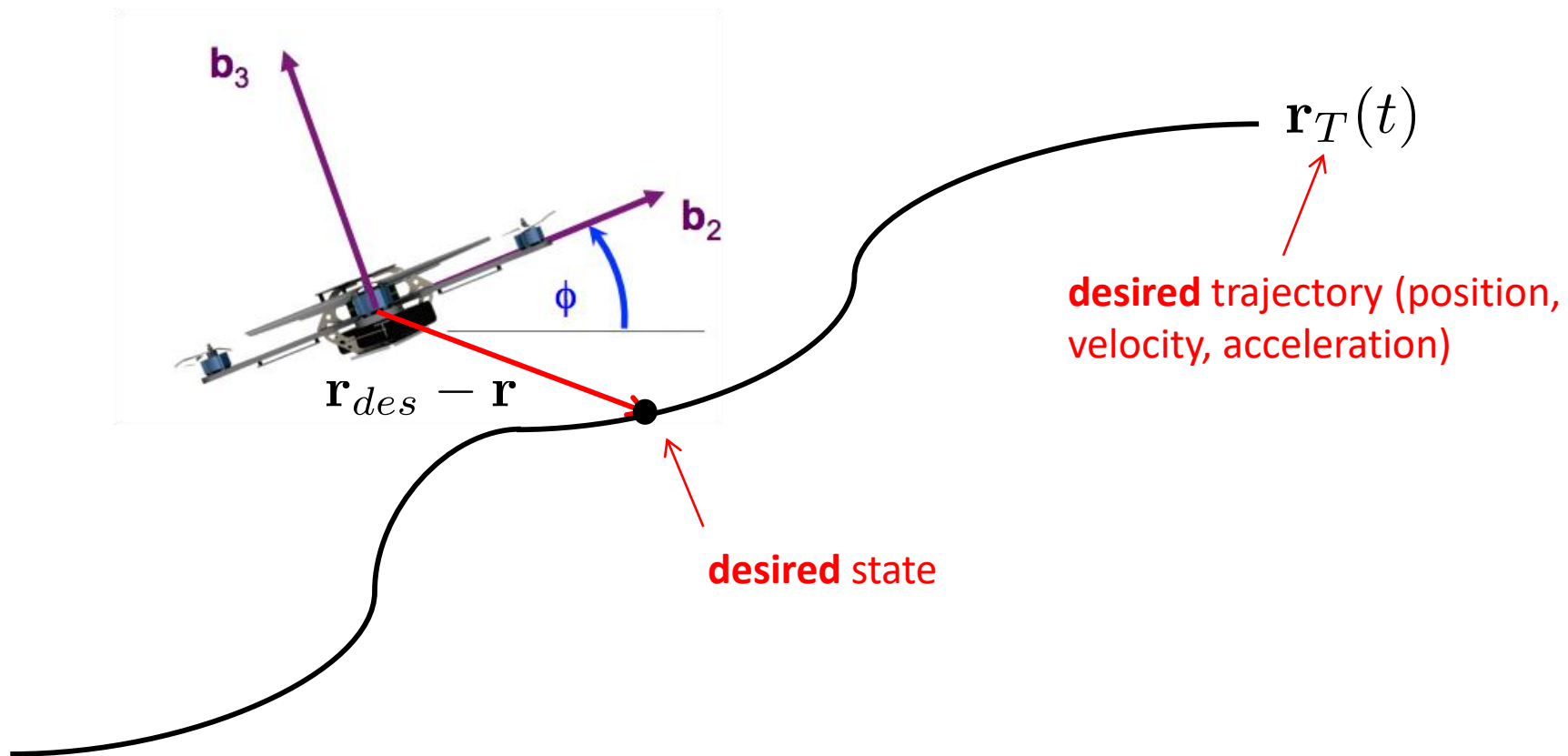


Feedback Control

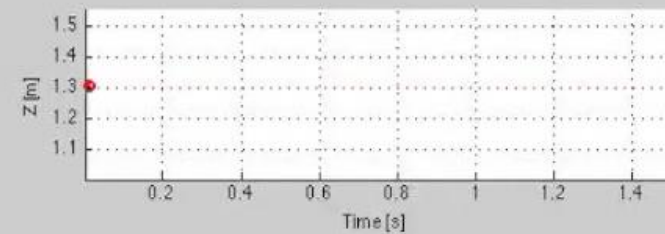
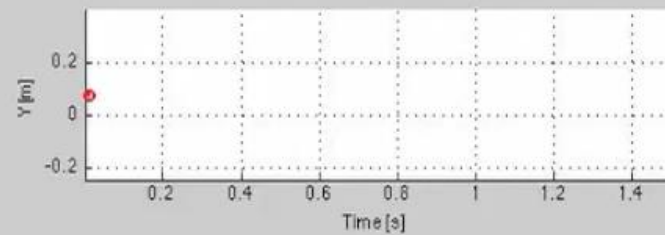
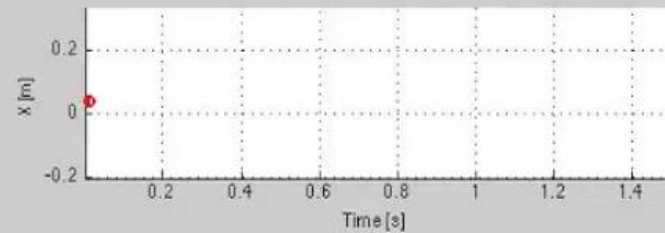
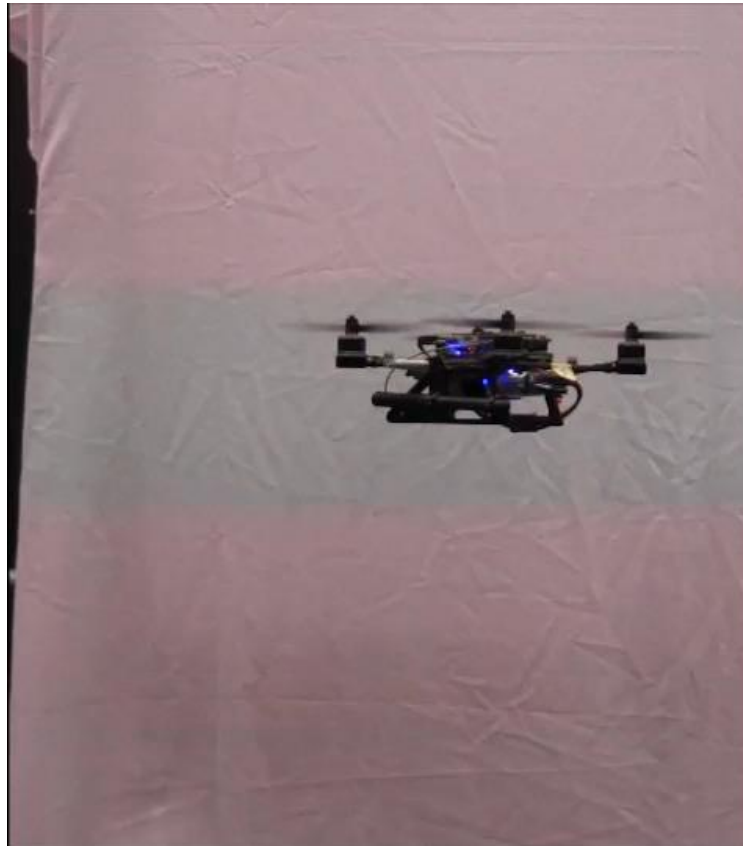
ENGINEERING DESIRABLE SYSTEM DYNAMICS



