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# Chapter 3

## The Physical Layer

### 3.1 INTRODUCTION

This chapter describes a physical layer for wireless sensor networks. A unique Direct Sequence Spread Spectrum (DSSS) modulation method is described and evaluated that enables a high data rate, which is desirable to minimize total transceiver active time and, therefore, maximize battery life, while minimizing transceiver complexity. Performance is simulated in Additive White Gaussian Noise (AWGN) and a Bluetooth™ interference environment.

A communication protocol physical layer

... provides mechanical, electrical, functional, and procedural characteristics to establish, maintain, and release physical connections (e.g., data circuits) between data link entities.<sup>1</sup>

Wireless sensor networks are designed to handle very low data throughput (as low as a few bits/day), exchanging lower throughput and higher message latency for longer node battery life, lower cost, and self-organization. Target applications for these networks are inventory management, industrial control and monitoring, security, intelligent agriculture, and consumer products such as wireless keyboards and personal computer (PC)-enhanced toys. The networks often have stringent cost and battery life goals; nodes in an Institute of Electrical and Electronics Engineers (IEEE) 802.15.4 Low-Rate Wireless Personal Area Network (LR-WPAN), for example, must have multiyear operation from a 750 mAh AAA cell while being considerably simpler (having fewer logic gates, smaller analog circuitry, and less memory) than a comparable Bluetooth device. In addition, the system must be capable of universal (worldwide) unlicensed operation, which greatly limits possible frequency band, modulation, and other physical layer alternatives.

Because the major design metrics of a wireless sensor network are its cost and power consumption, the physical layer design of a wireless sensor network is critical to its success.<sup>2</sup> Unfortunate choices of modulation, frequency band of operation, and coding can produce a network that, although functional, does not meet the cost or battery life goals needed for market acceptance. Although one-way networks have been proposed (in which sensors transmit to a central receiver) to achieve low cost and low

power consumption,<sup>3</sup> this work will consider only two-way networks, in which all network nodes may both transmit and receive. Further, the networks will be capable of multi-hop operation to reduce overall network power consumption.<sup>4,5</sup>

### 3.2 SOME PHYSICAL LAYER EXAMPLES

Although wireless sensor networks may be conceived to communicate via many different mechanisms, including both electromagnetic (both radio frequency (RF) and infrared) and audio means, this chapter will focus on an RF physical layer. A survey of some relevant RF physical layers includes the following subsections.

#### 3.2.1 BLUETOOTH

Bluetooth, a WPAN, operates in the 2.4 GHz Industrial, Scientific, and Medical (ISM) band. It employs binary Gaussian Frequency Shift Keying (GFSK), with a symbol rate of 1 MBaud. At the time of its development, devices in the 2.4 GHz ISM band were required by regulation in many countries to employ spread spectrum techniques. Bluetooth performs frequency hopping spread spectrum, randomly hopping across 79, 1-MHz channels (in the United States) at a rate of 1600 hops per second.<sup>6,7</sup>

Although Bluetooth is often suggested for sensor network applications, the Bluetooth physical layer is not very suitable for wireless sensor networks. Frequency hopping spread spectrum makes network discovery and association difficult because the network and prospective member node are asynchronous and the search must be done on a packet rate time scale. This causes a power consumption problem as the prospective member searches the band for the network, which may, in fact, not be present, and is especially problematic for low duty rate systems. Further, frequency hopping systems employ relatively narrowband modulation schemes (1 MHz wide in the case of Bluetooth); this means that integrated channel filtering will be difficult and expensive due to the large component (usually capacitor) values required to achieve the low-frequency filter corner. In addition, the large capacitor values associated with low-frequency circuits must be charged to a bias voltage during circuit warm-up, prior to operation; this lengthened warm-up period negatively affects node duty cycle. Further, the narrow channel separation makes the phase noise requirements of signal sources in both transmitter and receiver more difficult.

#### 3.2.2 IEEE 802.11b

The IEEE 802.11b WLAN standard also specifies operation in the 2.4 GHz ISM band. Although similar, regulations for the 2.4 GHz band are not the same around the world:

*The standard provides for 14 overlapping channels of 22 MHz between 2.4 and 2.5 GHz. Not all channels are usable in all regulatory areas; e.g., only channels 1 through 11 may be used in the United States. Channel centers are spaced 5 MHz apart.<sup>8</sup>*

As noted in Chapter 2, the original 802.11 standard specified three physical layer options at 1 Mb/s (with an optional 2 Mb/s) — infrared as well as both frequency hopping and direct sequence spread spectrum in the 2.4 GHz band. The direct sequence layer, operating at a chip rate of 11 Mc/s, employed differential binary phase shift keying (DBPSK) at 1 Mb/s, and differential quadrature phase shift keying (DQPSK) at 2 Mb/s; 802.11b extends the direct sequence layer to 5.5 and 11 Mb/s by a technique called complementary code keying (CCK). In CCK, the chip rate and modulation type remain the same as for the 2 Mb/s rate — 1 Mc/s and DQPSK, respectively — but additional information is placed in each symbol by selecting different spreading codes. For the 5.5 Mb/s rate, four possible spreading codes can be used, so two bits of information can be placed in the DQPSK modulation, and two bits of information can be placed by choice of spreading code, for a total of four bits per transmitted symbol. For the 11 Mb/s rate, 64 spreading codes are possible, so a total of 8 bits (1 byte) may be transmitted per symbol. The standard provides for an alternative, optional technique, packet binary convolutional coding (PBCC), which produces the same 5.5 and 11 Mb/s data rate as CCK but with improved sensitivity, at the cost of increased receiver complexity.<sup>9</sup>

The original 1- and 2-MHz direct sequence 802.11 physical layer is a possible candidate for a wireless sensor network; its hardware requirements are simple, the data rate is high enough, and the use of direct sequence means that it avoids the problems of frequency hopping systems. However, the use of an 11-Mc/s chip rate is somewhat onerous for a low power device; it would be desirable to operate circuits associated with the pseudonoise (PN) chip sequence at a lower rate. The cost and power consumption of the extended 802.11b systems, on the other hand, are far beyond that feasible for wireless sensor networks; for example, the large number of correlators needed to identify and decode the CCK chip sequences would be far too large, and dissipate far too much power, for the receiver of a wireless sensor node.<sup>10</sup>

#### 3.2.3 Wireless Sensor Networks

Many studies of wireless sensor networks have not defined the physical layer and have used existing wireless components for their first demonstration networks. However, some investigators have considered the physical layer.



