

# SISTEMI RETROAZIONATI: STABILITÀ E PRESTAZIONI

## Esercizio 1

Dato un sistema dinamico a tempo continuo senza autovalori nascosti con funzione di trasferimento

$$G(s) = 10 \frac{1+s}{(1+2s)(1+0.1s)}$$

$$R(s) \approx 1$$

1) TIPO:  $g = 0$

• GUADAGNO:  $\mu = G(0) = 10 = 20\text{dB}$

• Zero:  $z_1 = -1$

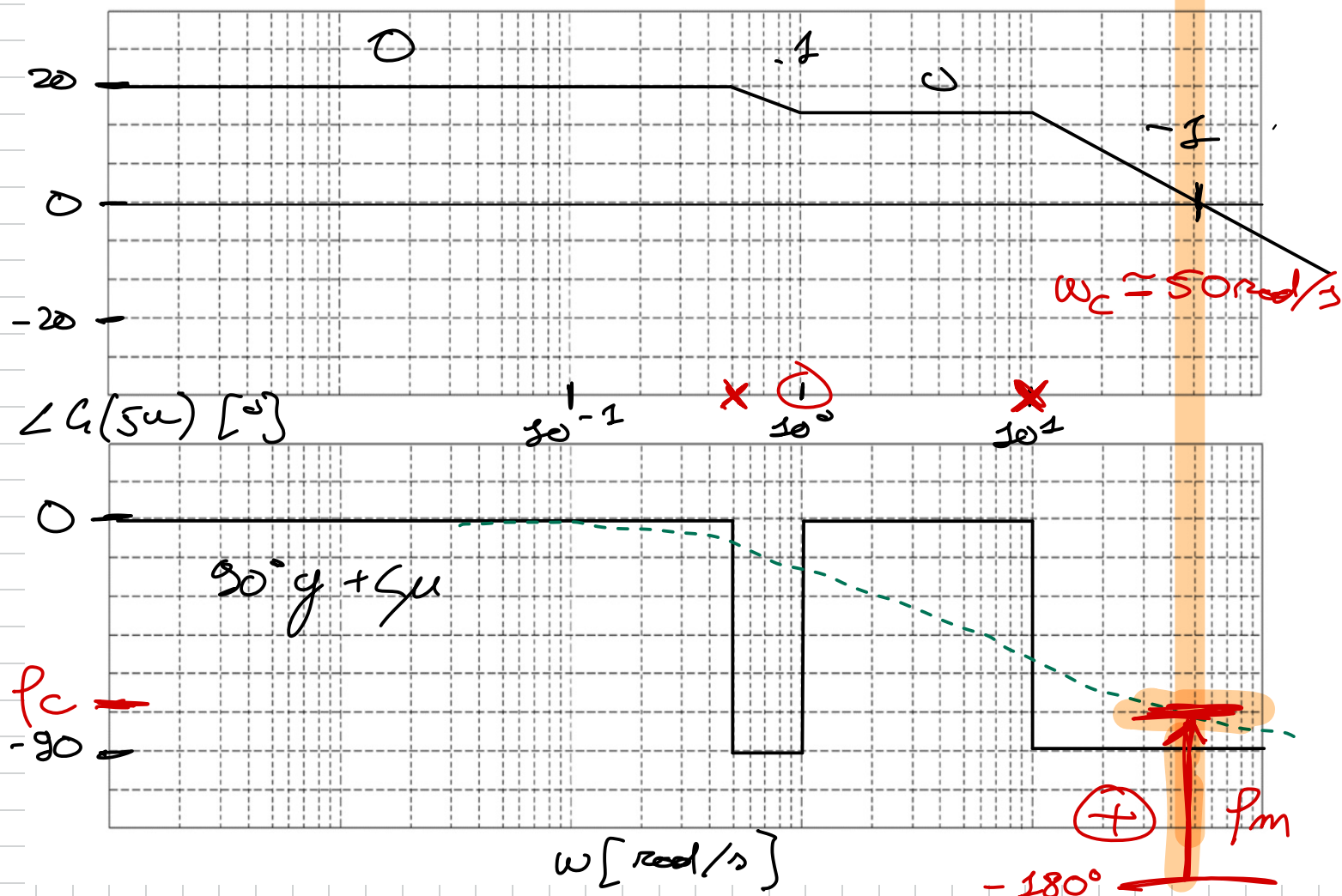
• poli:  $p_1 = -0.5$   $p_2 = -10$

SISTEMA  
A. STAB

SISTEMA  
A FASE MINIMA

2)

$|G(j\omega)| [\text{dB}]$



2)

$$R(s) = 1$$

$$L(s) = G(s) \cdot R(s) = G(s)$$

APPLICHIAMO IL CRITERIO DI BODE

$$\left[ \begin{array}{l} \text{è possibile:} \\ \bullet L(s) \text{ non ha poli "instabili"} \\ \bullet \omega_c \text{ è ben definita} \end{array} \right]$$

