

Rotation matrix

$$\begin{aligned} \underline{P} &= x\underline{i} + y\underline{j} + z\underline{k} \Rightarrow P_{xyz} \\ &= u\underline{i}' + v\underline{j}' + w\underline{k}' \Rightarrow P_{uvw} \end{aligned}$$

$$P_{xyz} = \underbrace{R}_{\substack{\text{*} \\ \text{coordinates}}} P_{uvw} \rightarrow \underline{\text{Rotation matrix (DCM method)}}$$

Properties

① $R^T = R^+$

$$\underbrace{R^i}_{\substack{\text{coordinates}}} = \underbrace{C_m^i}_{\substack{\downarrow \\ \text{coordinates}}} \underbrace{R^m}_{\substack{\text{coordinates}}}$$

② $R^T R = I$

③ $\det|R| = 1$

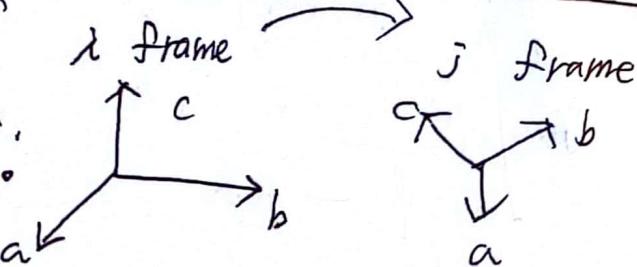
from m to i matrix
 { transformation matrix (almost 4×4)
 { rotation matrix (almost 3×3)

* Use DCM for robotics in this note

DCM: Direction Cosine Matrix

DCM is used for "frame change".

* Generally 'rotation matrix'
 is used as "value change":
 $(x, y) \rightarrow (x', y')$



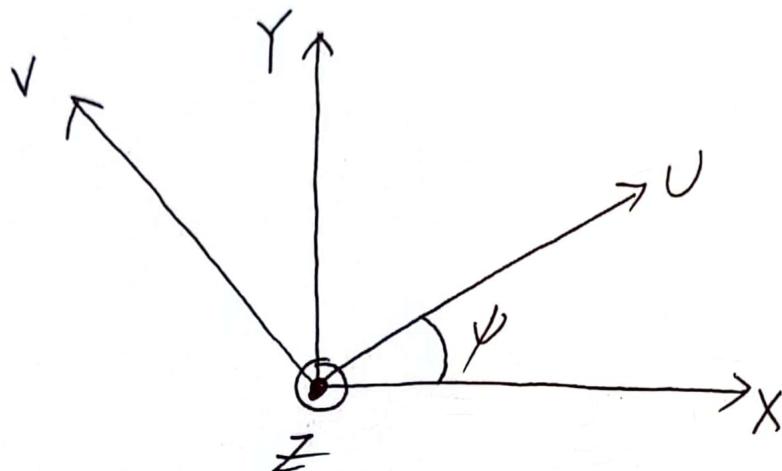
Remember!!

DCM

(Direction Cosine Matrix)

Rotation matrix

"frame change"



"value change"

$$R_z = R(0, 0, \psi) = \begin{bmatrix} i_x \cdot i_u & i_x \cdot j_v & i_x \cdot k_w \\ i_y \cdot i_u & i_y \cdot j_v & i_y \cdot k_w \\ i_z \cdot i_u & i_z \cdot j_v & i_z \cdot k_w \end{bmatrix}$$
$$= \begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Similarly R_y, R_z could be found.

Z-axis $R_z = R(\psi)$

$$\begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Y-axis $R_y = R(\theta)$

$$\begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix}$$

X-axis $R_x = R(\phi)$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \phi & -\sin \phi \\ 0 & \sin \phi & \cos \phi \end{bmatrix}$$

Remember

Z - rotation

$$\begin{bmatrix} \cos\phi & -\sin\phi & 0 \\ \sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Y - rotation

$$\begin{bmatrix} \cos\theta & 0 & \sin\theta \\ 0 & 1 & 0 \\ -\sin\theta & 0 & \cos\theta \end{bmatrix}$$

Z - rotation

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\psi & -\sin\psi \\ 0 & \sin\psi & \cos\psi \end{bmatrix}$$

Rotation Sequence

$$Z \rightarrow Y \rightarrow X$$

$$R = R_x R_y R_z = R(\phi) R(\theta) R(\psi)$$

$$R^{-1} = R_z R_y R_x = R(\psi) R(-\theta) R(-\phi)$$

Transformation Matrix

Vector
translation matrix

$$T = \begin{bmatrix} R_{3 \times 3} & C_{3 \times 1} \\ O_{1 \times 3} & 1 \end{bmatrix} : 4 \times 4$$

Rotation matrix (DCM) \rightarrow calibration vector

(or Orientation matrix)

0: zero.

