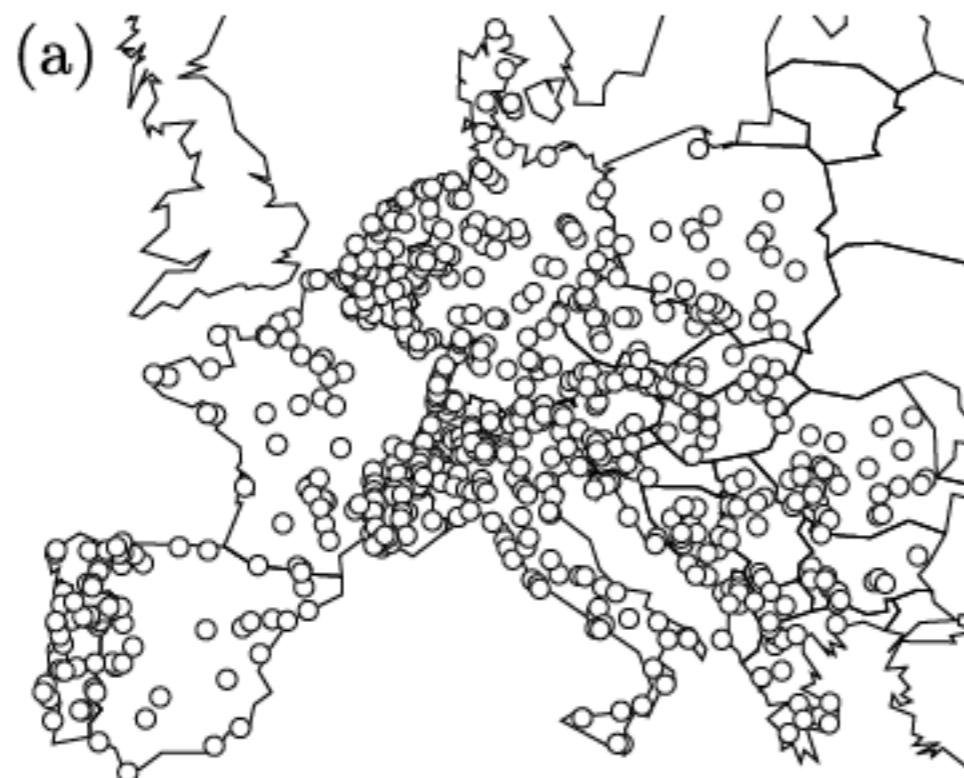
## **Optimal placement of inertia and primary control : a matrix perturbation theory approach**

- \*Optimization of a cost function ~magnitude of faults
- \*1st order perturbation theory about homogeneity

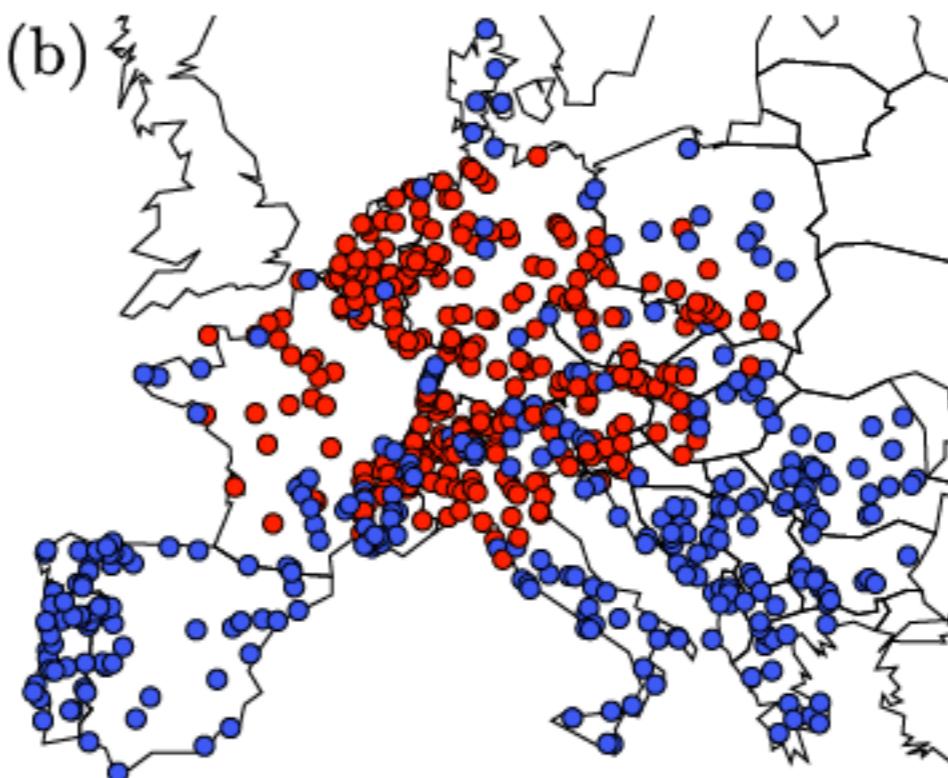
# Disturbance propagation vs. inertia

## Optimal placement of inertia and primary control : a matrix perturbation theory approach

- \*Optimization of a cost function  $\sim$ magnitude of faults
- \*1st order perturbation theory about homogeneity



Inertia  
Optimal when homogeneous



Primary control (a.k.a. damping)  
Optimal when on slow modes

# The team



Philippe



Laurent



Tommaso  
(now with Sophia genetics)

Robin,  
Melvyn  
André



Glory  
(still has to discover  
alpine activities)

**swissgrid**

**FNSNF**