**3.2.3.1 PicoRadio.** Rabaey et al.<sup>11</sup> find ultrawide band systems attractive for the physical layer of wireless sensor networks because ease of integration (i.e., low cost) is of higher priority than bandwidth efficiency. An interesting feature of the PicoRadio physical layer is the proposed use of "wake-up radios," namely:

*To support sleep mode, a wakeup radio is used in the physical layer, which consumes less than 1  $\mu$ W running at full duty cycle. It wakes up the main radio and informs it of the channel it should tune to. Because the destination ID is modulated into the wakeup signal, only the destination node will be waken [sic] up.<sup>12</sup>*

This concept had also been considered in the Piconet program of the University of Cambridge (England) and the Olivetti and Oracle Research Laboratory,<sup>13</sup> Cambridge, England, since renamed the Prototype Embedded Network (PEN) program.<sup>14-16</sup> (The PEN program was discontinued in 2002.) The wakeup receiver provides low average power consumption without the strict internode timing synchronization that would otherwise be necessary because only short pulses of the high power consumption ultrawide band receiver would be possible.<sup>17</sup>

**3.2.3.2 WINS.** The WINS system employs spread spectrum signaling, in either the 900 MHz or 2.4 GHz ISM bands. The physical layer design is "directed to CMOS circuit technology to permit low cost fabrication along with the additional WINS components."<sup>18</sup>

**3.2.3.3  $\mu$ AMPS.** Wang et al.<sup>19</sup> and Shih et al.<sup>20</sup> note the importance of multilevel signaling to minimize the time a network node is actively communicating and, therefore, maximize the time it is sleeping (and thereby conserving power). Further, they identify the problem of start-up energy, which is the energy taken by a wireless transceiver during its transition between the sleep and active modes, and note that the energy consumed during start-up may be greater than that consumed during active operation. This occurs because the transmission time may be very short, but the start-up time is limited by physical time constants inherent in the physical layer implementation.

### 3.3 A PRACTICAL PHYSICAL LAYER FOR WIRELESS SENSOR NETWORKS

This section concerns the design of a physical layer suitable for wireless sensor networks. Because the primary metrics of wireless sensor protocol design are cost and battery life, it is instructional to consider each in detail.

#### 3.3.1 Cost

The physical layer's effect on network cost is largely due to the cost of hardware — the cost of chip(s) and external parts. Integration typically reduces

cost because fewer discrete parts must be purchased, handled, and placed in the final product; in the limit, one may consider a single-chip design with only an antenna and a battery as external parts (the integration of antennas<sup>21</sup> and batteries<sup>22-24</sup> will be substantially more difficult, although not impossible). Aside from the antenna and battery, the most difficult component to integrate may be the quartz crystal frequency reference. A promising alternative to the discrete quartz crystal is the integrated microelectromechanical system (MEMS) resonator.<sup>25</sup> One consideration in the design of the physical layer is the required reference frequency stability. Although quartz crystal resonators routinely achieve less than five ppm (pages per minute) frequency variation over consumer temperature ranges, they are a mature technology; first- or second-generation MEMS resonators may not be capable of such stability, and the physical layer design should not require it.

Another consideration for low-cost integrated devices is the relative amounts of analog and digital circuitry required. As is well known, digital circuits dimensionally shrink with lithographic improvements in integrated circuit processing; analog circuits, however, generally do not shrink with process improvements. Not only are the dimensions of analog transistors controlled by factors other than process capability (such as current density), they also often employ passive components, the dimensions of which are controlled by physical factors such as capacitor dielectric constant. Therefore, as process technology advances, digital circuits become smaller and, therefore, cheaper, while the size of analog circuits remains relatively unchanged. Further, as integrated circuit technology advances and minimum feature size is reduced, the cost of die area actually increases. This penalizes analog circuits, which become more expensive with process improvements.

The lowest cost implementation, therefore, is either (1) a nearly all-analog approach in a large-dimension, relatively old process with a low cost per die area, or (2) a nearly all-digital approach in a small-dimension, state-of-the-art process with a low cost per digital gate. The deciding factor is that the desired system-on-a-chip (SoC) design must include RF circuits, as well. These likely cannot be made in a large-dimension process, due to the lower gain-bandwidth product of the transistors. The nearly all-digital approach is, therefore, the proper approach.

Note that the digital approach is the proper approach even if, at a given point in integrated circuit process development, the total circuit area of the digital-centric approach is larger than an alternative analog-centric approach. With process improvements over time, the cost of the digital approach will monotonically drop, while the cost of the analog approach will, at best, remain constant (if one stays with an aging process) or may even increase (if the integrated circuit (IC) vendor no longer supports the old process and the design must be moved to a more modern one).

One of the largest circuits in many transceivers is the channel filtering of the receiver. The channel filters, if analog, are typically large because the filters require relatively large capacitors to obtain sufficient strong signal (dynamic range) performance;<sup>26</sup> even if the main channel filtering is done with a digital filter, after an analog-to-digital converter, the analog-to-digital converter requires an antialias filter before it. The size of the analog channel filter is inversely proportional to the filter's corner frequency; if possible, the physical layer design should maximize the required channel filtering corner frequency (i.e., have a wide bandwidth) to minimize the die area, and therefore the cost, of the resulting IC. In addition, the amount of channel selectivity required in the physical layer should be as little as possible, consistent with proper network operation, so that as few poles of filtering as possible may be specified.

