Subject: ACS 547, Noise Control Applications - Module 2 Assignment

Date: February 24, 2025 (Submitted)

Problem 1 - Modal Behaviour of a Cylindrical Room

The Matlab code for this problem is listed in Appendix 1.

Problem 1a

Table 1 lists the ten lowest resonance mode orders for the room and the respective frequency.

Index	$\mathbf{Mode} (\mathbf{n}_{\!\scriptscriptstyle \mathrm{X}},\mathbf{n}_{\vartheta},\mathbf{n}_{\!\scriptscriptstyle \mathrm{T}})$	Frequency [Hz]
0	0, 0, 0	0
1	1, 0, 0	17.2
2	0, 1, 0	33.5
3	2, 0, 0	34.3
4	1, 1, 0	37.6
5	2, 1, 0	48.0
6	3, 0, 0	51.5
7	0, 2, 0	55.6
8	1, 2, 0	58.2
9	3, 1, 0	61.4
10	2, 2, 0	65.3

Table 1: Resonant modes of the cylindrical room.

Problem 1b

The two closest modes are (3, 0, 0) and (0, 2, 0) with frequencies of 51.5 Hz and 55.6 Hz, respectively.

Problem 1c

Figure 1 illustrates the (3, 0, 0) and (0, 2, 0) modes. The white lines in each figure show the modal lines for that mode. The machine can be placed where the modal lines for each mode overlap. The figures were produced using the Room Eigenmode Simulator Version 1.1 software package.

The pink rings in Figure 1b indicate 3 possible places where the machine could be placed. These points coincide with the three modal planes shown in Figure 1a. Theoretically, there are an infinite number of places where the machine could be placed. However, placement would take into account practical considerations such as accessibility, etc.

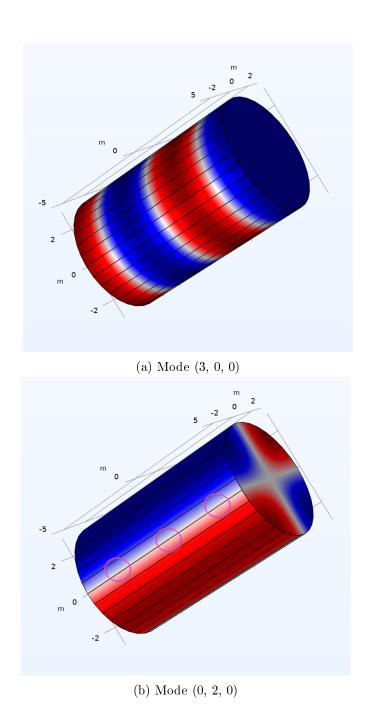


Figure 1: Visualization of modes. (a.) Mode (3, 0, 0). (b.) Model (0, 2, 0). The pink circles in 1b illustrate a few modal line intersections where the machine could be placed.

Problem 2 - Sabine Room

The Matlab code for this problem is listed in Appendix 2.

Problem 2a

The reverberant field sound pressure level is approximately 98.3 dB SPL.

Problem 2b

Figure 2 shows the direct, reverberant, and total sound pressure levels for a 25 mW, 125 Hz, broadband, omnidirectional source placed centrally in the room (i.e. the directivity factor is 1).

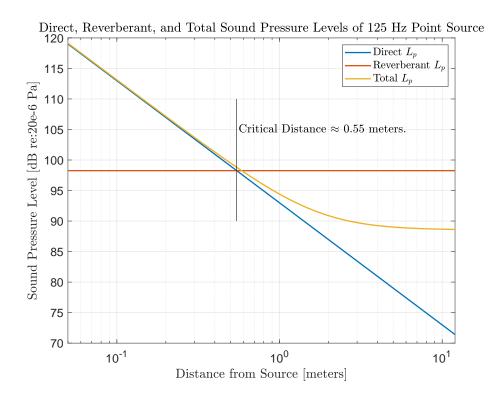


Figure 2: Sound levels for the room produced by a 25 mW, 125 Hz omnidirectional, broadband source.

Problem 3 - Transmission Loss Measurement

The Matlab code for this problem is listed in Appendix 3.

Figure 3 shows the average absorption per octave band based on the T60 data. The calibration plate isolates the receiver room and the absorption calculation does not consider the calibration plate.

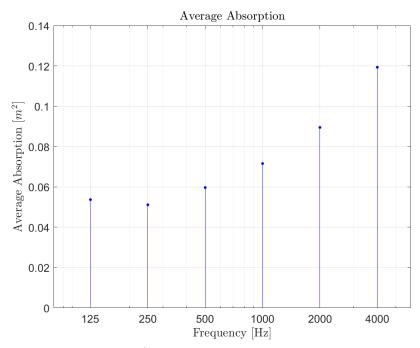


Figure 3: Average absorption per octave band.

Figure 4 shows the transmission loss per octave band.

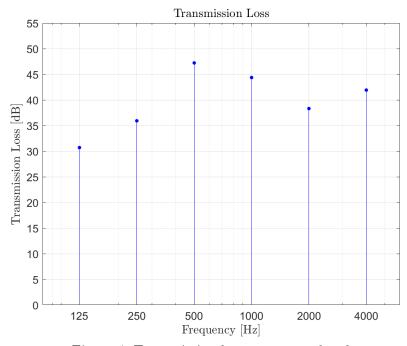


Figure 4: Transmission loss per octave band.

Problem 4 - Panel Transmission Loss

The Matlab code for this problem is listed in Appendix 4.

Problem 4a

The resonance frequency, f_0 , of the galvanized steel panel is 4 Hz or 22.6 $\frac{\text{radians}}{\text{s}}$.

Problem 4b

i - Critical Frequency and Coincidence Frequency at 75°

The critical frequency is 10,216 Hz and the coincidence frequency at 75° is 10,494 Hz.

ii - Transmission Loss at Angle of Incidence of 75°

Figure 5 shows the transmission loss for an angle of incidence of 75°.