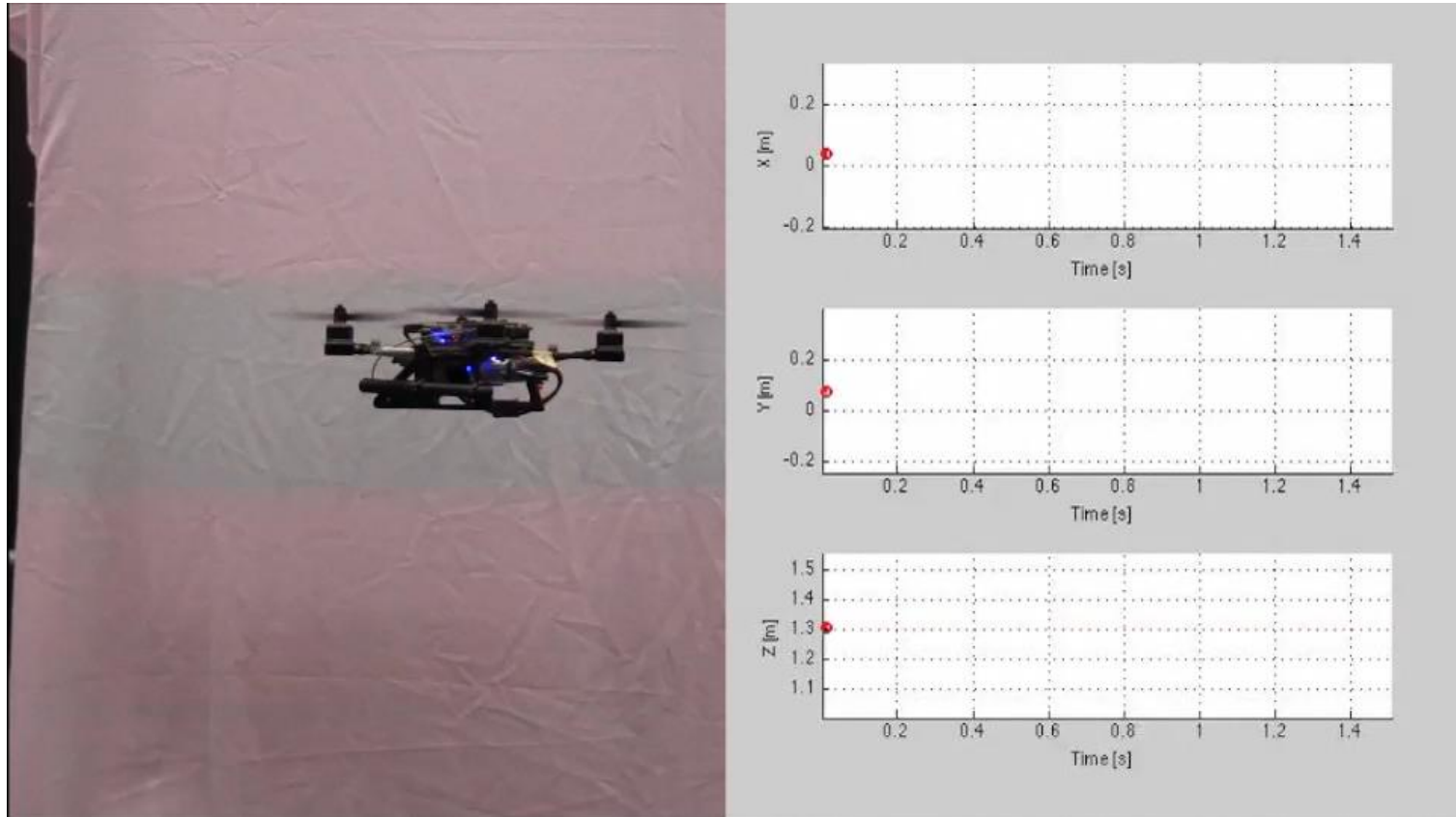
Trajectory Controller



Equilibrium.



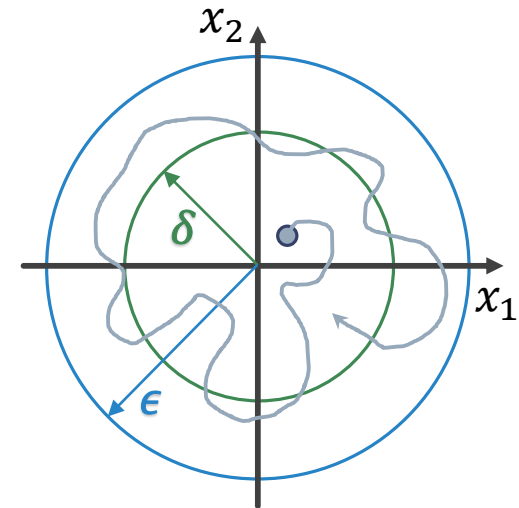
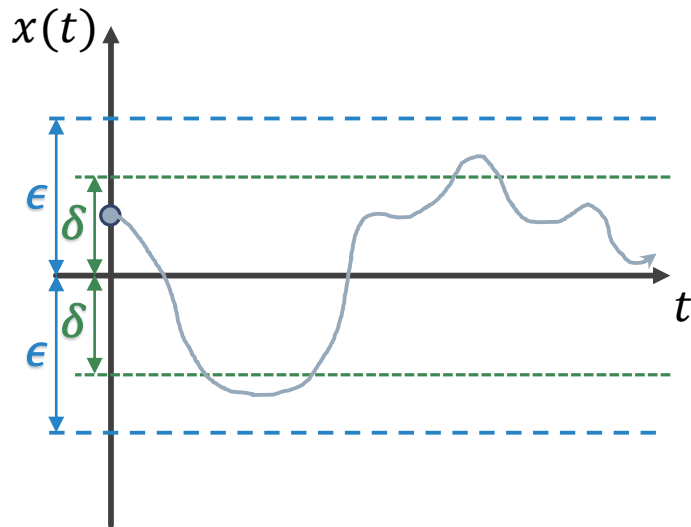
Stability?



Stability in the Sense of Lyapunov

“Stability i.s.L.”

An equilibrium point \mathbf{x}_e of the system $\dot{\mathbf{x}} = f(\mathbf{x})$ is **stable** in the sense of Lyapunov if for any $\epsilon > 0$, there exists a value $\delta(t_0, \epsilon) > 0$ such that if $\|\mathbf{x}(t_0, \mathbf{x}_0) - \mathbf{x}_e\| < \delta$ then $\|\mathbf{x}(t; t_0, \mathbf{x}_0) - \mathbf{x}_e\| < \epsilon$ for all $t \geq t_0$.



- An equilibrium point is unstable if it is not stable i.s.L.
- The equilibrium point is **uniformly stable** i.s.L. if $\delta = \delta(\epsilon)$.

Stability i.s.L. is Weak just by Itself

- Stability i.s.L. means that the system state will remain close to the equilibrium point.
- Stability i.s.L. bounds how much the system state will fluctuate around the equilibrium point.

Does not answer...

- Will it ever reach the equilibrium point?
- Will it stay at the equilibrium point for all future times?

Asymptotic Stability

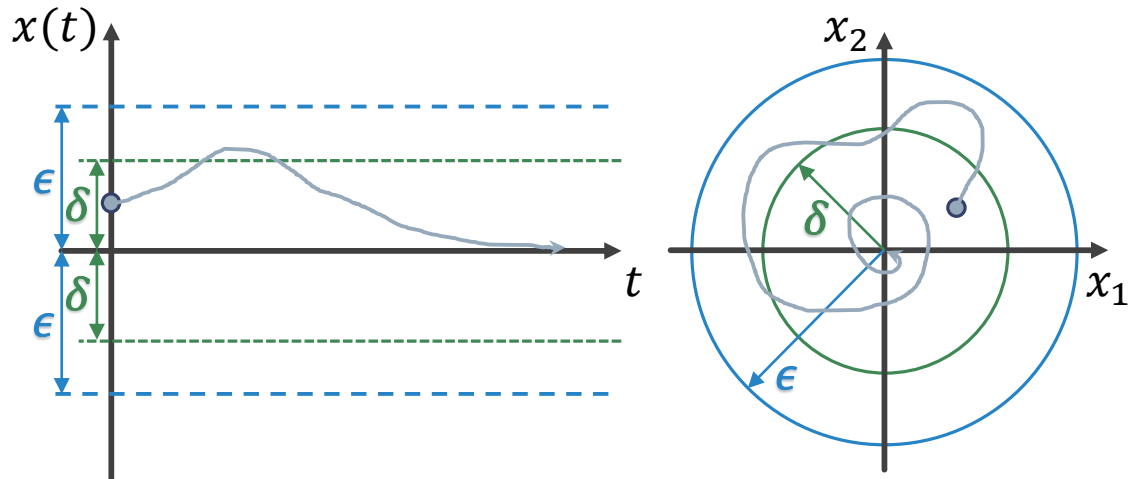
➤ An equilibrium point is asymptotically stable i.s.L. if it is:

1. *Stable (i.s.L.)*

For any $\epsilon > 0$, there exists a value $\delta(t_0, \epsilon) > 0$ such that if $\|\mathbf{x}(t_0, \mathbf{x}_0) - \mathbf{x}_e\| < \delta$ then $\|\mathbf{x}(t; t_0, \mathbf{x}_0) - \mathbf{x}_e\| < \epsilon$ for all $t \geq t_0$.

