

Additional structures:

④ Cascade structures

$$H(z) = H_1(z) \cdot H_2(z)$$

$$-\boxed{H(z)} \iff -\boxed{H_1(z)} - \boxed{H_2(z)}$$

④ Parallel structures

$$H(z) = H_1(z) + H_2(z)$$

partial fraction expansion

$$-\boxed{H(z)} \iff \boxed{-\frac{H_1(z)}{H_2(z)}} +$$

Ex of cascade structure:

$$H(z) = \frac{b_0 + \dots + b_4 z^{-4}}{1 + \dots + a_4 z^{-4}}$$

where a_i, b_i are real

$$= b_0 \frac{\prod_{i=1}^4 (1 - z_i z^{-1})}{\prod_{i=1}^4 (1 - p_i z^{-1})}$$

complex zeros/poles come in conjugate pairs

$$= b_0 \frac{(1 - z_1 z^{-1})(1 - z_2 z^{-1})}{(1 - p_1 z^{-1})(1 - p_2 z^{-1})} \cdot \frac{(1 - z_3 z^{-1})(1 - z_4 z^{-1})}{(1 - p_3 z^{-1})(1 - p_4 z^{-1})}$$

complex conjugates

we pair complex conjugates

$$= b_0 \cdot \underbrace{\frac{B_1(z)}{A_1(z)} \cdot \frac{B_2(z)}{A_2(z)}}_{\text{all coefficients are real}}$$

$$H(z) = \frac{10 + z^{-1} + 0.9z^{-2} + 0.8z^{-3} - 5.8z^{-4}}{1 - 2.54z^{-1} + 3.24z^{-2} - 2.06z^{-3} + 0.66z^{-4}} = H_1(z) \cdot H_2(z)$$