C:

upper side front side close side

\nwarrow \uparrow \nearrow

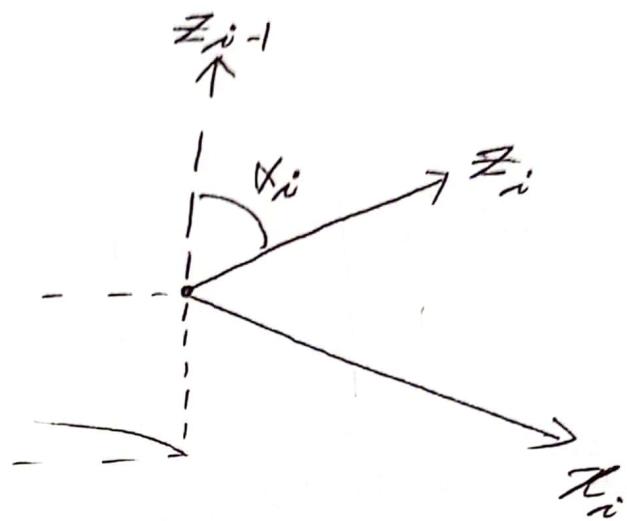
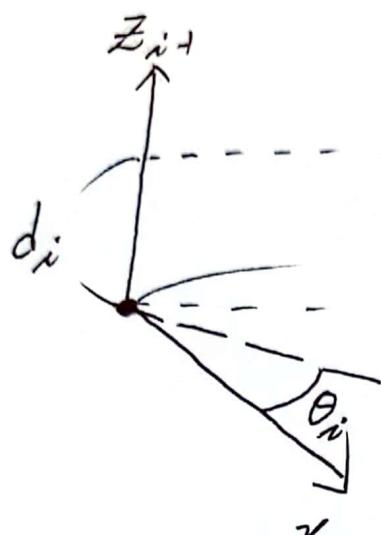
\downarrow \downarrow \downarrow

normal sliding approach

* $T_o^m = \begin{bmatrix} n & s & a & p \\ 0 & 0 & 0 & 1 \end{bmatrix}, R = \begin{bmatrix} n & s & a \\ v & u & w \\ u & v & w \end{bmatrix}$

\curvearrowright TBR..

D-H parameter



$i-1$ 과 i 간
" $i-1$ " 기준 물리적 관계

θ_i : x_{i+1} 과 x_i 간 각도

α_i : z_{i+1} 과 z_i 간 각도

d_i : x_{i-1} 과 x_i 간 " z_{i-1} " 기준 거리를 측정

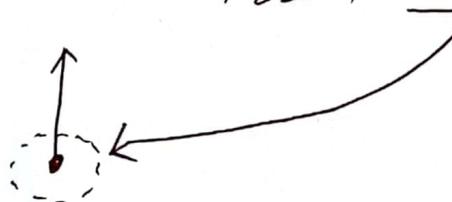
r_i : z_{i+1} 과 z_i 간 " x_i " 기준 거리 차이

* θ_i , α_i 는 모두 각각 두 축이 만드는 평면에서의 각도 관계

$\theta \rightarrow \alpha \rightarrow d \rightarrow r$ 순으로 해석

로봇 설계 및 해석 순서

- ① (x_0, y_0, z_0) 설정 / base 축 정의
- ② 회전축은 모두 " z " 축으로 통일
- ③ Z_{i-1} 과 Z_i 가 가지는 화살표의 시작점을 원점으로 설정



- ④ Z_{i-1} 과 Z_i 가 모두 주어진 선을 X_i 로 지정
※ 추가 설명 들어갈 수 있음

TBR

- ⑤ X_{i-1} 과 X_i 간 각도 θ_i

"화살" 방향
기준

⑥ D-H

- ⑥ Z_{i-1} 과 Z_i 간 각도 α_i

parameters
를 이용한

- ⑦ X_{i-1} 과 X_i 간 거리 $d_i \Rightarrow Z_{i-1}$ 기준

- ⑧ Z_{i-1} 과 Z_i 간 거리 $a_i \Rightarrow X_i$ 기준

D-H table 작성

Joint i	θ_i	X_i	d_i	a_i	???	$\Rightarrow TBR \dots$
i	:	:	:	:	:	
:	:	:	:	:	:	

- ⑩ Transformation Matrix 작성

$$T_0^m = T_0^1 T_1^2 T_2^3 \cdots T_{m-1}^m$$

Robot kinematics

$$DOF = \mathcal{J} (L - A - 1) + \sum_{i=1}^n f_i$$

(Degree Of Freedom)

$$\mathcal{J} = \begin{cases} 6 & (\text{공간 상 움직임}) \\ 3 & (\text{평면 상 움직임}) \end{cases}$$

