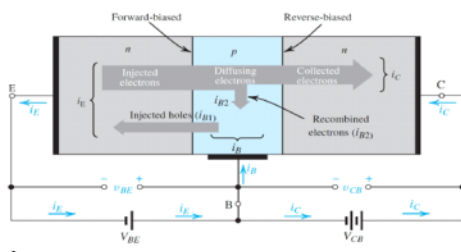
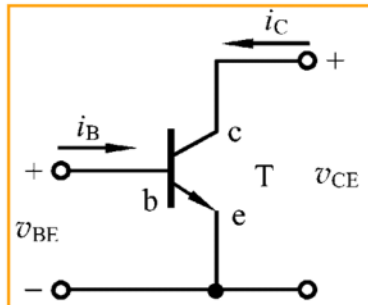




$i_C \sim v_{CE}$ curve:



i_C :

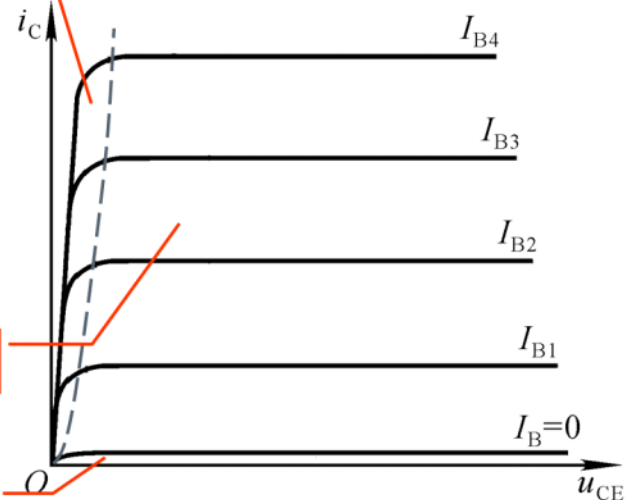
Electrons E \rightarrow B \rightarrow C

Saturation

$$i_C = f(u_{CE})|_{I_B}$$

Active

Cutoff



A big i_B results in a big i_C .



Mode	EBJ	CBJ
Cutoff	Reverse	Reverse
Active	Forward	Reverse
Saturation	Forward	Forward

Saturation region: i_C is mainly controlled by v_{ce} , $\beta i_b > i_c$

$$V_{BE} = 0.7V, V_{CE} < 1V$$

Active region: i_C is basically parallel with v_{ce} , $\beta i_b = i_c$

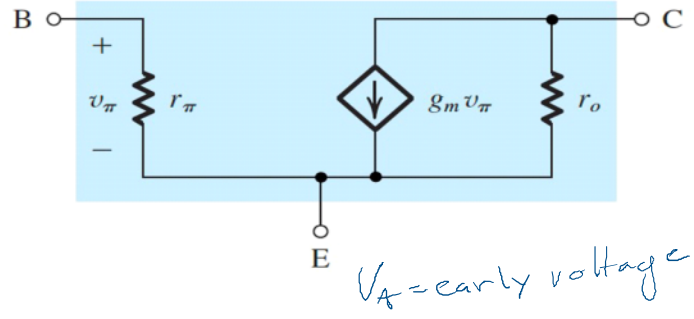
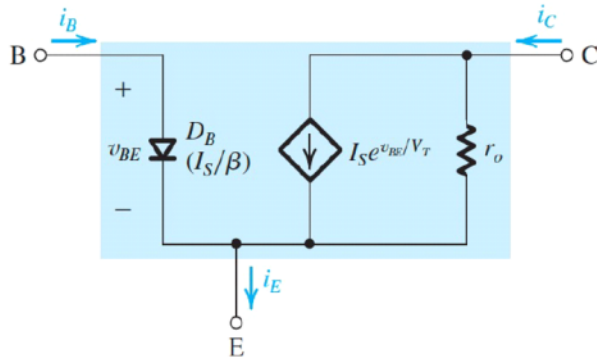
$$V_{BE} = 0.7V, V_{CE} > 1V$$

Cutoff region: i_C is approaching to 0, $i_b \approx i_c \approx 0$

$$V_{BE} < 0.5V$$



Inclusion of early effect in large-signal and small-signal models:



