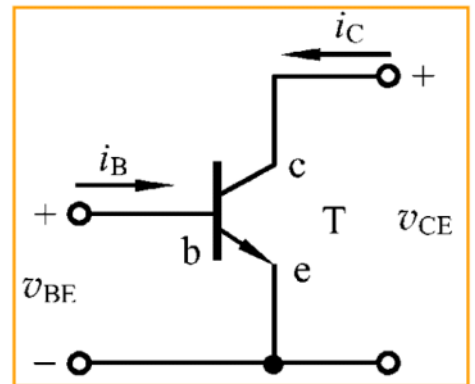


$$i_C = I_S \left(e^{(v_{BE}/V_T)} - 1 \right) = \frac{A_E q D_n n_i^2}{N_B W_B} \left(e^{(v_{BE}/V_T)} - 1 \right)$$

$$\approx \frac{A_E q D_n n_i^2}{N_B W_B} e^{(v_{BE}/V_T)}$$

$$i_B = \left(\frac{A_E q D_p n_i^2}{N_D L_p} + \frac{A_E q W n_i^2}{2 \tau_b N_A} \right) \left(e^{(v_{BE}/V_T)} - 1 \right)$$

$$\approx \left(\frac{A_E q D_p n_i^2}{N_D L_p} + \frac{A_E q W n_i^2}{2 \tau_b N_A} \right) e^{(v_{BE}/V_T)}$$

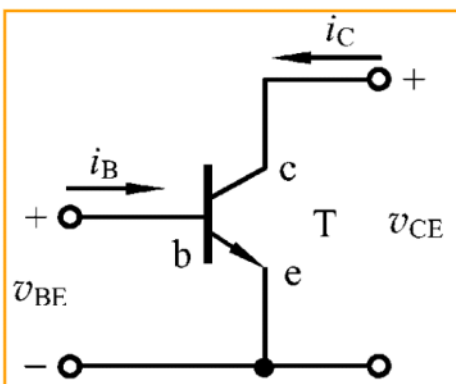


Current gain

$$\beta = \frac{i_C}{i_B}$$

$$i_B = \frac{i_C}{\beta} = \frac{I_S \left(e^{(v_{BE}/V_T)} - 1 \right)}{\beta} = \left(\frac{I_S}{\beta} \right) \left(e^{(v_{BE}/V_T)} - 1 \right)$$

According to KCL:



$$i_E = i_B + i_C = \frac{i_C}{\beta} + i_C$$

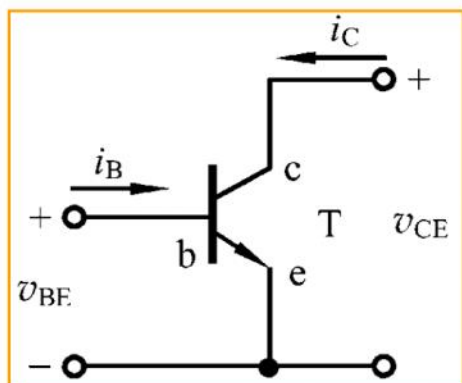
$$= \frac{\beta + 1}{\beta} i_C$$

$$= \frac{\beta + 1}{\beta} I_S \left(e^{(v_{BE}/V_T)} - 1 \right)$$

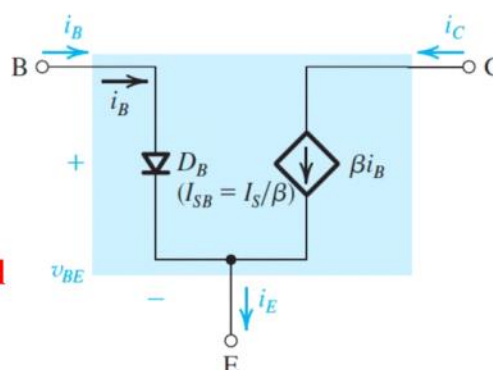
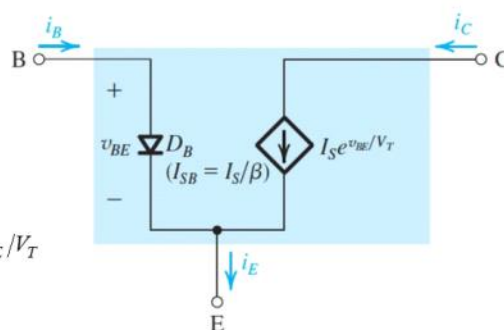
$$\alpha = \frac{i_C}{i_E} \quad \longrightarrow \quad \alpha = \frac{\beta}{\beta + 1} \quad \text{or} \quad \beta = \frac{\alpha}{1 - \alpha}$$



