

ECE 6310 - Advanced Electromagnetic Fields: Homework Set #1

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-2 days - 0 hours - 41 min until deadline!!

A B C D E F G H I J K L M N O P Q R S T U V W X Y Z
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1 Preliminaries

In this document, we use standard notation for electromagnetic theory. Key equations and concepts are summarized below:

Vector Notation

- \mathcal{E} : Electric field intensity
- \mathcal{H} : Magnetic field intensity
- \mathcal{D} : Electric flux density
- \mathcal{B} : Magnetic flux density
- \mathcal{J} : Current density
- ρ_v : Volume charge density

Differential Operators

- $\nabla \cdot$: Divergence of a vector field
- $\nabla \times$: Curl of a vector field

- ∇ : Gradient of a scalar field
- ∂_i : Partial derivative with respect to the independent basis element i

Maxwell's Equations

In integral form, Maxwell's equations are given by:

$$\oint_{\partial V} \mathcal{E} \cdot d\boldsymbol{\ell} = -\frac{d}{dt} \int_V \mathcal{B} \cdot d\boldsymbol{\mathcal{S}} \quad (\text{Faraday's Law of Induction}) \quad (1)$$

$$\oint_{\partial V} \mathcal{H} \cdot d\boldsymbol{\ell} = \int_V \mathcal{J} \cdot d\boldsymbol{\mathcal{S}} + \frac{d}{dt} \int_V \mathcal{D} \cdot d\boldsymbol{\mathcal{S}} \quad (\text{Ampère's Circuital Law}) \quad (2)$$

$$\oiint_{\partial V} \mathcal{D} \cdot d\boldsymbol{\mathcal{S}} = \int_V \rho_v dV \quad (\text{Gauss's Law for Electricity}) \quad (3)$$

$$\oiint_{\partial V} \mathcal{B} \cdot d\boldsymbol{\mathcal{S}} = 0 \quad (\text{Gauss's Law for Magnetism}) \quad (4)$$

Other Relevant Equations

- Continuity Equation: $\nabla \cdot \mathcal{J} + \partial_t \rho_v = 0$
- Relationship between \mathcal{E} , \mathcal{D} : $\mathcal{D} = \epsilon \mathcal{E}$
- Relationship between \mathcal{H} , \mathcal{B} : $\mathcal{B} = \mu \mathcal{H}$

Boundary Conditions

Discuss the boundary conditions for \mathcal{E} , \mathcal{H} , \mathcal{D} , and \mathcal{B} at interfaces between different media.

Problem 1.3

The electric flux density inside a cube is given by:

(a) $\vec{D} = \hat{a}_x(3 + x)$

(b) $\vec{D} = \hat{a}_y(4 + y^2)$

Find the total electric charge enclosed inside the cubical volume when the cube is in the first octant with three edges coincident with the x, y, z axes and one corner at the origin. Each side of the cube is 1 m long.

Ok, this one we can do by using the following expressions from the text [1]:

$$\oiint_s \mathcal{D} ds = \iiint_v \mathcal{q}_{ev} dv = \mathcal{Q}_e \quad (5)$$

$$\mathcal{q}_{ev} = \Delta \cdot \mathcal{D} \quad (6)$$

We apply expression 6 then plug into expression 5 to get the total electric charge.

$$\iiint_V \mathcal{q}_{ev} = \iiint_V \Delta \cdot (\hat{a}_x(3 + x)) dV = \iiint_V \partial_x(\hat{a}_x(3 + x)) dV = \iiint_0^1 1 dV = 1$$

$$\iiint_V \mathcal{q}_{ev} = \iiint_V \Delta \cdot (\hat{a}_y(4 + y^2)) dV = \iiint_V \partial_y(\hat{a}_y(4 + y^2)) dV = \iiint_0^1 2y dV$$

$$\iiint_0^1 2y dV = \iint_0^1 \int_0^1 2y dy ds = \iint_0^1 y^2|_0^1 ds = \iint_0^1 (1 - 0) ds = 1$$