V_A = early voltage

$15 > V_A > 200$

$$r_o = \frac{V_A}{I_S e^{V_{BE}/V_T}} \approx \frac{V_A}{I_C}$$



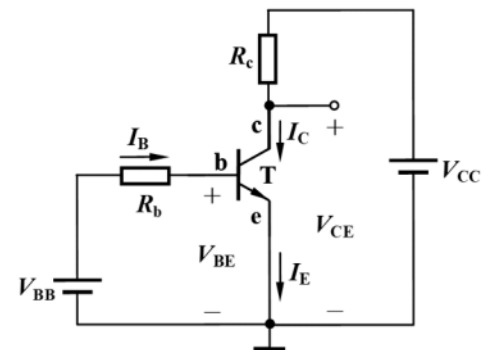
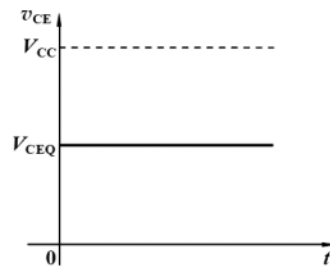
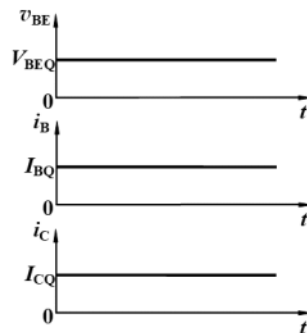
DC biasing (Static operating point (Q point)):

$$I_{BQ} = \frac{V_{BB} - V_{BEQ}}{R_b}$$

$$I_{CQ} \approx \beta \cdot I_{BQ}$$

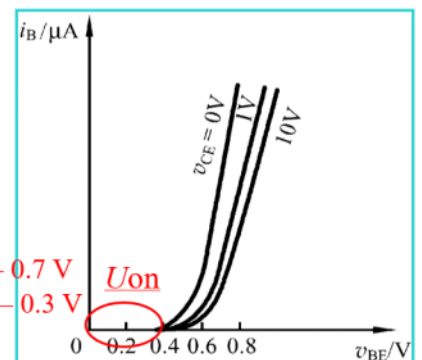
$$V_{CEQ} = V_{CC} - I_{CQ} R_c$$

$$Q(I_{BQ}, I_{CQ}, V_{CEQ})$$



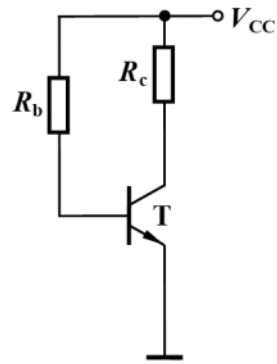
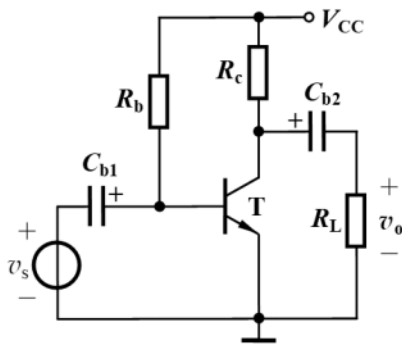
Si: 0.5 – 0.7 V

Ge: 0.1 – 0.3 V

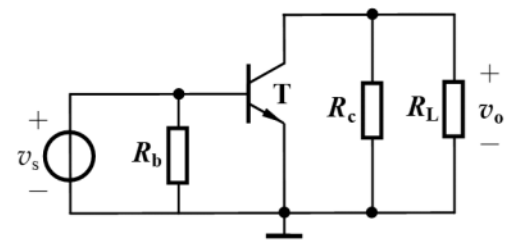




DC circuit and AC circuit:



DC circuit



AC circuit

DC circuit: capacitor is open, AC source is open;

AC circuit: capacitor is short, DC source is short;

slide 8:

A theoretical relationship between i_c and V_{CE} is that i_c is parallel with V_{CE} . When V_{CE} reaches a certain value, but in practical product, when you measure a NPN transistor, the i_c is not parallel with V_{CE} anymore. We call it early effects. To model the effects:

$$I_c = I_s \exp \frac{V_{BE}}{V_T} \left(1 + \frac{V_{CE}}{V_A} \right). \quad V_A \text{ is early voltage.}$$

slide 9:

if we have a small perturbation (ΔV) on V_{CE} , then $V_{CE} + \Delta V \rightarrow V_{CE}$

$$\begin{aligned} I_c &= I_s \exp \frac{V_{BE}}{V_T} \left(1 + \frac{V_{CE} + \Delta V}{V_A} \right) \\ &= I_s \exp \frac{V_{BE}}{V_T} \left(1 + \frac{V_{CE}}{V_A} + \frac{\Delta V}{V_A} \right) \\ &= I_s \exp \frac{V_{BE}}{V_T} \left(1 + \frac{V_{CE}}{V_A} \right) + I_s \exp \frac{V_{BE}}{V_T} \cdot \frac{\Delta V}{V_A} \\ &\approx I_{c0} + I_s \exp \frac{V_{BE}}{V_T} \cdot \frac{\Delta V}{V_A} \end{aligned}$$

It means with the inclusion of early effects, there is one more current ($I_s \exp \frac{V_{BE}}{V_T} \cdot \frac{\Delta V}{V_A}$) in the collector load, and the current is

$$\Delta I = I_s \exp \frac{V_{BE}}{V_T} \cdot \frac{\Delta V}{V_A} \Rightarrow \frac{\Delta V}{\Delta I} = \frac{V_A}{I_s \exp \frac{V_{BE}}{V_T}} \approx \frac{V_A}{I_c}$$

then can be modeled with a resistor (r_o)

slide 18:

When $V_s = 0$, Base and Emitter will be short, the transistor will operate at cutoff state.

Answers to practical exercise of lecture - 3

① the transistor is working at the cutoff region.

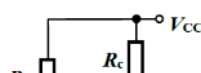
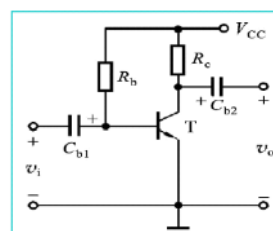
possible reasons:

a. (1). R_b is open

$$R_b \text{ is open} \Rightarrow I_B = 0 \Rightarrow I_c = 0 \Rightarrow V_{CE} = V_{CC} - I_c R_c = V_{CC}$$

(2). C_{b1} is short

$$C_{b1} \text{ is short} \Rightarrow V_{BE} = 0 \Rightarrow I_B = 0 \Rightarrow I_c = 0 \Rightarrow V_{CE} = V_{CC} - I_c R_c = V_{CC}$$



C_{b1} is short $\Rightarrow V_{b1} = V_{cc} \Rightarrow V_{b2} = V_{cc} \Rightarrow V_{ce} = V_{cc} - V_{ce} = 0$

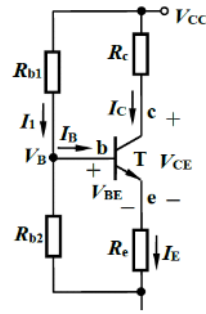
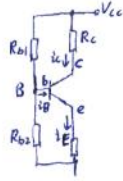
②

$$V_{BQ} \approx \frac{R_{b1}}{R_{b1} + R_{b2}} \cdot V_{cc}$$

$$I_{CQ} \approx I_{EQ} \approx \frac{V_{BQ} - V_{BEQ}}{R_e}$$

$$V_{CEQ} = V_{cc} - I_{CQ}R_c - I_{EQ}R_e = V_{cc} - I_{CQ}(R_c + R_e)$$

$$I_{BQ} = \frac{I_{CQ}}{\beta}$$

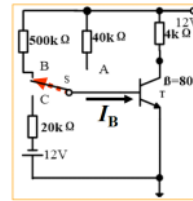


③

$$I_{BQ} = \frac{V_{cc} - V_{BEQ}}{500k\Omega} = \frac{12 - 0.6}{500k\Omega} \approx 23\mu A$$

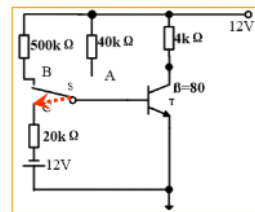
$$I_{CQ} = \beta I_{BQ} = 80 \times 23\mu A = 1.84mA$$

$$V_{CEQ} = V_{cc} - I_{CQ}R_c = 4.64V. \quad Q(23\mu A, 1.84mA, 4.64V)$$



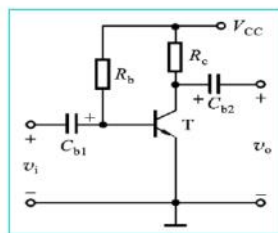
④

Due to Base and Emitter Junction is reversed, the transistor is working at the cutoff region.



