

The cable equation A.K.A. the monodomain model

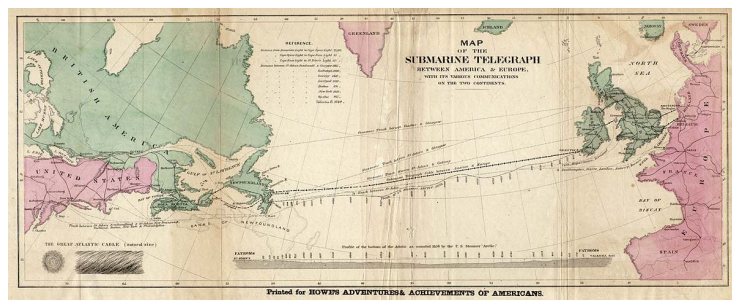
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Overview

- Introduction
 - History
 - Brief overview of neurons
- Derivation of the cable equation
- Scaling/dimensionless form
- Example models
- Gap junctions and cardiac conduction

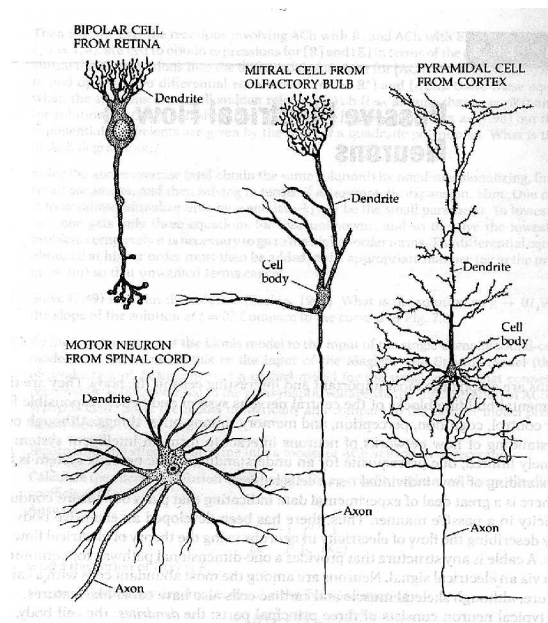
History lesson





The TAT-1 Cable used for the transatlantic cable system on board the HMCS Monarch

Neurons



Why is the cable equation important?

- Fundamental for modeling neurons
- Signal propagation in Purkinje network
- Extends to cardiac conduction in 3D (bidomain, monodomain)

Electric flow in neurons

The neuron consists of three parts:

- Dendrite-tree, the “input stage” of the neuron, converges on the soma.
- Soma, the cell body, contain the “normal” cellular functions
- Axon, the output of the neuron, may be branched. Synapses at the ends are connected to neighboring dendrites.

The axon has an excitable membrane, gives rise to active conduction. Will first look at conduction in the dendrites, passive conduction.

The cable equation (Chap 4.1)

The cell typically has a potential gradient along its length. Radial components will be ignored.

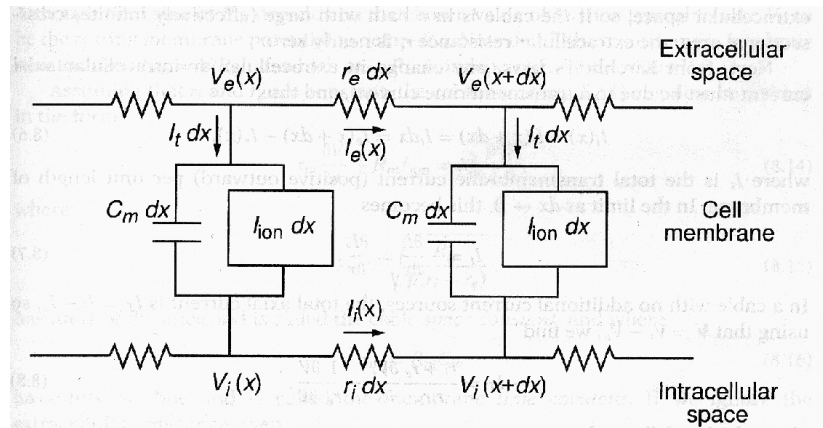
Notation:

- V_i and V_e are intra- and extra cellular potential
- I_i and I_e are intra- and extra cellular (axial) current
- r_i and r_e are intra- and extra cellular resistance per unit length

$$r_i = \frac{R_c}{A_i},$$

where R_c is the cytoplasmic resistivity and A_i is the cross sectional area of the cable.

Sketch of a discrete cable



Currents are assumed to be Ohmic

Current flowing from one point to the next is proportional to the voltage difference between the points:

$$V_i(x + \Delta x) - V_i(x) = -I_i(x)r_i\Delta x$$

$$V_e(x + \Delta x) - V_e(x) = -I_e(x)r_e\Delta x$$

In the limit we have:

$$I_i = -\frac{1}{r_i} \frac{\partial V_i}{\partial x} \text{ and } I_e = -\frac{1}{r_e} \frac{\partial V_e}{\partial x}$$

Conservation of current (1)

Any current leaving the intracellular domain has to enter the extracellular domain, and vice-versa. Total current is conserved between x and $x + \Delta x$:

$$I_i(x) - I_i(x + \Delta x) = -(I_e(x) - I_e(x + \Delta x)) = I_t\Delta x,$$

where I_t is transmembrane current, per unit length.

Again, taking the limit $\Delta x \rightarrow 0$ yields:

$$I_t = -\frac{\partial I_i}{\partial x} = \frac{\partial I_e}{\partial x}$$

Conservation of current (2)

We now have the membrane current I_t expressed in terms of I_i, I_e . We want a relation between the I_t and the membrane potential V .

$$\frac{1}{r_e} \frac{\partial^2 V_e}{\partial x^2} = -\frac{1}{r_i} \frac{\partial^2 V_i}{\partial x^2} = -\frac{1}{r_i} \left(\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V_e}{\partial x^2} \right)$$

$$\left(\frac{1}{r_e} + \frac{1}{r_i} \right) \frac{\partial^2 V_e}{\partial x^2} = -\frac{1}{r_i} \frac{\partial^2 V}{\partial x^2}$$

Conservation of current (3)

$$\left(\frac{1}{r_e} + \frac{1}{r_i} \right) \frac{\partial^2 V_e}{\partial x^2} = -\frac{1}{r_i} \frac{\partial^2 V}{\partial x^2}$$

$$\frac{\partial^2 V_e}{\partial x^2} = -\frac{\frac{1}{r_i}}{\frac{1}{r_e} + \frac{1}{r_i}} \frac{\partial^2 V}{\partial x^2} = -\frac{r_e}{r_e + r_i} \frac{\partial^2 V}{\partial x^2}$$

so

$$I_t = \frac{\partial I_e}{\partial x} = -\frac{1}{r_e} \frac{\partial^2 V_e}{\partial x^2} = \frac{1}{r_e + r_i} \frac{\partial^2 V}{\partial x^2}$$

Incorporating cell membrane physiology

From the membrane model previously derived we have

$$I_t = p(C_m \frac{\partial V}{\partial t} + I_{ion})$$

where p is the circumference of the cable. The total expression will be in Ampere/meter.

The total 1D cable model is then:

$$p(C_m \frac{\partial V}{\partial t} + I_{ion}(V)) = (\frac{1}{r_e + r_i} \frac{\partial^2 V}{\partial x^2})$$

Physical units

So far we have disregarded physical units in the equation. Typical units are

Quantity	Dimension	Typical unit
p	length	cm
C_m	capac./area	μ F/cm ²
V	voltage	mV
I_{ion}	current/area	μ A/cm ²
r_i, r_e	res./length	$10^{-3} \Omega$ cm
x	length	cm
t	time	ms

Exercise

Verify that all terms in the cable equation have the same physical units:

$$p(C_m \frac{\partial V}{\partial t} + I_{ion}(V)) = (\frac{1}{r_e + r_i} \frac{\partial^2 V}{\partial x^2})$$

Quantity	Dimension	Typical unit
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What is the unit of the terms in the equation?