$$\bullet \mu_c = 30 > 0 \quad \checkmark$$

$$\bullet \varphi_m > 90^\circ > 0^\circ \quad \checkmark$$

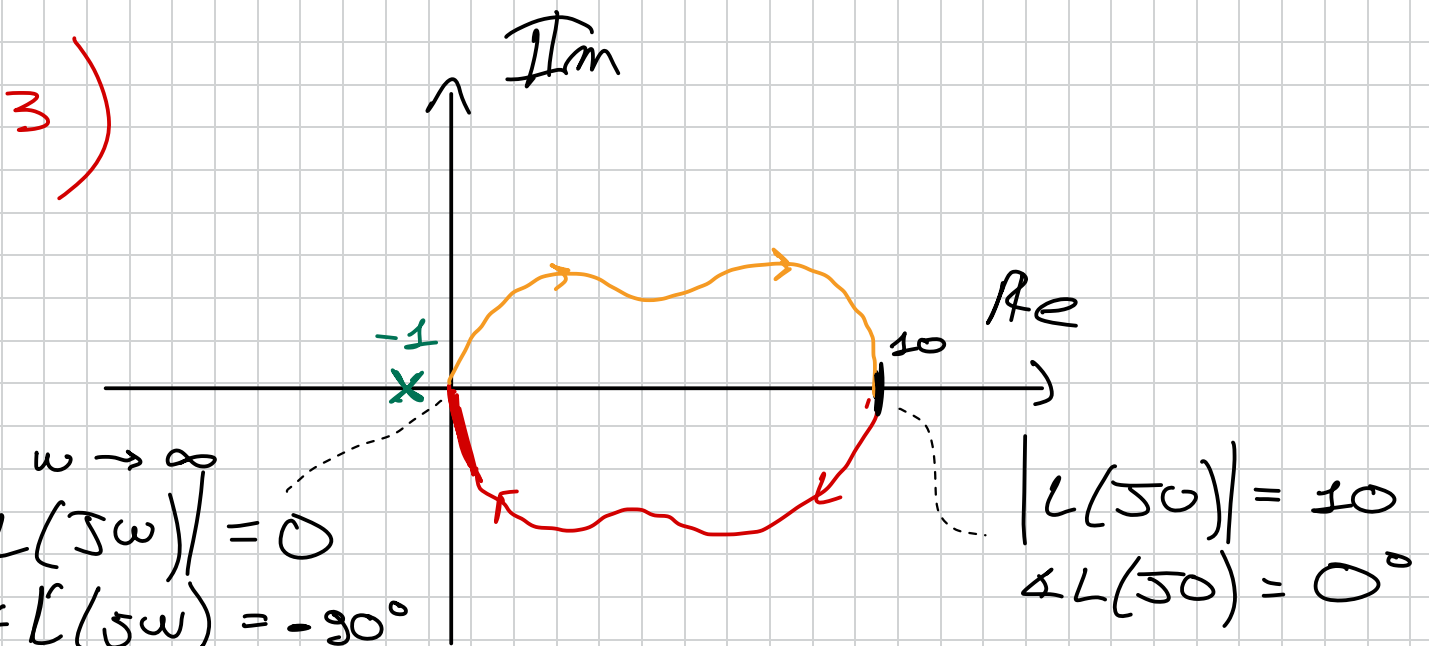
↳ la fase è al massimo  $-90^\circ$  (\*)

⇒ IL SISTEMA RETROAZIONATO È A.S.

OSS: È possibile concludere della stabilità del sistema avvalendosi del "CROCCIO DELLA PICCOLA FASE".

(\*)

"Per sistemi con  $P=0$ , se  $\angle L(j\omega) < -180^\circ$ , il sistema è A.STABILE"

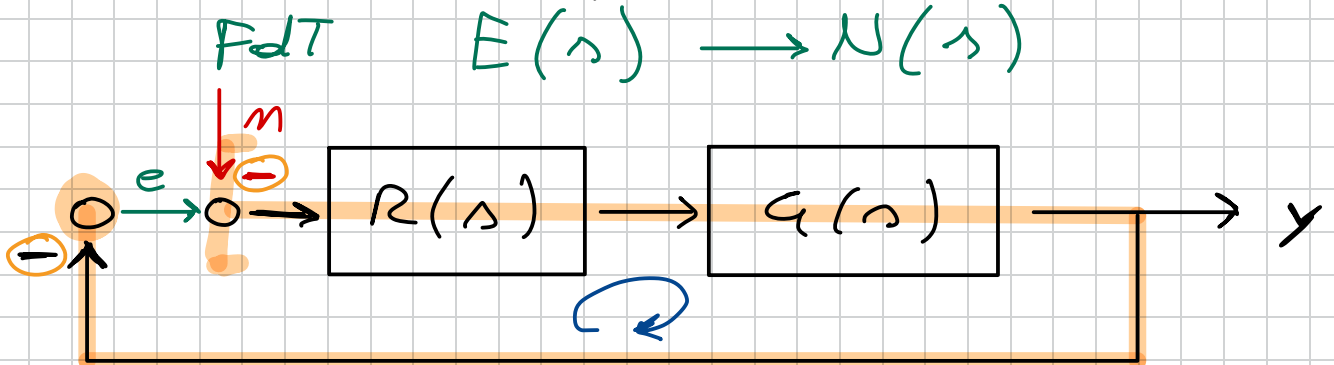


4)  $K_M = \frac{1}{|L(5\omega_c)|}$   $\omega_c$  non è ben definita  $\Rightarrow K_M = \infty$

$\varphi_c = \angle G(5\omega_c) = \cancel{\angle \mu} + \angle(1 + j50) -$   
 $\sim 50 \text{ rad/s}$   
 $\quad \quad \quad - \angle(1 + j250) - \angle(1 + j0,5050)$   
 $= \angle \tan(50) - \angle \tan(100) - \angle \tan(5)$   
 $= \cancel{+90^\circ} \quad \quad \quad \cancel{-90^\circ} \quad \quad \quad -78,7^\circ$   
 $\approx -78,7^\circ$

$\varphi_m = 180^\circ - |\varphi_c| = 101^\circ \rightarrow$  visibile anche graficamente

5) Errore statico  $n(t) \rightarrow \omega(t)$   
 $(y^o(t) = 0, v(t) = 0, d(t) = 0)$   
 $E(s) \rightarrow N(s)$



$$\frac{E(s)}{N(s)} = \frac{-R(s) \cdot G(s) \cdot (-1)}{1 + \underbrace{R(s) G(s)}}$$

retroazione  
negativa

$$\frac{E(s)}{N(s)}$$

=

$$\frac{R(s) \cdot G(s)}{1 + R(s) G(s)}$$

$F(s)$  :

SENSITIVITA'