$$L = \text{링크 수}$$

$$A = \text{조인트 수} (=n)$$

f_i : i 번째 조인트의 자유도

$$\underline{x}_p = F(\underline{q}, l)$$

\underline{x}_p : end-effector position

\underline{q} : joint angle vector

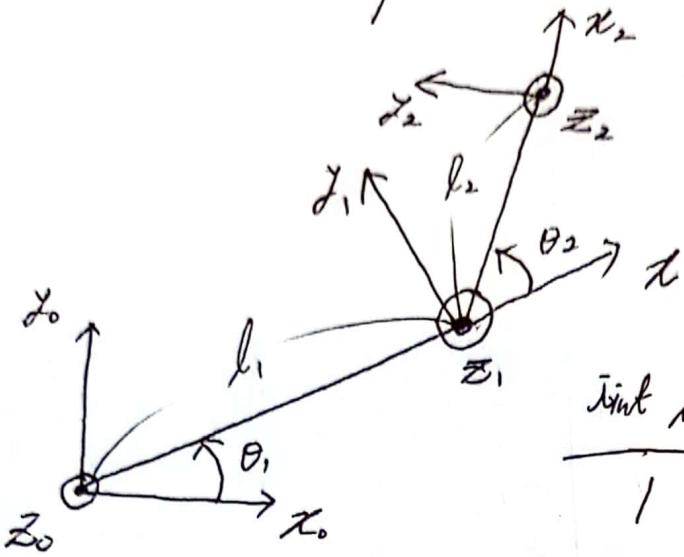
l : link length

$$\ast \underline{p}_o = T_o^n \underline{p}_n$$

\underline{p}_o : base location vector

\underline{p}_n : End Effector location vector

ex) 2 link planar manipulator



D-H parameter table

Joint i	θ_i	x_i	d_i	a_i
1	θ_1	0	0	l_1
2	θ_2	0	0	l_2

$$T_0' = \begin{bmatrix} C_1 & -S_1 & 0 & l_1 C_1 \\ S_1 & C_1 & 0 & l_2 S_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad T_1^2 = \begin{bmatrix} C_2 & -S_2 & 0 & l_2 C_2 \\ S_2 & C_2 & 0 & l_2 S_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_0^2 = T_0' T_1^2 = \begin{bmatrix} C_{12} & -S_{12} & 0 & l_1 C_1 + l_2 C_{12} \\ S_{12} & C_{12} & 0 & l_2 S_1 + l_2 S_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$C_1 = \cos \theta_1$,

$S_1 = \sin \theta_1$,

$C_{12} = \cos(\theta_1 + \theta_2)$

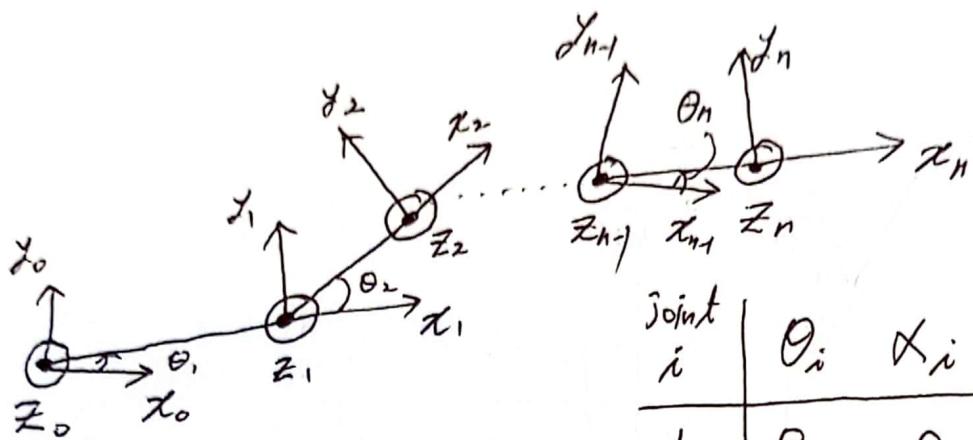
$S_{12} = \sin(\theta_1 + \theta_2)$

End Effector orientation

EE translation

$$T_0^2 = \begin{bmatrix} (R_0^2) & (C_0^2) \\ O_{3 \times 3} & 1 \end{bmatrix}$$

ex) n link planar robot



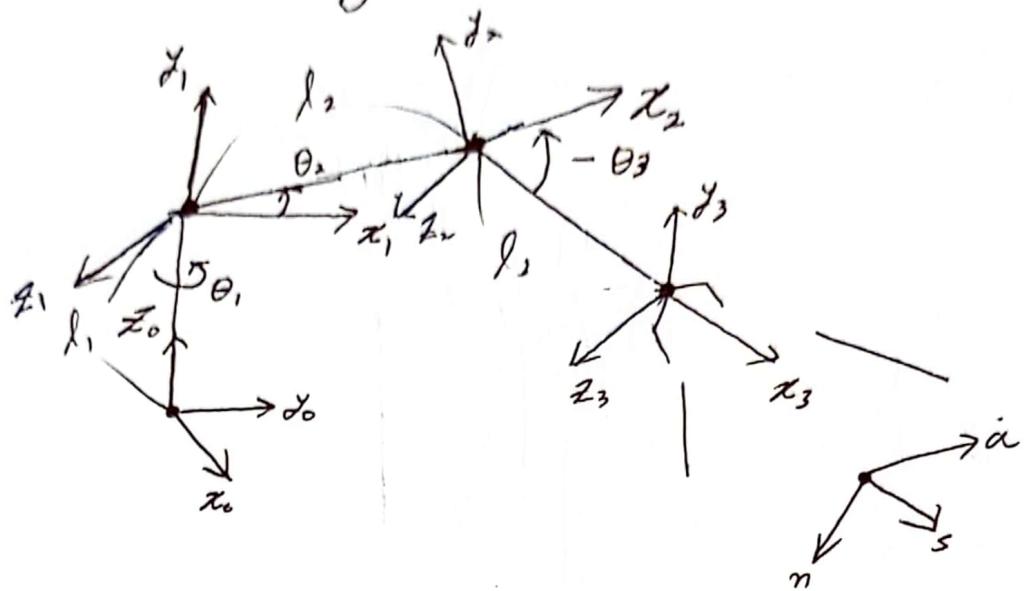
Joint i	θ_i	x_i	d_i	a_i
1	θ_1	0	0	l_1
2	θ_2	0	0	l_2
\vdots	\vdots	\vdots	\vdots	\vdots
n	θ_n	0	0	l_n