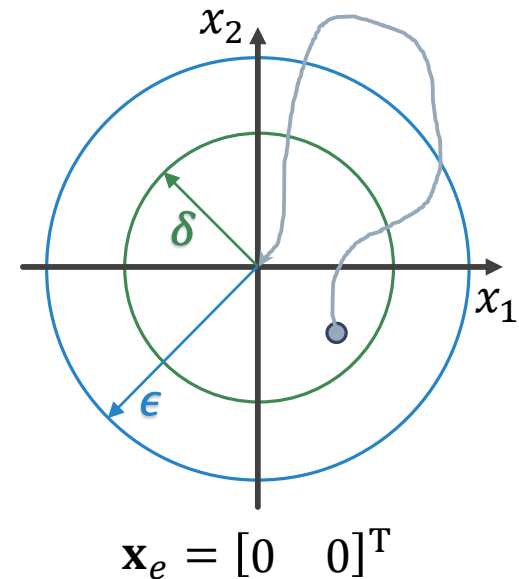
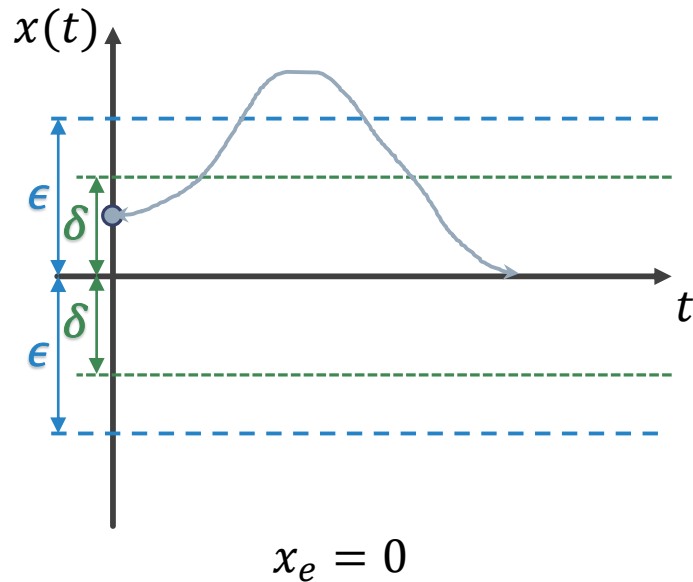
2. *Convergent*

$\mathbf{x}(t; t_0, \mathbf{x}_0) \rightarrow \mathbf{x}_e$ as $t \rightarrow \infty$.



Asymptotic Stability

- **Note:** Convergence alone does not necessarily imply (asymptotic) stability! Why?



Still does not answer...

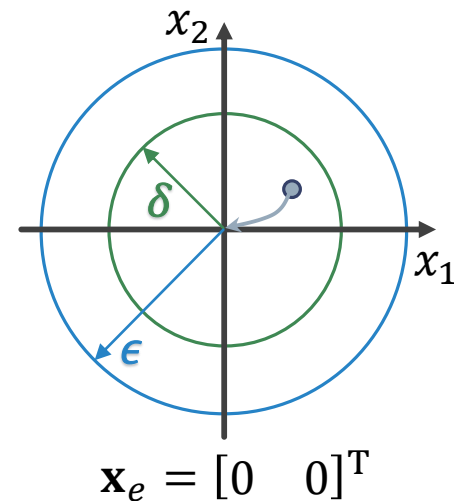
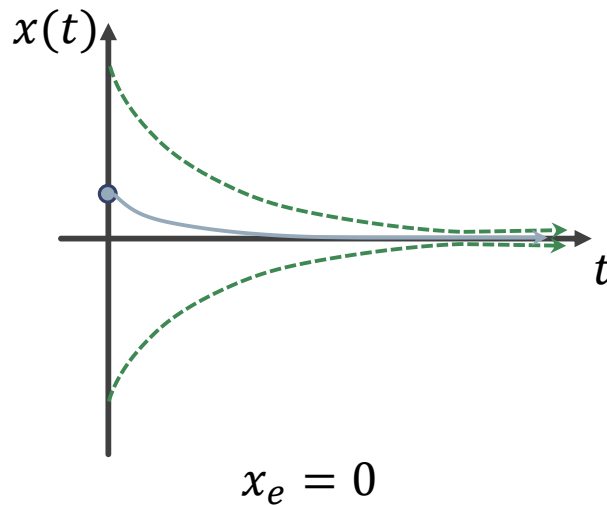
- How fast does it converge?

Exponential Stability

An equilibrium point $\mathbf{x}_e = 0$ is exponentially stable if there exists coefficient $m \geq 0$ and rate $\alpha \geq 0$ such that

$$\|\mathbf{x}(t)\| \leq \|\mathbf{x}_o\| m e^{-\alpha(t-t_0)}$$

For all \mathbf{x}_o in some ball around $\mathbf{x}_e = 0$.



Local vs Global

These are local definitions of stability about an equilibrium point.

- We were free to choose small δ in order to start \mathbf{x}_0 near \mathbf{x}_e .

We say an equilibrium point \mathbf{x}_e is **globally stable** if it is stable for all initial conditions \mathbf{x}_0 .

Stability of LTI Systems


Linear-Time Invariant (LTI) systems:

$$\dot{\mathbf{x}} = A\mathbf{x} \quad \begin{array}{l} \mathbf{x} \in \mathbb{R}^n \\ A \in \mathbb{R}^{n \times n}, \text{ constant} \end{array}$$

- An LTI system is **asymptotically stable** if and only if all the eigenvalues of A have **strictly negative** real parts.
- For LTI systems, asymptotic stability \Leftrightarrow exponential stability.
- The system is **marginally stable** if and only if all the eigenvalues of A have **nonpositive** real parts, at least one has zero real part, *and every eigenvalue with zero real parts has its algebraic multiplicity equal to its geometric multiplicity.*

Control of a First Order System

Problem

- State \mathbf{x} and input \mathbf{u}
- Kinematic model $\dot{\mathbf{x}} = \mathbf{u}$  u is a velocity
- Want to follow trajectory $\mathbf{x}^{\text{des}}(t)$

General approach

- Define error $\mathbf{e}(t) = \mathbf{x}^{\text{des}}(t) - \mathbf{x}(t)$
- Want $\mathbf{e}(t)$ to converge exponentially to 0

Strategy

- Find \mathbf{u} such that $\dot{\mathbf{e}} + K_p \mathbf{e} = 0$
- If $K_p > 0$ then $\mathbf{e}(t) = \exp(-K_p(t - t_0)) \mathbf{e}(t_0)$
- $\mathbf{u}(t) = \dot{\mathbf{x}}^{\text{des}}(t) + K_p \mathbf{e}(t)$

Control of a Second Order System

Problem

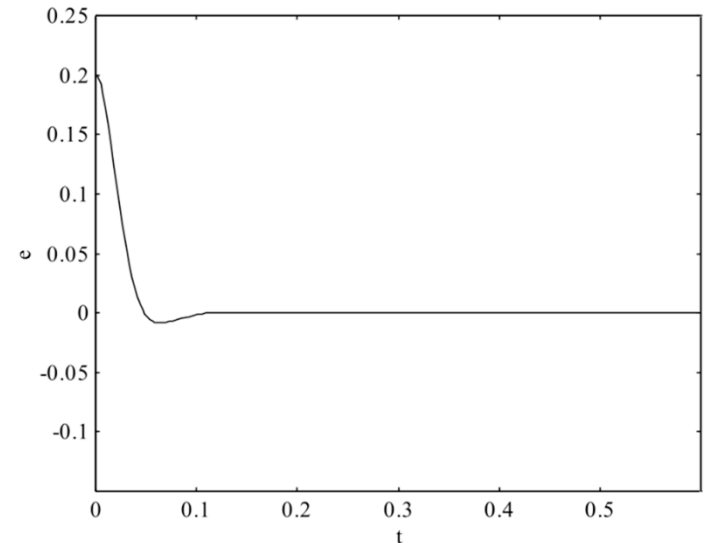
- State \mathbf{x} and input \mathbf{u}
- Kinematic model $\ddot{\mathbf{x}} = \mathbf{u}$ ← \mathbf{u} is an acceleration
- Want to follow trajectory $\mathbf{x}^{\text{des}}(t)$