Scaling the cable equation (1)

We can scale the variables to reduce the number of parameters. Define a membrane resistance:

$$\frac{1}{R_m} = \frac{\Delta I_{ion}}{\Delta V}(V_0)$$

where V_0 is the resting potential. Multiplication with R_m

$$C_m R_m \frac{\partial V}{\partial t} + R_m I_{ion} = \frac{R_m}{p(r_i + r_e)} \frac{\partial^2 V}{\partial x^2}$$

Here we have assumed r_i and r_e constant.

Defining $f = -R_m I_{ion}$, $\tau_m = C_m R_m$ (time constant) and $\lambda_m^2 = R_m/(p(r_i + r_e))$ (space constant squared) we can write

$$\tau_m \frac{\partial V}{\partial t} - f = \lambda_m^2 \frac{\partial^2 V}{\partial x^2} \quad (1)$$

Scaling the cable equation (2)

Introduce the dimensionless variables:

$$T = t/\tau_m \text{ and } X = x/\lambda_m$$

We can then write:

$$\frac{\partial V}{\partial T} = f + \frac{\partial^2 V}{\partial X^2} \quad (2)$$

A solution $\hat{V}(T, X)$ of (2) will imply that $V(t, x) = \hat{V}(t/\tau_m, x/\lambda_m)$ will satisfy (1).

The scaled equation has units of voltage, but can easily be non-dimensionalized by introducing $V = V_0 + \tilde{V}\tilde{V}$, where \tilde{V} is a characteristic voltage and \tilde{V} is a dimensionless variable.

The reaction term (Chapter 4.2,6.2,6.3)

The form of f depends on the cell type we want to study. For the axon

$I_{ion}(m, n, h, V)$ of the HH-model is a good candidate. For the dendrite, which is

non-excitable, a linear resistance model is good. Shift V so $V = 0$ is the resting potential:

$$\frac{\partial V}{\partial T} = \frac{\partial^2 V}{\partial X^2} - V$$

We need boundary and initial values. Initially at rest:

$$V(X, 0) = 0$$

Boundary conditions

Types of boundary conditions:

- Dirichlet: $V(x_b, T) = V_b$, voltage clamp.
- Neumann: $\frac{\partial V}{\partial x} = -r_i I_i$ (or $\frac{\partial V}{\partial X} = -r_i \lambda_m I_i$), current injection.

Justification:

$$\frac{\partial V_i}{\partial x} = -r_i I_i \Rightarrow \frac{\partial V}{\partial x} - \frac{\partial V_e}{\partial x} = -r_i I_i \xrightarrow{r_e=0} \frac{\partial V}{\partial x} = -r_i I_i$$

Passive condition (1)

The linear cable in dimensionless form:

$$\frac{\partial V}{\partial T} = \frac{\partial^2 V}{\partial X^2} - V$$

Set $V(0) = 0$

We consider a semi-infinite (i.e. long) cable with voltage clamped to V_c at $X = 0$. We have the equation

$$\frac{\partial^2 V}{\partial X^2} = V$$

with solution

$$V = V_c e^{-X} = V_c e^{-x/\lambda_m}$$

Passive conduction (2)

We can compute the space constant for the passive case

$$\lambda_m = \sqrt{R_m/(p(r_i + r_e))} \approx \sqrt{R_m/(pr_i)} = \sqrt{R_m/(pR_c/A)},$$

where we recall that R_c, A_i are cytosolic resistance and cross sectional area. If the cross section is circular with diameter d , we have

$$\lambda_m = \sqrt{R_m/(pR_c/A)} = \sqrt{R_m(\pi d R_c/(\pi(d/2)^2))} = \sqrt{\frac{R_m d}{4R_c}}$$

Typical values for a mammalian neuron; $R_m = 7000\Omega \text{ cm}^2$, $R_c = 150\Omega \text{ cm}$, $d = 10.0\mu \text{ m}$, gives $\lambda_m \approx 1.0 \text{ mm}$. A human axon can be up to a meter long.