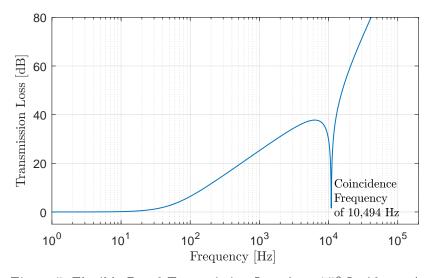


Figure 5: Flexible Panel Transmission Loss for a 75° Incidence Angle

iii - Transmission Loss for Angles of Incidence between $0-90^{\circ}$

Figure 6 shows the transmission loss angles of incidence from 0 to 90° in steps of 10°.

iv - Diffuse Transmission Loss

See the Matlab code in the Appendix 4

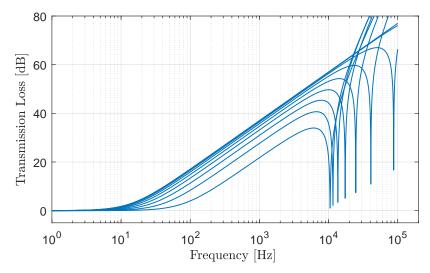


Figure 6: Flexible Panel Transmission Loss for angles of incidence between 0 and 90°.

Problem 4c

See the Matlab code in the Appendix 4

Problem 4d

Figure 7 shows the transmission loss angles of incidence from 0 to 90° in steps of 10° .

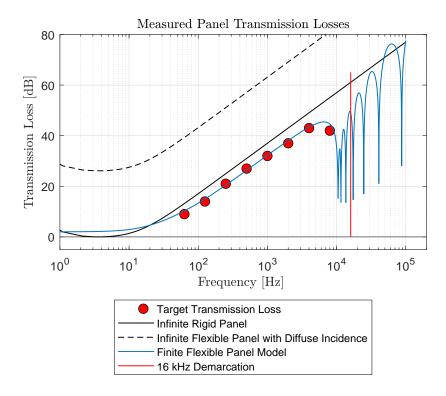


Figure 7: Measured data and the modeled responses.

The finite flexible panel appears to be the most appropriate model. As noted in class, the measured transmission loss at 8 kHz is smaller than the loss a 4 kHz. This indicates that the loss at 16 kHz should be less than the response of the infinite rigid panel at 16 kHz.

Problem 5 - Large Enclosure Design

The Matlab code for this problem is listed in Appendix 5.

My enclosure is a 2 m cube that sits on the ground (5 sides of enclosure material) over the machine. The machine is suspended above the pad (directivity factor of unity). It is assumed that there is no noise transmission through the ground.

Table 2 lists the target insertion losses, the calculated insertion losses for four materials, and the loss difference between the target and each type of material. A positive value indicates that the target insertion loss for the given octave band was not met.

Figure 8 shows calculated insertion loss differences for the data in Table 2.

Octave Band [Hz]	Target IL [dB]	QBV 2 [dB]	QBV 3 [dB]	HTL (100MM) [dB]	HTL 4 [dB]
250	44	28.0	19.7	10.6	5.6
500	54	26.7	22.2	6.6	-4.4
1,000	45	5.6	1.4	-15.4	-22.4
2,000	47	-8.4	-2.2	-18.4	-19.4
4,000	58	-2.4	5.7	-11.0	-13.0

Table 2: Calculated insertion losses for the 4 enclosure materials.

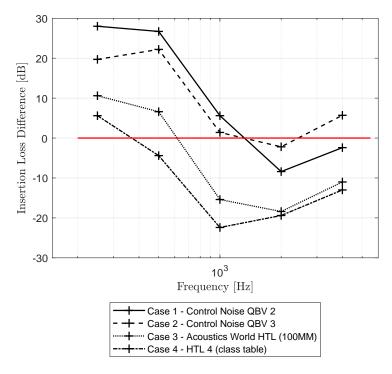


Figure 8: Insertion loss differences.

The most restrictive case given the 2 cubic-meter, 5-sided enclosure, is the HTL 4 material, Case 4, which was presented in class. The target insertion loss was reached by all of the octave bands except the 250 Hz band.

With the same enclosure dimensions and machine orientation, the HTL (100MM) material, Case 3, was found to be the second best material, not meeting the 250 Hz and 500 Hz targets. Figure 9 shows the transmission loss and absorption coefficient data for the material selected from Acoustics World.

The QBV-2 and QBV-3, Case 1 and Case 2, respectively, had the poorest performance. Figure 10 shows the transmission loss and absorption coefficient data for these material from Control Noise.

Using the HTL 4 material from class, a cube with 2 m sides appeared to produce the optimal insertion loss for the 250 Hz octave band. Making the size of the enclosure larger does not reduce this insertion loss and does not seem to be practical. A supplementary approach for this octave band should be considered.

				NRC Rating				
Sound Absorption Coefficients (ASTM C423)								
Acoustic Panel Type	Panel Construction	125 Hz	250Hz	500Hz	1000 Hz	2000 Hz	4000 Hz	NRC
STL (100MM)	18 ga. solid / 22 ga. perforated	0.60	1.13	1.12	1.09	1.03	0.91	1.00
STL (100MM)	16 ga. solid / 22 ga. perforated	0.60	1.13	1.12	1.09	1.03	0.91	1.00
HTL (100MM)	16 ga. solid / 22 ga. perforated with HD Soundbloc Layer	0.60	1.13	1.12	1.09	1.03	0.91	1.00
				STC Rating				
Sound Transmissi	ion Class							
Acoustic Panel Type	Panel Construction	125 Hz	250Hz	500Hz	1000 Hz	2000 Hz	4000 Hz	STC
STL (100MM)	18 ga. solid / 22 ga. perforated	21	28	39	48	56	58	40
STL (100MM)	16 ga. solid / 22 ga. perforated	24	32	41	51	60	66	43
HTL (100MM)	16 ga. solid / 22 ga.	27	34	48	61	66	70	48

Figure 9: HTL (100MM) data from Acoustics World.