COMPENSARE

$$[R(s) = 1]$$

$$= \frac{G(s)}{1 + G(s)} N(s)$$

$$G(s) = \frac{\text{num}}{\text{den}}$$

$$E(s) = \frac{\text{num/den}}{1 + \text{num/den}} = \frac{\text{num}}{\text{den} + \text{num}}$$

$$= \frac{10(1+s)}{10(1+s) + (1+2s)(1+0,1s)}$$

UTILIZZO TVF (il sistema e' a. stab.)

$$e_{\infty} = \lim_{s \rightarrow 0} s E(s) =$$

$$= \lim_{s \rightarrow 0} \cancel{s} \frac{10(1+s)}{10(1+s) + (1+2s)(1+0,1s)} \cancel{\frac{1}{s}}$$

$$= \frac{10}{11} = \frac{\mu_L}{\mu_L + 1} A$$



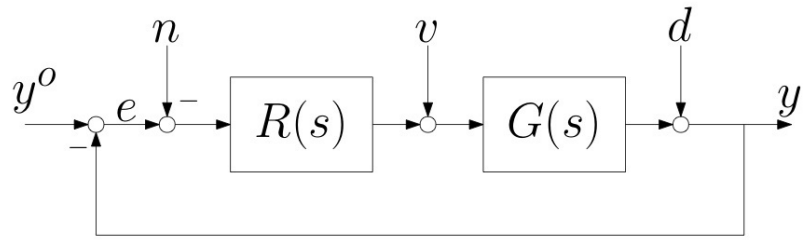
OSS : Riconoscibile da tabella  $F(s)$

$$\left[ g_L = 0, A = 1 \right]$$

↑ ampiezza sedino

## Esercizio 2

Si consideri lo schema di controllo in figura,



in cui

$$G(s) = 3 \frac{1 - 0.1s}{(1 + s)^2}.$$

2.1. Studiare la stabilità del sistema retroazionato quando

- $R(s) = 1$
- $R(s) = \frac{s+1}{3s}$
- $R(s) = \frac{s+1}{3s(1-0.1s)}$

1)  $R(s) = 1$   $L(s) = R(s) \cdot G(s) = G(s)$

• TIPO

• GUADAGNO

• Zero

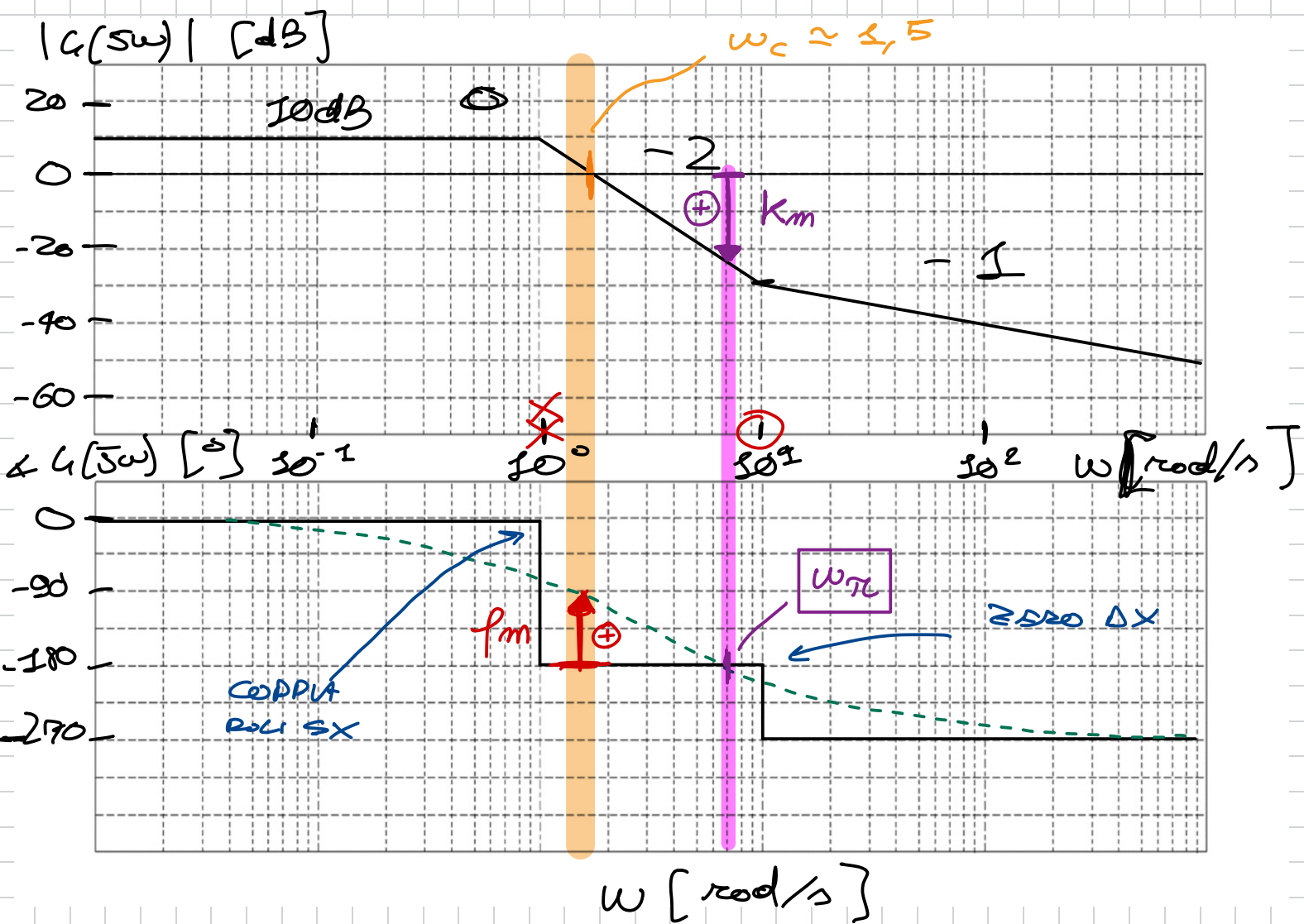
• poli

$$g = 0$$

$$\mu = G(0) = 3 \approx 10 \text{ dB}$$

$$z_z = 10$$

$$p_1 = p_2 = -1$$



BODE APPLICABILE

- $L(s)$  no poli inter.
- $\omega_c \approx 1,5$  rad/s

- $\mu_c > 0$  ✓
- $\phi_m > 0^\circ$  ✓  $\Rightarrow$  A. STAB. IN ANELLO CHIUSO