General approach

- Define error $\mathbf{e}(t) = \mathbf{x}^{\text{des}}(t) - \mathbf{x}(t)$
- Want $\mathbf{e}(t)$ to converge exponentially to 0

Strategy

- Find \mathbf{u} such that $\ddot{\mathbf{e}} + K_d \dot{\mathbf{e}} + K_p \mathbf{e} = 0$
- Pick some $K_p, K_d > 0$
- $\mathbf{u}(t) = \ddot{\mathbf{x}}^{\text{des}}(t) + K_d \dot{\mathbf{e}}(t) + K_p \mathbf{e}(t)$



Control for Trajectory Tracking

PD Control

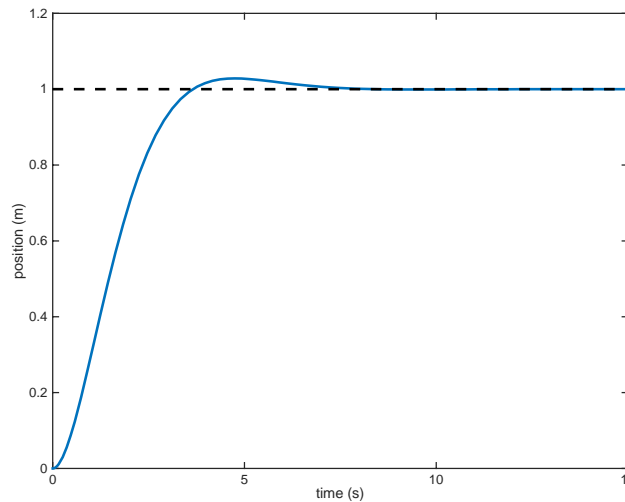
- $\mathbf{u}(t) = \ddot{\mathbf{x}}^{\text{des}}(t) + K_d \dot{\mathbf{e}}(t) + K_p \mathbf{e}(t)$
- Proportional term (K_p) has a spring (capacitance) response
- Derivative term (K_d) has a dashpot (resistance) response

PID Control

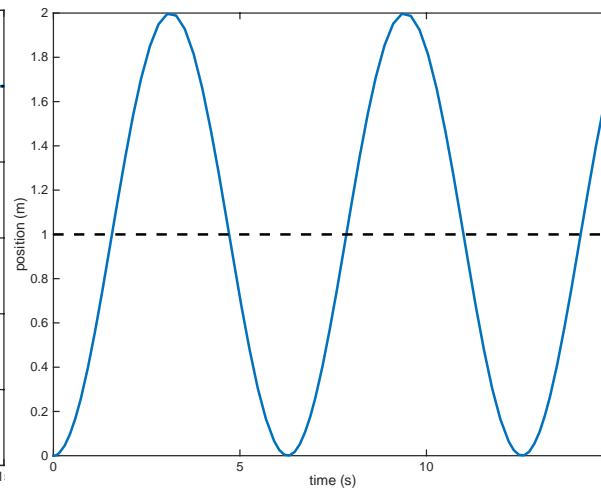
- $\mathbf{u}(t) = \ddot{\mathbf{x}}^{\text{des}}(t) + K_d \dot{\mathbf{e}}(t) + K_p \mathbf{e}(t) + K_I \int_0^t \mathbf{e}(\tau) d\tau$
- Integral term (K_I) makes steady state error go to 0
 - Accounts for model error or disturbances
- PID control generates a third-order closed-loop system

