ECE 6310 - Advanced Electromagnetic Fields: Homework Set #1

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1 Preliminaries

In this document, we use standard notation for electromagnetic theory. Key equations and concepts are summarized below:

Vector Notation

- 8: Electric field intensity
- **%**: Magnetic field intensity
- **2**: Electric flux density
- \mathcal{B} : Magnetic flux density
- **J**: Current density
- ρ_v : Volume charge density

Differential Operators

- $\bullet \ \nabla \cdot \ :$ Divergence of a vector field
- $\nabla \times$: Curl of a vector field
- \bullet ∇ : Gradient of a scalar field
- $\bullet \ \partial_i \ :$ Partial derivative with respect to the independent basis element i

Maxwell's Equations

In integral form, Maxwell's equations are given by:

$$\oint_{\partial V} \mathcal{E} \cdot d\mathcal{E} = -\frac{d}{dt} \int_{V} \mathcal{B} \cdot d\mathcal{S} \qquad \text{(Faraday's Law of Induction)}$$

$$\oint_{\partial V} \mathcal{H} \cdot d\mathcal{E} = \int_{V} \mathcal{J} \cdot d\mathcal{S} + \frac{d}{dt} \int_{V} \mathcal{D} \cdot d\mathcal{S} \qquad \text{(Ampère's Circuital Law)}$$

$$\oint_{\partial V} \mathcal{D} \cdot d\mathcal{S} = \int_{V} \rho_{v} dV \qquad \text{(Gauss's Law for Electricity)}$$

$$\iint_{\partial V} \mathcal{B} \cdot d\mathcal{S} = 0 \qquad \text{(Gauss's Law for Magnetism)}$$

$$(4)$$

Other Relevant Equations

- Continuity Equation: $\nabla \cdot \mathbf{J} + \partial_t \rho_v = 0$
- Relationship between \mathcal{E} , \mathcal{D} : $\mathcal{D} = \epsilon \mathcal{E}$
- Relationship between \mathcal{H} , \mathcal{B} : $\mathcal{B} = \mu \mathcal{H}$

Boundary Conditions

Discuss the boundary conditions for \mathcal{E} , \mathcal{H} , \mathcal{D} , and \mathcal{B} at interfaces between different media.

Problem 1.3

The electric flux density inside a cube is given by:

(a)
$$\vec{D} = \hat{a}_x(3+x)$$

(b)
$$\vec{D} = \hat{a}_y(4+y^2)$$

Find the total electric charge enclosed inside the cubical volume when the cube is in the first octant with three edges coincident with the x, y, z axes and one corner at the origin. Each side of the cube is 1 m long.

Ok, this one we can do by using the following expressions from the text [1]:

$$\iint_{s} \mathcal{D}ds = \iiint_{v} \mathcal{Q}_{ev}dv = \mathcal{Q}_{e}$$
 (5)

$$q_{ev} = \Delta \cdot \mathbf{D} \tag{6}$$

We apply expression 6 then plug into expression 5 to get the total electric charge.

$$\iiint_{V} \mathcal{Q}_{ev} = \iiint_{V} \Delta \cdot (\hat{a}_{x}(3+x))dV = \iiint_{V} \partial_{x}(\hat{a}_{x}(3+x))dV = \iiint_{0}^{1} 1dV = 1$$

$$\iiint_{V} \mathcal{Q}_{ev} = \iiint_{V} \Delta \cdot (\hat{a}_{y}(4+y^{2}))dV = \iiint_{V} \partial_{y}(\hat{a}_{y}(4+y^{2}))dV = \iiint_{0}^{1} 2y \ dV$$

$$\iiint_{0}^{1} 2y \ dV = \iint_{0}^{1} \int_{0}^{1} 2y dy \ ds = \iint_{0}^{1} y^{2}|_{0}^{1} ds = \iint_{0}^{1} (1-0) \ ds = 1$$

Problem 1.4

An infinite planar interface between media, as shown in the figure, is formed by having air (medium #1) on the left of the interface and lossless polystyrene (medium #2) to the right of the interface. An electric surface charge density $\sigma_{es} = 0.2 \,\mathrm{C/m^2}$ exists along the entire interface. The static electric flux density inside the polystyrene is given by $\vec{D}_2 = 6\hat{a}_x + 3\hat{a}_z \,\mathrm{C/m^2}$. Determine the corresponding vector:

(a) Electric field intensity inside the polystyrene. we can find this using the following expression for the Electric field intensity vector:

$$\epsilon_{poly} = 2.56\epsilon_0$$

$$\mathbf{\mathcal{G}} = \epsilon \mathbf{\mathcal{E}}$$

$$\mathbf{\mathcal{E}} = \epsilon^{-1} \mathbf{\mathcal{G}} = 0.390625\epsilon_0^{-1} \cdot \mathbf{\mathcal{G}} = \epsilon_0^{-1} (2.34 \cdot a_x + 1.17 \cdot a_z)$$

(b) Electric polarization vector inside the polystyrene. we can find this using the following expression for the polarization vector:

$$\mathbf{\mathcal{P}}_{e} = \epsilon_{0} \chi_{e} \mathbf{\mathcal{E}}$$

$$\chi_{e} = \epsilon_{r} - 1 = 2.56 - 1 = 1.56$$

$$\mathbf{\mathcal{P}}_{e} = 1.56 \epsilon_{0} \epsilon_{0}^{-1} (2.34 \cdot a_{x} + 1.17 \cdot a_{z}) = 3.6504 \cdot a_{x} + 1.8252 \cdot a_{z}$$

(c) Electric flux density inside the air medium.

By the continuity of tangential components at the boundary:

 $\hat{\mathbf{n}} \times (\mathbf{\mathcal{E}}_2 - \mathbf{\mathcal{E}}_1) = 0$

we apply the following.

$$\mathbf{\mathcal{E}}_{air} = \mathbf{\mathcal{E}}_{Poly}$$

$$\mathbf{\mathcal{D}}_{air} = \epsilon_{air} \mathbf{\mathcal{E}}_{air}$$

$$\therefore \mathbf{\mathcal{D}}_{air} \epsilon_{air}^{-1} = \mathbf{\mathcal{D}}_{Poly} \epsilon_{Poly}^{-1}$$

$$\mathbf{\mathcal{D}}_{air} = \frac{\epsilon_{air}}{\epsilon_{Poly}} \mathbf{\mathcal{D}}_{Poly} = \frac{\epsilon_{0} \cdot 1}{\epsilon_{0} \cdot 2.56} \cdot \mathbf{\mathcal{D}}_{Poly}$$

$$= \frac{6}{2.56} a_{x} = 2.34 \cdot a_{x}$$

The normal components at the boundary are not continuous and therefore we must do more.

The normal is \hat{a}_z

$$\hat{\mathbf{n}} \cdot (\mathbf{\mathcal{D}}_2 - \mathbf{\mathcal{D}}_1) = q_{es}$$

$$\hat{a}_z \cdot (\mathcal{D}_2 - \mathcal{D}_1) = 0.2$$

 $\mathcal{D}_{1z} = \mathcal{D}_{2z} - 0.2 = 3 - .2 = 2.8$

(d) Electric field intensity inside the air medium.

Again using the expression $\mathcal{D} = \epsilon \mathcal{E}$

$$\mathcal{D}_{air} = \epsilon_{air} \mathcal{E}_{air}$$

$$\mathcal{E}_{air} = \epsilon_{air}^{-1} \mathcal{D}_{air}$$

$$= \epsilon_0^{-1} (2.34 \cdot a_x + 2.8 \cdot a_z)$$

(e) Electric polarization vector inside the air medium. Again using $\mathbf{\mathscr{P}}_e = \epsilon_0 \chi_e \mathbf{\mathscr{E}}$

$$\mathcal{P}_{e_{air}} = \epsilon_0 \chi_{e_{air}} \mathcal{E}_{air}$$

$$= \chi_{e_{air}} \epsilon_0 \epsilon_0^{-1} (2.34 \cdot a_x + 2.8 \cdot a_z)$$

$$\chi_{e_{air}} = \epsilon_{r_{air}} - 1 = 1 - 1 = 0$$

$$\therefore \mathcal{P}_{e_{air}} = \mathbf{0}$$

Leave your answers in terms of ϵ_0, μ_0 .