$$T_o^n = T_o^1 T_1^2 T_2^3 \dots T_{n-1}^n$$

\rightarrow unofficial terminology
 $\neq 1 \rightarrow i = 12 \dots i$

$$T_o^n = \begin{bmatrix} C_{12\dots n} & -S_{12\dots n} & 0 & \sum_{i=1}^n l_i C_{1 \rightarrow i} \\ S_{12\dots n} & C_{1\dots n} & 0 & \sum_{i=1}^n l_i S_{1 \rightarrow i} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

ex) 3 axis rotary robot \Rightarrow 2/26 4/26 3/26



Joint i	θ_i	X_i	d_i	a_i
1	θ_1	90°	d_1	0
2	θ_2	0	0	d_2
3	$-\theta_3$ $(=\theta'_3)$	0	0	d_3

* Rotation sequence
 $Z \rightarrow Y \rightarrow X$
 $C = C_x C_y C_z$

$$P_f = C P_i = C_x C_y C_z P_i$$

$$R_o' = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos 90^\circ & -\sin 90^\circ \\ 0 & \sin 90^\circ & \cos 90^\circ \end{bmatrix} \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} C_1 & 0 & S_1 \\ S_1 & 0 & -C_1 \\ 0 & 1 & 0 \end{bmatrix}$$

$$T_o' = \begin{bmatrix} R_o' & C_o' \\ 0_{1 \times 3} & 1 \end{bmatrix} = \begin{bmatrix} C_1 & 0 & S_1 & 0 \\ S_1 & 0 & -C_1 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_o^3 = T_o' T_1^2 T_2^3 \quad * \text{ In this note, } -\theta_3 \text{ is represented as } \theta'_3.$$

$$= \begin{bmatrix} C_1(C_2C_3 - S_2S_3) & -C_1(C_2C_3 + S_2S_3) & S_1 & d_2C_2C_3 + d_3C_1(C_2C_3 - S_2S_3) \\ S_1(C_2C_3 - S_2S_3) & -S_1(C_2C_3 + S_2S_3) & -C_1 & d_2S_1C_1 + d_3S_1(C_2C_3 - S_2S_3) \\ C_2S_1 + S_2C_3 & C_2C_3 - S_2S_3 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Jacobian Matrix

$$\boxed{\underline{X}, \dot{\underline{X}}, \ddot{\underline{X}}} \xrightarrow{IK} \boxed{\underline{q}, \dot{\underline{q}}, \ddot{\underline{q}}}$$

$$\underline{X} = \begin{bmatrix} P_x \\ P_y \\ P_z \\ \phi \\ \theta \\ \psi \end{bmatrix}$$

$$\underline{q} = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \\ q_5 \\ q_6 \end{bmatrix}$$

$$\underline{X} = F(\underline{q})$$

→ kinematics

#6-Dof robot

$$\frac{d\underline{X}}{dt} = \frac{\partial F(\underline{q})}{\partial \underline{q}} \frac{\partial \underline{q}}{\partial t} = J \dot{\underline{q}}$$

$$J = \begin{bmatrix} \frac{\partial F_1}{\partial q_1} & \cdots & \frac{\partial F_1}{\partial q_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial F_n}{\partial q_1} & \cdots & \frac{\partial F_n}{\partial q_n} \end{bmatrix}$$

$$\{\dot{\underline{X}} = J \dot{\underline{q}} \quad \dots \quad \textcircled{1}$$

$$\{\ddot{\underline{X}} = \ddot{J} \dot{\underline{q}} + J \ddot{\underline{q}} \quad \dots \quad \textcircled{2}$$

* J^{-1} exists and is non-singular

From ①,

$$J^{-1} \dot{\underline{X}} = J^{-1} J \dot{\underline{q}}$$

$$J^{-1} \dot{\underline{X}} = \dot{\underline{q}}$$

$$\frac{d^2 \underline{X}}{dt^2} = \frac{\partial J(\underline{q})}{\partial \underline{q}} \frac{\partial \underline{q}}{\partial t} + J(\underline{q}) \frac{\partial^2 \underline{q}}{\partial t^2}$$

From ②,

$$J \ddot{\underline{q}} = \ddot{\underline{X}} - \ddot{J} \dot{\underline{q}}$$

$$\ddot{\underline{q}} = J^{-1} (\ddot{\underline{X}} - \ddot{J} \dot{\underline{q}})$$

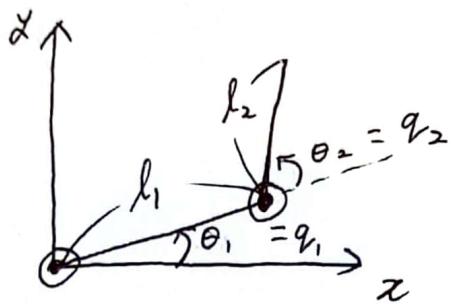
$$\det |J| \neq 0$$

$$* J_{i,j} = \frac{\partial F_i}{\partial q_j}$$

: i location's j angle

$$\left\{ \begin{array}{l} \dot{\underline{q}} = J^{-1} \dot{\underline{x}} \\ \ddot{\underline{q}} = J^{-1} (\ddot{\underline{x}} - J \dot{\underline{q}}) \end{array} \right.$$