ACOUSTICAL DATA:

The most effective noise reduction products combine both sound Flammability Ratings absorption and noise barrier properties. Tested under strict compliance to appropriate ASTM standards, we offer the following results: Product Descriptor Vinyl faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced loaded vinyl Sound Transmission Loss (dB) per Octave Band Frequency QBS-1 23 30 NetWell 4000 STC THK WT. 125 250 500 1000 2000 Model # parrier septum Silicone faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced noise barrier septum 1.3 30 35 1" 11 16 24 35 27 QBV-2 1.5 13 20 50 55 32 QBS-HT QBV-3 2.5" 2 19 46 58 37 25 33 53 QBS-1 1.5 43 29 QBS-2 2.5 19 22 40 33 Roof Par 12 Sound Absorption Data – Absorber Component Random Incident Sound Absorption Octave Band Center Frequencies (Hz) 23 30 reinforced loaded viny 125 250 500 1000 2000 4000 NRC Product QBV-1 .12 .47 .85 .64 .84 .62 .70 .07 1.13 1.08 .99 .85 .96 QBS-1 & 2 .45 QB-4 1.09 1.17 1.13 1.07 1.05

Figure 10: QBV-2 and QBV-3 data from Control Noise.

Problem 6 - Close-fitting Enclosure Design

The Matlab code for this problem is listed in Appendix 6.

The required target insertion loss is 13 dB. This is estimated with the given data and the assumption that the sound measurement distance is beyond the critical distance (i.e., in the diffuse field).

Table 3 lists the dimensions of the designed enclosure.

Height [m]	Width [m]	Depth [m]
3	1.25	1.5

Table 3: Dimensions of the designed enclosure.

Table 4 lists the design parameters for the design enclosure.

Wall	Width [m]	Height [m]	Area [m ²]	Aspect Ratio	Correction	Compliance $\left[\frac{\mathrm{m}^3\cdot\mathrm{s}^2}{\mathrm{kg}}\right]$
Top	1.25	1.5	1.875	1.2	1.8	1.42e-6
Side 1	1.5	3	4.5	2.0	0.6	2.57e-6
Side 2	1.5	3	4.5	2.0	0.6	2.57e-6
Side 3	1.25	3	3.75	2.4	0.5	1.49e-6
Side 4	1.25	3	3.75	2.4	0.5	1.49e-6

Table 4: Enclosure design summary.

The estimated insertion loss without the hole is 13.5 dB, which exceeds the target loss of 13.

