

# ECE 6310 - Advanced Electromagnetic Fields: Homework Set #1

Miguel Gomez

1 days - 8 hours - 7 min until deadline!!

*ABCDEFGHIJKLMNOPQRSTUVWXYZ  
ABCDEFGHIJKLMNOPQRSTUVWXYZ*

## 1 Preliminaries

In this document, we use standard notation for electromagnetic theory. Key equations and concepts are summarized below:

### Vector Notation

- $\mathcal{E}$ : Electric field intensity
- $\mathcal{H}$ : Magnetic field intensity
- $\mathcal{D}$ : Electric flux density
- $\mathcal{B}$ : Magnetic flux density
- $\mathcal{J}$ : Current density
- $\rho_v$ : Volume charge density

### Differential Operators

- $\nabla \cdot$  : Divergence of a vector field
- $\nabla \times$  : Curl of a vector field

- $\nabla$  : Gradient of a scalar field
- $\partial_i$  : Partial derivative with respect to the independent basis element  $i$

## Maxwell's Equations

In integral form, Maxwell's equations are given by:

$$\oint_{\partial V} \mathcal{E} \cdot d\boldsymbol{\ell} = -\frac{d}{dt} \int_V \mathcal{B} \cdot d\boldsymbol{\mathcal{S}} \quad (\text{Faraday's Law of Induction}) \quad (1)$$

$$\oint_{\partial V} \mathcal{H} \cdot d\boldsymbol{\ell} = \int_V \mathcal{J} \cdot d\boldsymbol{\mathcal{S}} + \frac{d}{dt} \int_V \mathcal{D} \cdot d\boldsymbol{\mathcal{S}} \quad (\text{Ampère's Circuital Law}) \quad (2)$$

$$\oiint_{\partial V} \mathcal{D} \cdot d\boldsymbol{\mathcal{S}} = \int_V \rho_v dV \quad (\text{Gauss's Law for Electricity}) \quad (3)$$

$$\oiint_{\partial V} \mathcal{B} \cdot d\boldsymbol{\mathcal{S}} = 0 \quad (\text{Gauss's Law for Magnetism}) \quad (4)$$

## Other Relevant Equations

- Continuity Equation:  $\nabla \cdot \mathcal{J} + \partial_t \rho_v = 0$
- Relationship between  $\mathcal{E}$ ,  $\mathcal{D}$ :  $\mathcal{D} = \epsilon \mathcal{E}$
- Relationship between  $\mathcal{H}$ ,  $\mathcal{B}$ :  $\mathcal{B} = \mu \mathcal{H}$

## Boundary Conditions

Discuss the boundary conditions for  $\mathcal{E}$ ,  $\mathcal{H}$ ,  $\mathcal{D}$ , and  $\mathcal{B}$  at interfaces between different media.

## Problem 1.3

The electric flux density inside a cube is given by:

$$(a) \quad \vec{D} = \hat{a}_x(3 + x)$$

$$(b) \quad \vec{D} = \hat{a}_y(4 + y^2)$$

Find the total electric charge enclosed inside the cubical volume when the cube is in the first octant with three edges coincident with the x, y, z axes and one corner at the origin. Each side of the cube is 1 m long.

Ok, this one we can do by using the following expressions from the text [1]:

$$\oiint_s \mathcal{D} ds = \iiint_v \mathcal{q}_{ev} dv = \mathcal{Q}_e \quad (5)$$

$$\mathcal{q}_{ev} = \Delta \cdot \mathcal{D} \quad (6)$$

We apply expression 6 then plug into expression 5 to get the total electric charge.

$$\iiint_V \mathcal{q}_{ev} = \iiint_V \Delta \cdot (\hat{a}_x(3 + x)) dV = \iiint_V \partial_x(\hat{a}_x(3 + x)) dV = \iiint_0^1 1 dV = 1$$

$$\iiint_V \mathcal{q}_{ev} = \iiint_V \Delta \cdot (\hat{a}_y(4 + y^2)) dV = \iiint_V \partial_y(\hat{a}_y(4 + y^2)) dV = \iiint_0^1 2y dV$$

$$\iiint_0^1 2y dV = \iint_0^1 \int_0^1 2y dy ds = \iint_0^1 y^2|_0^1 ds = \iint_0^1 (1 - 0) ds = 1$$

## Problem 1.4

An infinite planar interface between media, as shown in the figure, is formed by having air (medium #1) on the left of the interface and lossless polystyrene (medium #2) to the right of the interface. An electric surface charge density  $\sigma_{es} = 0.2 \text{ C/m}^2$  exists along the entire interface. The static electric flux density inside the polystyrene is given by  $\vec{D}_2 = 6\hat{a}_x + 3\hat{a}_z \text{ C/m}^2$ . Determine the corresponding vector:

(a) Electric field intensity inside the polystyrene.

we can find this using the following expression for the Electric field

intensity vector:

$$\epsilon_{poly} = 2.56\epsilon_0$$

$$\mathcal{D} = \epsilon \mathcal{E}$$

$$\mathcal{E} = \epsilon^{-1} \mathcal{D} = 0.390625\epsilon_0^{-1} \cdot \mathcal{D} = \epsilon_0^{-1}(2.34 \cdot a_x + 1.17 \cdot a_z)$$

- (b) Electric polarization vector inside the polystyrene.  
we can find this using the following expression for the polarization vector:

$$\mathcal{P}_e = \epsilon_0 \chi_e \mathcal{E}$$

$$\chi_e = \epsilon_r - 1 = 2.56 - 1 = 1.56$$

$$\mathcal{P}_e = 1.56\cancel{\epsilon_0}\epsilon_0^{-1}(2.34 \cdot a_x + 1.17 \cdot a_z) = 3.6504 \cdot a_x + 1.8252 \cdot a_z$$

- (c) Electric flux density inside the air medium.

By the continuity of tangential components at the boundary:

$$\hat{\mathbf{n}} \times (\mathcal{E}_2 - \mathcal{E}_1) = 0$$

we apply the following.

$$\mathcal{E}_{air} = \mathcal{E}_{Poly}$$

$$\mathcal{D}_{air} = \epsilon_{air} \mathcal{E}_{air}$$

$$\therefore \mathcal{D}_{air} \epsilon_{air}^{-1} = \mathcal{D}_{Poly} \epsilon_{Poly}^{-1}$$

$$\begin{aligned} \mathcal{D}_{air} &= \frac{\epsilon_{air}}{\epsilon_{Poly}} \mathcal{D}_{Poly} = \frac{\cancel{\epsilon_0} \cdot 1}{\cancel{\epsilon_0} \cdot 2.56} \cdot \mathcal{D}_{Poly} \\ &= \frac{1}{2.56} \mathcal{D}_{Poly} = 2.34 \cdot a_x \end{aligned}$$

The normal components at the boundary are not continuous and therefore we must do more.

The normal is  $\hat{a}_z$

$$\hat{\mathbf{n}} \cdot (\mathcal{D}_2 - \mathcal{D}_1) = q_{es}$$

$$\hat{a}_z \cdot (\mathcal{D}_2 - \mathcal{D}_1) = 0.2$$

$$\mathcal{D}_{1z} = \mathcal{D}_{2z} - 0.2 = 3 - .2 = 2.8$$

(d) Electric field intensity inside the air medium.

Again using the expression  $\mathcal{D} = \epsilon \mathcal{E}$

$$\begin{aligned}\mathcal{D}_{air} &= \epsilon_{air} \mathcal{E}_{air} \\ \mathcal{E}_{air} &= \epsilon_{air}^{-1} \mathcal{D}_{air} \\ &= \epsilon_0^{-1} (2.34 \cdot a_x + 2.8 \cdot a_z)\end{aligned}$$

(e) Electric polarization vector inside the air medium.

Again using  $\mathcal{P}_e = \epsilon_0 \chi_e \mathcal{E}$

$$\begin{aligned}\mathcal{P}_{e_{air}} &= \epsilon_0 \chi_{e_{air}} \mathcal{E}_{air} \\ &= \chi_{e_{air}} \cancel{\epsilon_0} \overset{1}{\epsilon_0} (2.34 \cdot a_x + 2.8 \cdot a_z) \\ \chi_{e_{air}} &= \epsilon_{r_{air}} - 1 = 1 - 1 = 0 \\ \therefore \mathcal{P}_{e_{air}} &= \mathbf{0}\end{aligned}$$

Leave your answers in terms of  $\epsilon_0, \mu_0$ .

## Problem 1.13

The instantaneous magnetic flux density in free space is given by:

$$\mathcal{B} = \hat{a}_x B_x \cos(2y) \sin(\omega t - \pi z) + \hat{a}_y B_y \cos(2x) \cos(\omega t - \pi z)$$

where  $B_x$  and  $B_y$  are constants. Assuming there are no sources at the observation points  $x, y$ , determine the electric displacement current density.