$$\phi_c = \angle G(j1,5) = \angle \mu + \angle(1 - 0,55 \cdot 1,5) - \angle(1 - j1,5)^2$$

$$= 0^\circ + \arctan(-0,825) - 2 \arctan(1,5)$$

$$= -8,5^\circ - 112,6^\circ = -121,1^\circ$$

$$\phi_m = 180^\circ - |-121,1| = 58,9^\circ > 0$$



$$2) R(s) = \frac{s+1}{3s}$$

$$L(s) = R(s) \cdot G(s) = \frac{s+1}{3s} \cdot \frac{3(1-0,1s)}{(s+1)^2} = \frac{(1-0,1s)}{s(s+1)}$$

• TIPO:  $g = 1$

• QUADAGNO GENERALIZZATO

$$\mu = \lim_{s \rightarrow 0} s^g L(s) = 1$$

• polo

$$p_1 = -1$$

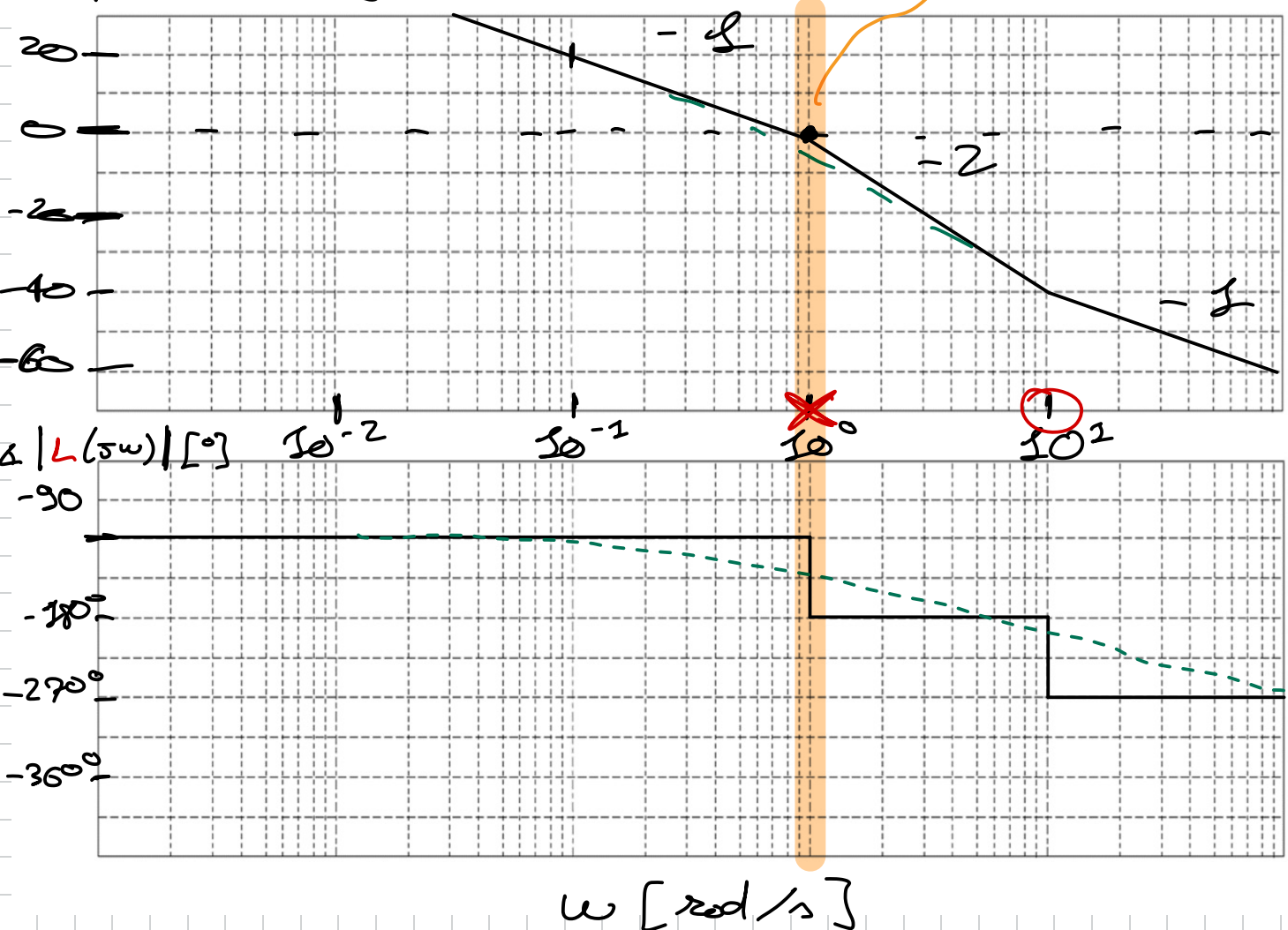
circa per il taglio del grafico RETE del modulo

$$\omega_c \approx 1 \text{ rad/s}$$

• zero

$$z_1 = 10$$

$|L(j\omega)|$  [dB]



BODE APPLICABILE ✓ ( $\omega_c \sim 1 \text{ rad/s}$ )

$$\begin{aligned} \varphi_c &= \angle G(j1) = \angle \mu + \angle(1 - j0, 1) - \angle(j) - \angle(1 + j) \\ &= 0^\circ + \angle(-0, 1) - 90^\circ - \arctan(1) \\ &= -5,7^\circ - 90^\circ - 45^\circ = -140^\circ \end{aligned}$$

$$\varphi_m = 180^\circ - |\varphi_c| = 40^\circ$$

$$\begin{aligned} \mu_c &> 0 \\ \varphi_m &> 0^\circ \end{aligned}$$

$\Rightarrow$

SIST. RETROAZIONATO  
A. STAB X BODE

COME CALCOLARE  $\omega_c$  ANALITICAMENTE?