Simple bipolar transistor model



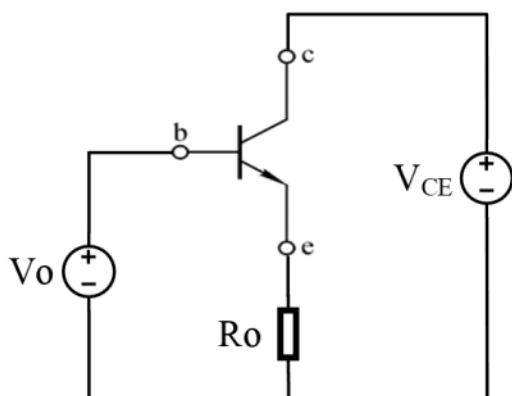
$$i_B = \frac{i_C}{\beta} = \frac{i_S}{\beta} e^{v_{BE}/V_T}$$



Application of a simple bipolar transistor model

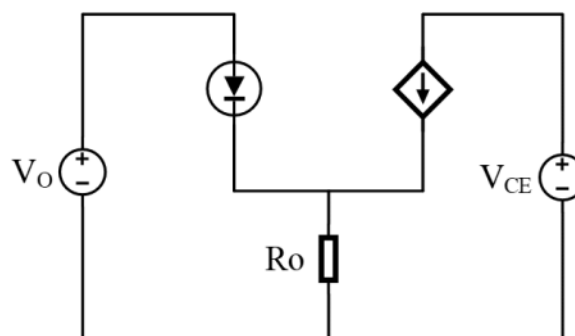


Application of a simple bipolar transistor model



$$V_o = 5V, V_{CE} = 12V, R_o = 100 \Omega$$

$$I_S = 5 \times 10^{-16} A$$

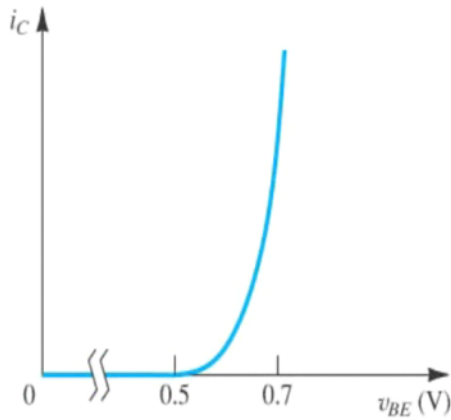


$$V_o = V_{BE} + R_o \cdot I_E \approx V_T \ln \frac{I_C}{I_S} + R_o \cdot I_C$$





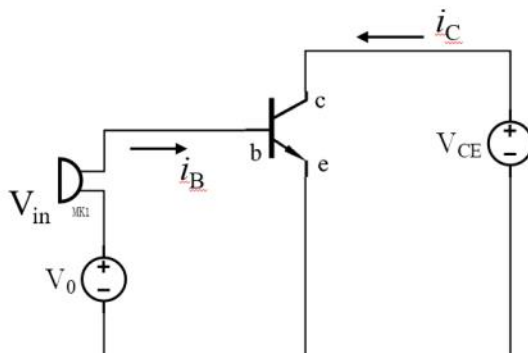
Concept of transconductance:



$$g_m = \frac{\Delta i_c}{\Delta v_{BE}} = \frac{di_c}{dv_{BE}}$$

$$i_c = I_S e^{v_{BE}/V_T}$$

$$g_m = \frac{d}{dv_{BE}} (I_S e^{v_{BE}/V_T}) = \frac{I_S}{V_T} e^{v_{BE}/V_T} = \frac{i_c}{V_T}$$



$$V_{in} = V_m \sin \omega t$$

$$\begin{aligned} i_C &= I_S e^{\frac{V_0 + V_m \sin \omega t}{V_T}} = I_S e^{\frac{V_0}{V_T}} \cdot e^{\frac{V_m \sin \omega t}{V_T}} \\ &= I_{CO} \cdot e^{\frac{V_m \sin \omega t}{V_T}} \approx I_{CO} \cdot \left(1 + \frac{V_m \sin \omega t}{V_T}\right) \\ &= I_{CO} + \frac{I_{CO}}{V_T} V_m \sin \omega t \\ &= I_{CO} + g_m V_m \sin \omega t \end{aligned}$$

slide 6:

To figure out the component over V_{BE} , we need to find out the relationship between i_b and V_{BE} in this circuit branch.

slide 7:

We know that:

$$i_b = \frac{i_c}{\beta} = \frac{I_s}{\beta} \exp\left(\frac{V_{BE}}{V_T}\right)$$

therefore, the component over V_{BE} is a PN diode.

slide 13:

When a small perturbation is added in the input side:

$V_{in} = V_m \sin \omega t$, then

$$\begin{aligned} I_c &= I_s \exp\left(\frac{V_0 + V_{in}}{V_T}\right) = I_s \exp\left(\frac{V_0}{V_T}\right) \cdot \exp\left(\frac{V_m \sin \omega t}{V_T}\right) \\ &= I_{c0} \cdot \exp\left(\frac{V_m \sin \omega t}{V_T}\right) \\ &\approx I_{c0} \cdot \left(1 + \frac{V_m \sin \omega t}{V_T}\right) \quad \text{we use an approximation here: } e^x \approx 1 + x, \text{ when } x \ll 1 \\ &= I_{c0} + \frac{I_{c0}}{V_T} V_m \sin \omega t \\ &= I_{c0} + g_m V_m \sin \omega t \\ &= I_{c0} + g_m V_{in} \end{aligned}$$

1. A bipolar transistor has a collector current of 1mA and $I_s = 5 \times 10^{-16}$ A, how much is V_{BE} ? If $\beta = 50$, how much is base current?

① $I_c = 1 \text{ mA}$, $I_s = 5 \times 10^{-16} \text{ A}$, $V_T = 26 \text{ mV}$

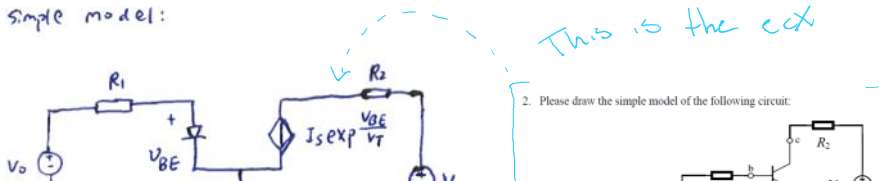
$$I_c = I_s \exp\left(\frac{V_{BE}}{V_T}\right) \rightarrow V_{BE} = \ln\left(\frac{I_c}{I_s}\right) \cdot V_T$$

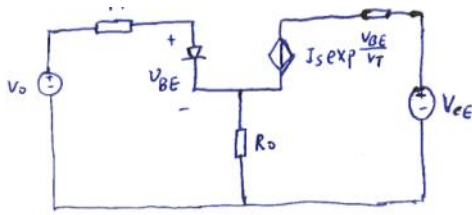
$I_c = I_s \exp\left(\frac{V_{BE}}{V_T}\right)$ This is big NONO

$$V_{BE} = 5 \times 778 \text{ mV} = 3.89 \text{ V} \quad \leftarrow \text{save it here or forget it}$$

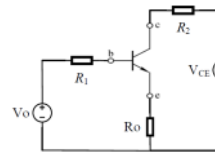
$$I_b = \frac{I_c}{\beta} = \frac{1 \text{ mA}}{50} = 20 \mu\text{A}$$

② simple model:





2. Please draw the simple model of the following circuit:



3. If $V_0 = 5\text{ V}$, $R_0 = 100\ \Omega$, $V_{CE} = 12\text{ V}$, $R_1 = 200\ \Omega$, $R_2 = 100\ \Omega$, $\beta = 50$, please calculate collector current? (Just give the final formula, not need to calculate the exact value).

③ $V_0 = 5\text{ V}$, $R_0 = 100\ \Omega$, $V_{CE} = 12\text{ V}$, $R_1 = 200\ \Omega$, $R_2 = 100\ \Omega$, $\beta = 50$, $I_S = 5 \times 10^{-16}\text{ A}$

$$V_0 = R_1 \cdot i_B + V_{BE} + R_0 \cdot i_E = R_1 \cdot i_B + V_T \cdot \ln \frac{i_C}{I_S} + R_0 \cdot i_E$$

input
output
 $i_C \approx i_E$

$$V_0 = R_1 \cdot \frac{i_C}{\beta} + V_T \cdot \ln \frac{i_C}{I_S} + R_0 \cdot i_C$$

V_{BE}
 i_C

Øg så her fra kan man isolere for I_C og det er jo så det jeg gerne vil have

$$V_0 = R_1 \cdot \frac{i_C}{\beta} + V_T \ln \left(\frac{i_C}{I_S} \right) + R_0 \cdot i_C$$

$$\Rightarrow i_C = \dots + \dots + \dots$$