Another factor in network cost that is affected by the physical layer is the need to maximize market size and, therefore, achieve cost reductions due to volume production. This means that the physical layer should be compatible with the regulations in as many countries worldwide as possible. The first decision is the frequency band in which to operate. Clearly, it is impractical to license individual wireless sensor network nodes, or even the actual networks, just due to their expected ubiquity and low maintenance and cost goals. This then requires the identification of a band, available nearly worldwide, that allows unlicensed operation and has sufficient bandwidth. The bands that meet these requirements are the unlicensed ISM bands.

An additional requirement is the ability to integrate, with available or soon-to-be-available technology, a radio transceiver for the chosen band in the network node SoC.<sup>27,28</sup> Although operation as high as 60 GHz has been proposed for some consumer products,<sup>29</sup> and future integration of a 60-GHz transceiver with SoC-compatible technologies (e.g., silicon CMOS) does not seem out of the question,<sup>30</sup> at present 60-GHz operation requires "exotic" materials (e.g., compound semiconductors, such as gallium arsenide) that make a SoC design impractical due to cost and current drain considerations. Node operation at relatively low frequencies, below 1 GHz, suffers from the poor efficiency of electrically small antennas because the physical size of network nodes is limited.<sup>31</sup> Choice of the proper ISM band is, therefore, a compromise between the cost and power drain associated with high-frequency operation, and the physical size and antenna efficiency limitations associated with low-frequency operation. Above 1 GHz and below 60 GHz, three ISM bands are used: the 2.4-GHz band (2.400–2.4835 GHz in the United States); the 5.8-GHz band (5.725–5.875 GHz in the United States);<sup>32</sup> and the 24-GHz band (24.000–24.250 GHz in the United States). Of these, the 2.4-GHz band was chosen as having the best combination of antenna efficiency and power consumption.

Note that the 2.4-GHz band is not unoccupied; similar to all ISM bands, it is populated with many services. The IEEE 802.11b (Wi-Fi™) WLAN and the Bluetooth WPAN, among a host of other services, are in the 2.4-GHz band. The study of how these services coexist is, therefore, of significant interest, and must be considered in the evaluation of the proposed wireless sensor network physical layer.<sup>33,34</sup> As discussed in this chapter and in Section 4.3.4 of Chapter 4, a complicating factor in unlicensed bands (beyond the simple reduction of data throughput caused by packet collisions and retransmissions) is that different services often employ different channel access mechanisms; this situation can result in unfair channel access to one service over another. These problems can be mitigated to a degree by a physical layer design that is resistant to the interference environment (e.g., by using spread spectrum techniques to provide processing gain).

An alternative that has recently become available is the use of the 3.1–10.6 GHz ultrawideband (UWB) frequency band, defined by the Federal Communications Commission (FCC).<sup>35</sup> The use of UWB techniques instead of conventional carrier-based modulation schemes can offer improved location determination performance (down to the centimeter range), can support very high network node densities, and can have a very low probability of detection — all critical factors for some wireless sensor network applications. Although much of the world may follow the lead of the FCC and establish similar regulations (perhaps after a period of cautious observation of the new technology), at present, such a physical layer would be limited to the United States.

### 3.3.2 Power

Two aspects of the power problem must be considered in the physical layer design: the behavior of the power source and the power consumption of the system.

**3.3.2.1 Power Source.** Because the average power consumption of a wireless sensor network node is expected to be very low, on the order of 50  $\mu$ W or less, unconventional power sources become plausible alternatives. These include those based on scavenging from ambient sources of energy, such as solar, RF, and mechanical vibration sources.<sup>36,37</sup> However, despite their usefulness in particular applications, each of these sources has limitations — solar-powered devices must be lit, and vibration-powered devices, of course, must have vibration. To maintain generality, this chapter considers the more conventional battery.

Although many battery technology alternatives are available, and many criteria exist for the selection of a battery technology for a specific application,<sup>38</sup> the design of a protocol physical layer can take advantage of a critical behavior of batteries that seems to be technology independent. A bat-



tery undergoing pulsed discharge has a greater capacity than an identical battery undergoing a constant discharge. Further, the lower the duty cycle of the pulsed discharge, the greater the battery capacity. This charge recovery effect has been demonstrated experimentally in manganese-zinc, alkaline-manganese,<sup>39</sup> and lead-acid<sup>40</sup> cells, modeled and demonstrated experimentally in manganese-zinc<sup>41</sup> and lithium-ion<sup>42</sup> cells, and modeled in zinc-zinc oxide cells;<sup>42</sup> it has even been modeled in more esoteric battery technologies, such as the lithium-aluminum, iron sulfide battery.<sup>43</sup>

Use of the charge recovery effect has been proposed as a method of extending the battery life of portable communication devices;<sup>45-48</sup> its use in the physical layer of wireless sensor networks, which have low duty cycle, bursty communication, is a clear opportunity. In practice, taking advantage of the charge recovery effect means that the protocol should activate high-power dissipation components (e.g., the transceiver) in infrequent bursts (resulting in a low duty cycle of operation). Also, the bursts should be separated from each other by the maximum extent possible, thereby giving the cell the maximum possible time to recover before the next discharge pulse.

**3.3.2.2 Power Consumption.** Because the active power consumption of the transceiver in a wireless sensor network node is much greater than its standby power consumption, the node must operate its transceiver in a low duty cycle mode to get low average power consumption. One is then placed in the happy position in which the operating condition of the node that provides the lowest average power drain is exactly the condition that maximizes the available battery capacity.

