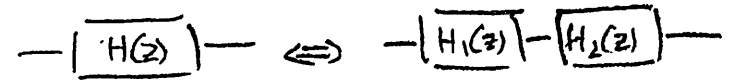


Additional structures:

⊗ Cascade structures

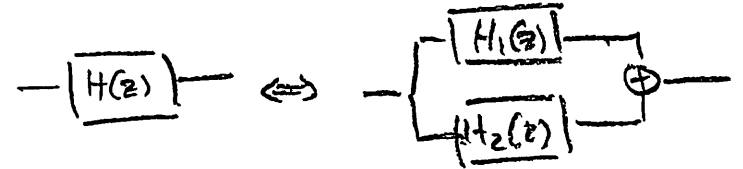
$$H(z) = H_1(z) \cdot H_2(z)$$



⊗ Parallel structures

$$H(z) = H_1(z) + H_2(z)$$

↑  
partial fraction expansion



Ex of cascade structure:

$$H(z) = \frac{b_0 + \dots + b_4 z^{-4}}{1 + \dots + a_4 z^{-4}}$$

where  $a_i, b_i$  are real

$$= \frac{b_0 \prod_{i=1}^4 (1 - z_i z^{-1})}{\prod_{i=1}^4 (1 - p_i z^{-1})}$$

> complex zeros/poles come in conjugate pairs

$$= b_0 \frac{(1 - z_1 z^{-1})(1 - z_2 z^{-1})}{(1 - p_1 z^{-1})(1 - p_2 z^{-1})} \cdot \frac{(1 - z_3 z^{-1})(1 - z_4 z^{-1})}{(1 - \bar{p}_1 z^{-1})(1 - \bar{p}_2 z^{-1})}$$

we pair complex conjugates

$$= b_0 \cdot \frac{B_1(z)}{A_1(z)} \cdot \frac{B_2(z)}{A_2(z)}$$

all coefficients are real

$$H(z) = \frac{10 + z^{-1} + 0.9z^{-2} + 0.8z^{-3} - 5.8z^{-4}}{1 - 2.54z^{-1} + 3.24z^{-2} - 2.06z^{-3} + 0.66z^{-4}} = H_1(z) \cdot H_2(z)$$