per ottenere energia "reale":  $|L(j\omega_c)| = 1$

$$|L(j\omega)| = \frac{|1 - j0,1j\omega_c|}{|j\omega_c + 1| |j\omega_c|} = \frac{\sqrt{1^2 + (10^{-1}\omega_c)^2}}{\sqrt{\omega_c^2 + 1} \sqrt{\omega_c^2}} = 1^2$$

$$\frac{1 + 10^{-2} \omega_c^2}{(\omega_c^2 + 1) \omega_c^2} = 1$$



$$\Rightarrow \omega_c^4 + \omega_c^2 = 1 + 10^{-2} \omega_c^2$$

$$\omega_c^4 + 0,99 \omega_c^2 - 1 = 0$$

$$z^2 + 0,99z - 1 = 0$$

$$\omega_c^2 = 2$$

$z_{1,2}$   
positivo

$$z_{1,2} = -\frac{0,99}{2} \pm \sqrt{\frac{0,99^2 + 4}{2}} = \begin{cases} +0,6208 \\ -1,6108 \end{cases}$$

$$\omega_c^2 = 0,6208 \text{ (rad/s)}^2$$

$$\varphi_c = 4L(50,7879) =$$

$$\omega_c = 0,7879 \text{ rad/s} \rightarrow$$

NOTA:

Utilizzando il valore preso dal diagramma abbiamo sovrastimato  $\omega_c$  e sottostimato  $\varphi_m$ . Ma l'approssimazione è efficace per l'analisi di stabilità!

$$3) R(s) = \frac{s+1}{3s(1-\underline{0,1s})}$$

REGOLATORE  
INSTABILE

$$L(s) = R(s) G(s) = \frac{s+1}{3s(1-\underline{0,1s})} \cdot \frac{3(1-\underline{0,1s})}{(s+1)^2} =$$

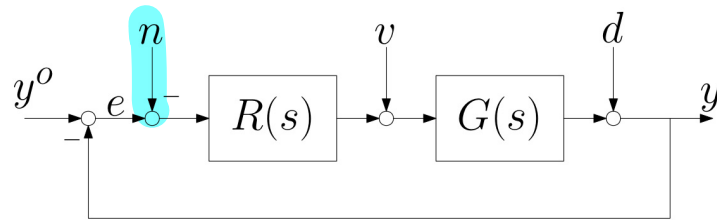
$$= \frac{1}{s(s+1)}$$

$\Rightarrow$  CANCELLAZIONE CRITICA

$\Rightarrow$  SISTEMA RETROAZIONATO È INSTABILE !!

