

1 Barotropic vorticity equation

- Momentum equations:

$$\boxed{\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \vec{\nabla} \vec{u} + f \vec{k} \times \vec{u} = -\frac{\vec{\nabla} P}{\rho_0} + \vec{\mathcal{F}}} \quad (1)$$

where $\vec{\mathcal{F}}$ includes all non-conservative forces.

$$\begin{aligned} \frac{\partial u}{\partial t} + u \cdot \frac{\partial u}{\partial x} + v \cdot \frac{\partial u}{\partial y} - f v &= -\frac{1}{\rho_0} \frac{\partial P}{\partial x} + \mathcal{F}_x \\ \frac{\partial v}{\partial t} + u \cdot \frac{\partial v}{\partial x} + v \cdot \frac{\partial v}{\partial y} + f u &= -\frac{1}{\rho_0} \frac{\partial P}{\partial y} + \mathcal{F}_y \end{aligned}$$

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- We define the vertical averaged quantities as:

$$\bar{u} = \frac{1}{H} \int_{-h}^{\zeta} u \, dz \quad (2)$$

where $H = \int_{-h}^{\zeta} dz = \zeta(i, j, t) + h(i, j)$ is the total depth of the water column, with $\zeta(x, y, t)$ the free-surface height and $h(x, y)$ the depth of the topography.

We integrate the momentum equations in the vertical:

$$\begin{aligned} \underbrace{\int_{-h}^{\zeta} \frac{\partial u}{\partial t} dz}_1 + \underbrace{\int_{-h}^{\zeta} (u \cdot \frac{\partial u}{\partial x} + v \cdot \frac{\partial u}{\partial y}) dz}_2 - \underbrace{\int_{-h}^{\zeta} f v dz}_3 &= \underbrace{-\frac{1}{\rho_0} \int_{-h}^{\zeta} \frac{\partial P}{\partial x} dz}_4 + \underbrace{\int_{-h}^{\zeta} F_x dz}_5 \\ \underbrace{\int_{-h}^{\zeta} \frac{\partial v}{\partial t} dz}_1 + \underbrace{\int_{-h}^{\zeta} (u \cdot \frac{\partial v}{\partial x} + v \cdot \frac{\partial v}{\partial y}) dz}_2 + \underbrace{\int_{-h}^{\zeta} f u dz}_3 &= \underbrace{-\frac{1}{\rho_0} \int_{-h}^{\zeta} \frac{\partial P}{\partial y} dz}_4 + \underbrace{\int_{-h}^{\zeta} F_y dz}_5 \end{aligned}$$

(1) - We can write the rate of change:

$$\frac{\partial}{\partial t} \left[\int_{-h(x,y)}^{\zeta(x,y,t)} u(x,y,z,t) dz \right] = \int_{-h}^{\zeta} \frac{\partial u}{\partial t} dz + u(x,y,\zeta,t) \frac{\partial \zeta}{\partial t}$$

which gives

$$\begin{aligned} \int_{-h}^{\zeta} \frac{\partial u}{\partial t} dz &= \frac{\partial H \bar{u}}{\partial t} - u(\zeta) \cdot \frac{\partial \zeta}{\partial t} \\ \int_{-h}^{\zeta} \frac{\partial v}{\partial t} dz &= \frac{\partial H \bar{v}}{\partial t} - v(\zeta) \cdot \frac{\partial \zeta}{\partial t} \end{aligned}$$

(2) - The advection terms are:

$$\begin{aligned} \int_{-h}^{\zeta} \left(u \cdot \frac{\partial u}{\partial x} + v \cdot \frac{\partial u}{\partial y} + w \cdot \frac{\partial u}{\partial z} \right) dz &= \int_{-h}^{\zeta} \left(\frac{\partial uu}{\partial x} + \frac{\partial uv}{\partial y} + \frac{\partial uw}{\partial z} \right) dz = \overline{\mathcal{A}_x} \\ \int_{-h}^{\zeta} \left(u \cdot \frac{\partial v}{\partial x} + v \cdot \frac{\partial v}{\partial y} + w \cdot \frac{\partial v}{\partial z} \right) dz &= \int_{-h}^{\zeta} \left(\frac{\partial uv}{\partial x} + \frac{\partial vv}{\partial y} + \frac{\partial vw}{\partial z} \right) dz = \overline{\mathcal{A}_y} \end{aligned}$$