Control Gains

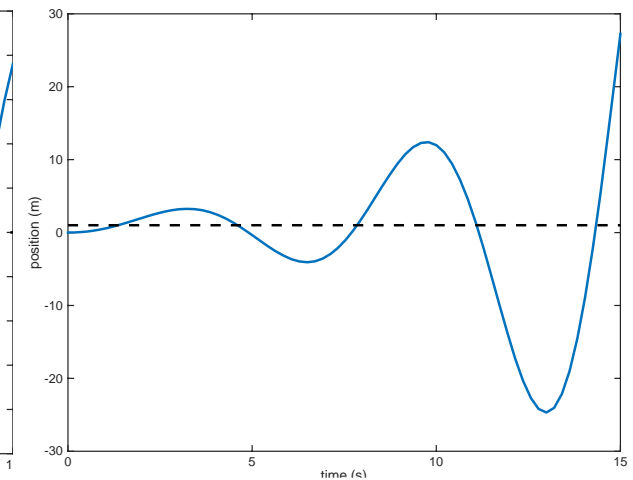
Gains change the system response



Stable



Marginally Stable



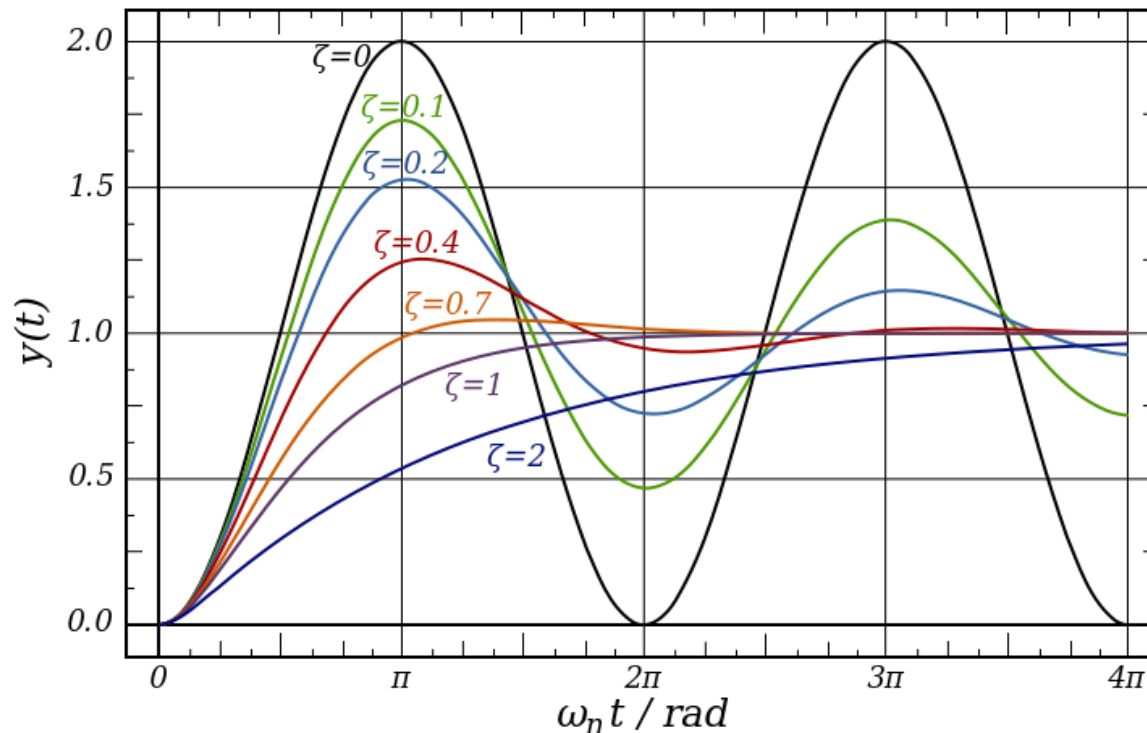
Unstable

Stereotyped 2nd Order Response

$$\ddot{e} + K_d \dot{e} + K_p e = 0$$

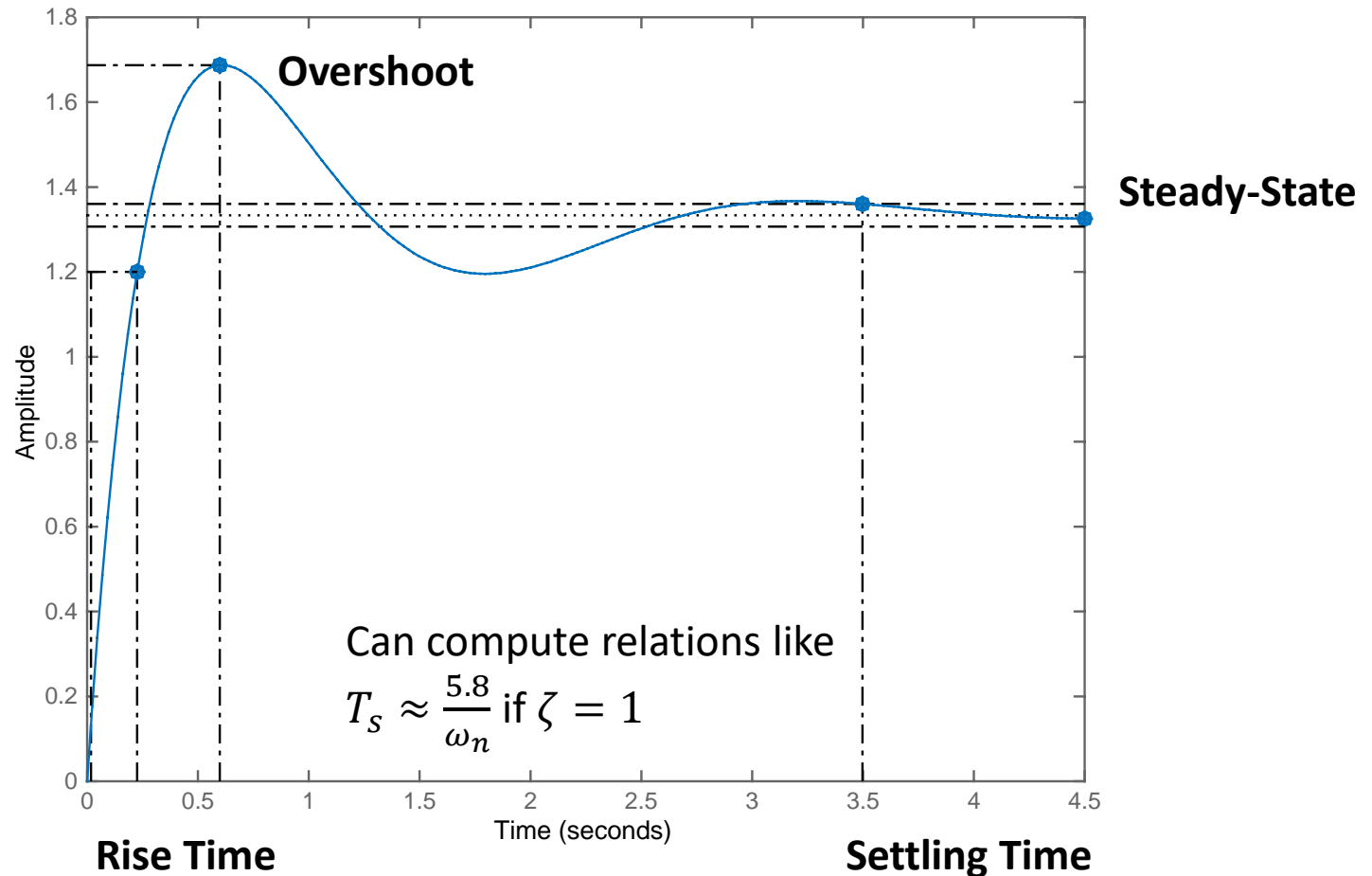
$$\ddot{e} + 2\zeta\omega_n \dot{e} + \omega_n^2 e = 0$$

$$\lambda = -\omega_n(\zeta \pm i\sqrt{1 - \zeta^2})$$

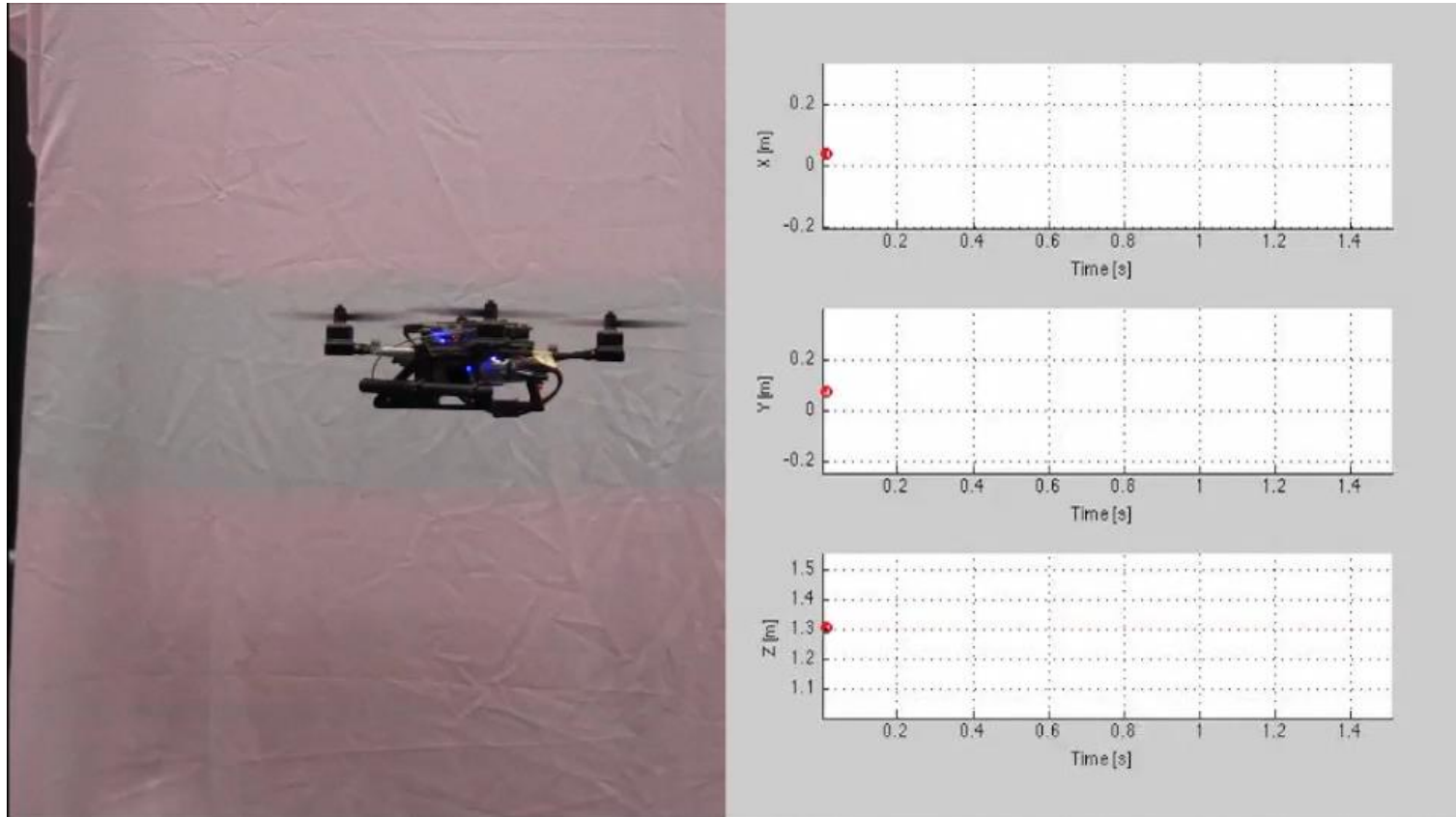


For this simple example, can choose K_p and K_d to get a desired damping ratio.

