ECE 6310 - Advanced Electromagnetic Fields: Homework Set #4

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-1 days - -1 hours - 29 min until deadline!!

Preliminaries

In this document, we use standard notation for electromagnetic theory. Key equations and concepts are summarized below:

Vector Notation

- **%**: Electric field intensity
- **%**: Magnetic field intensity
- **2**: Electric flux density
- **3**: Magnetic flux density
- **7**: Current density
- ρ_v : Volume charge density

Differential Operators

- $\nabla \cdot$: Divergence of a vector field
- $\nabla \times$: Curl of a vector field
- \bullet ∇ : Gradient of a scalar field
- ullet ∂_i : Partial derivative with respect to the independent basis element i

Maxwell's Equations

In integral form, Maxwell's equations are given by:

$$\oint_{\partial V} \mathcal{E} \cdot d\mathbf{\ell} = -\frac{d}{dt} \int_{V} \mathcal{B} \cdot d\mathbf{\ell}$$
 (Faraday's Law of Induction) (1)

$$\oint_{\partial V} \mathcal{H} \cdot d\boldsymbol{\ell} = \int_{V} \boldsymbol{\mathcal{J}} \cdot d\boldsymbol{\mathcal{S}} + \frac{d}{dt} \int_{V} \boldsymbol{\mathcal{D}} \cdot d\boldsymbol{\mathcal{S}}$$
 (Ampère's Circuital Law) (2)

$$\iint_{\partial V} \mathbf{\mathcal{D}} \cdot d\mathbf{\mathcal{S}} = \int_{V} \rho_{v} dV$$
 (Gauss's Law for Electricity) (3)

$$\iint_{\partial V} \mathcal{B} \cdot d\mathcal{S} = 0$$
 (Gauss's Law for Magnetism) (4)

Other Relevant Equations

• Continuity Equation: $\nabla \cdot \mathbf{J} + \partial_t \rho_v = 0$

• Relationship between \mathcal{E} , \mathcal{D} : $\mathcal{D} = \epsilon \mathcal{E}$

• Relationship between \mathcal{H} , \mathcal{B} : $\mathcal{B} = \mu \mathcal{H}$

Boundary Conditions

Discuss the boundary conditions for \mathcal{E} , \mathcal{H} , \mathcal{D} , and \mathcal{B} at interfaces between different media.

1 - 8.2

A standard X-band (8.2–12.4GHz) rectangular waveguide with inner dimensions of 0.9 in. (2.286 cm) by 0.4 in. (1.016 cm) is filled with lossless polystyrene ($\epsilon_r = 2.56$). For the lowest-order mode of the waveguide, determine at 10GHz the following values.

(a) Cutoff Freq (f_c) in GHz

We can find this with expression (8-16) from [1] with a = 2.286 cm.

$$(f_c)_{mn} = \frac{1}{2\pi\sqrt{\mu\epsilon}}\sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$(f_c)_{10} = \frac{1}{2\pi\sqrt{\mu\epsilon}}\sqrt{\left(\frac{1\pi}{a}\right)^2 + \left(\frac{0\pi}{b}\right)^2}$$

$$= \frac{1}{2\pi\sqrt{\mu\epsilon}}\sqrt{\left(\frac{\pi}{a}\right)^2}$$

$$= \frac{1}{2\pi\sqrt{\mu\epsilon}}\sqrt{\left(\frac{\pi}{2.86*10^{-2}}\right)^2} = 4.09832GHz$$

(b) Guide wavelength (λ_g) in cm

This one can be done with a combination of expressions from chapter 8 in [1], (8-21a,b,c). we can do this with a because the frequency in question is 10GHz which us above the cutoff found in part a.

$$(\lambda_g)_{mn} = \frac{\lambda}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

$$= \frac{\lambda}{\sqrt{1 - \left(\frac{4.09832e^9}{1e^{10}}\right)^2}}$$

$$= \frac{0.0187375}{\sqrt{1 - (.409832)^2}}$$

$$= 0.0205419 \ [m] = 2.05419 \ [cm]$$

(c) Wave impedance (η)

This can be found with (8-20a) in [1].

$$Z_w^+ = \frac{\sqrt{\frac{\mu}{\epsilon}}}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{\eta}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$

$$Z_w^+ = \frac{\sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_r}}}{\sqrt{1 - \left(.409832\right)^2}}$$

$$\eta_0 = 120\pi$$

$$= \frac{\frac{\eta_0}{\sqrt{\epsilon_r}}}{\sqrt{1 - \left(.409832\right)^2}} = \frac{120\pi}{\sqrt{2.56} \cdot 0.912161}$$

$$= 258.309 \Omega$$

- (d) Phase velocity (v_p) in $\frac{m}{s}$
- (e) Group velocity in $\frac{m}{s}$ This velocity, as well as the group velocity, can be found using expression (8.49a-c) from [1]. These reduce to a simple expression in (8-52)

$$v_p = \frac{v}{\cos(\Psi)}$$

$$v_g = v\cos(\Psi)$$

$$\Psi = \cos^{-1}\left(\sqrt{1 - \left(\frac{f_c}{f}\right)^2}\right)$$

Since inverse cos returns an angle, taking the cos of the inverse is the argument to the inverse itself.

$$v_p = \frac{v}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}}$$
$$v_g = v\sqrt{1 - \left(\frac{f_c}{f}\right)^2}$$

Since v is the expression $\frac{c}{\sqrt{\epsilon_r}}$, we can input those into the expression and solve for the speeds.

$$v_p = \frac{c}{\sqrt{\epsilon_r} \sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = 2.05419 * 10^8 \left[\frac{m}{s}\right]$$
$$v_g = \frac{c}{\sqrt{\epsilon_r}} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = 1.70916 * 10^8 \left[\frac{m}{s}\right]$$

2 - 9.14

A circular waveguide with radius of 3cm is made of copper ($\sigma = 5.76107 \frac{S}{m}$). For the dominant TE_{11} and low-loss TE_{01} modes, determine their corresponding cut-off frequencies and attenuation constants (in $\frac{Np}{m}$ and $\frac{dB}{m}$ at a frequency of 7GHz. Assume that the waveguide is filled with air. This problem can be modeled using CST, or Ansys, and we can also solve for the values directly.