Problem 1.13

The instantaneous magnetic flux density in free space is given by:

$$\mathcal{B} = \hat{a}_x B_x \cos(2y) \sin(\omega t - \pi z) + \hat{a}_y B_y \cos(2x) \cos(\omega t - \pi z)$$

where B_x and B_y are constants. Assuming there are no sources at the observation points x, y, determine the electric displacement current density. We can obtain the electric displacement current \mathcal{J}_d by using the following expressions:

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_i + \boldsymbol{J}_c + \boldsymbol{J}_d \tag{7}$$

$$\boldsymbol{B} = \mu \boldsymbol{H} \tag{8}$$

$$\boldsymbol{J}_d = \frac{\partial \boldsymbol{D}}{\partial t} \tag{9}$$

We take $J_i + J_c$ to be 0 since we have no sources at the observation points. Using expression 7 and solving expression 8 for H:

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_{d}$$

$$\boldsymbol{J}_{d} = \nabla \times \mu^{-1} \boldsymbol{B}$$

$$\boldsymbol{J}_{d} = \mu^{-1} \nabla \times \boldsymbol{B}$$

$$= \mu^{-1} \left[\hat{a}_{x} \left(\frac{\partial \boldsymbol{B}_{z}}{\partial y} - \frac{\partial \boldsymbol{B}_{y}}{\partial z} \right) - \hat{a}_{y} \left(\frac{\partial \boldsymbol{B}_{z}}{\partial x} - \frac{\partial \boldsymbol{B}_{x}}{\partial z} \right) + \hat{a}_{z} \left(\frac{\partial \boldsymbol{B}_{y}}{\partial x} - \frac{\partial \boldsymbol{B}_{x}}{\partial y} \right) \right]$$

$$\boldsymbol{B}_{z} = 0$$

$$= \mu^{-1} \left[\hat{a}_{x} \left(0 - \frac{\partial \boldsymbol{B}_{y}}{\partial z} \right) - \hat{a}_{y} \left(0 - \frac{\partial \boldsymbol{B}_{x}}{\partial z} \right) + \hat{a}_{z} \left(\frac{\partial \boldsymbol{B}_{y}}{\partial x} - \frac{\partial \boldsymbol{B}_{x}}{\partial y} \right) \right]$$

$$= \mu^{-1} \left[-\hat{a}_{x} \frac{\partial \boldsymbol{B}_{y}}{\partial z} + \hat{a}_{y} \frac{\partial \boldsymbol{B}_{x}}{\partial z} + \hat{a}_{z} \left(\frac{\partial \boldsymbol{B}_{y}}{\partial x} - \frac{\partial \boldsymbol{B}_{x}}{\partial y} \right) \right]$$

$$\frac{\partial \boldsymbol{B}_{x}}{\partial z} = -\pi B_{x} \cos(2y) \cos(\omega t - \pi z)$$

$$\frac{\partial \boldsymbol{B}_{y}}{\partial z} = \pi B_{y} \cos(2x) \sin(\omega t - \pi z)$$

$$\frac{\partial \boldsymbol{B}_{y}}{\partial z} = -2 \sin(2x) \cos(\omega t - \pi z)$$

$$\frac{\partial \boldsymbol{B}_{y}}{\partial x} = -2 \sin(2y) \sin(\omega t - \pi z)$$

$$= \mu^{-1} \left[\hat{a}_{x} (-\pi B_{y} \cos(2x) \sin(\omega t - \pi z)) + \hat{a}_{y} (-\pi B_{x} \cos(2y) \cos(\omega t - \pi z) \right]$$

$$\hat{a}_{z} 2 (\sin(2y) \sin(\omega t - \pi z) - \sin(2x) \cos(\omega t - \pi z))$$

Problem 1.20

The instantaneous electric field inside a conducting rectangular pipe (waveguide) of width a is given by:

$$\mathscr{E} = \hat{a}_y E_0 \sin\left(\frac{\pi x}{a}\right) \cos(\omega t - \beta_z z)$$

where β_z is the waveguide's phase constant. Assuming there are no sources within the free-space-filled pipe determine the:

- (a) Corresponding instantaneous magnetic field components inside the conducting pipe. (\mathcal{H})
- (b) Phase constant β_z .

The height of the waveguide is b. This can be found by relating \mathscr{E} to \mathscr{H} and we know how to get there using the instantaneous forms of these:

$$\mathcal{E} = -j\omega\mu\nabla\times\mathcal{H}$$

$$\mathcal{H} = \frac{j}{\omega\mu}\nabla\times\mathcal{E}$$

$$\frac{j}{\omega\mu}\nabla\times\mathbf{\mathcal{E}} = \frac{j}{\omega\mu}\left[\hat{a}_x\left(\frac{\partial\mathbf{E}_z}{\partial y} - \frac{\partial\mathbf{E}_y}{\partial z}\right) - \hat{a}_y\left(\frac{\partial\mathbf{E}_z}{\partial x} - \frac{\partial\mathbf{E}_x}{\partial z}\right) + \hat{a}_z\left(\frac{\partial\mathbf{E}_y}{\partial x} - \frac{\partial\mathbf{E}_x}{\partial y}\right)\right]$$