We can obtain the electric displacement current  $\mathcal{J}_d$  by using the following expressions:

$$\nabla \times \mathbf{H} = \mathbf{J}_i + \mathbf{J}_c + \mathbf{J}_d \quad (7)$$

$$\mathbf{B} = \mu \mathbf{H} \quad (8)$$

$$\mathbf{J}_d = \frac{\partial \mathbf{D}}{\partial t} \quad (9)$$

We take  $\mathbf{J}_i + \mathbf{J}_c$  to be 0 since we have no sources at the observation points. Using expression 7 and solving expression 8 for  $\mathbf{H}$ :

$$\begin{aligned}
\nabla \times \mathbf{H} &= \mathbf{J}_d \\
\mathbf{J}_d &= \nabla \times \mu^{-1} \mathbf{B} \\
\mathbf{J}_d &= \mu^{-1} \nabla \times \mathbf{B} \\
&= \mu^{-1} \left[ \hat{a}_x \left( \frac{\partial \mathbf{B}_z}{\partial y} - \frac{\partial \mathbf{B}_y}{\partial z} \right) - \hat{a}_y \left( \frac{\partial \mathbf{B}_z}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial z} \right) + \hat{a}_z \left( \frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
\mathbf{B}_z &= 0 \\
&= \mu^{-1} \left[ \hat{a}_x \left( 0 - \frac{\partial \mathbf{B}_y}{\partial z} \right) - \hat{a}_y \left( 0 - \frac{\partial \mathbf{B}_x}{\partial z} \right) + \hat{a}_z \left( \frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
&= \mu^{-1} \left[ -\hat{a}_x \frac{\partial \mathbf{B}_y}{\partial z} + \hat{a}_y \frac{\partial \mathbf{B}_x}{\partial z} + \hat{a}_z \left( \frac{\partial \mathbf{B}_y}{\partial x} - \frac{\partial \mathbf{B}_x}{\partial y} \right) \right] \\
\frac{\partial \mathbf{B}_x}{\partial z} &= -\pi B_x \cos(2y) \cos(\omega t - \pi z) \\
\frac{\partial \mathbf{B}_y}{\partial z} &= \pi B_y \cos(2x) \sin(\omega t - \pi z) \\
\mathcal{B} &= \hat{a}_x B_x \cos(2y) \sin(\omega t - \pi z) + \hat{a}_y B_y \cos(2x) \cos(\omega t - \pi z)
\end{aligned}$$

## Problem 1.20

The instantaneous electric field inside a conducting rectangular pipe (waveguide) of width  $a$  is given by:

$$\mathcal{E} = \hat{a}_y E_0 \sin\left(\frac{\pi x}{a}\right) \cos(\omega t - \beta_z z)$$

where  $\beta_z$  is the waveguide's phase constant. Assuming there are no sources within the free-space-filled pipe determine the:

- Corresponding instantaneous magnetic field components inside the conducting pipe.
- Phase constant  $\beta_z$ .
- The height of the waveguide is  $b$ .

## Problem 2.18

The time-varying electric field inside a lossless dielectric material of polystyrene, of infinite dimensions and with a relative permittivity (dielectric constant) of 2.56, is given by:

$$\vec{\mathcal{E}} = \hat{a}_x 10^{-3} \sin(2\pi \times 10^7 t) \text{ V/m}$$

Determine the corresponding:

- (a) Electric susceptibility of the dielectric material.
- (b) Time-harmonic electric flux density vector.
- (c) Time-harmonic electric polarization vector.
- (d) Time-harmonic displacement current density vector.
- (e) Time-harmonic polarization current density vector defined as the partial derivative of the corresponding electric polarization vector.

Leave your answers in terms of  $\epsilon_0, \mu_0$ .

## Problem 2.25

Aluminum has a static conductivity of about  $\sigma = 3.96 \times 10^7 \text{ S/m}$  and an electron mobility of  $\mu_e = 2.2 \times 10^{-3} \text{ m}^2/(\text{V}\cdot\text{s})$ . Assuming that an electric field of  $\vec{E} = \hat{a}_x 2 \text{ V/m}$  is applied perpendicularly to the square area of an aluminum wafer with cross-sectional area of about  $10 \text{ cm}^2$ , find the:

- (a) Electron charge density  $q_{ve}$ .
- (b) Electron drift velocity  $v_e$ .
- (c) Electric current density  $J$ .
- (d) Electric current flowing through the square cross section of the wafer.
- (e) Electron density  $N_e$ .

Leave your answers in terms of  $\epsilon_0, \mu_0$ .

## References

- [1] Constantine A. Balanis. *advanced engineering electromagnetics*, chapter 1, page 2–3. John Wiley & Sons, 2024.