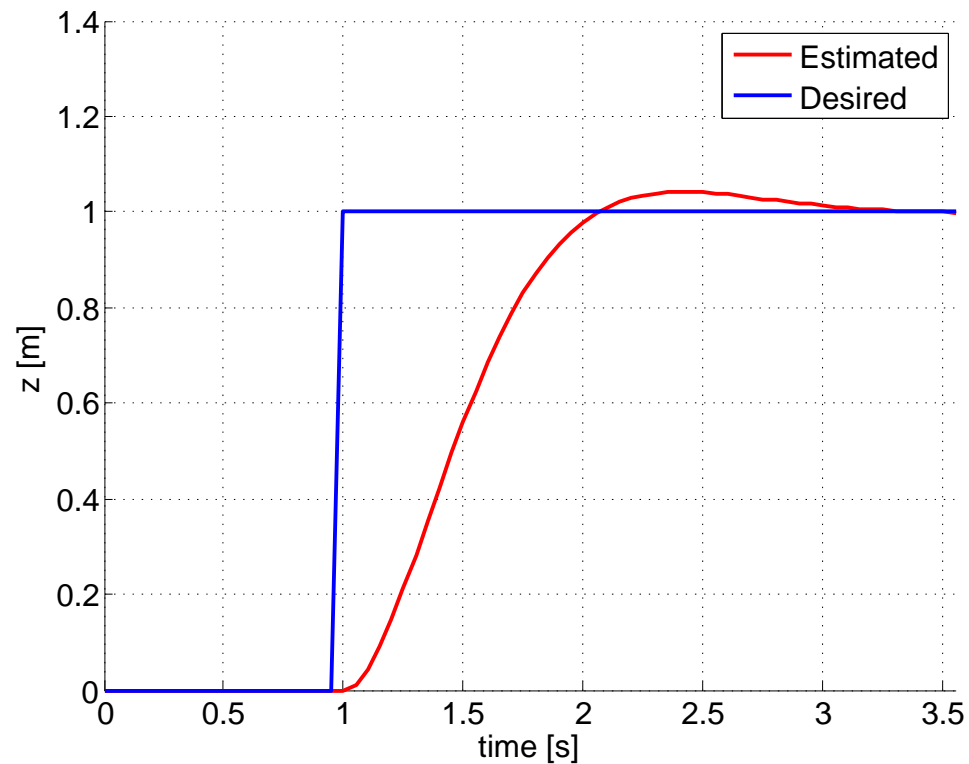
Response to Disturbance



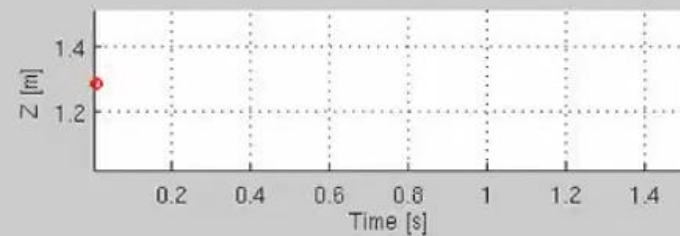
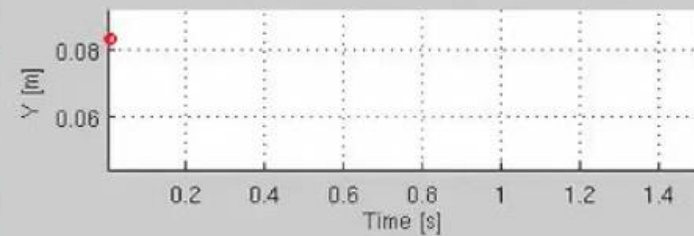
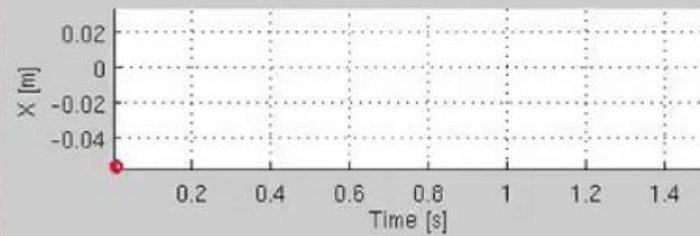
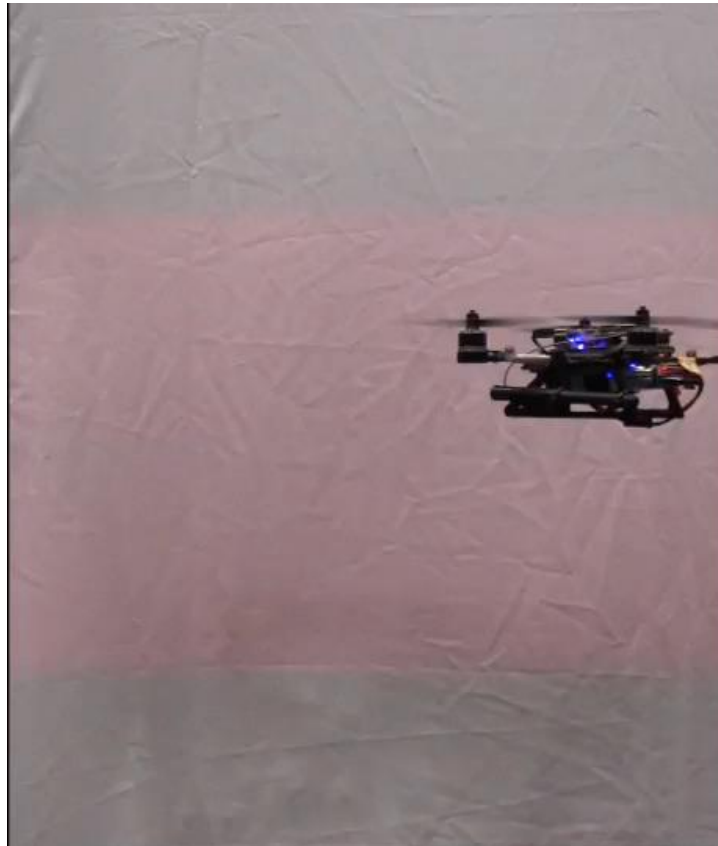
PD Position Controller