$$\begin{split} \frac{j}{\omega\mu} \nabla \times \mathbf{\mathcal{E}} &= \frac{j}{\omega\mu} \left[\hat{a}_x \left(0 - \frac{\partial \mathbf{E}_y}{\partial z} \right) - \hat{a}_y \left(0 - 0 \right) + \hat{a}_z \left(\frac{\partial \mathbf{E}_y}{\partial x} - 0 \right) \right] \\ \frac{j}{\omega\mu} \nabla \times \mathbf{\mathcal{E}} &= -\frac{j}{\omega\mu} \left[\hat{a}_x \frac{\partial \mathbf{E}_y}{\partial z} - \hat{a}_z \frac{\partial \mathbf{E}_y}{\partial x} \right] \\ \mathbf{\mathcal{E}} &= \hat{a}_y E_0 \sin \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z) \\ \frac{\partial \mathbf{E}_y}{\partial x} &= \left(\frac{\pi}{a} \right) E_0 \cos \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z) \\ \frac{\partial \mathbf{E}_y}{\partial z} &= (\beta_z) E_0 \sin \left(\frac{\pi x}{a} \right) \sin(\omega t - \beta_z z) \\ \mathbf{\mathcal{E}} &= -\frac{j}{\omega\mu} \left[\hat{a}_x \left(\beta_z \right) E_0 \sin \left(\frac{\pi x}{a} \right) \sin(\omega t - \beta_z z) - \hat{a}_z \left(\frac{\pi}{a} \right) E_0 \cos \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z) \right] \end{split}$$

Solving for β_z , we can use first expression for the $\nabla \times \mathcal{H}$:

$$\nabla \times \mathcal{H} = (-j\omega\mu)^{-1}\mathcal{E}$$

$$\nabla \times \mathcal{H} = \left[\hat{a}_x \left(\frac{\partial \mathbf{H}_z}{\partial y} - \frac{\partial \mathbf{H}_y}{\partial z} \right) - \hat{a}_y \left(\frac{\partial \mathbf{H}_z}{\partial x} - \frac{\partial \mathbf{H}_x}{\partial z} \right) + \hat{a}_z \left(\frac{\partial \mathbf{H}_y}{\partial x} - \frac{\partial \mathbf{H}_x}{\partial y} \right) \right]$$

The expression for \mathcal{H} we found does not have any dependence on y, and only has x and z components:

$$\nabla \times \mathcal{H} = \left[\hat{a}_x (0 - 0) - \hat{a}_y \left(\frac{\partial \mathbf{H}_z}{\partial x} - \frac{\partial \mathbf{H}_x}{\partial z} \right) + \hat{a}_z (0 - 0) \right]$$

$$= -\hat{a}_y \left(\frac{\partial \mathbf{H}_z}{\partial x} - \frac{\partial \mathbf{H}_x}{\partial z} \right)$$

$$= -\frac{j}{\omega \mu} \hat{a}_y \left(\left(\frac{\pi}{a} \right)^2 E_0 \sin \left(\frac{\pi x}{a} \right) \cos \left(\omega t - \beta_z z \right) - \beta_z^2 E_0 \sin \left(\frac{\pi x}{a} \right) \cos \left(\omega t - \beta_z z \right) \right)$$

$$= \hat{a}_y \frac{j}{\omega \mu} \left(\beta_z^2 - \left(\frac{\pi}{a} \right)^2 \right) E_0 \sin \left(\frac{\pi x}{a} \right) \cos \left(\omega t - \beta_z z \right) = \hat{a}_y \frac{j}{\omega \mu} \left(\beta_z^2 - \left(\frac{\pi}{a} \right)^2 \right) \mathcal{H}$$

$$\therefore \omega \mu = \frac{1}{\omega \mu} \left(\beta_z^2 - \left(\frac{\pi}{a} \right)^2 \right)$$

$$\beta_z^2 = (\omega \mu)^2 + \left(\frac{\pi}{a} \right)^2$$

$$\beta_z = \pm \sqrt{(\omega \mu)^2 + \left(\frac{\pi}{a} \right)^2}$$

Problem 2.18

The time-varying electric field inside a lossless dielectric material of polystyrene, of infinite dimensions and with a relative permittivity (dielectric constant) of 2.56, is given by:

$$\vec{\mathscr{E}} = \hat{a}_z 10^{-3} \sin(2\pi \times 10^7 t) \,\mathrm{V/m}$$

Determine the corresponding:

(a) Electric susceptibility of the dielectric material.