ex) 2 link planar robot



$$\begin{bmatrix} p_x \\ p_z \end{bmatrix} = \begin{bmatrix} l_1 c_1 + l_2 c_{12} \\ l_1 s_1 + l_2 s_{12} \end{bmatrix} = \underline{x}$$

$$\begin{aligned} \dot{\underline{x}} &= J \dot{\underline{q}} = \begin{bmatrix} \frac{\partial p_x}{\partial q_1} & \frac{\partial p_x}{\partial q_2} \\ \frac{\partial p_z}{\partial q_1} & \frac{\partial p_z}{\partial q_2} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} \\ &= \begin{bmatrix} -l_1 s_1 - l_2 s_{12} & -l_2 s_{12} \\ +l_1 c_1 + l_2 c_{12} & l_2 c_{12} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} \\ &= \underline{J} \end{aligned}$$

$$|J| = l_1 l_2 s_2$$

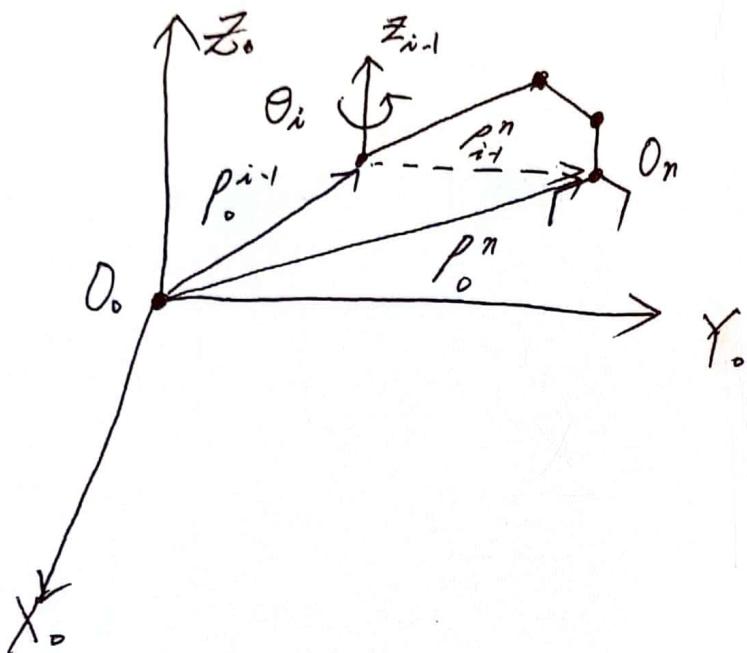
We have to avoid this angle kinematically!!



$q_2 = 0 \text{ or } \pi \Rightarrow \text{Singularity!!!}$

General Jacobian

$$T_o^n = \begin{bmatrix} R_o^n & P_o^n \\ 0_{1 \times 3} & 1 \end{bmatrix}$$



$$\dot{\underline{X}} = J \dot{\underline{q}}$$

$$\underline{P}_o^n = \underline{P}_o^{n-1} + R_o^{n-1} \underline{P}_{n-1}^n$$

$$\underline{V}_o^n = \underline{V}_o^{n-1} + R_o^{n-1} \underline{V}_{n-1}^n$$

$$\underline{W}_o^n = \underline{W}_o^{n-1} + R_o^{n-1} \underline{W}_{n-1}^n$$

$$\underline{X} = \begin{bmatrix} P_x \\ P_y \\ P_z \\ \phi \\ \theta \\ \psi \end{bmatrix}$$

$$\underline{q} = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \\ q_5 \\ q_6 \end{bmatrix}$$

$$\begin{aligned} \dot{\underline{X}} &= \begin{bmatrix} \dot{P}_x \\ \dot{P}_y \\ \dot{P}_z \\ \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} \underline{V}_o^n \\ \underline{W}_o^n \end{bmatrix} = \begin{bmatrix} J_v \\ J_w \end{bmatrix} \dot{\underline{q}} \\ &= J_o^n \underline{q} \end{aligned}$$

Def. of link's angular velocity (revolute joint)

$$\underline{\omega}_{i-1}^i = \dot{q}_i \underline{k} \quad \underline{k} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\underline{\omega}_0^n = \underline{\omega}_0' + \sum_{i=1}^{n-1} R_0^i \underline{\omega}_i^{i+1}$$

$$= \dot{q}_1 \underline{k} + R_0^1 \dot{q}_2 \underline{k} + \dots + R_0^{n-1} \dot{q}_n \underline{k}$$

$$= \dot{q}_1 \underline{z}_0 + \dot{q}_2 \underline{z}_1 + \dots + \dot{q}_n \underline{z}_{n-1}$$

$$= \sum_{i=1}^n \dot{q}_i \underline{z}_{i-1} \quad (\underline{z}_{i-1} = R_0^{i-1} \underline{k})$$

$$\therefore J_\omega = \left[\frac{\partial \underline{\omega}_0^n}{\partial q_1} \quad \frac{\partial \underline{\omega}_0^n}{\partial q_2} \quad \dots \quad \frac{\partial \underline{\omega}_0^n}{\partial q_n} \right]$$

$$= [\underline{z}_0 \ \underline{z}_1 \ \dots \ \underline{z}_{n-1}]$$

$$J_\omega = [\underline{z}_0 \ \underline{z}_1 \ \underline{z}_2 \ \dots \ \underline{z}_{n-1}]$$