### Esercizio 3

Si consideri lo schema di controllo in figura,



in cui

$$R(s) = \frac{1}{s}$$

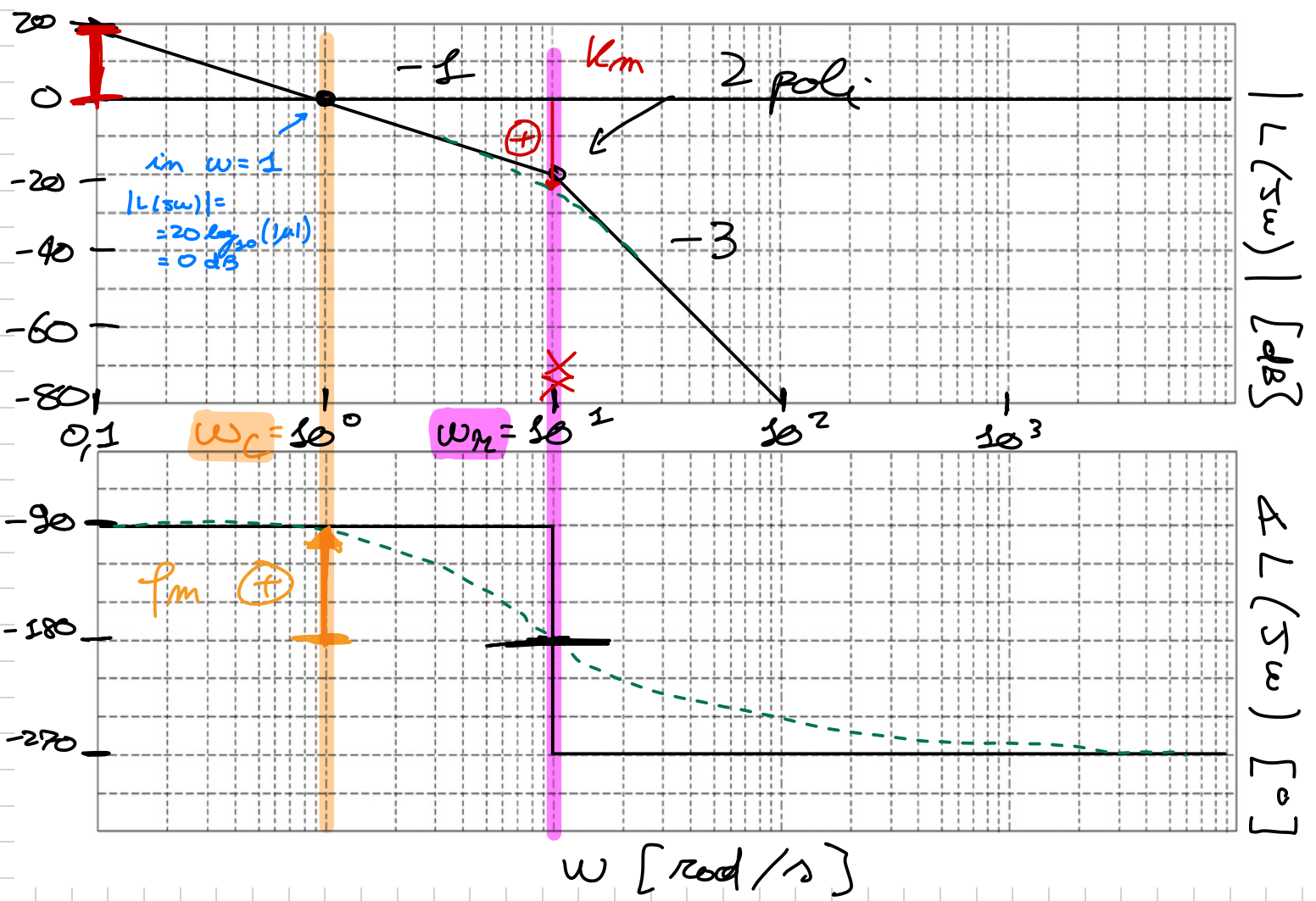
e

$$G(s) = \frac{1}{(1 + 0.1s)^2}$$

1)  $L(s) = R(s) \cdot G(s) = \frac{1}{s(1 + 0.1s)^2}$

- TIPO :  $y = 1$
- QUADRO :  $\mu = 1$
- poli :  $p_1 = p_2 = -10$

SISTEMA A  
FASE MINIMA



IL SISTEMA RETROAZIONATO È STABILE?

$$\bullet \mu_L = 1 > 0 \quad \checkmark$$

$$\bullet \varphi_m = 180^\circ - |\varphi_c| \approx 90^\circ > 0^\circ \quad \checkmark$$

$\Rightarrow$  SISTEMA RETROAZ. A. STAB. x BODE  
(BODE APPLICABILE:  $\bullet L(s)$  no poli int.  $\bullet \omega_c$  ben definita  $\sim 1 \text{ rad/s}$ )

COME CALCOLARE  $\omega_{\pi}$  ANALITICAMENTE?

$$K_m = \frac{1}{|L(j\omega_{\pi})|} \quad (\text{margine di guadagno})$$

$$\angle L(j\omega_{\pi}) = -180^\circ$$

$$\underbrace{-j\omega_{\pi}}_{-90^\circ} - \arctan\left(\frac{0,1\omega_{\pi}}{1}\right) = -180^\circ$$

$$-\arctan(0,1\omega_{\pi}) = -90^\circ$$

$$\arctan\left(\underbrace{0,1\omega_{\pi}}_1\right) = 45^\circ$$

$$\Rightarrow 0,1\omega_{\pi} = 1$$

$$\Rightarrow \omega_{\pi} = 10 \text{ rad/s}$$

$$\left| L(j\omega_c) \right| = \frac{1}{|10j| |1 + 0,1j \cdot 10|^2} = \frac{1}{20}$$

$$K_m = \frac{1}{|L(j\omega_c)|} = 20$$

$$K_m|_{dB} \approx 26 \text{ dB}$$

CHECK DAT. GRAFICO!

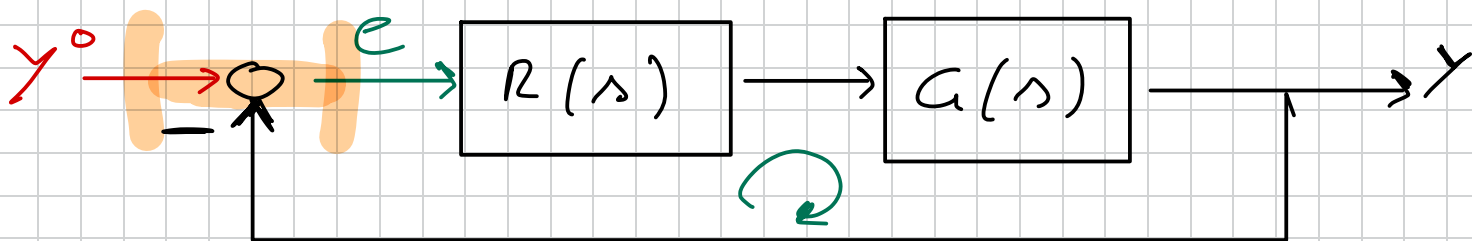
2)  $|e_\infty|_{\text{con}} \cdot y^\circ(t) = 4 \text{ ramp}(t)$

•  $n(t) = 0,1 \text{ sco}(t)$

•  $d(t) = 2 \sin(0,1 t)$

Andiamo a calcolare le FdT tra  $Y^\circ(s)$ ,  $N(s)$ ,  $D(s)$  e  $E(s)$

•  $Y^\circ(s) \rightarrow E(s)$

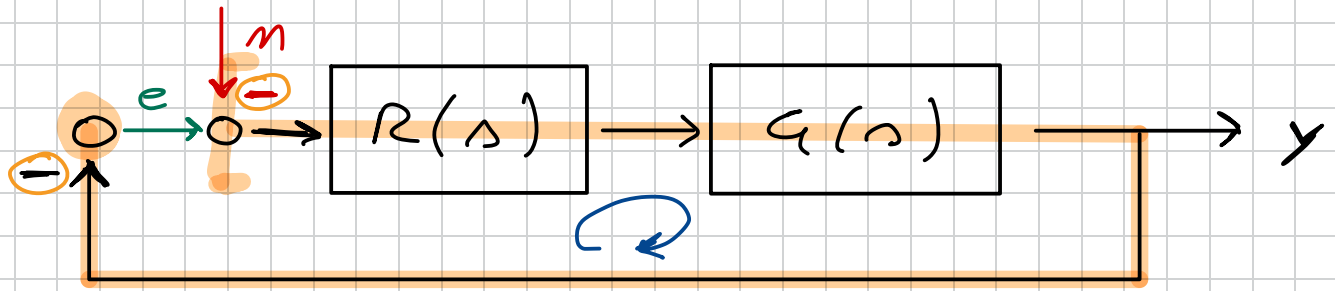


$$\frac{E(s)}{Y^\circ(s)} = \frac{1}{1 + \underbrace{R(s)}_{\text{RETRAS. NEG}} \underbrace{G(s)}_{\text{FUNZIONE D'ANFELLO}}}$$