$$\chi_e = \epsilon_r - 1 = 1.56$$

(b) Time-harmonic electric flux density vector.

$$\mathbf{D} = \epsilon \mathbf{E} = \hat{a}_z 2.56 \times 10^{-3} \epsilon_0 \sin(2\pi \times 10^7 t)$$

(c) Time-harmonic electric polarization vector.

$$\mathbf{P} = \chi_e \epsilon_0 \mathbf{E} = \hat{a}_z 1.56 \times 10^{-3} \epsilon_0 \sin(2\pi \times 10^7 t)$$

(d) Time-harmonic displacement current density vector.

$$\mathbf{J}_d = \frac{\partial \mathbf{D}}{\partial t} = \hat{a}_z 2.56 \times 10^{-3} \times 2\pi \times 10^7 \epsilon_0 \cos(2\pi \times 10^7 t)
= \hat{a}_z 1.65 \times 10^5 \epsilon_0 \cos(2\pi \times 10^7 t)$$

(e) Time-harmonic polarization current density vector defined as the partial derivative of the corresponding electric polarization vector.

$$J_p = \frac{\partial \mathbf{P}}{\partial t} = \hat{a}_z 1.56 \times 10^{-3} \times 2\pi \times 10^7 \epsilon_0 \cos(2\pi \times 10^7 t)$$
$$= \hat{a}_z 9.80 \times 10^4 \epsilon_0 \cos(2\pi \times 10^7 t)$$

Leave your answers in terms of ϵ_0, μ_0 .

Problem 2.25

Aluminum has a static conductivity of about $\sigma = 3.96 \times 10^7 \,\mathrm{S/m}$ and an electron mobility of $\mu_e = 2.2 \times 10^{-3} \,\mathrm{m^2/(V-s)}$. Assuming that an electric field of $\vec{E} = \hat{a}_x 2 \,\mathrm{V/m}$ is applied perpendicularly to the square area of an aluminum wafer with cross-sectional area of about $10 \,\mathrm{cm^2}$, find the: Here are a few things that will be useful in this set of problems:

$$v_e = -\mu_e \mathbf{E}$$
 $\mathbf{J} = -q_{ve}\mu_e \mathbf{E}$
 $\sigma_s = -q_{ve}\mu_e$
 $q_{ve} = N_e q_e$

(a) Electron charge density q_{ve} .

$$\sigma_s = -q_{ve}\mu_e$$

$$q_{ve} = -\sigma_s\mu_e^{-1} = -3.96 \times 10^7 (2.2 \times 10^{-3})^{-1} = -\frac{3.96}{2.2} \times 10^{10} \left[\frac{C}{m^3} \right]$$

(b) Electron drift velocity v_e .

$$v_e = -\mu_e \mathbf{E}$$

 $v_e = -2.2 \times 10^{-3} \hat{a}_x 2 = -\hat{a}_x 4.4 \times 10^{-3} \left[\frac{m}{s} \right]$

(c) Electric current density J.

$$J = -q_{ve}\mu_{e}E$$

$$= -\frac{3.96}{2.2} \times 10^{10} \times 2.2 \times 10^{-3} \hat{a}_{x} \times 2$$

$$= \frac{3.96}{2.2} \times 10^{10} \times 2.2 \times 10^{-3} \hat{a}_{x} \times 2$$

$$= 2 \times 3.96 \times 10^{7} \hat{a}_{x} = \hat{a}_{x} 7.92 \times 10^{7} \left[\frac{A}{m^{2}} \right]$$

(d) Electric current flowing through the square cross section of the wafer.

$$I = \iint_{0}^{A} \mathbf{J} dA = \mathbf{J} \iint_{0}^{A} 1 dA = \mathbf{J} A = 10cm^{2} \times 7.92 \times 10^{7} \hat{a}_{x}$$
$$= 10^{-3} \times 7.92 \times 10^{7} \hat{a}_{x} = \hat{a}_{x} 7.92 \times 10^{4} [A]$$

(e) Electron density N_e .

$$q_{ve} = N_e q_e$$

$$q_e = 1.6 \times 10^{-19}$$

$$\therefore N_e = \left| \frac{q_{ve}}{q_e} \right| = \frac{3.96}{2.2 \cdot 1.6} \times 10^{10} \times 10^{19} = 1.125 \times 10^{29} \left[\frac{e}{m^2} \right]$$

Leave your answers in terms of ϵ_0, μ_0 .

References

[1] Constantine A. Balanis. advanced engineering electromagnetics, chapter 1, page 2–3. John Wiley & Sons, 2024.