Def of link's velocity

$$\dot{\underline{P}}_o^n = \frac{\partial \underline{P}_o^n}{\partial q_1} \dot{q}_1 + \frac{\partial \underline{P}_o^n}{\partial q_2} \dot{q}_2 + \dots + \frac{\partial \underline{P}_o^n}{\partial q_n} \dot{q}_n$$

$$= \sum_{i=1}^n \frac{\partial \underline{P}_o^n}{\partial q_i} \dot{q}_i$$

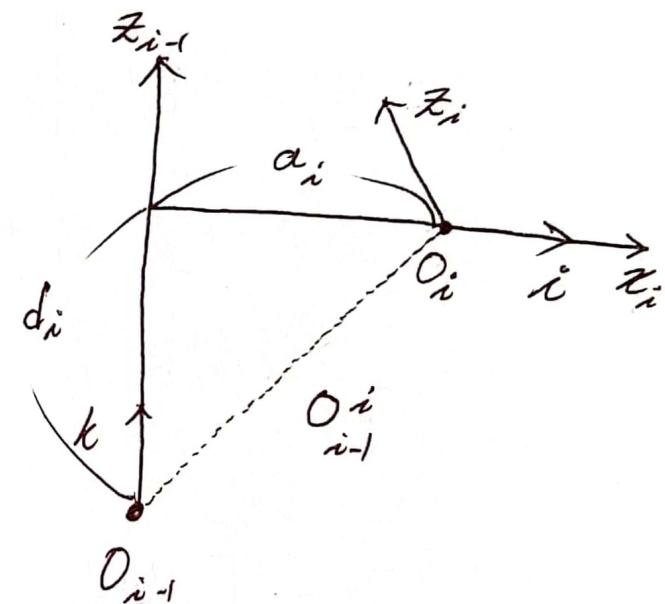
* i joint : sliding joint

$$\underline{d}_{i-1}^i = d_i \underline{k} + R_{i-1}^{i-1} \alpha_i \underline{i}$$

$$\dot{\underline{d}}_{i-1}^i = \dot{d}_i \underline{k}$$

(Assume i joint only move)

$$\underline{P}_o^n = \underline{P}_o^{n-1} + R_o^{n-1} \underline{P}_{i-1}^n$$



$$\dot{\underline{P}}_o^n = R_o^{n-1} \dot{\underline{P}}_{i-1}^i$$

$$\dot{\underline{P}}_o^n = R_o^{n-1} \dot{d}_i \underline{k} = \dot{d}_i \underline{z}_{i-1}$$

$$\therefore \frac{\partial \underline{P}_o^n}{\partial q_i} = \frac{\partial \underline{P}_o^n}{\partial d_i} = \underline{z}_{i-1}$$

$$(d_i = \frac{d_{i-1}}{d_{i-1}} = 1)$$

$$\frac{\partial \underline{P}_o^n}{\partial q_i} = \underline{z}_{i-1}$$

i joint : revolute joint

$$\underline{\Omega}_n - \underline{\Omega}_{i-1} = \underline{R}_o^{i-1} \underline{P}_{i-1}^n$$

$$\begin{cases} \dot{\underline{P}}_o^n = \underline{R}_o^{i-1} \dot{\underline{P}}_{i-1}^n \\ \dot{\underline{P}}_{i-1}^n = \dot{q}_i \underline{k} \times \underline{P}_{i-1}^n \end{cases} \quad \# \underline{\nu} = \underline{\omega} \times \underline{r}$$



$$\dot{\underline{P}}_o^n = \underline{R}_o^{i-1} (\dot{q}_i \underline{k} \times \underline{P}_{i-1}^n)$$

$$= \dot{q}_i \underline{z}_{i-1} \times (\underline{\Omega}_n - \underline{\Omega}_{i-1}) \quad \# \dot{q}_i = \frac{\partial q_i}{\partial q_i} = 1$$

$$\boxed{\frac{\partial \underline{P}_o^n}{\partial q_i} = \underline{z}_{i-1} \times (\underline{\Omega}_n - \underline{\Omega}_{i-1})}$$

$$\therefore J_V = \left[\frac{\partial \underline{P}_o^n}{\partial q_1} \quad \frac{\partial \underline{P}_o^n}{\partial q_2} \quad \cdots \quad \frac{\partial \underline{P}_o^n}{\partial q_n} \right]$$

$$= \left[\underline{z}_0 \times (\underline{\Omega}_n - \underline{\Omega}_0) \quad \underline{z}_1 \times (\underline{\Omega}_n - \underline{\Omega}_1) \quad \cdots \quad \underline{z}_{n-1} \times (\underline{\Omega}_n - \underline{\Omega}_{n-1}) \right]$$

$$\boxed{J_V = \left[\underline{z}_0 \times (\underline{\Omega}_n - \underline{\Omega}_0) \quad \underline{z}_1 \times (\underline{\Omega}_n - \underline{\Omega}_1) \quad \cdots \quad \underline{z}_{n-1} \times (\underline{\Omega}_n - \underline{\Omega}_{n-1}) \right]}$$

$$J = \begin{bmatrix} J_v \\ J_w \end{bmatrix} = \begin{bmatrix} \underline{J}_1 & \underline{J}_2 & \dots & \underline{J}_n \end{bmatrix}$$