The estimated insertion loss with the hole is 1.2 dB, based on the hole depth correction of Deng (1998). The hole reduces the required insertion loss. The intake silencer needs to provide 11.8 dB of insertion loss.

```
2
   % Synopsis
4
   % Problem 1 - Modal Behaviour of a Cylindrical Room
9
10 % Environment
   close all; clear; clc;
13
   % restored efault path;
   % addpath( genpath( ''' ), '-begin' );
addpath( genpath( './00 Support' ), '-begin' );
16
   % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineWidth', 1.5);
18
19
   set( 0, 'DefaultTextInterpreter', 'Latex' );
24
   format ShortG;
26
   pause ( 1 );
28
29
30 %% Define Room
   room.radius = 3; % m
   room.length = 10; \% m
   7% Test Circular Mode Function
38
   40
41
   7% Define Anonymous Function for the Natural Frequencies
45
   46
        .^2);
47
50 % Calculate the Natural Frequencies
   % The maximum number of radial modes is 5 (indexed from 0 to 4).
52
   % The maximum number of angular modes is 8 (indexed from 0 to 7).
54
   NX SIZE = 20;
   \overline{NTHETA}_{SIZE} = 7;
   NR SIZE = 4;
58
        natural frequencies = nan( NX SIZE, NTHETA SIZE, NR SIZE );
59
60
   for nx = 0:1:NX SIZE
        for ntheta = 0:1:NTHETA SIZE
61
62
            \begin{array}{lll} \textbf{for} & \textbf{nr} = 0:1: NR\_SIZE \end{array}
                natural\_frequencies (\ nx+1,\ ntheta+1,\ nr+1\ ) \ = \ h\_natural\_frequencies (\ 343\,,\ nx\,,\ ntheta\,,
                     nr, 10, 3, false);
        end
   end
68
70
   % Part a - Find 10 Lowest Resonance Frequencies
   NUMBER OF LOWEST FREQUENCIES = 11;
```

```
73
          mode indices = ( 1:1:NUMBER OF LOWEST FREQUENCIES ).';
 74
     sortedValues, sortedIndices = sort(natural frequencies(:)); % 21-by-8-by-5 -> 840 elements
 76
 77
     smallestValues = sortedValues ( 1:NUMBER\_OF\_LOWEST\_FREQUENCIES );\\
 78
         % [ mode indices
                               round (smallest Values, 1)
 79
         % 1
 80
 81
         % 2
                       17.2
         % 3
 82
                       33.5
         % 4
 83
                       34.3
         % 5
 84
                       37.6
         % 6
 85
                       47.9
 86
         % 7
                       51.5
 87
         % 8
                       55.6
         % 9
                       58.2
 89
         \% 10
                        61.4
         % 11
                        65.3
     smallestIndices = sortedIndices( 1:NUMBER OF LOWEST FREQUENCIES);
     [x, y, z] = ind2sub(size(natural\_frequencies), smallestIndices);
 94
         % ( [ x y z ] - 1 )
 95
 97
    % Verify the calculated mode indices.
98
    h_natural_frequencies( 343, 0, 0, 0, 10, 3, false );
                                                                   % 0 Hz
    h_natural_frequencies( 343, 1, 0, 0, 10, 3, false );
                                                                   \% 17.2 \text{ Hz}
    h_natural_frequencies( 343, 0, 1, 0, 10, 3, false );
h_natural_frequencies( 343, 2, 0, 0, 10, 3, false );
                                                                    % 34.3 Hz
    h_natural_frequencies( 343, 1, 1, 0 , 10, 3, false );
                                                                    \% 37.6 Hz
    h_natural_frequencies( 343, 2, 1, 0 , 10, 3, false h_natural_frequencies( 343, 3, 0, 0 , 10, 3, false
                                                                    % 48.0 Hz
                                                                );
                                                                    \% 51.5 Hz
    h\_natural\_frequencies (\ 343\,,\ 0\,,\ 2\,,\ 0\,\ ,\ 10\,,\ 3\,,\ false
                                                                    % 55.6 Hz
    h_natural_frequencies( 343, 1, 2, 0 , 10, 3, false h_natural_frequencies( 343, 3, 1, 0 , 10, 3, false
                                                                    % 58.2 Hz
                                                                );
                                                                    % 61.4 Hz
    h natural frequencies (343, 2, 2, 0, 10, 3, false);
108
110
112 %% Part b — Two
113
114
    \% [ (1:11). abs(smallest Values - 53)]
    temp = [x y z] - 1; temp(7:8, :, :)
116
118
     \  \, h\_natural\_frequencies(\ 343,\ 3,\ 0,\ 0,\ 10,\ 3,\ false\ );\ \%\ 51.5\ Hz,\ (3\,,\ 0,\ 0) \\
119
     h natural frequencies ( 343, 0, 2, 0, 10, 3, false ); % 55.6 Hz, (0, 2, 0)
123 %% Part c
124
    % See the report.
126
128
129
    % Clean-up
    fprintf( 1, \n\n\n*** Processing Complete ***\n\n\n');
    % Reference(s)
    \% \ \text{https://www.mathworks.com/matlabcentral/answers/1883747-how-to-find-the-5-minimum-values-in-a-property.}
         multidimensional-matrix-and-the-indices-to-which-these-entries\\
```

```
2
               % Synopsis
   4
               % Problem 2 - Sabine Room
10 % Environment
                 close all; clear; clc;
13 % restored efault path;
                % addpath( genpath( '' ), '-begin' );
addpath( genpath( '../00 Support' ), '-begin' );
16
               % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
18
               set(0, 'DefaultFigurePaperPositionMode', 'manual');
set(0, 'DefaultFigureWindowStyle', 'normal');
set(0, 'DefaultLineLineWidth', 1.5);
set(0, 'DefaultTextInterpreter', 'Latex');
19
24
                 format ShortG;
26
                 pause ( 1 );
28
29
30 % Define Room
              room.width = 8; % m
                room.length = 6; \% m

room.height = 3; \% m
                                      room.volume = room.width * room.length * room.height; % 144 m^3
                                      {\tt room.area} \ = \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.length*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.height}) \ + \ 2*(
                                                         length); \% 180 m<sup>2</sup>
                 alpha\_average\_walls\_and\_floor = \ 0.05; \ \% \ For \ the \ walls \ and \ the \ floor \, .
38
                  alpha_average_ceiling = 0.15; % For the ceiling.
39
                % For the 125 Hz octave band.
41
44
                %% Part a - Estimate the Reverberant Sound Pressure Level
45
47
                Lw = 10 * log 10 ( 25e-3 / 1e-12 ); \% 103.98 dB
48
                  average\_absorption\_coefficient = (\ (room.width*room.length)*alpha\_average \ ceiling \ + \ (room.width*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*ro
                                      *room.length + 2*(room.width*room.height) + 2*(room.length*room.height))*
alpha_average_walls_and_floor) / room.area; % 0.076667 unitless
                  room constant = room.area * average absorption coefficient / ( 1 - average absorption coefficient
                                          ); % 14.9 m<sup>2</sup> or Sabin
                  sound pressure level = Lw + 10*log10 (4 / room constant); % 98.3 dB
56
58 % Part b - Calculate the Critical Distance
59
60 \quad D0 = 1;
61
                 r = 0:0.05:12; % m
                 h Lp direct = @(Lw, D0, r) Lw + 10*log10(D0./(4.*pi.*r.^2));
                 h Lp reverberant = @( Lw, room constant ) Lw + 10*log10( 4 ./ room constant );
66 %
                 h\_Lp\_net = @( \ Lw, \ D0, \ r \,, \ room\_constant \ ) \\ Lw + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \,
67
                                       10*\log 10 (343*1.2/400);
68
                 figure ( ); ...
```

```
h1 = plot(r, h_Lp_direct(Lw, D0, r)); hold on;
          h1 = plot( r, h_bp_alrect( bw, bo, r) ), hold on, h2 = plot( r, ones( size(r) ).*h_Lp_reverberant( Lw, room_constant) ); h3 = plot( r, h_Lp_net( Lw, D0, r, room.volume )); grid on; legend( [ h1, h2 h3 ], { 'Direct $L_p$', 'Reverberant $L_p$', 'Total $L_p$' }, 'Interpreter', 'Latex' );
 73
 74
 76
          text( 0.56, 105, 'Critical Distance $\approx$ 0.55 meters.', 'Interpreter', 'Latex' );
               line([0.545 0.545], [90 110], 'Color', 'k', 'LineWidth', 0.6);
 78
          xlabel( 'Distance from Source [meters]' ); ylabel( 'Sound Pressure Level [dB re:20e-6 Pa]' )
 79
          title ( 'Direct, Reverberant, and Total Sound Pressure Levels of 125 Hz Point Source' );
 80
          %
 81
 82
          set ( gca, 'XScale', 'log');
 83
 84
 85 % Estimate the critical distance (see page 84 of "06-Indoors.pdf" notes for ACS 537).
 86
     rc = 0.141 * sqrt ( D0 * room_constant ); % 0.5451 meters
 87
 88
     return
 89
90 % Clean—up
91
     if ( ~isempty( findobj( 'Type', 'figure') ) )
   monitors = get( 0, 'MonitorPositions');
   if ( size( monitors, 1 ) == 1 )
92
93
94
                autoArrangeFigures(2,2,1);
elseif (1 < size(monitors,1))
96
                    autoArrangeFigures(2,2,1);
97
98
99
     end
     104
106 % Reference(s)
```

```
2
   % Synopsis
4
   % Question 3 - Transmission Loss Measurement
9
   % Note(s):
10 %
        1.) Lp1 depends on the transmission loss.
12 %
13 %
             If the transmission loss is low, then more energy goes to room 2 (i.e., the receiver room
   %
14
15 %
            The noise reduction from the source room to the receiver room.
16 %
17
   %
             Adding the barrier will change the level in the source room. Typically making the sound
        level higher in the source room.
18
19
21 % Environment
   close all; clear; clc;
24 % restored efault path;
   % addpath( genpath( '' ), '-begin' );
26
   addpath ( genpath ( '../00 Support'), '-begin');
28
   % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
29
   set(0, DefaultFigurePaperPositionMode', 'manual');
30
   set( 0, 'DefaultFigureWindowStyle', 'n
set( 0, 'DefaultLineLineWidth', 1.2 );
             'DefaultFigureWindowStyle', 'normal');
   set( 0, Default LineMarker', 'x');
set( 0, 'Default LineMarkerSize', 15 );
% set( 0, 'Default AxesLineStyleOrder', { '-' '--o' '+' } );
   set (0, Default TextInterpreter, Latex);
38
   format ShortG;
40
   pause ( 1 );
41
43
   % Dimensions of Rooms and Panel
44
46 \operatorname{room.length} = 4; % m
47
   room.width = 4; \% m
   room.height = 4; \% m
48
        room.volume = room.length * room.width * room.height; % 64 m^3
        {\tt room.area} = 2*({\tt room.length} \ * \ {\tt room.width}) \ + \ 2*({\tt room.length} \ * \ {\tt room.height}) \ + \ 2*({\tt room.width}) \ *
            room.height); % 96 m^2
   \begin{array}{lll} panel.width &=& 0.8\,; &\%~m\\ panel.height &=& 0.8\,; &\%~m \end{array}
53
        panel.area = panel.width * panel.height; % 0.64 m^2
56
   c = 343; \% m/s
58
59
60 % Measurement Data
61
   1000 2000 4000 ].'; % Hz
                                             spl.source room spl.receiver room (spl.source room - spl.
             receiver_room) ]
68
```