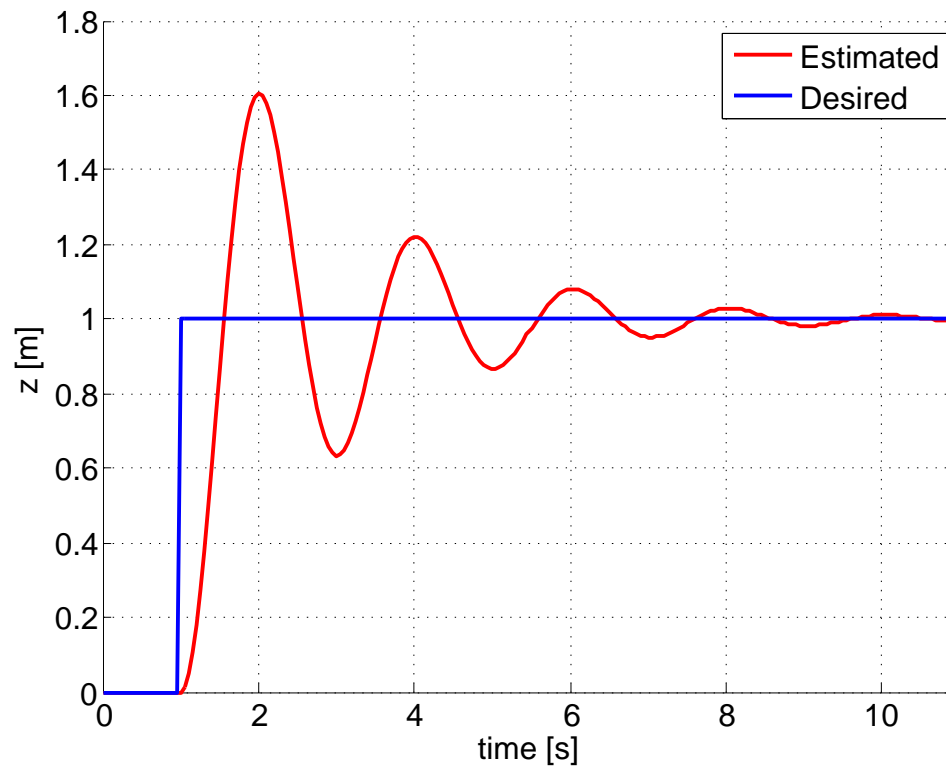
PD Controller for Z



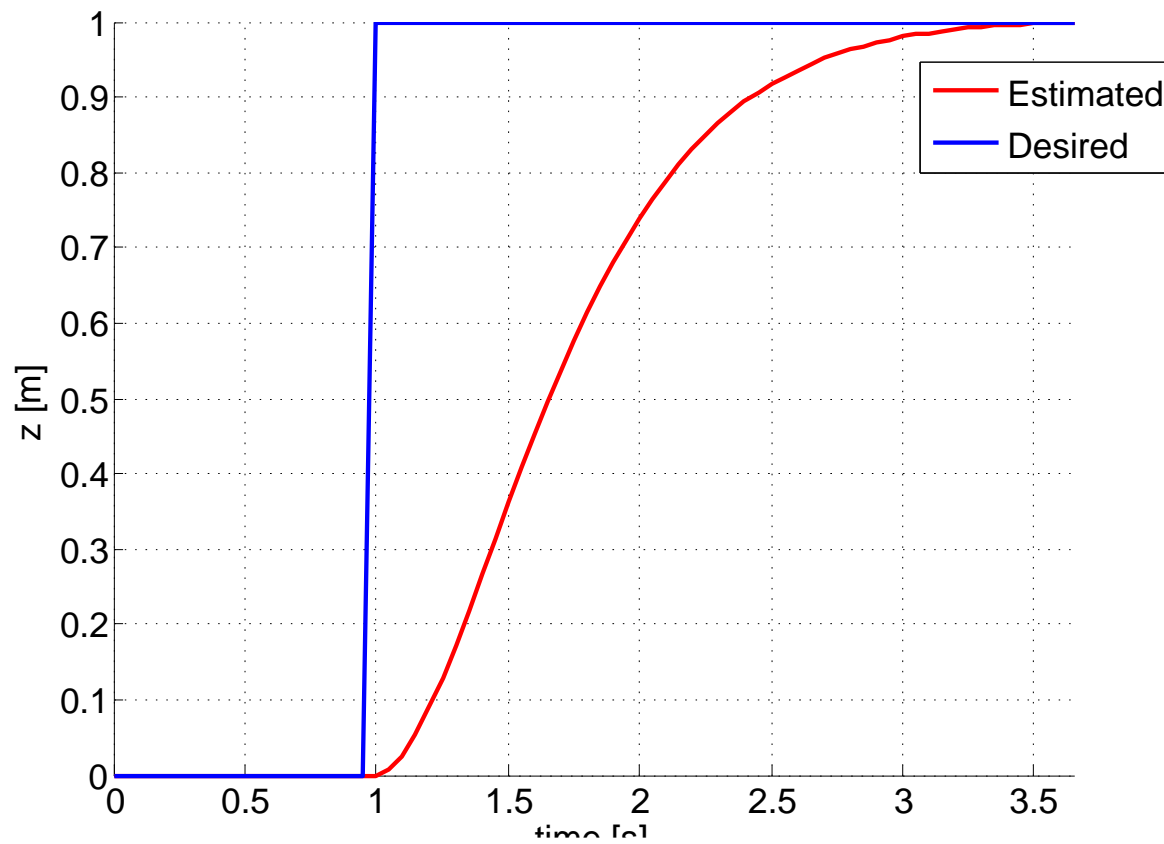
High K_p



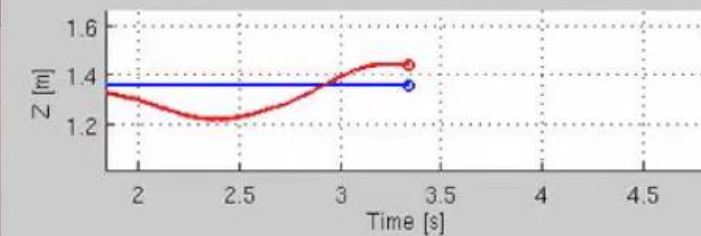
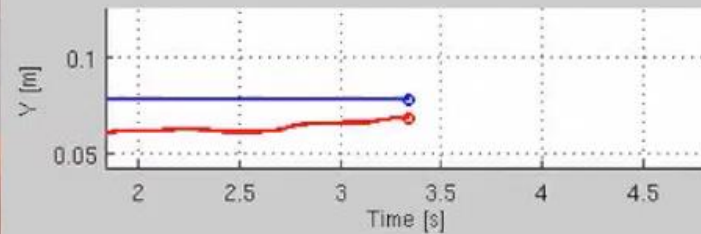
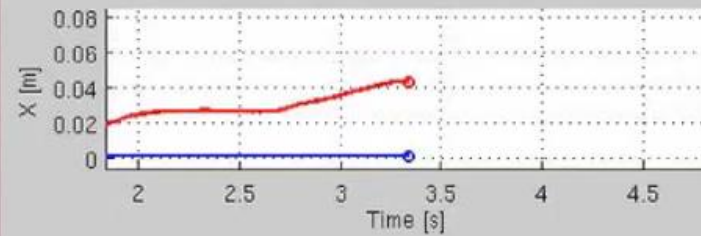
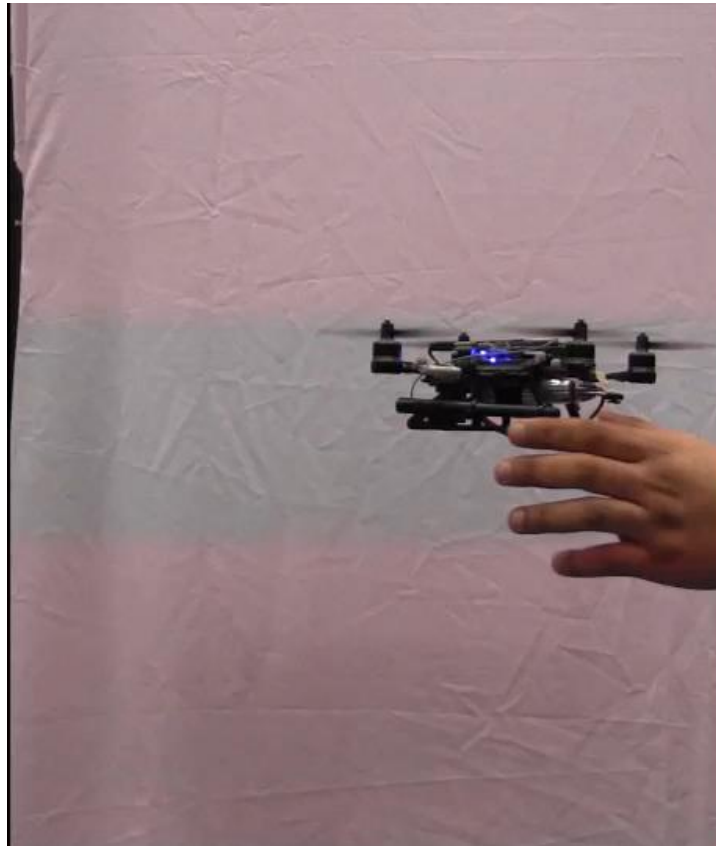
High K_p



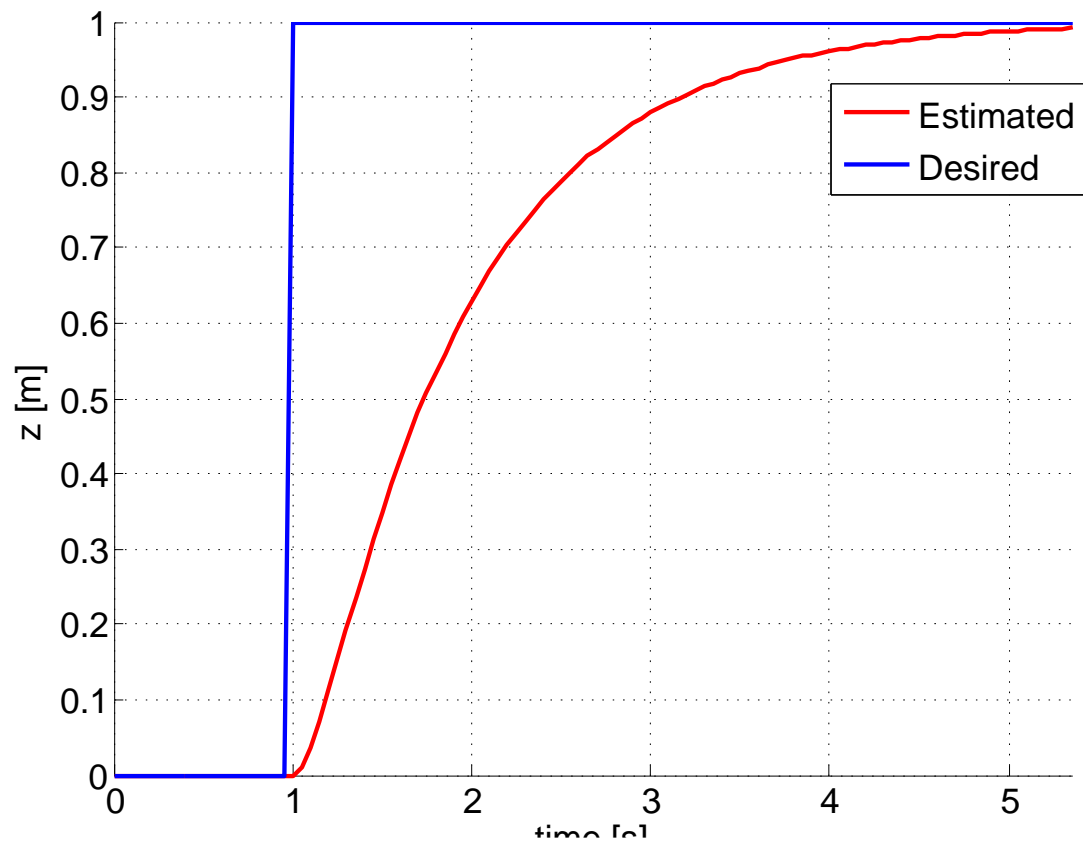
Low K_p



High K_d



High K_d



Manual Tuning

Parameter Increased	K_p	K_d	K_I
Rise Time	Decrease	-	Decrease
Overshoot	Increase	Decrease	Increase
Settling Time	-	Decrease	Increase
Steady-State Error	Decrease	-	Eliminate

- “If I increase K_p , then
Rise Time will *Decrease*, and
Overshoot will *Increase*, and
Steady-State Error will *Decrease*.”
- These are only general guidelines for “typical systems.”