with real coefficients

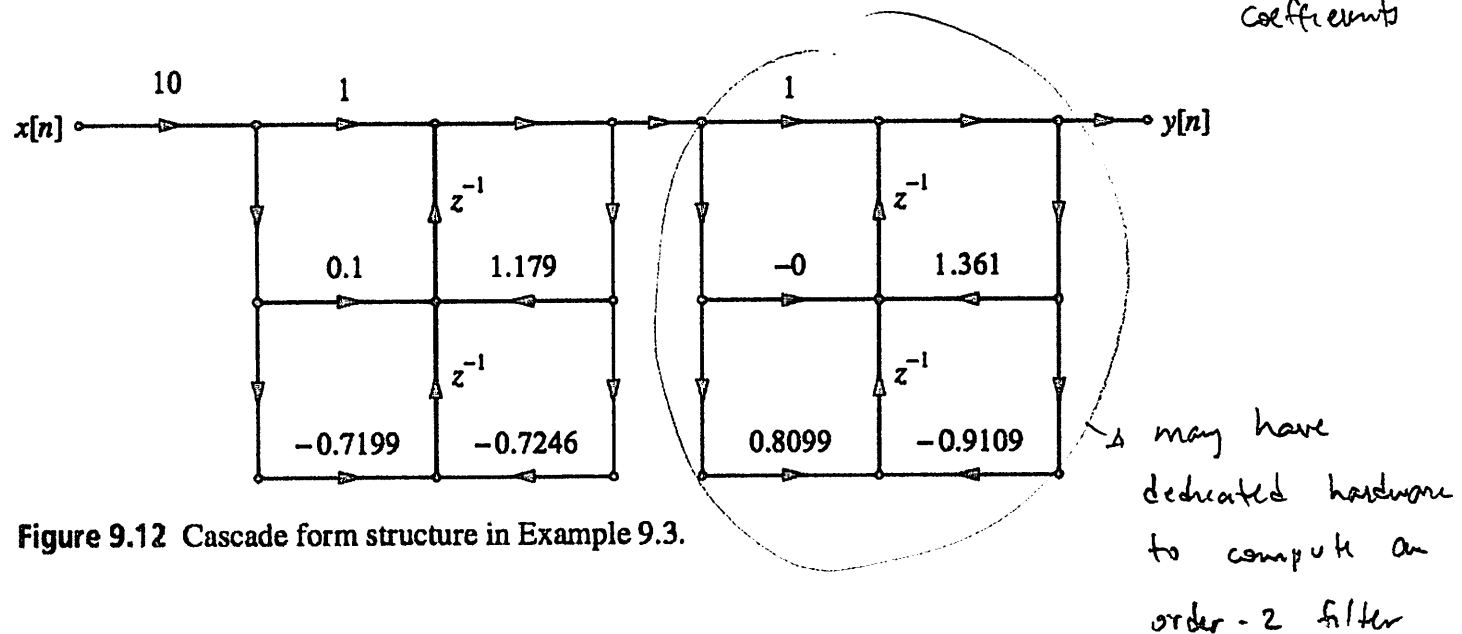


Figure 9.12 Cascade form structure in Example 9.3.

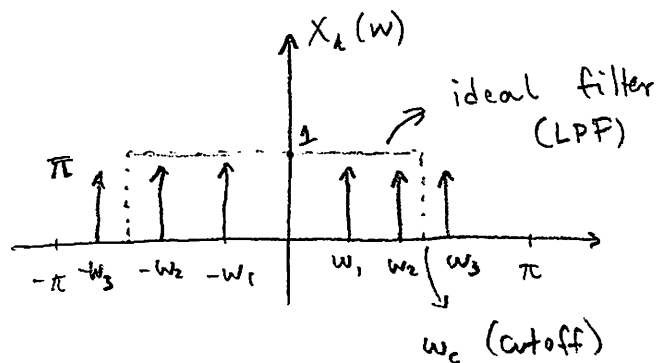
## Lecture 20: From ideal to practical filters (Generalized Linear Phase)

$$\{x[n]\} \rightarrow \boxed{h} \rightarrow \{y[n]\}$$

Typical application: Filter out frequencies in stop band and let the frequencies in the pass band pass unaltered

$$\text{Ex: } x[n] = \cos(\omega_1 n) + \cos(\omega_2 n) + \cos(\omega_3 n), \quad \omega_1 < \omega_2 < \omega_3$$

Suppose I want to remove  $\cos(\omega_3 n)$  (it's noise)

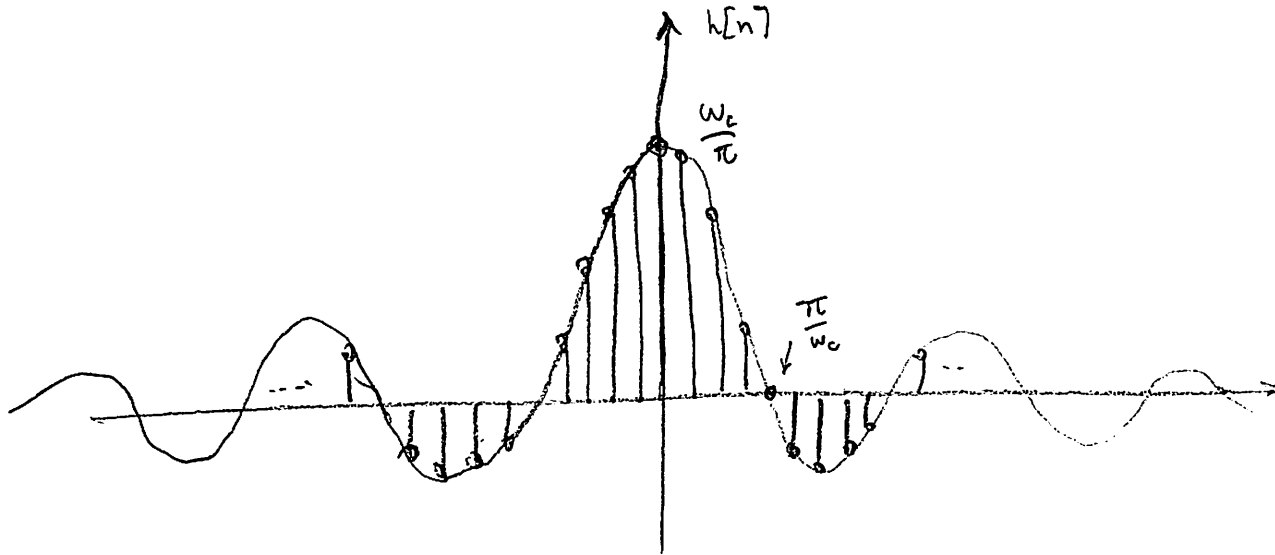


$$H_d(\omega) = \begin{cases} 1 & |\omega| < \omega_c \\ 0 & \text{otherwise} \end{cases}$$