with real
coefficients

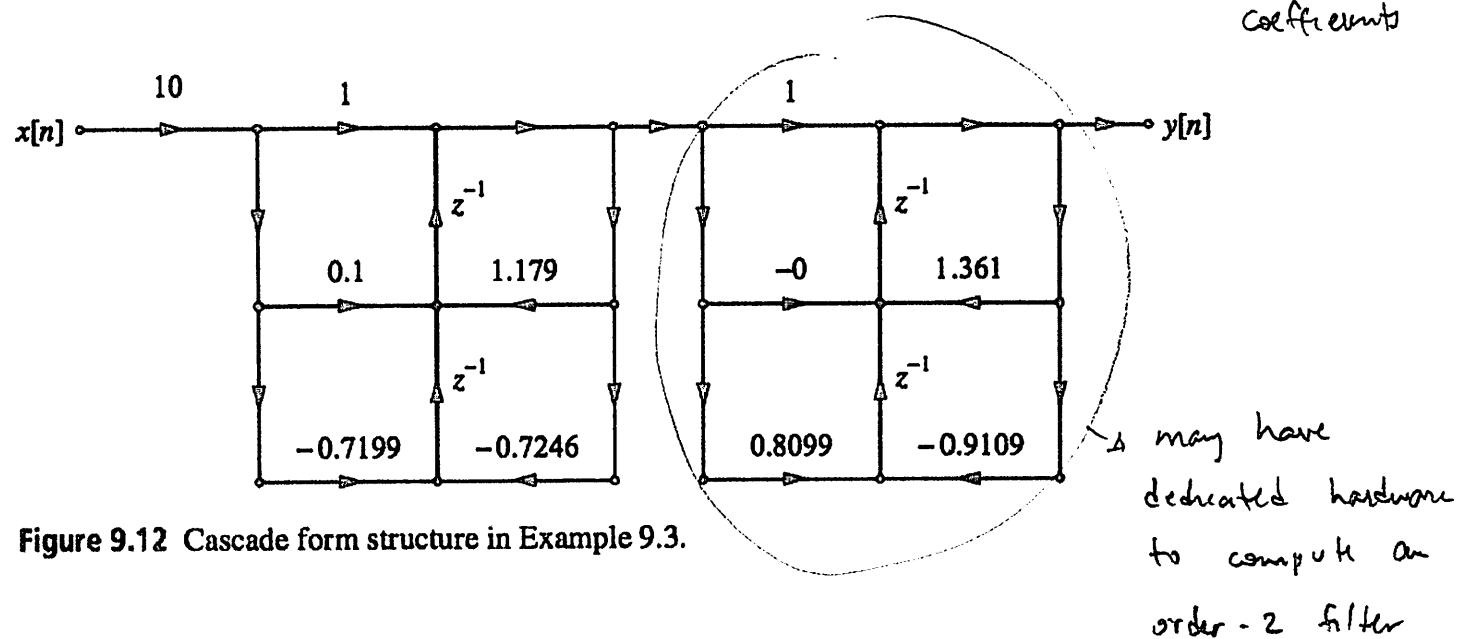


Figure 9.12 Cascade form structure in Example 9.3.

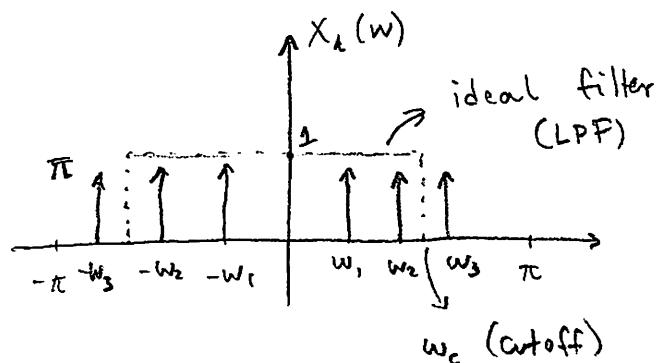
Lecture 20 : From ideal to practical filters (Generalized Linear Phase)

$$\{x[n]\} \rightarrow \boxed{h} \rightarrow \{y[n]\}$$

Typical application : Filter out frequencies in stop band and let the frequencies in the pass band pass unaltered

$$\text{Ex. } x[n] = \cos(\omega_1 n) + \cos(\omega_2 n) + \cos(\omega_3 n), \quad \omega_1 < \omega_2 < \omega_3$$

Suppose I want to remove $\cos(\omega_3 n)$ (it's noise)

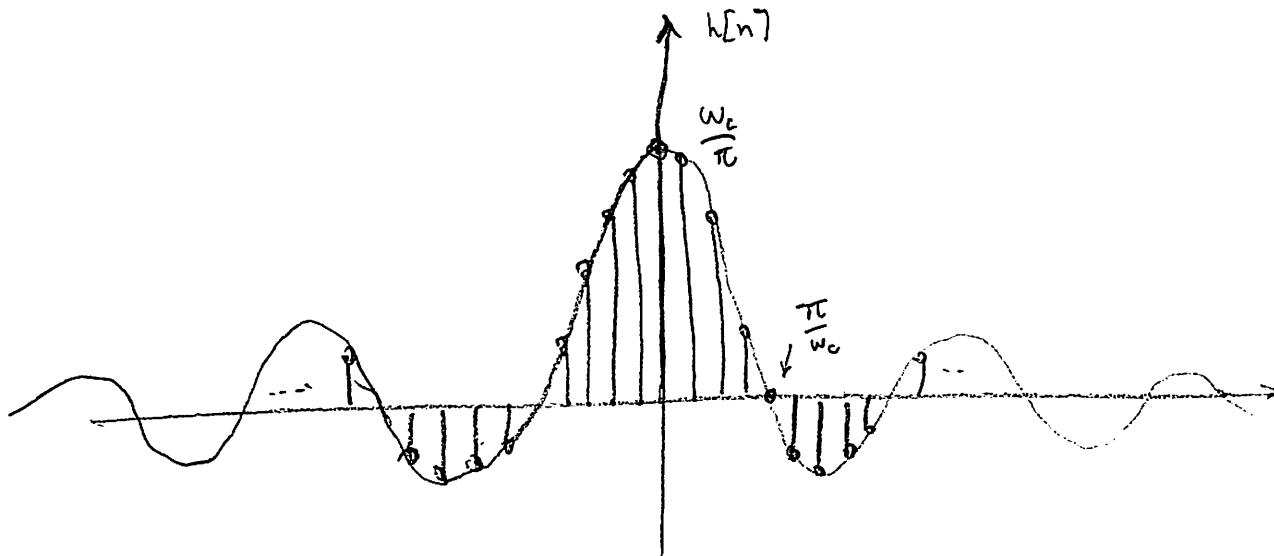


$$H_d(w) = \begin{cases} 1 & |w| < w_c \\ 0 & \text{otherwise} \end{cases}$$

$$\angle H_d(w) = 0 \quad \text{for all } w$$

Impulse response of ideal LPF :

$$h[n] = DTFT^{-1} \{ H_a(\omega) \} = \frac{\sin(\omega_0 n)}{\pi n}$$



Issues :

- Extends to $\pm \infty$ \Rightarrow impractical
- It's non-causal .