A typical 2.4-GHz CMOS transceiver of modest specification and power output (e.g., 0 dBm) will have a power drain of about 32 mW while transmitting and about 38 mW while receiving (taking the values from Appendix C<sup>49</sup> and adding 5 mW for microcomputer power consumption). For the purpose of a duty cycle calculation in a peer-to-peer network, one may make the simplifying approximation that the power drains of both transmitter and receiver are the same (an average of 35 mW), and the further simplifying assumption that the communication links are symmetrical (that is to say, equal time is spent transmitting and receiving). To meet a 1-year battery life goal with such a transceiver under these assumptions, its duty cycle must be extremely low: if we assume a battery life goal of one year (8760 hours) from two, 750-mAh AAA cells in series, an average current drain of

$$I_{avg} = 750 \text{ mAh} / 8760 \text{ h} = 86 \mu\text{A} \quad (1)$$

is required. If the node transceiver is supplied from these batteries through a 1.8 V linear voltage regulator, in which the output current equals the input current, an average power drain

$$P_{avg} = 1.8 \text{ V} * 86 \mu\text{A} = 154.8 \mu\text{W} \quad (2)$$

is required. For this system, the average current drain is

$$I_{avg} = T_{on} * I_{on} + (1 - T_{on}) * I_{stby} \quad (3)$$

where

- $T_{on}$  = Fraction of time either receiver or transmitter is on
- $I_{on}$  = Current drain from the battery when either the receiver or transmitter is on
- $I_{stby}$  = Current drain from the battery when both transmitter and receiver are off

From this equation, and estimates of the current consumption of practical hardware, the maximum acceptable  $T_{on}$  may be determined as a function of the maximum device average battery current. For example, if  $I_{on} = 19.5 \text{ mA}$ ,  $I_{stby} = 30 \mu\text{A}$ , and  $I_{avg} = 86 \mu\text{A}$ ,  $T_{on} = 0.0029$ , or 0.29 percent. This low value implies that, despite the low data throughput of wireless sensor networks, a relatively high data rate is required so that an active device may finish communication quickly and return to sleep, to produce the low duty cycle needed to meet the system battery life requirements. This must be achieved, of course, without increasing  $I_{on}$  excessively.

Active power consumption of a transceiver is more closely tied to the symbol rate than to the raw data rate. Although it is desirable to maximize the raw data rate to minimize power consumption (by minimizing  $T_{on}$ ), it is, therefore, also desirable to minimize the symbol rate, to minimize  $I_{on}$ . The simultaneous requirements of maximizing data rate and minimizing symbol rate leads one to the conclusion that multilevel or *M*-ary signaling (i.e., sending more than one bit per symbol) should be employed in the physical layer of wireless sensor networks.<sup>50,51</sup> The use of *M*-ary signaling, however, cannot be done indiscriminately; for example, if simple multiple phase *M*-ary signaling were used, the result would be a reduction of detection sensitivity that, to recover link margin, would require an increase in transmit power that could result in no net power consumption savings. To avoid this, some type of orthogonal *M*-ary signaling should be employed.<sup>52</sup>

The value of  $T_{on}$  includes any warm-up time of the communication circuits, during which no communication is possible, but large amounts of current may be drawn from the battery. If the actual communication time is sufficiently small, the primary factor determining battery life may, in fact, be warmup current drain.<sup>53,54</sup> It is, therefore, important to minimize the length of the warmup time; the physical layer protocol may ease the

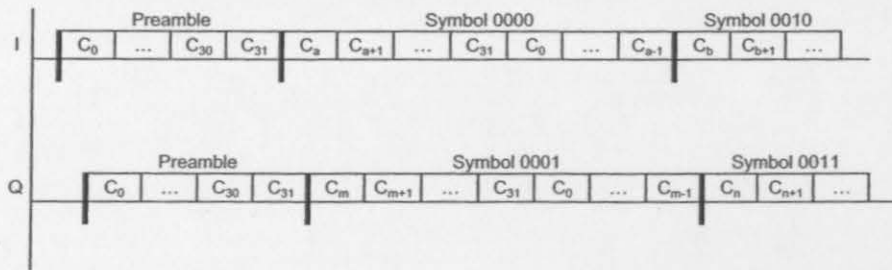


Exhibit 1. Code Position Modulation

task of the hardware designer by considering channel frequencies and spacing that allow a high synthesizer reference frequency to be used (for fast lock time) and reducing or eliminating requirements for narrow bandwidth filtering (for example, in channel selectivity filters). This gives wide bandwidth systems, such as direct sequence spread spectrum systems, an advantage over narrowband systems for low duty cycle networks.<sup>55</sup> To minimize  $I_{on}$ , however, it is important to minimize the chip rate of the direct sequence system, just as the symbol rate should be minimized.

An additional advantage of direct sequence systems is that their implementations have a high digital circuit content, and relatively low analog circuit content. As noted earlier, this is desirable for cost reasons due to the economics of integrated circuit fabrication.

Although the rules have recently been modified in the United States,<sup>56-58</sup> in many other parts of the world, operation in the 2.4-GHz band requires some form of spread spectrum modulation if a significant amount of transmitted power is to be employed. (Lower-power classes of operation that do not require spreading are used in most countries.) Further, the European regulations allow a higher transmit power, which may be desired in certain applications if the raw data rate is at least 250 kb/s.<sup>59</sup> For these reasons, plus its cost and low power advantages, the proposed physical layer employs direct sequence spread spectrum modulation, with a raw data rate of 250 kb/s.