We can develop them as:

$$\begin{aligned} \int_{-h}^{\zeta} \frac{\partial uu}{\partial x} dz &= \frac{\partial H \bar{uu}}{\partial x} - u^2(\zeta) \cdot \frac{\partial \zeta}{\partial x} - u^2(-h) \cdot \frac{\partial h}{\partial x} \\ \int_{-h}^{\zeta} \frac{\partial uv}{\partial y} dz &= \frac{\partial H \bar{uv}}{\partial y} - u(\zeta)v(\zeta) \frac{\partial \zeta}{\partial y} - u(-h)v(-h) \frac{\partial h}{\partial y} \\ \int_{-h}^{\zeta} \frac{\partial uw}{\partial z} dz &= u|_{\zeta} \left(\frac{\partial \zeta}{\partial t} + u|_{\zeta} \frac{\partial \zeta}{\partial x} + v|_{\zeta} \frac{\partial \zeta}{\partial y} \right) - u|_{-h} \left(u|_{-h} \frac{\partial -h}{\partial x} + v|_{-h} \frac{\partial -h}{\partial y} \right) \\ \int_{-h}^{\zeta} \frac{\partial uv}{\partial x} dz &= \frac{\partial H \bar{uv}}{\partial x} - u(\zeta)v(\zeta) \frac{\partial \zeta}{\partial x} - u(-h)v(-h) \frac{\partial h}{\partial x} \\ \int_{-h}^{\zeta} \frac{\partial vv}{\partial y} dz &= \frac{\partial H \bar{vv}}{\partial y} - v^2(\zeta) \cdot \frac{\partial \zeta}{\partial y} - v^2(-h) \cdot \frac{\partial h}{\partial y} \\ \int_{-h}^{\zeta} \frac{\partial vw}{\partial z} dz &= v|_{\zeta} \left(\frac{\partial \zeta}{\partial t} + u|_{\zeta} \frac{\partial \zeta}{\partial x} + v|_{\zeta} \frac{\partial \zeta}{\partial y} \right) - v|_{-h} \left(u|_{-h} \frac{\partial -h}{\partial x} + v|_{-h} \frac{\partial -h}{\partial y} \right) \end{aligned}$$

using boundary conditions:

$$\begin{aligned}\omega|_{\zeta} &= \frac{\partial \zeta}{\partial t} + u|_{\zeta} \frac{\partial \zeta}{\partial x} + v|_{\zeta} \frac{\partial \zeta}{\partial y} \\ \omega|_{-h} &= u|_{-h} \frac{\partial -h}{\partial x} + v|_{-h} \frac{\partial -h}{\partial y}\end{aligned}$$

and write:

$$\begin{aligned}\overline{\mathcal{A}_x} &= \frac{\partial H \overline{uu}}{\partial x} + \frac{\partial H \overline{uv}}{\partial y} + u|_{\zeta} \cdot \frac{\partial \zeta}{\partial t} \\ \overline{\mathcal{A}_y} &= \frac{\partial H \overline{vv}}{\partial y} + \frac{\partial H \overline{uv}}{\partial x} + v|_{\zeta} \cdot \frac{\partial \zeta}{\partial t}\end{aligned}$$

Note that the $u|_{\zeta} \cdot \frac{\partial \zeta}{\partial t}$ and $v|_{\zeta} \cdot \frac{\partial \zeta}{\partial t}$ terms will disappear when added to the term (1).