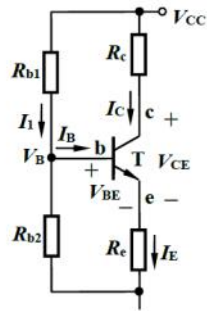
== CAN WE CALCULATE ==

1. For a BJT-based amplification circuit, we measure the voltage of V_{CE} , and find its value approximately equal to V_{CC} , please evaluate the operating state of the circuit and also list the possible reasons resulting in the phenomenon.



1. First reason is that V_{CC} is to ground and therefore we measure the exact same.
2. R_c is so FUCKING small, that we ignore it instead R_b is open and ALL runs through R_c
3. C_{b1} is short and there is no voltage generator.

2. Give the formulae to calculate the Q point of the following circuit? ($I_1 \gg I_B$)



Q point (I_{BQ} , I_{CQ} , V_{CEQ})

$$I_{BQ} = \frac{V_{BQ} - V_{BEQ}}{R_B} \approx \frac{I_{CQ}}{\beta}$$

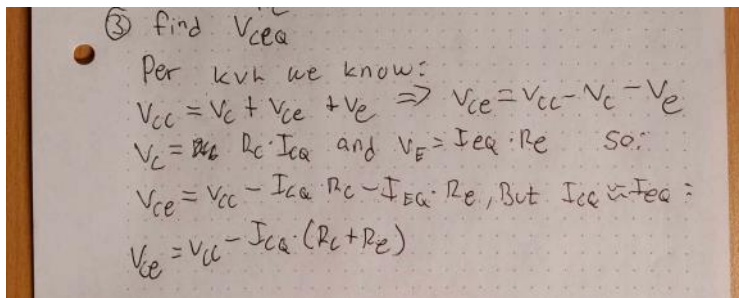
$$I_{CQ} \approx \beta \cdot I_{BQ}$$

$$; V_{BEQ} = 0.6 < V_{BEQ} < 0.8$$

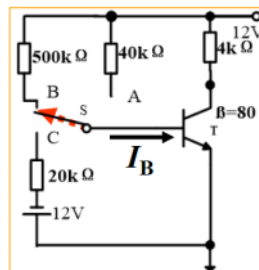
$$; R_B = R_{b1} \parallel R_{b2}$$

$$V_{CEQ} = V_{CC} - I_{CQ} \cdot R_C \quad ; \quad V_{BQ} = \frac{R_{b2}}{R_{b1} + R_{b2}} V_{CC}$$

$I_{CQ} \approx I_{EQ}$ as I_{BQ} is very small for $\frac{I_{CQ}}{\beta}$ and that it will be very large



3. Calculate the Q point of the following circuit and also evaluate what region does the transistor operate? ($V_{BEQ} = 0.6 \text{ V}$)



Q = (I_{BQ} , I_{CQ} , V_{CEQ})

$$V_{BEQ} = 0.6 \text{ V}$$

$$I_{BQ} = \frac{V_{BB} - V_{BEQ}}{R_B} = \frac{12\text{V} - 0.6\text{V}}{20\text{k}\Omega} = 23\mu\text{A}$$

$$I_{BQ} = \frac{V_{bb} - V_{BEQ}}{R_b} = \frac{12V - 0.6V}{500k\Omega} = 23\mu [A]$$

$$I_{CQ} = \beta \cdot I_{BQ} = 80 \cdot 23\mu = 1.84m [A]$$

$$V_{CEQ} = V_{CC} - I_{CQ} \cdot R_c = 12 - 1.8mA \cdot 4k[\Omega] = 4.64 [V]$$

$$\underline{\underline{Q \text{ point}(23\mu[A], 1.84m[A], 4.64 [V])}}$$