The modulation scheme used in this work is called differential code (or pulse) position modulation; it employs two 32-chip (augmented) random pseudonoise (PN) sequences, one each on the I and Q channels, transmitted with offset-quadrature phase shift keying (QPSK). Half-sinusoidal pulse shaping of the chips is employed; the resulting modulation then has a constant envelope<sup>60</sup> and is, therefore, suitable for inexpensive nonlinear power amplifiers. The PN sequences used are maximal-length sequences (m-

sequences). The I channel uses the PN sequence with the characteristic polynomial 45 (octal), and the Q channel uses the PN sequence with the characteristic polynomial 75 (octal).<sup>61</sup> The symbol rate is 31.25 kSymbols/s. As illustrated in Exhibit 1, information is placed on each channel in each symbol by cyclically shifting the PN sequence of each channel by one of 16 possible shift values.<sup>62,63</sup> The information is placed on each channel differentially (i.e., the information is the difference in shift values between that of the present symbol and the one immediately preceding it on the same channel). Because one of  $M = 16$  shift values (each containing  $k = 4$  bits of information) are placed on each of the I and Q channels during one symbol time, a total of eight bits (one byte) are transmitted per symbol. (Because 32 chips are in the PN sequence, it is possible to set  $M = 32$  and send  $k = 5$  bits in each symbol, but this was not done for reasons of complexity; it is easier to parse eight-bit bytes into four bits than five, and having fewer shift values simplifies receiver implementation.) Because the packet lengths will be short ( $< 100$  bytes), symbol synchronization is achieved during a PHY packet preamble and fixed during data transmission.

Code position modulation is a form of orthogonal coding in which the symbols transmitted on each of the I and Q channels are selected from a set of orthogonal codewords, in this case each 32 chips long. For equally likely, equal-energy orthogonal signals, the probability of bit error  $P_B(k)$  in a single I or Q channel can be bounded by<sup>64</sup>

$$P_B(k) \leq (2^{k-1})Q\left(\sqrt{\frac{kE_b}{N_0}}\right) \quad (4)$$

where

$$Q(x) = \frac{1}{\sqrt{2\pi}} \int_x^\infty \exp\left(-\frac{u^2}{2}\right) du \quad (5)$$

is the complementary error function,  $k$  is the number of information bits sent in each symbol,  $E_b$  is the received signal energy/bit, and  $N_0$  is the thermal noise power spectral density.<sup>65</sup> Because data is encoded differentially in the proposed modulation method, however, symbol errors occur in pairs; this doubles the bit error rate (BER):

$$P_B(k) \leq (2^k)Q\left(\sqrt{\frac{kE_b}{N_0}}\right) \quad (6)$$

Orthogonal coding enjoys increased, instead of decreased, detection sensitivity over the uncoded binary waveform; that is, the value of  $E_b/N_0$

required for a given bit error probability is lower for orthogonal coding than for the uncoded binary waveform. The cost is an increase in bandwidth; however, bandwidth efficiency is not a critical performance metric for wireless sensor networks, due to their low offered data throughput.

Code position modulation, by employing a single PN sequence per channel, offers significant cost savings over a conventional multilevel direct sequence system, by simplifying PN code generation. The conventional system requires that separate PN sequences be generated for each possible transmitted sequence and compared with the received sequence. Code position modulation allows the PN code to be generated once, compared with the received sequence, and then cyclically shifted and compared again. In many integrated circuit implementations, the generation and storage of PN sequences can represent a large portion of the die area, and, therefore, the cost, of the receiver. For the proposed system in which 16 possible sequences per channel may be sent, the reduction in die area enabled by generating one sequence per symbol, instead of 16, can be significant; because shifting a PN sequence is a lower-power activity than generating a PN sequence, power consumption is also lower.

The orthogonal signaling technique has been applied to high-speed physical layers (e.g., IEEE 802.11b<sup>66</sup>), but its application to wireless sensor networks is believed to be a novel approach.

### 3.4 SIMULATIONS AND RESULTS

This physical layer was simulated in version 4.5 of the Signal Processing Worksystem (SPW) from Cadence Design Systems, San Jose, California, to determine the detector sensitivity ( $E_b/N_0$ ), and susceptibility to interference from Bluetooth transmissions, which may also be present in the 2.4-GHz band. SPW is described in Appendix A.

#### 3.4.1 Simulations

As illustrated in Exhibit 2, the BER simulation is both simple and flexible. Both I and Q channels are generated and detected independently, so that studies of possible differences in performance between them (due to autocorrelation differences between PN sequences, for example) may be made. This results in some slowdown of simulations, but because the packet size in these systems is so small ( $< 800$  bits), there is little need for BER information below  $BER = 10^{-5}$ . This means that the long simulations needed (to achieve a statistically significant number of bit errors) for lower BERs are unnecessary, so simulation speed is not of critical importance.

The modulator block (Exhibit 3) produces the desired shifted PN sequence, based on the incoming data, from the 16 possible choices. After combining the I and Q channels, the transmitted signal is sent over an