$$\angle H_d(\omega) = 0 \quad \text{for all } \omega$$

Impulse response of ideal LPF :

$$h[n] = \text{DTFT}^{-1}\{H_d(\omega)\} = \frac{\sin(\omega_c n)}{\pi n}$$



Issues :

- Extends to  $\pm \infty$
  - It's non-causal .
- $\Rightarrow$  impractical

Possible solution : shift and truncate

What happens when we shift  $h[n]$ ? Output is delayed.

Let us relax the requirement and accept delayed outputs :

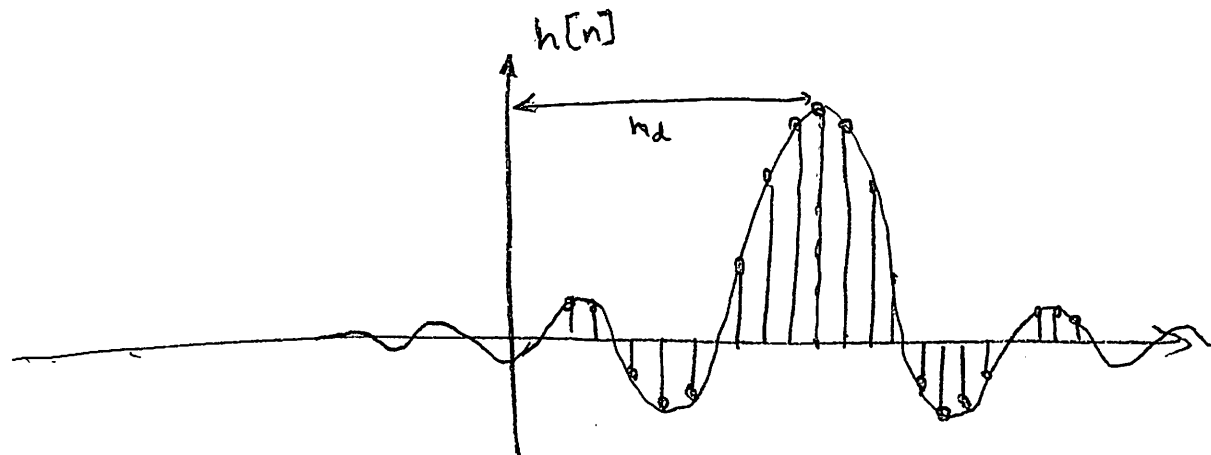
$$x[n] = \underbrace{\cos(\omega_1 n) + \cos(\omega_2 n) + \cos(\omega_3 n)}_{\text{"noise"}} \xrightarrow{\text{(real)} \boxed{h}} y[n] = \cos(\omega_1(n-n_d)) + \cos(\omega_2(n-n_d)) \\ = \cos(\omega_1 n - \omega_1 n_d) + \cos(\omega_2 n - \omega_2 n_d)$$

$$\angle H_d(\omega_1) = -\omega_1 n_d$$

$$\angle H_d(\omega_2) = -\omega_2 n_d$$

In general,  $\boxed{\angle H_d(\omega) = -\omega n_d} \rightarrow \text{linear phase (LP)}$

$$\Rightarrow H_d(\omega) = \begin{cases} 1 \cdot e^{-j\omega n_d} & |\omega| < \omega_c \\ 0 & \text{otherwise} \end{cases}$$



In general, linear phase is desirable (for most filters)

Linear Phase

$$H_d(\omega) = \underbrace{|H_d(\omega)|}_{\geq 0} e^{j(-\alpha\omega)}$$

However, LP is hard to impose in filter design.