70 %% Calculate Average Absorption in the Receiver Room using Reverberation Time Measurements

```
average absorption = @( volume, area, c, T60 ) ( 55.25 .* volume ) ./ ( area .* c .* T60 );
 73
 74
         receiver room.average absorption = average absorption (room.volume, room.area, c, T60);
 76
        % Assumption: Calibration panel has very high transmission loss.
 78
          figure(); ...
                  stem (\ octave\_band\_frequencies \,,\ receiver\_room.\, average\_absorption \,,\ 'Marker' \,,\ '.\,',\ 'MarkerSize' \,,
 79
                  12, 'Color', 'b'); grid on; xlabel( 'Frequency [Hz]'); ylabel( 'Average Absorption [$m^2$]'); title( 'Average Absorption');
 80
 81
 82
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) ); set( gca, 'XScale', 'log'); xlim( [ 80 6e3 ] ); ylim( [ 0 0.14 ] );
 83
 84
 85
 87
 88
 89 % Calculate the Receiver Room Constant
 91 % The calibration plate isolates the receiver room.
 93
        % The receiver room does not consider the calibration plate.
         \label{eq:constant} \begin{array}{lll} room\_constant = @(\ average\_absorption\ ,\ area\ ) & (\ average\_absorption\ )\ ; & \% \ Unitless \\ \end{array}
 97
          receiver room.room constant = room constant ( receiver room.average absorption, room.area );
 98
        % Calculate the Transmission Loss in Each Octave Band
         transmission\_coefficient = @(\ receiver\_room\_pressure \,,\ source\_room\_pressure \,,\ panel\_area \,,
                  receiver_room_constant ) ( ( receiver_room_pressure ./ source_room_pressure ) .*
                  receiver room constant ) / panel_area;
         tau = transmission\_coefficient ( 10.^(spl.receiver\_room./10)*20e-6, 10.^(spl.source\_room/10)*20e-6, 10.^(spl.source\_room/10)
                  -6, panel.area, receiver room.room constant);
         TL = -10*log10 (tau);
108
         figure( ); ...
                  stem (octave band frequencies, TL, '.', 'MarkerSize', 15, 'Color', 'b'); grid on;
110
                  xlabel( 'Frequency [Hz]'); ylabel( 'Transmission Loss [dB]');
                  title ( Transmission Loss );
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) );
114
                  set ( gca, 'XScale', 'log');
                  xlim( [ 80 6e3 ] ); ylim( [ 0 55 ] );
116
118
119
120 % Clean—up
          if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
                           if (size(monitors, 1) == 1)
                                    autoArrangeFigures(2,2,1);
126
                            elseif (1 < size (monitors, 1))
                                   autoArrangeFigures(2,2,1);
128
                           end
129
         end
         fprintf( 1, \n\n\n*** Processing Complete ***\n\n\n');
```