(3) - Coriolis terms are:

$$\begin{aligned}- \int_{-h}^{\zeta} f v \, dz &= -f H \overline{v} \\ \int_{-h}^{\zeta} f u \, dz &= f H \overline{u}\end{aligned}$$

(4) Pressure terms are-

$$\begin{aligned}- \frac{1}{\rho_0} \int_{-h}^{\zeta} \frac{\partial P}{\partial x} \, dz &= - \frac{1}{\rho_0} \frac{\partial H \overline{P}}{\partial x} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial x} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial x} \\ - \frac{1}{\rho_0} \int_{-h}^{\zeta} \frac{\partial P}{\partial y} \, dz &= - \frac{1}{\rho_0} \frac{\partial H \overline{P}}{\partial y} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial y} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial y}\end{aligned}$$

(5) and finally-

$$\begin{aligned}\int_{-h}^{\zeta} F_x dz &= \int_{-h}^{\zeta} \left(\frac{\partial}{\partial z} \left(K_{Mv} \frac{\partial u}{\partial z} \right) + \mathcal{D}_x \right) dz \\ \int_{-h}^{\zeta} F_y dz &= \int_{-h}^{\zeta} \left(\frac{\partial}{\partial z} \left(K_{Mv} \frac{\partial v}{\partial z} \right) + \mathcal{D}_y \right) dz\end{aligned}$$

where

$$\begin{aligned}\int_{-h}^{\zeta} \frac{\partial}{\partial z} \left(K_{Mv} \frac{\partial u}{\partial z} \right) dz &= K_{Mv} \frac{\partial u}{\partial z} \Big|_{\zeta} - K_{Mv} \frac{\partial u}{\partial z} \Big|_{-h} = \frac{1}{\rho_0} (\tau_x^{wind} - \tau_x^{bot}) \\ \int_{-h}^{\zeta} \frac{\partial}{\partial z} \left(K_{Mv} \frac{\partial v}{\partial z} \right) dz &= K_{Mv} \frac{\partial v}{\partial z} \Big|_{\zeta} - K_{Mv} \frac{\partial v}{\partial z} \Big|_{-h} = \frac{1}{\rho_0} (\tau_y^{wind} - \tau_y^{bot})\end{aligned}$$

and

$$\begin{aligned}\int_{-h}^{\zeta} \mathcal{D}_x dz &= \overline{\mathcal{D}_x} \\ \int_{-h}^{\zeta} \mathcal{D}_y dz &= \overline{\mathcal{D}_y}\end{aligned}$$

So we get finally the depth-averaged momentum equations.

$$\begin{aligned}\frac{\partial H\bar{u}}{\partial t} &+ \frac{\partial H\bar{u}\bar{u}}{\partial x} + \frac{\partial H\bar{u}\bar{v}}{\partial y} - fH\bar{v} = \\ &- \frac{1}{\rho_0} \frac{\partial H\bar{P}}{\partial x} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial x} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial x} + \tau_x^{wind} - \tau_x^{bot} + \overline{\mathcal{D}_x} \\ \underbrace{\frac{\partial H\bar{v}}{\partial t}}_1 &+ \underbrace{\frac{\partial H\bar{v}\bar{v}}{\partial y} + \frac{\partial H\bar{u}\bar{v}}{\partial x}}_2 + \underbrace{fH\bar{u}}_4 = \\ &- \underbrace{\frac{1}{\rho_0} \frac{\partial H\bar{P}}{\partial y} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial y} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial y}}_5 + \underbrace{\tau_y^{wind} - \tau_y^{bot} + \overline{\mathcal{D}_y}}_6\end{aligned}$$

Now we cross differentiates them to get the barotropic vorticity equations.

(1) :

$$\begin{aligned}\frac{\partial}{\partial y} \left(\frac{\partial H \bar{u}}{\partial t} \right) &= \frac{\partial}{\partial t} \left(\bar{u} \frac{\partial H}{\partial y} + H \frac{\partial \bar{u}}{\partial y} \right) \\ \frac{\partial}{\partial x} \left(\frac{\partial H \bar{v}}{\partial t} \right) &= \frac{\partial}{\partial t} \left(\bar{v} \frac{\partial H}{\partial x} + H \frac{\partial \bar{v}}{\partial x} \right)\end{aligned}$$