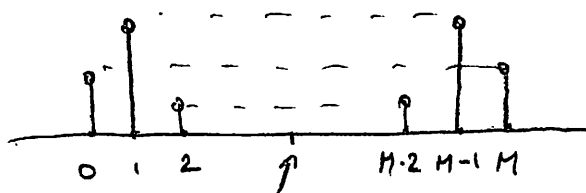
A weaker requirement:

Generalized linear phase:  $H_d(\omega) = \underbrace{A(\omega)}_{\text{real}} e^{j(\alpha\omega + \beta)}$   $\alpha, \beta$  are constants

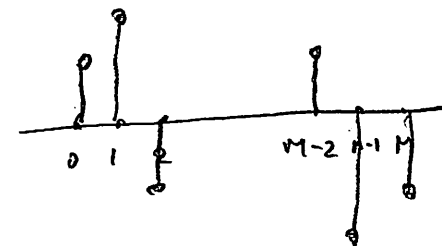
For FIR filters, GLP is attained if  $\{h[n]\}_{n=0}^M$  is  $\begin{cases} \text{symmetric, or} \\ \text{anti-symmetric} \end{cases}$

symmetric:  $h[n] = h[M-n]$   
(even symmetry)

anti-symmetric:  
(odd symmetry)  $h[n] = -h[M-n]$



midpoint  $\frac{M}{2}$  (not necessarily a sample)



Ex:  $M=2$ :  $\{h[n]\}_{n=0}^2 = \{1, 3, 1\}$  (even symmetry)

$$H_d(\omega) = \sum_{n=0}^2 h[n] e^{-j\omega n} = e^0 + 3e^{-j\omega} + 1e^{-j(2\omega)}$$

$$= e^{-j\omega} (e^{j\omega} + 3 + e^{-j\omega}) = \underbrace{(3 + 2\cos(\omega))}_{A(\omega)} e^{-j\omega}$$

linear phase  
and GLP

Ex 2: Anti-symmetric:  $\{h[n]\}_{n=0}^3 = \{1, 2, -2, -1\}$

$$H_d(\omega) = e^0 + 2e^{-j\omega} - 2e^{-j(2\omega)} - e^{-j(3\omega)} = e^{-j\frac{3}{2}\omega} (e^{j\frac{1}{2}\omega} + 2e^{j\frac{\omega}{2}} - 2e^{-j\frac{\omega}{2}} - e^{-j\frac{3}{2}\omega})$$

Type 4

$$= (2j\sin(\frac{3}{2}\omega) + 4j\sin(\frac{\omega}{2})) e^{-j\frac{3}{2}\omega} = \underbrace{(2\sin(\frac{3}{2}\omega) + 4\sin(\frac{\omega}{2}))}_{A(\omega)} e^{-j(-\frac{3}{2}\omega + \frac{\pi}{2})}$$

GLP

In general, for

$\left\{ \begin{array}{l} \text{symmetric,} \\ \text{anti-symmetric.} \end{array} \right.$	$H_d(\omega) = A(\omega) e^{-j\frac{M}{2}\omega}$ $H_d(\omega) = A(\omega) e^{j(-\frac{M}{2}\omega + \frac{\pi}{2})}$
--	--

We end up with 4 types of GLP FIR filters.

## Design of FIR filters

**Table 10.1** Properties of impulse response sequence  $h[n]$  and frequency response function  $H(e^{j\omega}) = A(e^{j\omega})e^{j\Psi(e^{j\omega})}$  of FIR filters with linear phase.

Type	$h[k]$	$M$	$A(e^{j\omega})$	$A(e^{j\omega})$	$\Psi(e^{j\omega})$
I	even (symmetric)	even	$\sum_{k=0}^{M/2} a[k] \cos \omega k$	even—no restriction	$-\frac{\omega M}{2}$
II	even	odd	$\sum_{k=1}^{\frac{M+1}{2}} b[k] \cos \left[ \omega \left( k - \frac{1}{2} \right) \right]$	even $A(e^{j\pi}) = 0$	$-\frac{\omega M}{2}$
III	odd (anti-symmetric)	even	$\sum_{k=1}^{M/2} c[k] \sin \omega k$	odd $A(e^{j0}) = 0$ $A(e^{j\pi}) = 0$	$\frac{\pi}{2} - \frac{\omega M}{2}$
IV	odd	odd	$\sum_{k=1}^{\frac{M+1}{2}} d[k] \sin \left[ \omega \left( k - \frac{1}{2} \right) \right]$	odd $A(e^{j0}) = 0$	$\frac{\pi}{2} - \frac{\omega M}{2}$

↓  
not suitable  
for LPF