Ziegler-Nichols Method

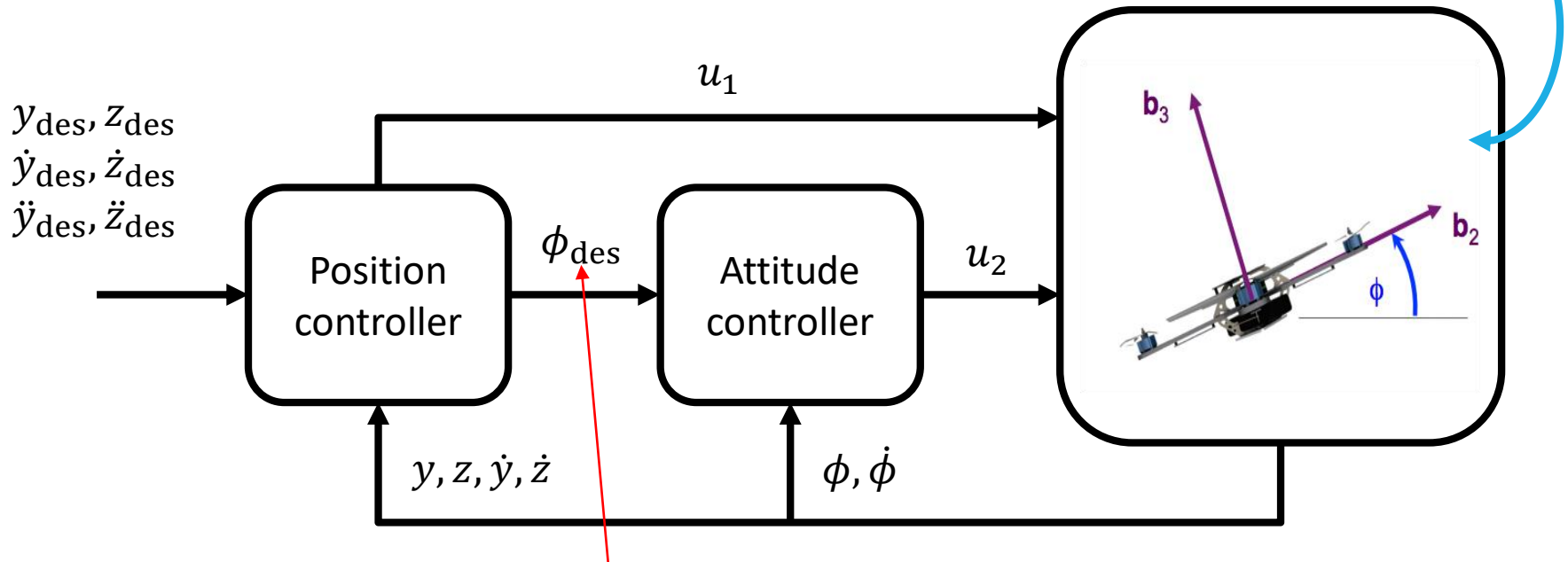
Heuristic method for PID gain tuning

1. Set $K_d = K_I = 0$
2. Increase K_p until ultimate gain K_u where system starts to oscillate
3. Find oscillation period T_u at K_u
4. Set gains according to:

Controller	K_p	K_d	K_I
P	$0.5K_u$	--	--
PD	$0.8K_u$	$K_p T_u / 8$	--
PID	$0.6K_u$	$K_p T_u / 8$	$2K_p / T_u$

Nested Control Structure

$$\begin{aligned}\ddot{y} &= -g\phi \\ \ddot{z} &= -g + \frac{u_1}{m} \\ \ddot{\phi} &= \frac{u_2}{I_{xx}}\end{aligned}$$



Specified by the position controller, **not** the user

Works when inner (attitude) control loop runs much faster (10x) than the outer (position) control loop

Control Equations

Recall for a second order system $\ddot{\mathbf{e}} + K_d \dot{\mathbf{e}} + K_p \mathbf{e} = 0$

For any configuration variable q we have

$$\begin{array}{c} \text{commanded} \\ \downarrow \\ (\ddot{q}_{\text{des}} - \ddot{q}) + K_{d,q}(\dot{q}_{\text{des}} - \dot{q}) + K_{p,q}(q_{\text{des}} - q) = 0 \\ \uparrow \qquad \qquad \qquad \uparrow \qquad \qquad \qquad \uparrow \\ \text{specified} \end{array} \quad \begin{array}{c} \text{actual (feedback)} \\ \downarrow \end{array}$$

Control Equations

Lateral dynamics

- $\dot{y} = -g\phi$
- $\ddot{\phi} = \frac{u_2}{I_{xx}}$

Desired attitude

- $\phi_{\text{des}} = -\frac{\ddot{y}_c}{g}$
- $\dot{\phi}_{\text{des}} = 0$
- $\ddot{\phi}_{\text{des}} = 0$

Attitude controller

- $u_2 = I_{xx}\ddot{\phi}_c$

Vertical dynamics

- $\ddot{z} = -g + \frac{u_1}{m}$

Z-position controller

- $u_1 = m(\ddot{z}_c + g)$

Control Equations

Control equations

$$u_1 = m \left(g + \ddot{z}_{\text{des}} + k_{d,z}(\dot{z}_{\text{des}} - \dot{z}) + k_{p,z}(z_{\text{des}} - z) \right)$$

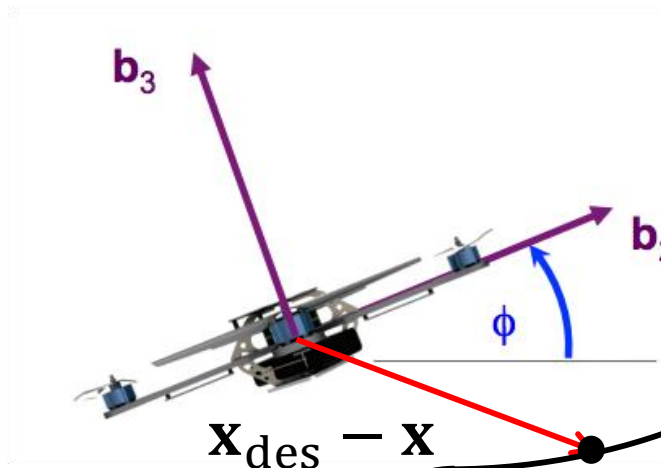
$$u_2 = I_{xx} \left(\ddot{\phi}_{\text{des}} + k_{d,\phi}(\dot{\phi}_{\text{des}} - \dot{\phi}) + k_{p,\phi}(\phi_{\text{des}} - \phi) \right)$$

$$\phi_{\text{des}} = -\frac{1}{g} \left(\ddot{y}_{\text{des}} + k_{d,y}(\dot{y}_{\text{des}} - \dot{y}) + k_{p,y}(y_{\text{des}} - y) \right)$$

- Three sets of PD gains.
- Systematically tune using step responses.
 - Thrust
 - Roll
 - Position (depends on roll being well-tuned)

Trajectory Tracking (in time)

Follow trajectory exactly



$\mathbf{x}_{\text{des}}(t)$

desired trajectory (position, velocity, acceleration)

$$\mathbf{e}_p = \mathbf{x}_{\text{des}} - \mathbf{x}$$

$$\mathbf{e}_d = \dot{\mathbf{x}}_{\text{des}} - \dot{\mathbf{x}}$$

$$(\ddot{\mathbf{x}}_{\text{des}} - \ddot{\mathbf{x}}_c) + k_d \mathbf{e}_d + k_p \mathbf{e}_p = \mathbf{0}$$

Project

Make plots in your sandbox!

Run tests locally.

Gain tuning: Finding 12 magic numbers by trial and error won't work.

How to judge controller quality.

Order of tuning the cascaded controller.

Choose reasonable trajectories.

Practical constraints: actuator limits.