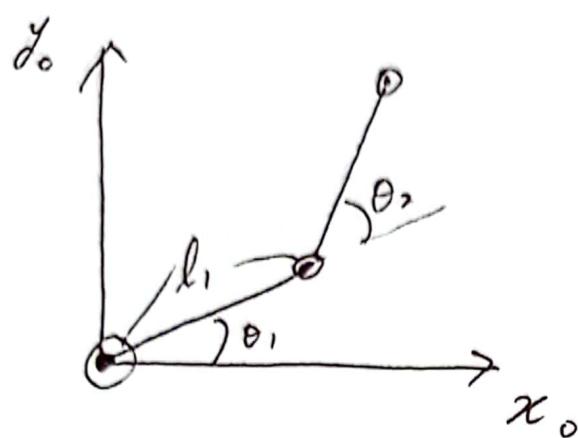
i) revolute joints Jacobian

$$\underline{J}_i = \begin{bmatrix} \underline{z}_{i-1} \times (\underline{o}_n - \underline{o}_{i-1}) \\ \underline{z}_{i-1} \end{bmatrix}$$

ii) sliding joints Jacobian

$$\underline{J}_i = \begin{bmatrix} \underline{z}_{i-1} \\ 0 \end{bmatrix}$$

Ex) 2 link planar robot



$$T_1^{-1} = \begin{bmatrix} C_{11} & -S_{12} & 0 & l_1 C_1 + l_2 C_{12} \\ S_{12} & C_{11} & 0 & l_1 S_1 + l_2 S_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\dot{\underline{x}} = \underline{J} \dot{\underline{q}}$$

$$\underline{J} = \begin{bmatrix} \underline{J}_1 & \underline{J}_2 \end{bmatrix}$$

$$= \begin{bmatrix} \underline{z}_0 \times (\underline{\Omega}_2 - \underline{\Omega}_0) & \underline{z}_1 \times (\underline{\Omega}_2 - \underline{\Omega}) \\ \underline{z}_0 & \underline{z}_1 \end{bmatrix}$$

$$\underline{z}_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \underline{z}_1 = R'_0 \underline{z}_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$\underline{\Omega}_2 = \begin{bmatrix} l_1 C_1 + l_2 C_{12} \\ l_1 S_1 + l_2 S_{12} \\ 0 \end{bmatrix} \quad \underline{\Omega}_1 = \begin{bmatrix} l_1 C_1 \\ l_2 S_1 \\ 0 \end{bmatrix} \quad \underline{\Omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\underline{J} = \begin{bmatrix} -l_1 S_1 - l_2 S_{12} & -l_2 S_{12} \\ l_1 C_1 + l_2 C_{12} & l_2 C_{12} \\ 0 & 0 \\ 0 & 0 \\ 1 & 0 \end{bmatrix}$$

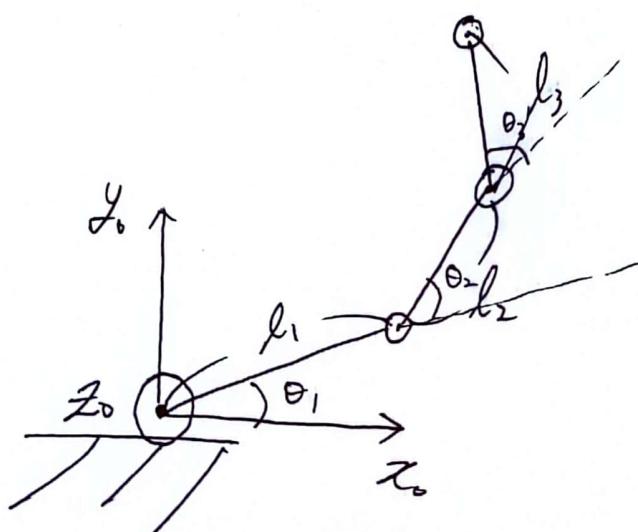
Inverse Kinematics

\Rightarrow To find desired angle!!

Ex) 3 link planar robot

$$T_0^3 = \begin{bmatrix} C_{123} & -S_{123} & 0 & l_1C_1 + l_2C_{12} + l_3C_{123} \\ S_{123} & C_{123} & 0 & l_1S_1 + l_2S_{12} + l_3S_{123} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix} = \begin{bmatrix} l_1C_1 + l_2C_{12} + l_3C_{123} \\ l_1S_1 + l_2S_{12} + l_3S_{123} \\ 0 \end{bmatrix}$$



$$\phi = \theta_1 + \theta_2 + \theta_3 \quad (\# \text{almost } \phi \text{ is const.})$$