Problem 1.4

An infinite planar interface between media, as shown in the figure, is formed by having air (medium #1) on the left of the interface and lossless polystyrene (medium #2) to the right of the interface. An electric surface charge density $\sigma_{es} = 0.2 \text{ C/m}^2$ exists along the entire interface. The static electric flux density inside the polystyrene is given by $\vec{D}_2 = 6\hat{a}_x + 3\hat{a}_z \text{ C/m}^2$. Determine the corresponding vector:

(a) Electric field intensity inside the polystyrene.

we can find this using the following expression for the Electric field

intensity vector:

$$\epsilon_{poly} = 2.56\epsilon_0$$

$$\mathcal{D} = \epsilon \mathcal{E}$$

$$\mathcal{E} = \epsilon^{-1} \mathcal{D} = 0.390625\epsilon_0^{-1} \cdot \mathcal{D} = \epsilon_0^{-1}(2.34 \cdot a_x + 1.17 \cdot a_z)$$

- (b) Electric polarization vector inside the polystyrene.
we can find this using the following expression for the polarization vector:

$$\mathcal{P}_e = \epsilon_0 \chi_e \mathcal{E}$$

$$\chi_e = \epsilon_r - 1 = 2.56 - 1 = 1.56$$

$$\mathcal{P}_e = 1.56\cancel{\epsilon_0}\epsilon_0^{-1}(2.34 \cdot a_x + 1.17 \cdot a_z) = 3.6504 \cdot a_x + 1.8252 \cdot a_z$$

- (c) Electric flux density inside the air medium.

By the continuity of tangential components at the boundary:

$$\hat{\mathbf{n}} \times (\mathcal{E}_2 - \mathcal{E}_1) = 0$$

we apply the following.

$$\mathcal{E}_{air} = \mathcal{E}_{Poly}$$

$$\mathcal{D}_{air} = \epsilon_{air} \mathcal{E}_{air}$$

$$\therefore \mathcal{D}_{air} \epsilon_{air}^{-1} = \mathcal{D}_{Poly} \epsilon_{Poly}^{-1}$$

$$\begin{aligned} \mathcal{D}_{air} &= \frac{\epsilon_{air}}{\epsilon_{Poly}} \mathcal{D}_{Poly} = \frac{\cancel{\epsilon_0} \cdot 1}{\cancel{\epsilon_0} \cdot 2.56} \cdot \mathcal{D}_{Poly} \\ &= \frac{1}{2.56} \mathcal{D}_{Poly} = 2.34 \cdot a_x \end{aligned}$$

The normal components at the boundary are not continuous and therefore we must do more.

The normal is \hat{a}_z

$$\hat{\mathbf{n}} \cdot (\mathcal{D}_2 - \mathcal{D}_1) = q_{es}$$

$$\hat{a}_z \cdot (\mathcal{D}_2 - \mathcal{D}_1) = 0.2$$

$$\mathcal{D}_{1z} = \mathcal{D}_{2z} - 0.2 = 3 - .2 = 2.8$$

(d) Electric field intensity inside the air medium.

Again using the expression $\mathcal{D} = \epsilon \mathcal{E}$

$$\begin{aligned}\mathcal{D}_{air} &= \epsilon_{air} \mathcal{E}_{air} \\ \mathcal{E}_{air} &= \epsilon_{air}^{-1} \mathcal{D}_{air} \\ &= \epsilon_0^{-1} (2.34 \cdot a_x + 2.8 \cdot a_z)\end{aligned}$$

(e) Electric polarization vector inside the air medium.

Again using $\mathcal{P}_e = \epsilon_0 \chi_e \mathcal{E}$

$$\begin{aligned}\mathcal{P}_{e_{air}} &= \epsilon_0 \chi_{e_{air}} \mathcal{E}_{air} \\ &= \chi_{e_{air}} \cancel{\epsilon_0} \overset{1}{\epsilon_0} (2.34 \cdot a_x + 2.8 \cdot a_z) \\ \chi_{e_{air}} &= \epsilon_{r_{air}} - 1 = 1 - 1 = 0 \\ \therefore \mathcal{P}_{e_{air}} &= \mathbf{0}\end{aligned}$$

Leave your answers in terms of ϵ_0, μ_0 .