FUNZIONE DI ANDATA

$$= \boxed{S(s)} \quad \text{SENSITIVITA'}$$

- $N(s) \rightarrow E(s)$

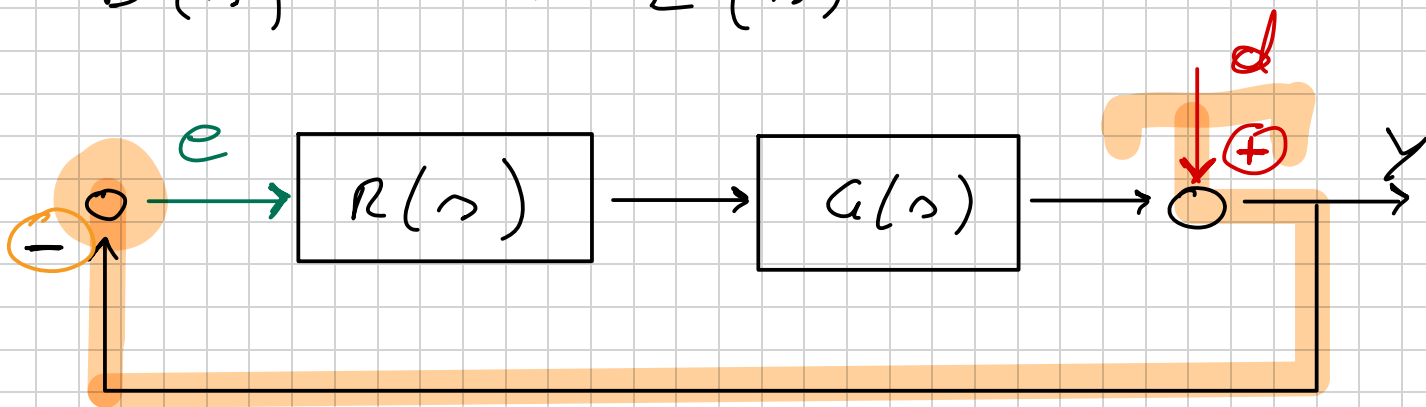


$$\frac{E(s)}{N(s)} = \frac{-R(s) \cdot G(s) \cdot (-1)}{1 + \underbrace{R(s)G(s)}} = \boxed{F(s)}$$

retroazione negativa

SENSITIVITÀ COMPENSARE

- $D(s) \rightarrow E(s)$



$$\frac{E(s)}{D(s)} = \frac{-1}{1 + R(s)G(s)} = \boxed{-S(s)}$$

SOVRAPPONENDO GLI EFFETTI ABBIAMO  
COSÌ OTTENUTO LA DIPENDENZA DINAMICA  
DI  $E(s)$  DAGLI ALTRI SEGNALE

$$E(s) = S(s) Y^o(s) - S(s) D(s) + F(s) N(s)$$

①  $Y^o(s) = \frac{4}{s^2}$

$e_{\infty, y_0} \stackrel{\text{TVE}}{=} \lim_{s \rightarrow 0} s \cdot S(s) \frac{4}{s^2} =$

$$= \lim_{s \rightarrow 0} \frac{4 [s(1 + 0,1s)^2]}{s(1 + s(1 + 0,1s)^2)} = 4$$

OSS : da tabella di  $S(s)$  :  $e_{\infty} = \frac{A}{\mu_L}$

②  $N(s) = \frac{0,1}{s}$

$e_{\infty, n} \stackrel{\text{TVE}}{=} \lim_{s \rightarrow 0} s F(s) \frac{0,1}{s} = \lim_{s \rightarrow 0} 0,1 F(s)$

$$= \lim_{s \rightarrow 0} \frac{0,1}{1 + s(1 + 0,1s)^2} = 0,1$$

③  $d(e) = 2 \sin(0,1e)$

T. RISPOSTA  
IN FREQ  
(non modulo)

:  $|e_{\infty, d}| = 2 | \cancel{S}(j0,1) |$



$$\omega = 0,1 \ll \omega_c = 1 \text{ rad/s}$$

APPROSSIMAZ. BASSA FREQ

$$|S(j\omega)| = \frac{1}{1 + |L(j\omega)|} \approx \frac{1}{|L(j\omega)|} \approx \frac{2}{10}$$