so

$$\begin{aligned}\vec{k} \cdot \vec{\nabla} \times (1) &= \frac{\partial}{\partial t} \left[H \left(\frac{\partial \bar{v}}{\partial x} - \frac{\partial \bar{u}}{\partial y} \right) + \bar{v} \frac{\partial H}{\partial x} - \bar{u} \frac{\partial H}{\partial y} \right] \\ &= \frac{\partial H \omega_r}{\partial t} \\ &+ \frac{\partial}{\partial t} \left[\bar{v} \frac{\partial \zeta}{\partial x} - \bar{u} \frac{\partial \zeta}{\partial y} \right] - \frac{\partial h}{\partial x} \frac{\partial \bar{v}}{\partial t} + \frac{\partial h}{\partial y} \frac{\partial \bar{u}}{\partial t}\end{aligned}$$

where $\omega_r = \frac{\partial \bar{v}}{\partial x} - \frac{\partial \bar{u}}{\partial y}$ is the barotropic vorticity.

(2) - Advective non-linear terms are:

$$\begin{aligned}\vec{k} \cdot \vec{\nabla} \times (2) &= \frac{\partial}{\partial x} \left(\frac{\partial H \bar{v} \bar{v}}{\partial y} + \frac{\partial H \bar{u} \bar{v}}{\partial x} \right) - \frac{\partial}{\partial y} \left(\frac{\partial H \bar{u} \bar{u}}{\partial x} + \frac{\partial H \bar{u} \bar{v}}{\partial y} \right) \\ &= \frac{\partial^2 H (\bar{v} \bar{v} - \bar{u} \bar{u})}{\partial x y} + \frac{\partial^2 H \bar{u} \bar{v}}{\partial x x} - \frac{\partial^2 H \bar{u} \bar{v}}{\partial y y}\end{aligned}$$

(4) - The coriolis terms simplify as:

$$\begin{aligned}\vec{k} \cdot \vec{\nabla} \times (4) &= \frac{\partial f}{\partial x} H \bar{u} + \frac{\partial f}{\partial y} H \bar{v} + f \left(\frac{\partial H \bar{u}}{\partial x} + \frac{\partial H \bar{v}}{\partial y} \right) \\ &= H \vec{\bar{u}} \cdot \vec{\nabla} f + f \left(\frac{\partial H \bar{u}}{\partial x} + \frac{\partial H \bar{v}}{\partial y} \right)\end{aligned}$$

with the use of the integral of the continuity equation:

$$\int_{-h}^{\zeta} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) dz = 0$$

which gives

$$\frac{\partial H \bar{u}}{\partial x} + \frac{\partial H \bar{v}}{\partial y} = - \frac{\partial \zeta}{\partial t}$$

we get:

$$\vec{k} \cdot \vec{\nabla} \times (4) = H \vec{u} \cdot \vec{\nabla} f - f \frac{\partial \zeta}{\partial t}$$

Also note that we don't write $\frac{\partial f}{\partial x} = 0$ because we don't necessarily use zonal-meridional coordinates.

(5) - The pressure terms simplify as:

$$\begin{aligned} \vec{k} \cdot \vec{\nabla} \times (5) &= \frac{\partial}{\partial x} \left(-\frac{1}{\rho_0} \frac{\partial H \bar{P}}{\partial y} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial y} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial y} \right) \\ &\quad - \frac{\partial}{\partial y} \left(-\frac{1}{\rho_0} \frac{\partial H \bar{P}}{\partial x} + \frac{1}{\rho_0} P(\zeta) \cdot \frac{\partial \zeta}{\partial x} + \frac{1}{\rho_0} P(-h) \frac{\partial h}{\partial x} \right) \\ &= \frac{1}{\rho_0} \left(\left. \frac{\partial P}{\partial x} \right|_{-h} \frac{\partial h}{\partial y} - \left. \frac{\partial P}{\partial y} \right|_{-h} \frac{\partial h}{\partial x} \right) \\ &= \frac{1}{\rho_0} J(P_b, h) \end{aligned}$$

considering that with $\frac{\partial P(\zeta)}{\partial x} = \frac{\partial P(\zeta)}{\partial y} = 0$ at the surface, and writing $P_b = P(-h)$ the pressure at the bottom.