Possible solution : shift and truncate

What happens when we shift $\cdot h[n]$? Output is delayed.

Let us relax the requirement and accept delayed outputs:

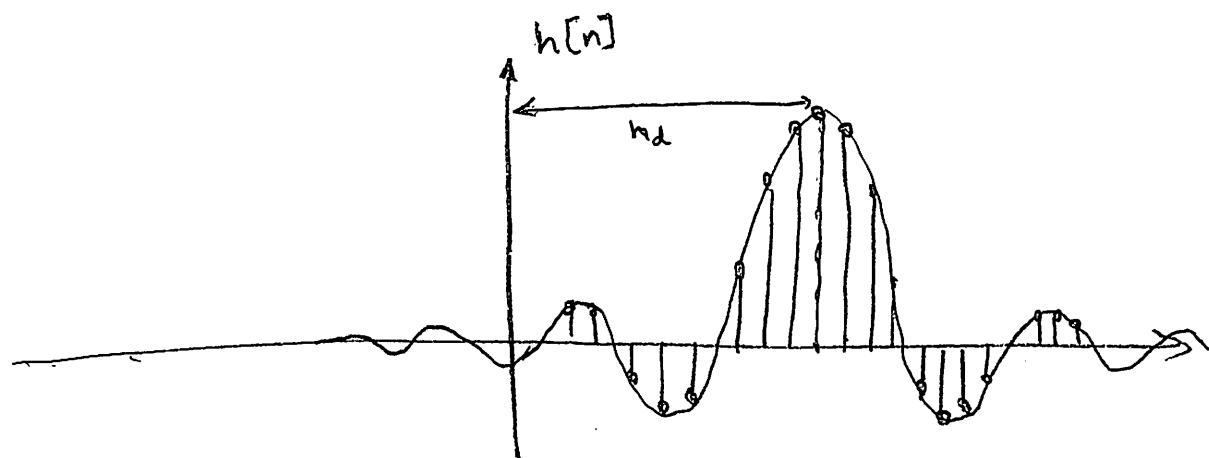
$$x[n] = \cos(\omega_1 n) + \cos(\omega_2 n) + \cos(\omega_3 n) \xrightarrow[\text{"noise"}]{\text{real}} h \rightarrow y[n] = \cos(\omega_1(n-n_d)) + \cos(\omega_2(n-n_d)) \\ = \cos(\omega_1 n - \omega_1 n_d) + \cos(\omega_2 n - \omega_2 n_d)$$

$$\angle H_d(\omega_1) = -\omega_1 n_d$$

$$\angle H_d(\omega_2) = -\omega_2 n_d$$

In general, $\boxed{\angle H_d(\omega) = -\omega n_d}$ linear phase (LP)

$$\Rightarrow H_d(\omega) = \begin{cases} 1 \cdot e^{-j\omega n_d} & |\omega| < \omega_0 \\ 0 & \text{otherwise} \end{cases}$$



In general, linear phase is desirable (for most filters)

Linear Phase

$$H_d(\omega) = \underbrace{|H_d(\omega)|}_{\geq 0} e^{j(-\alpha\omega)}$$

However, LP is hard to impose in filter design.