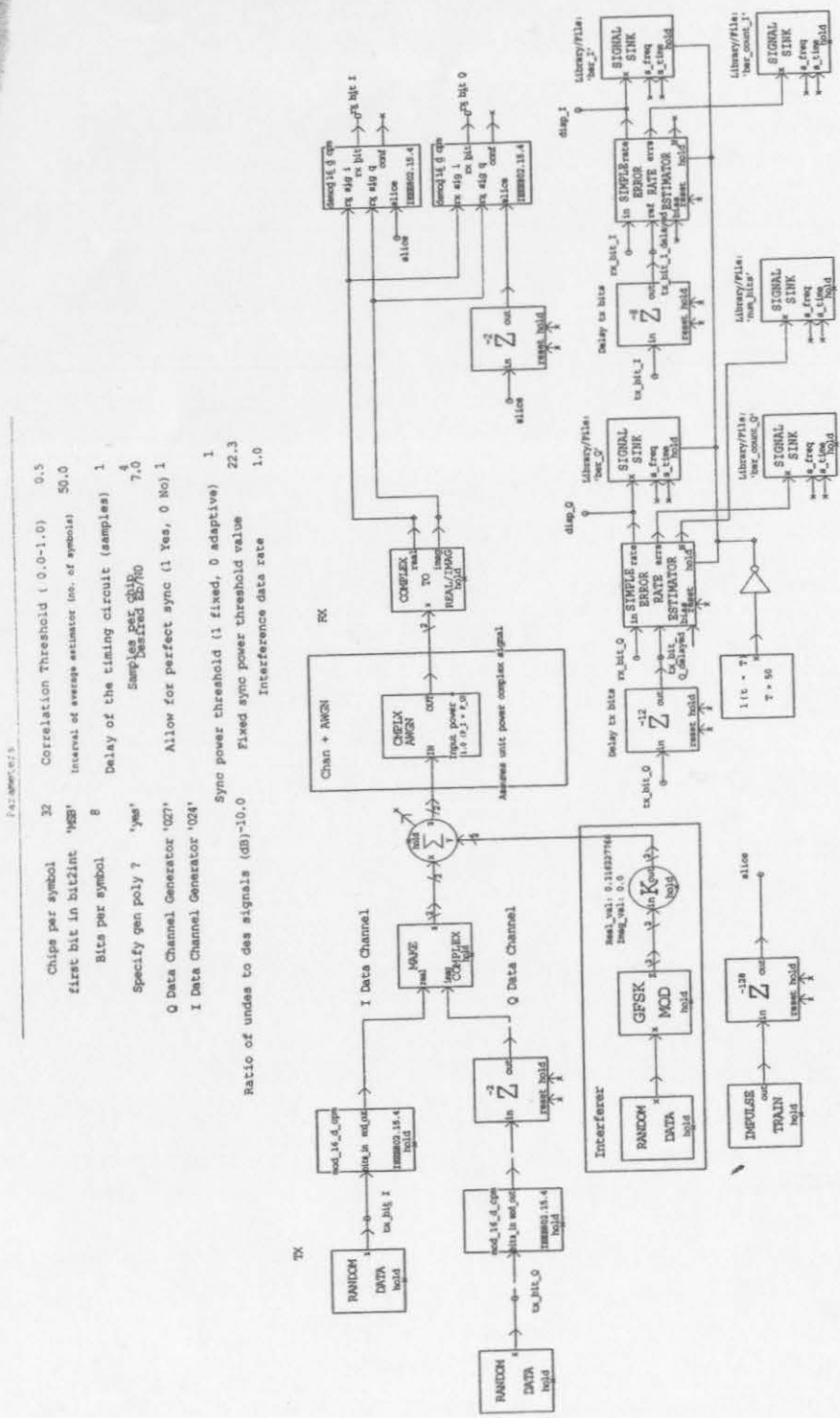


Exhibit 2. Code Position Modulation Simulation in SPW







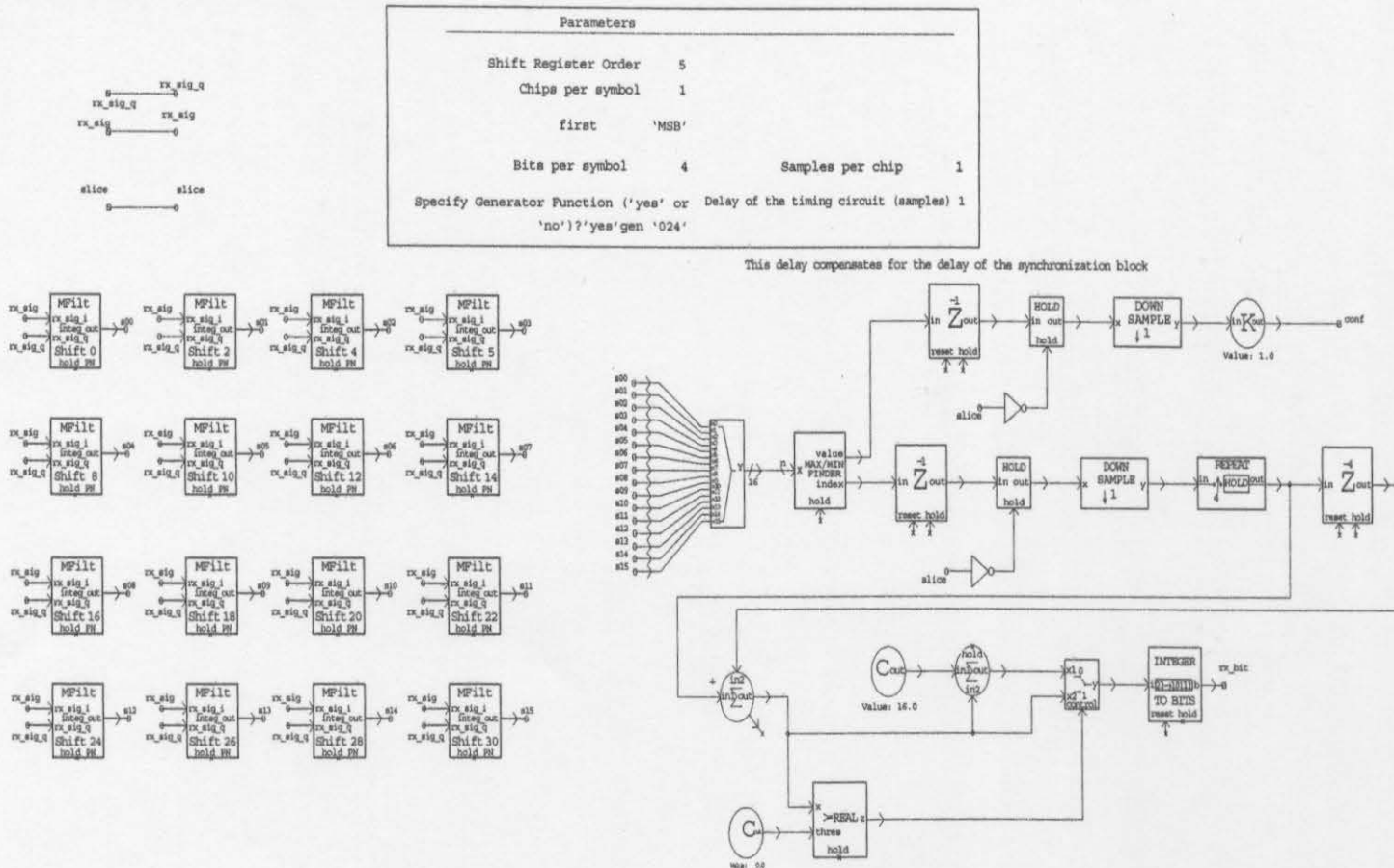


Exhibit 4. SPW Simulation of CPM Demodulator

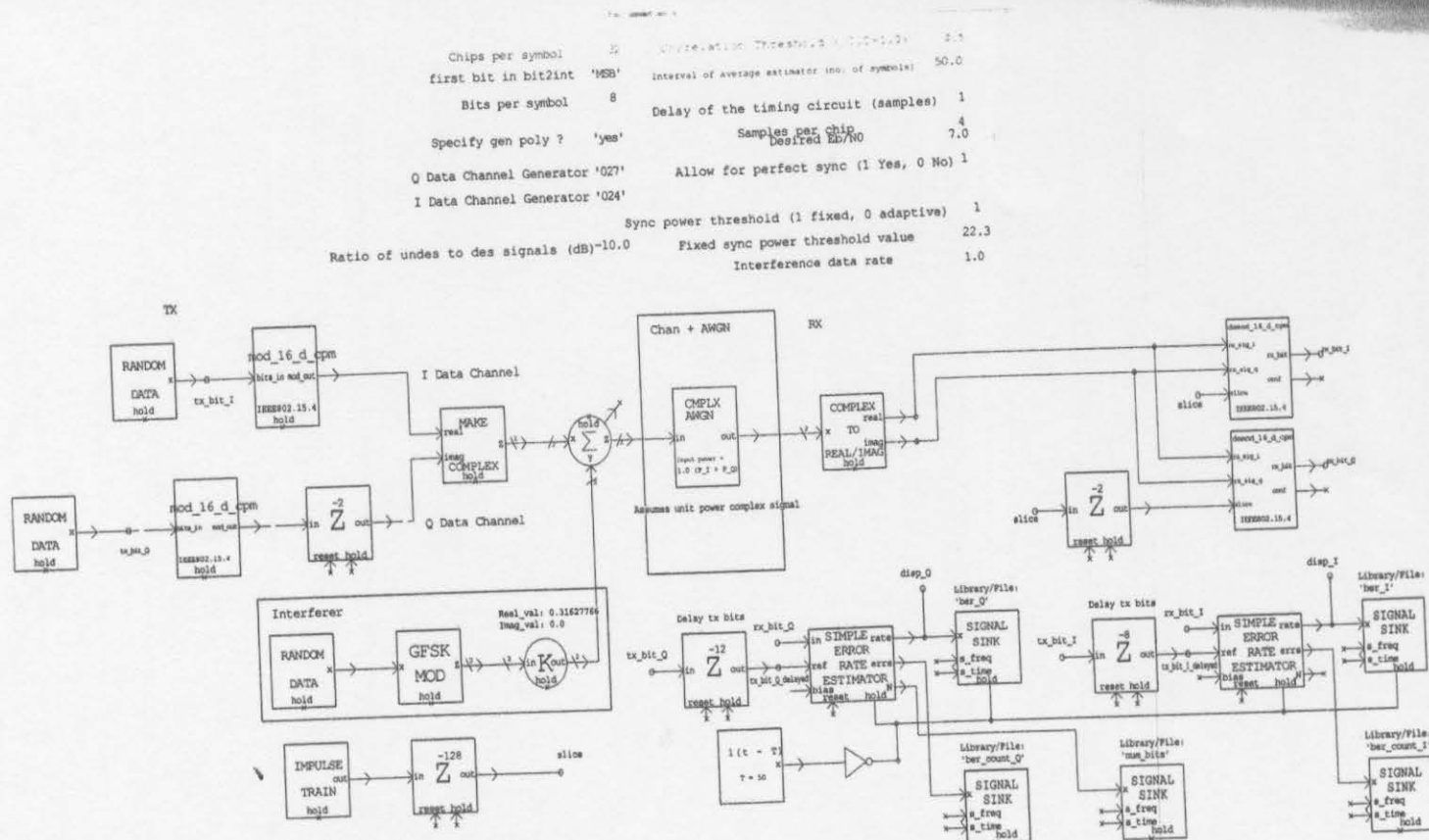