Problem 1.13

The instantaneous magnetic flux density in free space is given by:

$$\mathcal{B} = \hat{a}_x B_x \cos(2y) \sin(\omega t - \pi z) + \hat{a}_y B_y \cos(2x) \cos(\omega t - \pi z)$$

where B_x and B_y are constants. Assuming there are no sources at the observation points x, y , determine the electric displacement current density.

We can obtain the electric displacement current \mathcal{J}_d by using the following expressions:

$$\nabla \times \mathbf{H} = \mathbf{J}_i + \mathbf{J}_c + \mathbf{J}_d \quad (7)$$

$$\mathbf{B} = \mu \mathbf{H} \quad (8)$$

$$\mathbf{J}_d = \frac{\partial \mathbf{D}}{\partial t} \quad (9)$$

We take $\mathbf{J}_i + \mathbf{J}_c$ to be 0 since we have no sources at the observation points. Using expression 7 and solving expression 8 for \mathbf{H} :

$$\begin{aligned}
\nabla \times \mathbf{H} &= \mathbf{J}_d \\
\mathbf{J}_d &= \nabla \times \mu^{-1} \mathbf{B} \\
\mathbf{J}_d &= \mu^{-1} \nabla \times \mathbf{B} \\
&= \mu^{-1} \left[\hat{a}_x \left(\frac{\partial \mathbf{B}_z}{\partial y} - \frac{\partial \mathbf{B}_y}{\partial z} \right) - \hat{a}_y \left(\frac{\partial \mathbf{B}_z}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial z} \right) + \hat{a}_z \left(\frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
\mathbf{B}_z &= 0 \\
&= \mu^{-1} \left[\hat{a}_x \left(0 - \frac{\partial \mathbf{B}_y}{\partial z} \right) - \hat{a}_y \left(0 - \frac{\partial \mathbf{B}_x}{\partial z} \right) + \hat{a}_z \left(\frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
&= \mu^{-1} \left[-\hat{a}_x \frac{\partial \mathbf{B}_y}{\partial z} + \hat{a}_y \frac{\partial \mathbf{B}_x}{\partial z} + \hat{a}_z \left(\frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
\frac{\partial \mathbf{B}_x}{\partial z} &= -\pi B_x \cos(2y) \cos(\omega t - \pi z) \\
\frac{\partial \mathbf{B}_y}{\partial z} &= \pi B_y \cos(2x) \sin(\omega t - \pi z) \\
\frac{\partial \mathbf{B}_y}{\partial x} &= -2 \sin(2x) \cos(\omega t - \pi z) \\
\frac{\partial \mathbf{B}_x}{\partial y} &= -2 \sin(2y) \sin(\omega t - \pi z) \\
&= \mu^{-1} [\hat{a}_x (-\pi B_y \cos(2x) \sin(\omega t - \pi z)) \\
&\quad + \hat{a}_y (-\pi B_x \cos(2y) \cos(\omega t - \pi z)) \\
&\quad + \hat{a}_z (2(\sin(2y) \sin(\omega t - \pi z) - \sin(2x) \cos(\omega t - \pi z)))]
\end{aligned}$$

Problem 1.20

The instantaneous electric field inside a conducting rectangular pipe (waveguide) of width a is given by:

$$\mathcal{E} = \hat{a}_y E_0 \sin\left(\frac{\pi x}{a}\right) \cos(\omega t - \beta_z z)$$

where β_z is the waveguide's phase constant. Assuming there are no sources within the free-space-filled pipe determine the:

(a) Corresponding instantaneous magnetic field components inside the conducting pipe. (\vec{H})

(b) Phase constant β_z .