136 **% Reference(s)**

```
2
   % Synopsis
4
   % Problem 4 - Panel Tramission Loss
10 % Environment
   close all; clear; clc;
13 % restored efault path;
   \% addpath( genpath( ^{-++} ), ^{+}-begin \,^{+-});
   addpath ( genpath ( '../40 Assignments/00 Support'), '-begin');
16
  % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineLineWidth', 0.8); set(0, 'DefaultTextInterpreter', 'Latex');
18
19
24
   format ShortG;
26
   pause ( 1 );
28
29
30 %% Define Panel
   panel.length = 80e-2; % m
   panel.E = 200e9; % Pa
panel.density = 7800; % kg/m^3
34
35 panel.v = 0.29; % Poisson's Ratio (unitless)
   panel.thickness = 1.2e-3; % m
   panel.eta = 0.001; % Loss factor (unitless)
38
   c = 343; \% m/s
39
40
   rho0 = 1.21; \% kg/m^3
41
44 % Measured Panel Data
45
   46
47
48
49
  7 Problem 4a - Infinite, Rigid Panel Model with Normal Incidence
  D = (panel.E * panel.thickness.^3) / (12 * (1 - panel.v^2)); % 31.4
54
55 \quad ms = panel.density * panel.thickness; \ \% \ 9.4 \ kg/m^2
56
   wo = pi^2 / panel.length * sqrt(D / ms); % 22.6 radians/s
58
        s = wo^2 * ms; % 4,785.9 kg radians / m^2s^2
59
   fo = wo / (2*pi); \% 4 Hz
61
62
   \% Define an Anonymous function for the rigid panel with normal incidence.
64
   h_{tau}_{infinite}_{rigid}_{panel} = @(f, wo, ms, s, rho0, c, eta) + 4 ./ ((2*pi.*f*ms - s./(2*pi.*f))
         ./ (rho0 * c) ).^2 + ((wo*ms*eta) ./ (rho0*c) + 2 ).^2);
66
68 % Problem 4b - Infinite, Flexible Panel Model with Random Incidence
70 % The panel has bending waves.
   % Part (i.)
73
```

```
75 % The critical frequency.
     critical frequency = c^2 / (2*pi) * sqrt(ms / D); \% 10.22 kHz
76
   \% Verify the critical frequency using a 90 degree angle of incidence.
79
    critical frequency verify 1 = 1./(2*pi) .* sqrt( ms / D ) .* ( c / sind( 90 )).^2; \% 10.22 kHz
80
81
   % Verify the critical frequency using the properties of the panel.
    critical\_frequency\_verify\_2 = c^2 \ / \ (\ 1.8 \ * \ panel.thickness \ * \ sqrt \ (\ panel.E \ / \ (\ panel.density \ * \ (
82
        1 - panel.v^2) ) ); % 10.3 kHz
83
84
   % Coincidence frequency for a 75 degree angle of incidence.
85
        h coincidence frequency = @( ms, D, c, phi ) 1./(2*pi) * sqrt( ms / D ) .* ( c ./ sind( phi
87
            )).^2;
            h\_coincidence\_frequency(ms, D, c, phi); % 10,949 Hz
89
   \% Define an Anonymous function for the flexible panel with random incidence.
    (2*pi.*f*ms - D*(2*pi.*f./c).^4./(2*pi.*f)*sind(phi)^4).^2);
   \% Part (ii.) - Transmission loss for a 75 degree angle of incidence.
9.8
   f = 0.1:1:100 e3;
    figure( ); ...
        LineStyle', '-', 'Marker', 'none', 'Color', [0.00, 0.45, 0.74]'); grid on; text( 12e3, 5, sprintf( 'Coincidence\nFrequency\nof 10,494 Hz'));
        xlabel( 'Frequency [Hz] '); ylabel( 'Transmission Loss [dB]'); set( gca, 'XScale', 'log'); avis( [1,20062, 7,00])
        axis( [ 1 200e3 -5 80 ] );
       % Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
       %
       % set ( gcf, 'units', 'point', 'pos', [ 200 200 
% pos = get ( gcf, 'Position');
                                                      493*0.8 744*0.3 );
                 set ( gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3)
       %
            , pos(4)]);
       %
                     print (gcf, 'Q4 TL for 75 AOI', '-dpdf', '-r0');
   %
114
   \% \ \text{https://tex.stackexchange.com/questions/} 179382/\text{best-practices-for-using-matlab-images-in-latex}
116
118 % Part (iii.)
119
   f = 0.1:1:100 e3:
    eta = panel.eta; phi set = 0:10:90; t set = [];
    figure(); ...
        hold on;
        for phi = phi_set
           128
        end
       %
        grid on; box on;
xlabel( 'Frequency [Hz] ' ); ylabel( 'Transmission Loss [dB]' );
set( gca, 'XScale', 'log' );
        axis([1 200e3 -5 80]);
134
       %
       \% Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
       %
       , pos(4)]);
       %
                     print (gcf, 'Q4iii TL for 75 AOI', '-dpdf', '-r0');
141
   %
   \%\ https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
145
    tau_d = nanmean(t_set .* sind(2*phi_set).', 1);
```

```
148
           % Combined Transmission Loss Plot
149
                         h1 = stem(\ octave\_band\_frequencies\ ,\ TL,\ 'LineStyle',\ 'none',\ 'Marker',\ 'o',\ 'MarkerSize',\ 8,
                                     'MarkerFaceColor', 'r', 'MarkerEdgeColor', 'k'); hold on;
                         h2 = plot(f, -10*log10(h tau infinite rigid panel(f, wo, ms, s, rho0, c, panel.eta)),
                         \begin{array}{l} LineStyle', \ '-', \ 'Color', \ '\overline{k}' \ ); \\ h3 = plot(\ f, \ -10*log10(\ h\_tau\_infinite\_rigid\_panel(\ f, \ wo, \ ms, \ s, \ rho0, \ c, \ panel.eta \ ) \end{array}
                         0.74]);
                         h5 = line([16e3\ 16e3\ ], [0\ 65\ ], "Color", "r"); grid on; <math>\%\ 16\ kHz Demarcation
                         legend ( ...
158
                                     [ h1, h2, h3, h4, h5 ], ...
                                        Target Transmission Loss', ...
                                     'Infinite Rigid Panel', ...
                                      'Infinite Flexible Panel with Diffuse Incidence', ...
                                      'Finite Flexible Panel Model', ...
                                     116 kHz Demarcation , ...
                                      'Location', 'SouthOutside');
                         xlabel( 'Frequency [Hz] '); ylabel( 'Transmission Loss [dB]');
title( 'Measured Panel Transmission Losses');
                         set ( gca, 'XScale', 'log');