$$|L(j\omega)|_{dB} = 20 \text{ dB} = 10$$

dol' ditz di Bode

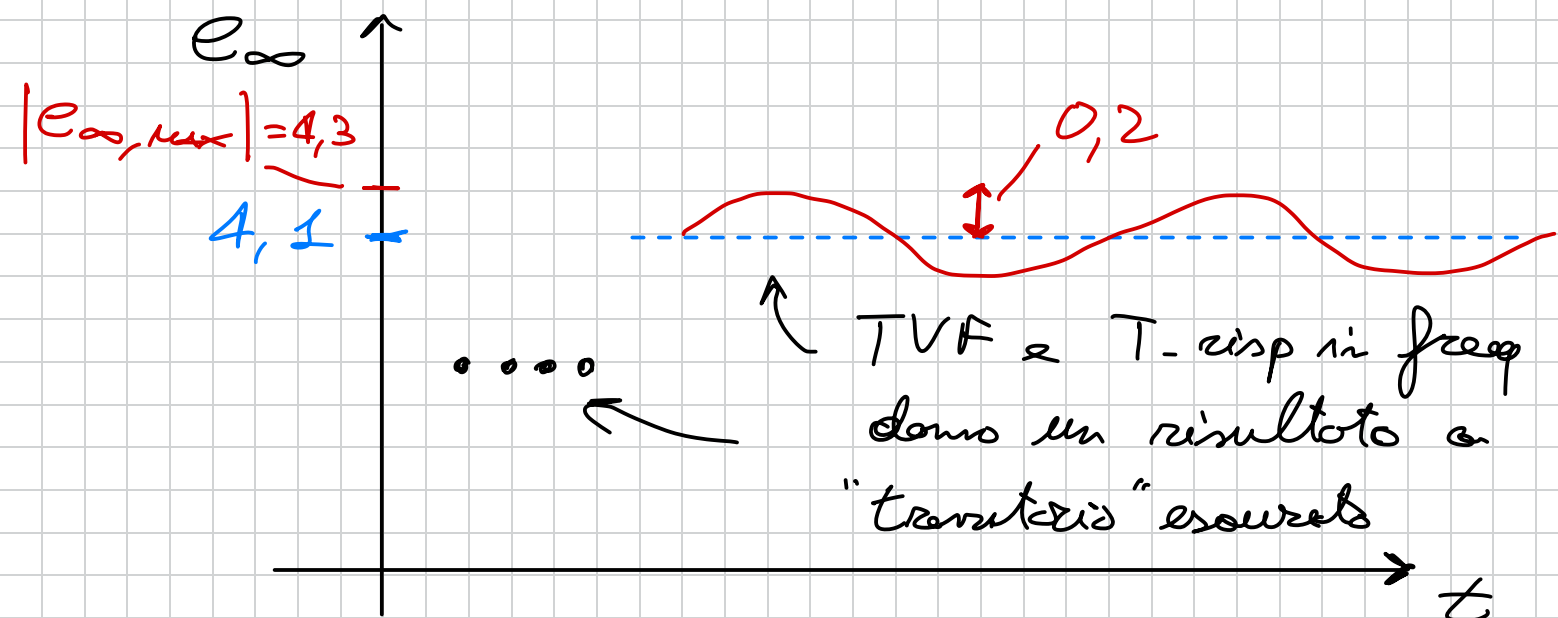
$$\Rightarrow |e_{\infty, d}| = 0,2$$

SOVRAPPONENDO GLI EFFETTI ①, ②, ③ :

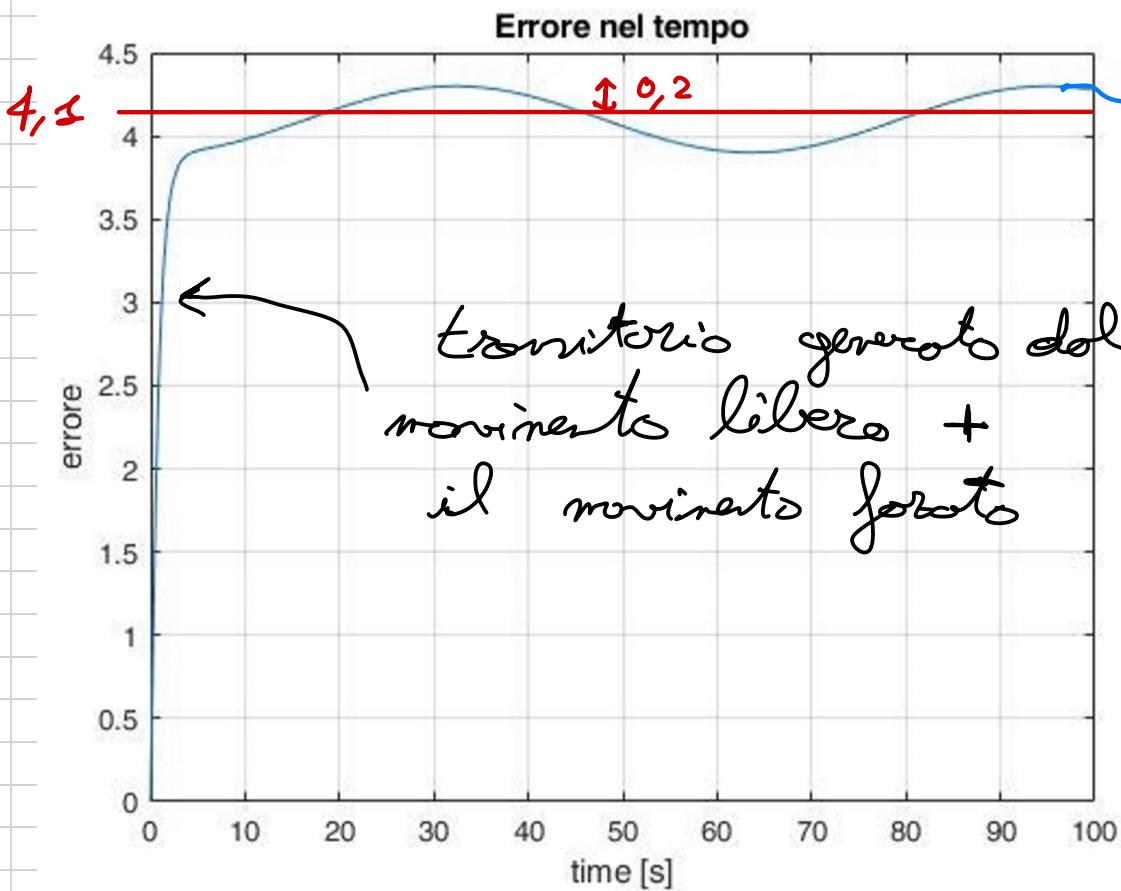
$$|e_{\infty}| = \underline{e_{\infty, y^0}} + \underline{e_{\infty, m}} + \underline{e_{\infty, d}}$$

$$|e_{\infty, \max}| = 4 + 0,1 + \underline{0,2} = 4,3$$

$|e_{\infty, d}|_{\max}$



SIMULAZIONE CON MATLAB:



A REGIME  
MOVIMENTO  
DATO SOLO  
DALLA  
FORZANTE  
( $y$ ,  $m$ ,  $d$ )