(6) - Forcing and dissipative terms can be written as:

$$\vec{k} \cdot \vec{\nabla} \times (6) = \frac{1}{\rho_0} \left(\frac{\partial \tau_y^{wind}}{\partial x} - \frac{\partial \tau_x^{wind}}{\partial y} \right) - \frac{1}{\rho_0} \left(\frac{\partial \tau_y^{bot}}{\partial x} - \frac{\partial \tau_x^{bot}}{\partial y} \right) + \frac{\partial \overline{\mathcal{D}_y}}{\partial x} - \frac{\partial \overline{\mathcal{D}_x}}{\partial y}$$

So we get the equation:

$$\underbrace{H \frac{\partial \omega_r}{\partial t}}_{\text{rate}} + \underbrace{H \vec{u} \cdot \vec{\nabla} f}_{\text{planet. vort.}} = \underbrace{\frac{J(P_b, h)}{\rho_0}}_{\text{bot. pres. torque}} + \underbrace{\vec{k} \cdot \vec{\nabla} \times \frac{\vec{\tau}^{wind}}{\rho_0}}_{\text{wind curl}} - \underbrace{\vec{k} \cdot \vec{\nabla} \times \frac{\vec{\tau}^{bot}}{\rho_0}}_{\text{bot. drag curl}} \\
 + \underbrace{F}_{\text{horiz. dissip.}} - \underbrace{A}_{\text{NL adv terms}} - \underbrace{L}_{\text{left overs}}$$

where the curl of NL advection terms is:

$$A = \frac{\partial^2 H(\overline{v\overline{v}} - \overline{u\overline{u}})}{\partial xy} + \frac{\partial^2 H \overline{u\overline{v}}}{\partial xx} - \frac{\partial^2 H \overline{u\overline{v}}}{\partial yy}$$

Horiz. dissip. is included in:

$$F = \frac{\partial \overline{\mathcal{D}_y}}{\partial x} - \frac{\partial \overline{\mathcal{D}_x}}{\partial y}$$

Note that we are using implicit diffusion so the \mathcal{D} terms are numerically “included” in the advection terms.

And finally left overs are:

$$L = \frac{\partial}{\partial t} \left[\overline{v} \frac{\partial H}{\partial x} - \overline{u} \frac{\partial H}{\partial y} \right] + \omega_r \frac{\partial \zeta}{\partial t} - f \frac{\partial \zeta}{\partial t}$$

We can alternatively use the depth-integrated barotropic vorticity (instead of depth averaged):

$$\omega_\Sigma = \frac{\partial H \bar{v}}{\partial x} - \frac{\partial H \bar{u}}{\partial y} = H \omega_r + \left[\bar{v} \frac{\partial H}{\partial x} - \bar{u} \frac{\partial H}{\partial y} \right]$$

where the only difference in the equation will be the term L replaced by:

$$L_\Sigma = -f \frac{\partial \zeta}{\partial t} = f \left[\frac{\partial H \bar{u}}{\partial x} + \frac{\partial H \bar{v}}{\partial y} \right] = f \vec{\nabla} \cdot (H \vec{u})$$

which can be interpreted as planetary vortex stretching of the total layer thickness.

So finally we can write:

$$\underbrace{\frac{\partial \omega_\Sigma}{\partial t}}_{\text{rate}} = - \underbrace{H \vec{u} \cdot \vec{\nabla} f}_{\text{planet. vort.}} - \underbrace{f \vec{\nabla} \cdot (H \vec{u})}_{\text{vort. stretch}} + \underbrace{\frac{J(P_b, h)}{\rho_0}}_{\text{bot. pres. torque}} + \underbrace{\vec{k} \cdot \vec{\nabla} \times \frac{\tau^{\vec{wind}}}{\rho_0}}_{\text{wind curl}} - \underbrace{\vec{k} \cdot \vec{\nabla} \times \frac{\tau^{\vec{bot}}}{\rho_0}}_{\text{bot. drag curl}} + \underbrace{F}_{\text{horiz. dissip.}} - \underbrace{A}_{\text{NL adv terms}} \quad (3)$$