The height of the waveguide is b . This can be found by relating \mathcal{E} to \mathcal{H} and we know how to get there using the instantaneous forms of these:

$$\mathcal{E} = -j\omega\mu\nabla \times \mathcal{H}$$

$$\mathcal{H} = \frac{j}{\omega\mu}\nabla \times \mathcal{E}$$

$$\frac{j}{\omega\mu}\nabla \times \mathcal{E} = \frac{j}{\omega\mu} \left[\hat{a}_x \left(\frac{\partial \mathbf{E}_z}{\partial y} - \frac{\partial \mathbf{E}_y}{\partial z} \right) - \hat{a}_y \left(\frac{\partial \mathbf{E}_z}{\partial x} - \frac{\partial \mathbf{E}_x}{\partial z} \right) + \hat{a}_z \left(\frac{\partial \mathbf{E}_y}{\partial x} - \frac{\partial \mathbf{E}_x}{\partial y} \right) \right]$$

$$\frac{j}{\omega\mu}\nabla \times \mathcal{E} = \frac{j}{\omega\mu} \left[\hat{a}_x \left(0 - \frac{\partial \mathbf{E}_y}{\partial z} \right) - \hat{a}_y (0 - 0) + \hat{a}_z \left(\frac{\partial \mathbf{E}_y}{\partial x} - 0 \right) \right]$$

$$\frac{j}{\omega\mu}\nabla \times \mathcal{E} = -\frac{j}{\omega\mu} \left[\hat{a}_x \frac{\partial \mathbf{E}_y}{\partial z} - \hat{a}_z \frac{\partial \mathbf{E}_y}{\partial x} \right]$$

$$\mathcal{E} = \hat{a}_y E_0 \sin \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z)$$

$$\frac{\partial \mathbf{E}_y}{\partial x} = \left(\frac{\pi}{a} \right) E_0 \cos \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z)$$

$$\frac{\partial \mathbf{E}_y}{\partial z} = (\beta_z) E_0 \sin \left(\frac{\pi x}{a} \right) \sin(\omega t - \beta_z z)$$

$$\mathcal{H} = -\frac{j}{\omega\mu} \left[\hat{a}_x (\beta_z) E_0 \sin \left(\frac{\pi x}{a} \right) \sin(\omega t - \beta_z z) - \hat{a}_z \left(\frac{\pi}{a} \right) E_0 \cos \left(\frac{\pi x}{a} \right) \cos(\omega t - \beta_z z) \right]$$

$$|\mathcal{H}| = \left| -\frac{j}{\omega\mu} E_0 \right|$$

Since there is no source components here or external driving, both \mathcal{J}_c and \mathcal{J}_i are 0.

$$\nabla \times \mathcal{H} = \frac{\partial \mathcal{D}}{\partial t}$$

Problem 2.18

The time-varying electric field inside a lossless dielectric material of polystyrene, of infinite dimensions and with a relative permittivity (dielectric constant) of 2.56, is given by:

$$\vec{\mathcal{E}} = \hat{a}_x 10^{-3} \sin(2\pi \times 10^7 t) \text{ V/m}$$

Determine the corresponding:

- (a) Electric susceptibility of the dielectric material.

$$\chi_e = \epsilon_r - 1 = 1.56$$

- (b) Time-harmonic electric flux density vector.

- (c) Time-harmonic electric polarization vector.

- (d) Time-harmonic displacement current density vector.

- (e) Time-harmonic polarization current density vector defined as the partial derivative of the corresponding electric polarization vector.

Leave your answers in terms of ϵ_0, μ_0 .

Problem 2.25

Aluminum has a static conductivity of about $\sigma = 3.96 \times 10^7 \text{ S/m}$ and an electron mobility of $\mu_e = 2.2 \times 10^{-3} \text{ m}^2/(\text{V}\cdot\text{s})$. Assuming that an electric field of $\vec{E} = \hat{a}_x 2 \text{ V/m}$ is applied perpendicularly to the square area of an aluminum wafer with cross-sectional area of about 10 cm^2 , find the:

- (a) Electron charge density q_{ve} .

- (b) Electron drift velocity v_e .

- (c) Electric current density J .

- (d) Electric current flowing through the square cross section of the wafer.

- (e) Electron density N_e .

Leave your answers in terms of ϵ_0, μ_0 .

References

- [1] Constantine A. Balanis. *advanced engineering electromagnetics*, chapter 1, page 2–3. John Wiley & Sons, 2024.