Homework Set #3

ECE 6310 - Advanced Electromagnetic Fields

Balanis (2nd Edition): 6.19, 6.20, 6.25, 6.26, 6.38

Balanis (2nd Edition): 7.3, 7.15, 7.37

Verify your solutions for the far field E_{θ} for a half-wavelength dipole (6.26) in HFSS; design the antenna to be resonant at 1GHz.

6.19. Show that for observations made at very large distance $(\beta r \gg 1)$ the electric and magnetic fields of Example 6-3 reduce to

$$E_{\theta} = j \eta \frac{\beta I_{e} \ell e^{-j\beta r}}{4\pi r} \sin \theta$$
 $H_{\phi} \simeq \frac{E_{\theta}}{\eta}$
 $E_{r} \simeq 0$
 $E_{\phi} = H_{r} = H_{\theta} = 0$

6.20. For Problem 6.19, show that the:

· Time-average power density is

$$\mathbf{S}_{av} = \frac{1}{2} \operatorname{Re} \left[\mathbf{E} \times \mathbf{H}^* \right] = \hat{\mathbf{a}}_r W_{av} = \hat{\mathbf{a}}_r W_r$$
$$= \hat{\mathbf{a}}_r \frac{\eta}{8} \left| \frac{I_o \ell}{\lambda} \right|^2 \frac{\sin^2 \theta}{r^2}$$

· Radiation intensity is

$$U = r^2 S_{av} = \frac{\eta}{8} \left| \frac{I_o \ell}{\lambda} \right|^2 \sin^2 \theta$$

• Radiated power is

$$P_{rad} = \int_{0}^{2\pi} \int_{0}^{\pi} U(\theta, \phi) \times \sin\theta d\theta d\phi = \eta \left(\frac{\pi}{3}\right) \left|\frac{I_0 \ell}{\lambda}\right|^2$$

• Directivity is $D_o = \frac{4\pi U_{\text{max}}(\theta, \phi)}{P_{rad}}$ = $\frac{3}{2}$ (dimensionless) = 1.761 dB

· Radiation resistance is

$$R_r = \frac{2P_{rad}}{|I_o|^2} = 80\pi^2 \left(\frac{\ell}{\lambda}\right)^2$$

6.25. The current distribution on a very thin wire dipole antenna of overall length ℓ is given by

$$\mathbf{I}_{\varepsilon} = \begin{cases} \hat{\mathbf{a}}_{z} I_{0} \sin \left[\beta \left(\frac{\ell}{2} - z'\right)\right] & 0 \leq z' \leq \frac{\ell}{2} \\ \hat{\mathbf{a}}_{z} I_{0} \sin \left[\beta \left(\frac{\ell}{2} + z'\right)\right] & -\frac{\ell}{2} \leq z' \leq 0 \end{cases}$$

where I_0 is a constant. Representing the distance R of (6-112) by the far-field approximations of (6-112a) through (6-112b), derive the far-zone electric and magnetic fields radiated by the dipole using (6-97a) and the far-field formulations of Section 6.7.

6.26. Show that the radiated far-zone electric and magnetic fields derived in Problem 6.25 reduce for a half-wavelength dipole (ℓ = λ/2) to

$$E_{ heta} \simeq j \eta rac{I_0 e^{-j eta r}}{2 \pi r} \left[rac{\cos \left(rac{\pi}{2} \cos heta
ight)}{\sin heta}
ight]$$
 $H_{\phi} \simeq rac{E_{ heta}}{n}$

$$E_r \simeq E_{\phi} \simeq H_r \simeq H_{\theta} \simeq 0$$

6.38. A coaxial line of inner and outer radii *a* and *b*, respectively, is mounted on an infinite conducting ground plane. Assuming that the electric field over the aperture of the coax is

$$\mathbf{E}_{a} = -\hat{\mathbf{a}}_{\rho} \frac{V}{\varepsilon \ln(b/a)} \frac{1}{\rho'}, \qquad a \le \rho' \le b$$

where V is the applied voltage and ε is the permittivity of medium in the coax, find

the far-zone spherical electric and magnetic field components radiated by the aperture.

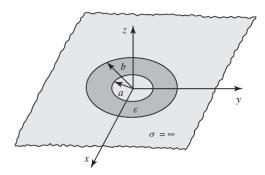


Figure P6-38

- 7.3. An infinitesimal vertical magnetic dipole of length l and constant current I_m is placed symmetrically about the origin and it is directed along the z axis, as shown in Figure 6-2a. Derive expressions valid everywhere, near and far field, for the:
 - Electric vector potential components (F_r, F_θ, F_ϕ) .
 - Electric field components (E_r, E_θ, E_ϕ) .
 - Magnetic field components (H_r, H_θ, H_ϕ) .
 - Time-average power density, defined as $\mathbf{S}_{av} = \frac{1}{2} \text{Re} \left[\mathbf{E} \times \mathbf{H}^* \right].$ • Radiation intensity, defined in the far field
 - as $U \approx r^2 S_{av}$.
 - Power radiated, defined as
 - Prad = $\int_0^{2\pi} \int_0^{\pi} U(\theta, \phi) \sin \theta d\theta d\phi$. Maximum directivity, defined as $D_0 = \frac{4\pi U_{\text{max}}(\theta, \phi)}{D}$
 - $D_0 = \frac{P_{rad}}{P_{rad}}$ Radiation resistance, defined as $R_r = \frac{2P_{rad}}{|I_m|^2}$ You can minimize the derivations as long as

you justify the procedure.

7.15. An infinitesimal electric dipole is placed at an angle of 30° at a height h above a perfectly conducting electric ground plane. Determine the location and orientation of its image. Do this by sketching the image.

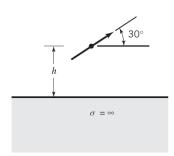


Figure P7-15

- **7.37.** For the aperture shown in Figure 6-4c and assuming it is mounted on an infinite PEC ground plane:
 - (a) Form the most practical, exact or approximate (when necessary to solve the problem), equivalent currents J_s and M_s .
 - (b) Find the far-zone electric and magnetic fields. The electric field distribution at the aperture is given by (E_o) is a constant)

$$\mathbf{E}_{a} = \hat{\mathbf{a}}_{y} E_{o}$$

 $-a/2 \le x' \le a/2; -b/2 \le y' \le b/2$