The bistable equation (Chapter 6.2.1) (1)

The simplest model of active conduction in neuron is obtained by choosing the reaction term

$$f(V) = AV(1 - V)(V - \alpha),$$

where α is a parameter between 0 and 1, and A is a scaling parameter for the reaction term.

The bistable equation (2)

We have

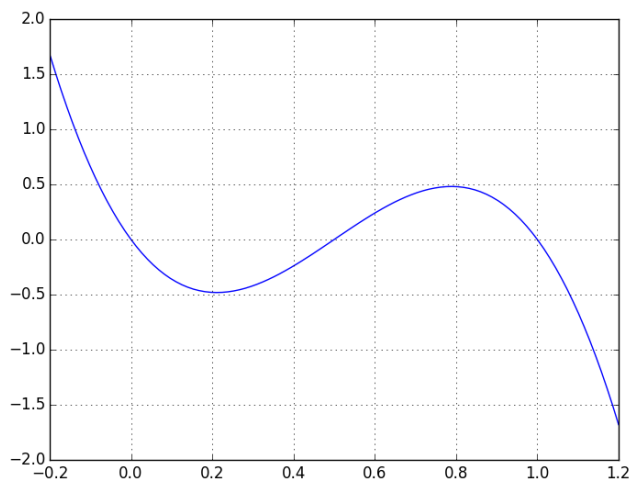
$$\frac{\partial V}{\partial t} = \frac{\partial^2 V}{\partial x^2} + AV(1 - V)(V - \alpha),$$

and if we neglect the diffusion term we get

$$\frac{\partial V}{\partial t} = AV(1 - V)(V - \alpha),$$

The right hand side has three zero's; $V = 0, V = 1, V = \alpha$. These are equilibrium points for the equation ($\partial V / \partial t = 0$).

The bistable equation (3)



Here $\alpha = 0.5$. What happens if the solution is perturbed away from the three equilibrium points $V = 0, V = 1, V = \alpha$? (Recall that $dV/dt = f(V)$)

The bistable equation (4)

- The equation has one unstable and two stable equilibrium points

- Any initial condition $V < \alpha$ will approach $V = 0$
- Any initial condition $V > \alpha$ will approach $V = 1$
- In 1D (with diffusion), the solution is a traveling front (demo)

The FitzHugh-Nagumo model (1)

- The bistable equation describes a traveling front, but never returns to the resting potential
- To describe a propagating action potential we need to add a *recovery variable*
- The result is the Fitzhugh-Nagumo (FHN) model, the simplest model for qualitatively realistic propagation in excitable cells

$$\begin{aligned}\frac{\partial V}{\partial t} &= \frac{\partial^2 V}{\partial x^2} + f(V) - w \\ \frac{\partial w}{\partial t} &= \epsilon(V - \gamma w),\end{aligned}$$

with $\epsilon, \gamma > 0$, and $w(0) = 0$.

The FitzHugh-Nagumo model (2)

Again, we can examine the behavior of the model by neglecting diffusion:

$$\begin{aligned}\frac{\partial V}{\partial t} &= f(V) - w \\ \frac{\partial w}{\partial t} &= \epsilon(V - \gamma w).\end{aligned}$$

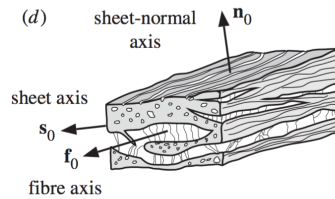
- Initially, the model behaves as the bistable equation
- As V increases, $\frac{\partial w}{\partial t} > 0$
- $w > 0$ will "pull" V back towards $V = 0$
- In 1D, the solution is a traveling wave resembling an action potential (demo)