                         axis( [ 1 200e3 -5 80 ] );
170
                        \% Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
                        %
                       , pos(4)]);
                                                                  print(gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0');
176
178
           % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
180
181
182 % Plot Data and Model - Different Side Materials
183
            \% \ h\_tau\_infinite\_rigid\_panel\_side\_materials = @( \ f, \ wo, \ ms, \ s, \ rho0 \,, \ c \,, \ eta \,, \ n \ ) \quad (4*n) \ ./ \ ( \ (4*n) \,, \ (4*n
184
                         (2*pi.*f*ms - s./(2*pi.*f)). / (rho0 * c) ). ^2 + ( (wo*ms*eta) . / (rho0*c) + n + 1 ). ^2 );
185
           \% f = 1e-2:1e-2:20e3:
187
188
           \% \text{ phi} = 15;
           \% eta = panel.eta;
          %
           %
            % figure();
                           plot (f./ (wo / (2*pi) ), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1)), 'LineStyle', '-'); hold on; plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1/3600)), 'LineStyle', '-'); plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy and panel_side_materials (f, wo, ms, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy are grid_energy and panel_side_materials (f, wo, ms, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy are grid_ene
194
           %
           %
                            s, rho0, c, panel.eta, 3600 ) ), 'LineStyle', '-' ); grid on;
                                          %
          %
                                           legend ( ...
                                                      Same Fluid', ...
Water to Air', ...
Air to Water', ...
           %
198
          %
200 %
                                                       'Location', 'North');
           %
203 %
                               xlabel( 'Frequency [\$ frac \{omega\} \{omega o\} \$] ' ); ylabel( 'Transmission Loss [dB]' );
           %
                               title ( 'Measured Panel Transmission Losses');
                              set ( gca, 'XScale', 'log');
% axis([ 40 12e3 -5 45]);
           %
           %
208
210 % Change is Stiffness
           % figure(); ...
                              stem( octave band frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', '
```

```
MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
    %
214
          plot(\ f\ ./\ (wo\ /\ (2*pi)\ )\ ,\ -10*log10(\ h\_tau\_infinite\_rigid\_panel(\ f\ ,\ wo,\ ms,\ s\ ,\ rho0\ ,\ c\ ,\ panel.\ eta\ )\ )\ ,\ 'LineStyle'\ ,\ '-'\ );
    %
         216 %
217
219 %
                legend ( ...
                     'Target TL Values', ...
220 %
    %
                     'Infinite Rigid Panel with Normal Incidence Sound', ...
222 %
                     'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
                     'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
223 %
224
                     'Location', 'North');
    %
226 %
            xlabel( 'Frequency [$\frac{\omega}{\omega o}$] '); ylabel( 'Transmission Loss [dB]');
            title ( 'Measured Panel Transmission Losses - Change in Stiffness ');
    %
            set ( gca, 'XScale', 'log');
    %
228
229 %
            \% axis( [ 40 12e3 -5 45] );
233 % Change in Mass
    % figure(); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
     %
          \begin{array}{c} \text{plot( f ./ (wo / (2*pi) ), } -10*log10( \ h\_tau\_infinite\_rigid\_panel( f , wo, ms*100, s, rho0, c , panel.eta ) ), 'LineStyle', '-' ); \\ \text{plot( f ./ (wo / (2*pi) ), } -10*log10( \ h\_tau\_infinite\_rigid\_panel( f , wo, ms, s, rho0, c , panel.eta ) ), 'LineStyle', '-' ); \\ \text{panel.eta ) ), 'LineStyle', '-' ); \\ \end{array} 
    %
238
    %
          plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*le-2, s, rho0, c, panel.eta ) ), 'LineStyle', '-');
240 %
241 %
                %
242 %
                legend ( ...
243 %
                     'Target TL Values', ...
244 %
                     'Infinite Rigid Panel with Normal Incidence Sound', ...
245 %
                     'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
247 %
                     'Location',
                                   North );
248 %
           %
            xlabel( \ 'Frequency \ [\$\frac{\omega}{\omega_o}\$] \ ' \ ); \ ylabel( \ 'Transmission \ Loss \ [dB]' \ );
249
    %
    %
            title ( 'Measured Panel Transmission Losses - Change in Mass' );
    %
            set ( gca, 'XScale', 'log');
    %
            % axis( [40 \ 12e3 \ -5 \ 45] );
254
256 %% Change in Loss Factor
258
    % figure(); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
    %
    %
         %
    %
          panel.eta*1e2 ) ), 'LineStyle', ':' ); plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rhoo, c,
263 %
          panel.eta*1e-2 ) ), 'LineStyle', ':' );
265 %
                legend ( ...
266 %
                     'Target TL Values', ...
267
                     'Infinite Rigid Panel with Normal Incidence Sound', ...
                     'Infinite Rigid Panel with Normal Incidence Sound (eta * 100)', ...
    %
268
269 %
                     'Infinite Rigid Panel with Normal Incidence Sound (eta / 100)', ...
    %
                     'Location', 'North');
    %
    %
            xlabel( 'Frequency [$\frac{\omega}{\omega o}$] '); ylabel( 'Transmission Loss [dB]');
            title ( 'Measured Panel Transmission Losses - Change in Loss Factor ');
273 %
274
    %
            set ( gca, 'XScale', 'log', 'YScale', 'log');
            % axis( [40 \ 12e3 \ -5 \ 45] );
```