A weaker requirement :

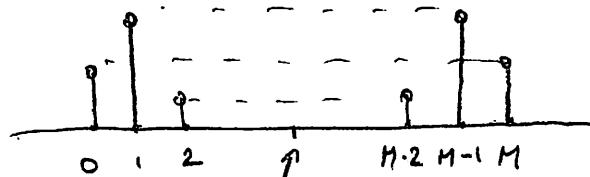
Generalized linear phase : $H_d(\omega) = \underbrace{A(\omega)}_{\text{real}} e^{j(\alpha\omega + \beta)}$ α, β are constants

For FIR filters, GLP is attained if $\{h[n]\}_{n=0}^M$ is

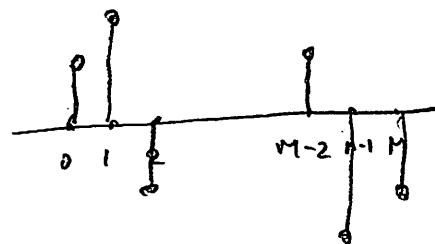
$\begin{cases} \text{symmetric, or} \\ \text{anti-symmetric} \end{cases}$

symmetric: $h[n] = h[M-n]$
(even symmetry)

anti-symmetric: $h[n] = -h[M-n]$
(odd symmetry)



midpoint $\frac{M}{2}$ (not necessarily a sample)



$$\text{Ex: } M=2 : \quad \left\{ h[n] \right\}_{n=0}^2 = \{ 1, 3, 1 \} \quad (\text{even symmetry})$$

$$\begin{aligned} H_d(w) &= \sum_{n=0}^2 h[n] e^{-jnw} = e^0 + 3e^{-jw} + 1e^{-j(2w)} \\ &= e^{-jw} (e^{jw} + 3 + e^{-jw}) = \underbrace{(3 + 2\cos(w))}_{A(w)} e^{-jw} \end{aligned}$$

linear phase
and GLP

$$\text{Ex 2: Anti-symmetric: } \left\{ h[n] \right\}_{n=0}^3 = \{ 1, 2, -2, -1 \}$$

$$\begin{aligned} H_d(w) &= e^0 + 2e^{-jw} - 2e^{-j(2w)} - e^{-j(3w)} = e^{-j\frac{3}{2}w} \left(e^{j\frac{1}{2}w} + 2e^{j\frac{w}{2}} - 2e^{-j\frac{w}{2}} - e^{-j\frac{3}{2}w} \right) \\ &= \left(2j\sin\left(\frac{3}{2}w\right) + 4j\sin\left(\frac{w}{2}\right) \right) e^{-j\frac{3}{2}w} = \underbrace{\left(2\sin\left(\frac{3}{2}w\right) + 4\sin\left(\frac{w}{2}\right) \right)}_{A(w)} e^{-j\left(-\frac{3}{2}w + \frac{\pi}{2}\right)} \end{aligned}$$

GLP

$$\begin{cases} \text{symmetric, } H_d(w) = A(w) e^{-j\frac{N}{2}w} \\ \text{anti-symmetric, } H_d(w) = A(w) e^{j\left(\frac{N}{2}w + \frac{\pi}{2}\right)} \end{cases}$$

We end up with 4 types of GLP FIR filters.

Design of FIR filters

Table 10.1 Properties of impulse response sequence $h[n]$ and frequency response function $H(e^{j\omega}) = A(e^{j\omega})e^{j\Psi(e^{j\omega})}$ of FIR filters with linear phase.

| Type | $h[k]$ | M | $A(e^{j\omega})$ | $A(e^{j\omega})$ | $\Psi(e^{j\omega})$ |
|------|-------------------------|------|---|---|--------------------------------------|
| I | even (symmetric) | even | $\sum_{k=0}^{M/2} a[k] \cos \omega k$ | even-no restriction | $-\frac{\omega M}{2}$ |
| II | even | odd | $\sum_{k=1}^{\frac{M+1}{2}} b[k] \cos \left[\omega \left(k - \frac{1}{2} \right) \right]$ | even $A(e^{j\pi}) = 0$ | $-\frac{\omega M}{2}$ |
| III | odd (anti-symmetric) | even | $\sum_{k=1}^{M/2} c[k] \sin \omega k$ | odd $A(e^{j0}) = 0$ $A(e^{j\pi}) = 0$ | $\frac{\pi}{2} - \frac{\omega M}{2}$ |
| IV | odd | odd | $\sum_{k=1}^{\frac{M+1}{2}} d[k] \sin \left[\omega \left(k - \frac{1}{2} \right) \right]$ | odd <u>$A(e^{j0}) = 0$</u> | $\frac{\pi}{2} - \frac{\omega M}{2}$ |

↓
not suitable
for LPF