Conduction in cardiac tissue (1)

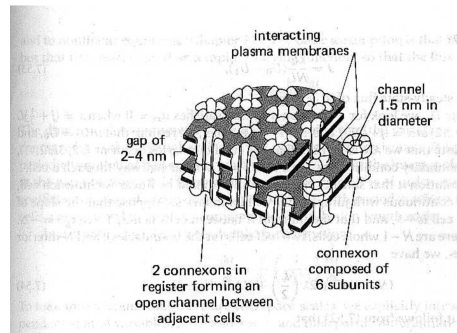
- Neurons are long, cardiac muscle cells are only about 0.1mm
- How is the electrical signal conducted in cardiac tissue?
- Can cardiac conduction be described using similar models as the cable equation?

Conduction in cardiac tissue (2)

- Cardiac myocytes are connected end-to-end, and form fiber-like tissue structure
- The structure has important implications both for mechanical and electrical properties of the tissue
- Electrical conduction between cells is mediated by *gap junctions*



Gap junctions



- Gap junctions are located between cells, and ions may pass through them.
- The junctions have a high resistance to flow compared to the intra cellular environment

Effective conductivity (1)

Consider a 1D line of cell and assume that Fick's law holds in the interior:

$$J = -D \frac{dc}{dx}$$

Between cells we must have continuity of flow:

$$-D \frac{dc(x_b^-)}{dx} = -D \frac{dc(x_b^+)}{dx}$$

Here x_b^- and x_b^+ indicates that the function is evaluated in the limit from left and right, respectively.

Furthermore we assume this flow to be proportional to the fall:

$$J = F[c(x_b^-) - c(x_b^+)]$$

where F is a permeability constant.

Effective conductivity (2)

We would like to relate F and D into an average, large scale, effective diffusion coefficient. Consider N cells of length L :

$$J = -D_e \frac{\Delta c}{\Delta x} = -D_e \frac{c_1 - c_0}{NL}$$

- Steady flux with fixed gradient.
- At steady state J is constant, so from $J = -D(dc/dx)$ we have that c is linear in the interior. The solution c will be piecewise linear with jump at the cell boundaries.
- Continuity of flow over the gaps gives $dc/dx = -\lambda$ for all interfaces.
- For the same reason the steps must all be equal, $c(x_b^-) - c(x_b^+) = \Delta$.

Effective conductivity (3)

The size of Δ and λ must fit the drop ($c_0 - c_1$):

- N intervals of length L : $NL\lambda$
- N jumps of size Δ : $N\Delta$

So in total we must have:

$$NL\lambda + N\Delta = c_0 - c_1$$

From the definition of F we have $D\lambda = F\Delta$. In steady state the flux is the same on every scale:

$$\begin{aligned} J = D\lambda &= \frac{D_e}{NL}(c_0 - c_1) = \frac{D_e}{NL}(NL\lambda + N\Delta) \\ &= \frac{D_e}{NL}(NL\lambda + N\frac{D\lambda}{F}) = D_e\lambda(1 + \frac{D}{FL}) \end{aligned}$$

So

$$D = D_e(1 + \frac{D}{FL}) \Rightarrow \frac{1}{D_e} = \frac{1}{D} + \frac{1}{FL}$$

Summary

- The cable equation describes electrical signals in *leaky* cables
- 1D reaction-diffusion equation, the form of the reaction term depends on the properties of the membrane:
 - Linear; passive membrane
 - Cubic; bistable equation (propagating front)
 - Fitzhugh-Nagumo; coupled to ODE (propagating AP)
- Cardiac tissue can be modeled with a similar approach because of *gap junctions*
- Monodomain and bidomain models of cardiac conduction; 3D extensions of cable equation