Exhibit 5. SPW Simulation of Bluetooth Interference Scenario

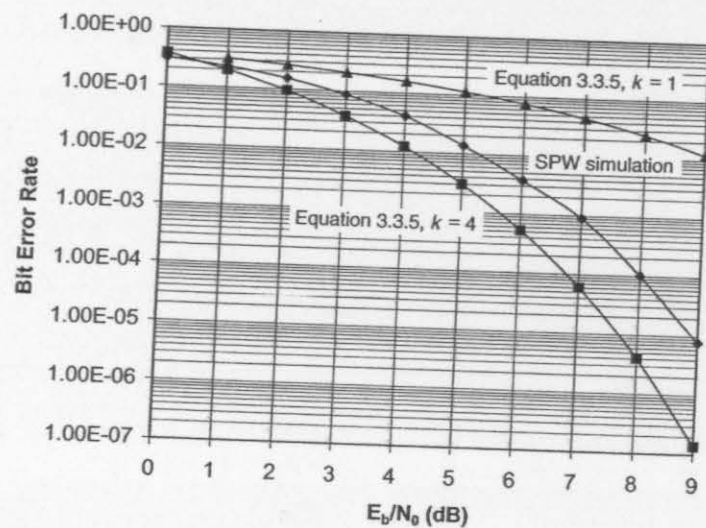


Exhibit 6. BER Performance of Code Position Modulation versus  $E_b/N_0$

mately 4 dB better than that obtained with  $k = 1$  (i.e., binary orthogonal signaling).