(defined)

$$P'_x = P_x - l_3 C_{123} = P_x - l_3 C_\phi = l_1 C_1 + l_2 C_{12} \quad \}$$

$$P'_y = P_y - l_3 S_{123} = P_y - l_3 S_\phi = l_1 S_1 + l_2 S_{12} \quad \}$$

$$P'^2_x + P'^2_y = l_1^2 + l_2^2 + 2l_1 l_2 C_{12}$$

III

$$C_2 = \frac{P'^2_x + P'^2_y - l_1^2 - l_2^2}{2l_1 l_2}$$

$$\therefore \theta_2 = \tan^{-1} \left(\frac{S_2}{C_2} \right)$$

From I,

$$P'_x = (l_1 + l_2 C_2) C_1 - l_2 S_2 S_1$$

$$P'_y = (l_1 + l_2 C_2) S_1 + l_2 S_2 C_1$$

$$\begin{bmatrix} -l_2 S_2 & l_1 + l_2 C_2 \\ l_1 + l_2 C_2 & l_2 S_2 \end{bmatrix} \begin{bmatrix} S_1 \\ C_1 \end{bmatrix} = \begin{bmatrix} P'_x \\ P'_y \end{bmatrix}$$

$\underbrace{\quad}_{=A}$

$$\det A = -P'^2_x - P'^2_y$$

$$\therefore \begin{bmatrix} S_1 \\ C_1 \end{bmatrix} = \frac{1}{-(P_x^{2'} + P_y^{2'})} \begin{bmatrix} l_2 s_2 & -l_1 + l_2 c_2 \\ l_1 + l_2 c_2 & -l_2 s_2 \end{bmatrix} \begin{bmatrix} P_x' \\ P_y' \end{bmatrix}$$

$$\left\{ \begin{array}{l} C_1 = \frac{(l_1 + l_2 c_2) P_x' + l_2 s_2 P_y'}{P_x'^2 + P_y'^2} \\ S_1 = \frac{(l_1 + l_2 c_2) P_y' - l_2 s_2 P_x'}{P_x'^2 + P_y'^2} \end{array} \right. \quad \therefore \theta_1 = \tan^{-1} \left(\frac{S_1}{C_1} \right).$$

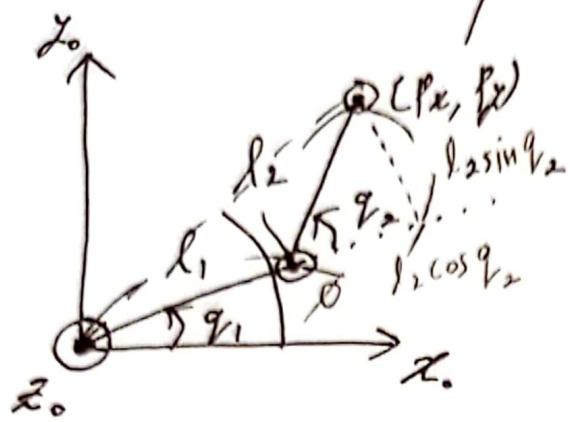
$$\left\{ \begin{array}{l} \phi = \theta_1 + \theta_2 + \theta_3 \\ C_1 = \frac{(l_1 + l_2 c_2) P_x' + l_2 s_2 P_y'}{P_x'^2 + P_y'^2} \\ S_1 = \frac{(l_1 + l_2 c_2) P_y' - l_2 s_2 P_x'}{P_x'^2 + P_y'^2} \end{array} \right.$$

$$\theta_2 = \tan^{-1} \left(\frac{S_2}{C_2} \right) \quad C_2 = \frac{P_x'^2 + P_y'^2 - l_1^2 - l_2^2}{2 l_1 l_2}$$

$$S_2 = \pm \sqrt{1 - C_2^2}$$

$$\theta_3 = \phi - \theta_1 - \theta_2$$

Ex) 2 link planar robot circle trajectory



$$T_0^2 = \begin{bmatrix} C_{12} & -S_{12} & 0 & l_1 C_1 + l_2 C_{12} \\ S_{12} & C_{12} & 0 & l_1 S_1 + l_2 S_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\rho = \begin{bmatrix} l_1 C_1 + l_2 C_{12} \\ l_1 S_1 + l_2 S_{12} \\ 0 \end{bmatrix} = \begin{bmatrix} p_x \\ p_y \\ p_z \end{bmatrix}$$

$$p_x^2 + p_y^2 = l_1^2 + l_2^2 + 2l_1 l_2 C_2$$

$$C_2 = \frac{p_x^2 + p_y^2 - l_1^2 - l_2^2}{2l_1 l_2}$$

$$S_2 = \pm \sqrt{1 - C_2^2}$$

$$\begin{cases} \phi = q_1 + q_2 \\ \phi = \tan^{-1}\left(\frac{p_x}{p_y}\right) \\ r = \sqrt{p_x^2 + p_y^2} \end{cases}$$

$$\therefore \begin{cases} C_2 = \frac{r^2 - l_1^2 - l_2^2}{2l_1 l_2} \\ S_2 = \pm \sqrt{1 - C_2^2} \end{cases}$$

$$q_2 = \tan^{-1}\left(\frac{s_2}{c_2}\right)$$

$$q_1 = \phi - q_2$$

$$= \tan^{-1}\left(\frac{p_x}{p_y}\right) - \tan^{-1}\left(\frac{l_2 s_2}{l_1 + l_2 c_2}\right)$$

$$\tan^{-1}\left(\frac{s_2}{c_2}\right)$$

$$\therefore \begin{cases} \underline{q} = \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} = \begin{bmatrix} \tan^{-1}\left(\frac{p_x}{p_y}\right) - \tan^{-1}\left(\frac{l_2 s_2}{l_1 + l_2 c_2}\right) \\ \tan^{-1}\left(\frac{s_2}{c_2}\right) \end{bmatrix} \end{cases}$$