This problem can be modeled using CST, or Ansys, and we can also solve for the values directly. Using the expression for the cutoff frequency seen in 9-12a of [1], we can solve for f_c , and using expression 9-34a in [1], we can solve for the attenuation constant for our modes. χ'_{mn} depends on the mode and can be found with table 9-1 of [1].

$$f_c = \frac{\chi'_{mn}}{2\pi a \sqrt{\mu \epsilon}}$$

$$\alpha_{mn} = \frac{R_s}{a\eta \sqrt{1 - \left(\frac{f_c}{f}\right)^2}} \left[\left(\frac{f_c}{f}\right)^2 + \frac{m^2}{\chi'_{mn}^2 - m^2} \right]$$

 $TE_{11}: \chi'_{11} = 1.8412$

- a) f_c
- b) α_c

 $TE_{01}: \chi'_{01} = 3.8318$

- a) f_c
- b) α_c

3 - 11.2

A magnetic line source of infinite length and constant magnetic current Im is placed parallel to the z axis at a height h above a PEC ground plane of infinite extent, as shown in Figure 11-2 except that we now have a magnetic line source.

- (a) Determine the total magnetic field at ρ , ϕ for $0 \le \phi \le 180^{\circ}$.
- (b) Simplify the expressions when the observations are made at very large distances (far field).
- (c) Determine the smallest height h (in λ) that will introduce a null in the far field amplitude pattern at:
 - $\cdot \ \phi = 30^{\circ}$
 - $\cdot \phi = 90^{\circ}$

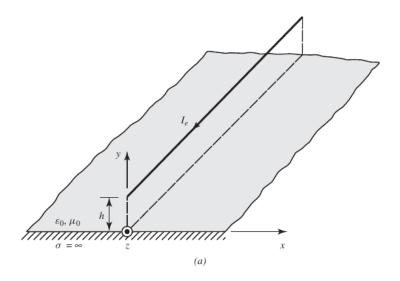


Figure 1: fig. 11-2

4 - 11.20

For a strip of width $w = 2\lambda$, plot the $\frac{RCS}{\lambda_o^2}$ (in dB) when the length of the strip is $l = 5\lambda$, 10λ and 20λ (plot all three graphs on the same figure). Use the approximate relation between the 2D SW and the 3D RCS. Assume normal incidence.

Attempting to solve these was a bit of a challenge in Ansys. I was having issues with getting the answers due to an error that kept crashing the machines. It was the following:

Solving adaptive frequency ..., process hf3d error: Matrix solver exception: SOLVER_OUT_OF_MEMORY: please verify RAM Limit (%) setting. Please contact Ansys technical support. (11:00:12 PM Mar 12, 2024)
Solving adaptive frequency ..., process hf3d: Out of memory (11:00:12 PM Mar 12, 2024)
Simulation completed with execution error on server. Local Machine. (11:00:17 PM Mar 12, 2024)
Mar 12, 2024)
The trace 'd6(NormRCSTotal)' refers to a solution that has been either deleted or is no longer applicable for trace's report type. The trace has been deleted as a result. (11:05:13 PM Mar 12, 2024)
The report 'Normalized Bistatic RCS Plot 1' was deleted because its traces were invalidated due to the edit. (11:05:13 PM Mar 12, 2024)
Solving adaptive frequency ..., process hf3d error. Matrix solver exception: SOLVER_OUT_OF_MEMORY: please verify RAM Limit (%) setting. Please contact Ansys technical support. (11:14:14 PM Mar 12, 2024)
Solving adaptive frequency ..., process hf3d: Out of memory (11:14:14 PM Mar 12, 2024)
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Figure 2: error seen

Because of this, the plot for the 20λ plot did not work out. It kept failing no matter the changes I made to the bounding box. In order for the plots to be generated for these, I had to change the number of points quite a bit. I usually prefer to leave these with a min resolution of 10 but it was not possible in this case. instead, here is a plot that includes 7.5λ in 3.

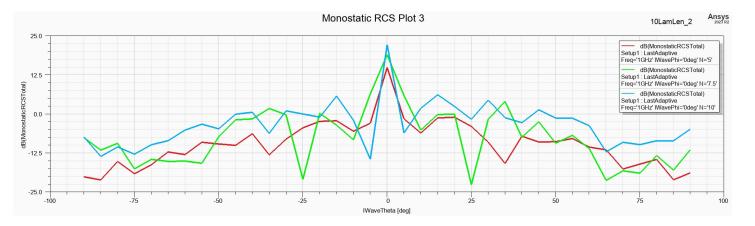


Figure 3: plots for 5λ , 7.5λ and 10λ

References

[1] Constantine A. Balanis. advanced engineering electromagnetics, chapter 1, page 2–3. John Wiley & Sons, 2024.