The 1.25-dB difference between the simulation results and Equation 5 is largely due to the nonideal autocorrelation and cross-correlation properties of the PN sequences chosen for the I and Q codes. The correlation between a code and, itself shifted in time, is close to, but not exactly, zero; similarly, the correlation between the 45 (octal) code on the I channel and the 75 (octal) code on the Q channel is not zero. This means that the signals used are not precisely orthogonal, as assumed by the theory; this trade of sensitivity was made in exchange for the simple circuit implementation that results.

The effect of Bluetooth interference on the sensor network BER was also simulated. The scenarios simulated were interference to a relatively weak sensor network signal, with an  $E_b/N_0$  level of 4 dB, a somewhat stronger sensor network signal, with an  $E_b/N_0$  level of 7 dB, and a very strong sensor network signal, with an  $E_b/N_0$  level of 50 dB. The amount of Bluetooth interference was parameterized and allowed to vary in amplitude relative to the desired signal level, from -10 to +15 dB. The results, presented in Exhibit 7, demonstrate clearly the effect of spread-spectrum processing gain, and the ability of the system to survive, albeit at an increased BER, even in the presence of interfering Bluetooth signals stronger than the desired sensor network signal.

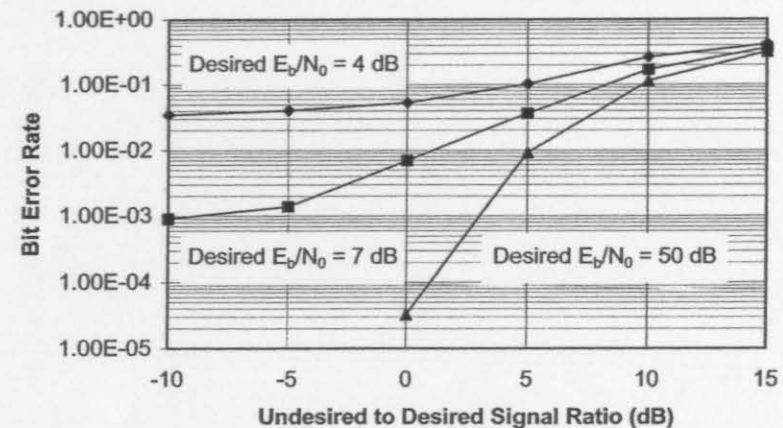


Exhibit 7. BER Performance of Code Position Modulation in the Presence of Bluetooth Interference

### 3.5 CONCLUSION

Features required to meet the cost and power consumption requirements of a wireless sensor network physical layer were reviewed, including the need to support high levels of integration and low duty cycle operation. Code position modulation, a type of modulation not previously proposed for wireless sensor networks, was shown to be compatible with these features. This modulation method enables a relatively high data rate, which is needed to reduce device duty cycle and thus improve battery life. This method is also compatible with a high level of digital, as opposed to analog, integration and, therefore, can enable low-cost implementations. The BER versus  $E_b/N_0$  performance of code position modulation was simulated with SPW, and good agreement was found between the simulation result and that predicted by analytical theory. Because the network will operate in the 2.4-GHz band, and may experience interference from Bluetooth devices, a second simulation was performed to evaluate the BER in the presence of varying levels of Bluetooth interference. The expected resistance to narrowband signals caused by the processing gain of the spread spectrum modulation was observed in the simulation.

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$$P_B(k) = \frac{M}{2(M-1)} \sum_{m=1}^{M-1} (-1)^{m+1} \frac{1}{m+1} C_m^{M-1} \exp\left(-\frac{mk}{m+1} \left(\frac{E_b}{N_0}\right)\right)$$

may be derived from Marvin K. Simon, Sami M. Hinedi, and William C. Lindsey, *Digital Communication Techniques: Signal Design and Detection*. Englewood Cliffs, NJ: PTR Prentice Hall. 1995. p. 325.

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## Chapter 4

# The Data Link Layer

### 4.1 INTRODUCTION<sup>1</sup>

Recent technology advances have made it conceivable to place wireless sensor networks in many applications. The wireless nodes of these networks will be comprised of a transducer (sensor or actuator), communications circuitry, and behavior logic. These nodes will be embedded in ceiling tiles, in factory equipment, in farmland, and on the battlefield, and will locate things, sense danger, and control the environment with minimal human effort. Crucial to the success of these ubiquitous networks is the availability of small, lightweight, low-cost nodes. Even more important, the nodes must consume ultra-low power to eliminate frequent battery replacement.<sup>2</sup>

To reduce the power consumption of these devices, both the operation and standby power consumption must be minimized; also, as described in Chapter 3, because the operation power consumption is greater than the standby power consumption, the communication time or time the communication circuits are active must be minimized. That is, the communication duty cycle must be reduced to a minimum.<sup>3</sup> For an asynchronous, multi-hop network (one in which no single node can serve as a global, centralized time reference), however, an ultra-low duty cycle makes it difficult for the wireless devices to discover and synchronize with each other, because they are so rarely active.

Low-cost crystal, ceramic, and on-chip Micro Electro-Mechanical System (MEMS) resonators<sup>4</sup> are regarded as key enabling technologies for ultra-low-cost wireless devices. The issue with these technologies is their relatively poor frequency stability, which compounds the device synchronization problem for ad hoc networks employing conventional time-division duplex (TDD) or time-division multiple access (TDMA) methods. Therefore, if the TDD beacon (or frame) period is nominally  $T_{\text{beacon}}$  seconds, and the timebase stability of each node is  $\epsilon$  ppm, a node must begin every receiving period at least  $2\epsilon T_{\text{beacon}}$  seconds prior to the nominal reception time to ensure reception of the beacon (because both transmitter and receiver time bases may vary). Further, in the worst-case scenario, reception of the beacon may not begin until  $2\epsilon T_{\text{beacon}}$  seconds after the nominal reception time, so the receiver could stay active until that time, waiting for