279 **%% Clean—up**

```
280
281 % if (~isempty( findobj( 'Type', 'figure' ) ) )
282 % monitors = get( 0, 'MonitorPositions' );
283 % if ( size( monitors, 1 ) == 1 )
284 % autoArrangeFigures( 2, 2, 1 );
285 % elseif ( 1 < size( monitors, 1 ) )
286 % autoArrangeFigures( 2, 2, 1 );
287 % end
288 % end
289
290
291 fprintf( 1, '\n\n\n*** Processing Complete ***\n\n\n' );
292
293
294
295 % Reference(s)
```

```
2
      % Synopsis
 4
       % Problem 5 - Large Enclosure Design
10 % Environment
        close all; clear; clc;
13 % restored efault path;
       \% addpath( genpath( ^{-++} ), ^{+}-begin \,^{+-});
       addpath ( genpath ( '../40 Assignments/00 Support'), '-begin');
16
      % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineLineWidth', 1.2); set(0, 'DefaultTextInterpreter', 'Latex');
18
19
24
        format ShortG;
26
       pause ( 1 );
28
29
30 %% Define Machine
        machine.area = 3; \% m^2
        machine.absorption = 0.07; % m<sup>2</sup> or Sabin
        machine.D = 1; % Unitless - In air.
        machine.distance = 10; % m
38
40 % Measurement Data
41
       42
43
       Lw = \begin{bmatrix} 105 & 115 & 106 & 108 \end{bmatrix}
45
46
47 % Per Octave Band Insertion Loss
48
49
        Lp_10\_meters = Lw + 10*log10 ( machine.D / ( 4 * pi * machine.distance^2 ) ); \% dB re: 20e-6 Palenter ( 20e-6 Palenter) ( 20e-6 Palente
       % The value of R is infinite. The machine is outside in open air.
        octave band IL = Lp 10 meters - 30;
54
56
57 % Define Anonymous Function for Insertion Loss
58
59
        h IL large = @(Sw, alpha w, Si, alpha i, TL) 10*log10(1 + (Sw*alpha w + Si*alpha i)./(Sw
                    + Si)*10^(TL/10) );
61
63 % Find Values of TL and Aborption that will Meet the Target Insertion Loss — Ground Reflecting
64
       % Assumption(s):
66 %
       %
                             The enclosure is a cube.
                  1.)
68
                             The machine sits on the ground.
69
                  2.) There is no noise transmission through the ground.
70
        enclosure.dimension = 2.0; % m
                  enclosure.area = 5 * enclosure.dimension^2; % 20 m^2
       % Volume of the enclosure is much bigger than the machine Diffuse sound field in the enclosure.
```

```
76
     switch (4)
 78
 79
         case 1
 80
              % https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.
 81
                   pdf
 82
              \% 250 Hz - QBV–2
 83
              alpha_w = 0.27; % From specification sheet.
 84
              TL = 22; % From specification sheet.
 85
                   IL\_estimates\,(1)\ =\ h\_IL\_large\,(\ enclosure.area\,,\ alpha\_w\,,\ machine.area\,,\ machine.
                       absorption, TL);
 87
              \% 500 Hz - QBV-2
              alpha\_w\,=\,\,0.96\,;\quad\%\,\, \text{From specification sheet}\,.
 89
              TL = 28; % From specification sheet.
                   IL\_estimates\,(2\,) \ = \ h\_IL\_large\,(\ enclosure.area\,,\ alpha\_w\,,\ machine.area\,,\ machine.
                       absorption, TL);
              \% 1 kHz - QBV-2
              \% alpha w = 1.13; \% From specification sheet.
              alpha_w = 0.99; % From specification sheet. See comment on slide 28 of Lecture 10.
              TL = 40; % From specification sheet.
 96
                   IL\_estimates\left(3\right) \ = \ h\_IL\_large\left( \ enclosure.area \, , \ alpha\_w \, , \ machine.area \, , \ machine.
                       absorption, TL );
              \% 2 kHz - QBV-2
              \% alpha_w = 1.08; \% From specification sheet.
              alpha\_w = 0.99; ~\% \ \text{From specification sheet}. ~~\text{See comment on slide 28 of Lecture 10}.
              TL = 56; % From specification sheet.
                   IL estimates (4) = h IL large (enclosure.area, alpha w, machine.area, machine.
                       absorption, TL );
              \% 4 kHz - QBV-2
              alpha\_w \, = \, \, 0.99 \, ; \quad \% \  \, \text{From specification sheet} \, .
              TL = 61; % From specification sheet.
                   IL\_estimates\left(5\right) \ = \ h\_IL\_large\left( \ enclosure.area \, , \ alpha\_w \, , \ machine.area \, , \ machine.
                       absorption, TL );
         case 2
              \%\ \ https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.
114
              % Note: Aboseption values are carried over from QBV-2.
116
              \% 250 Hz - QBV-3
              alpha w = 0.96; % From specification sheet.
118
              TL = 25; % From specification sheet.
119
                   \begin{array}{ll} IL\_estimates\left(1\right) = h\_IL\_large\left( \begin{array}{ll} enclosure.area\;,\; alpha\_w\;,\; machine.area\;,\; machine.\\ absorption\;,\; TL\;); \end{array} 
              \% 500 Hz - QBV-3
              alpha w = 0.87; % From specification sheet.
              TL = 33; % From specification sheet.
                   IL\_estimates(2) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                       absorption, TL );
              \% 1 kHz - QBV-3
              \% alpha_w = 1.13; \% From specification sheet.   
alpha_w = 0.66; \% From specification sheet. See comment on slide 28 of Lecture 10.
128
              TL = 46; % From specification sheet.
                   \% 2 kHz - QBV-3
              \% alpha w=1.08\,; % From specification sheet. alpha w=0.47\,; % From specification sheet. See comment on slide 28 of Lecture 10.
              \overline{TL} = 53; % From specification sheet.
                   IL estimates (4) = h IL large (enclosure.area, alpha w, machine.area, machine.
                       absorption, TL );
139
              \% 4 kHz - QBV–3
              alpha w=0.30; % From specification sheet.
              TL = 58; % From specification sheet.
141
```

```
IL estimates (5) = h IL large (enclosure.area, alpha w, machine.area, machine.
                     absorption, TL);
        case 3
            % https://www.acousticsworld.com/machine-acoustic-enclosures/
148
149
            \% alpha_w = 1.13; \% From specification sheet.
            alpha_w = 0.99;
            TL = 34; % From specification sheet.
                IL_estimates(1) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
    absorption, TL );
154
            % 500 Hz
            \% alpha w = 1.12; \% From specification sheet.
            alpha_w = 0.99;
            TL = 48; % From specification sheet.
                IL estimates (2) = h IL large (enclosure.area, alpha w, machine.area, machine.
                    absorption, TL );
161
            \% 1 kHz
            \% alpha_w = 1.09; \% From specification sheet.
            alpha w = 0.99;
            TL = 61; % From specification sheet.
                \% 2 kHz
            \%~alpha\_w = 1.03;~\%~From~specification~sheet.
            alpha_w = 0.99;
            TL = 66; % From specification sheet.
                \% 4 kHz
            alpha_w = 0.91; % From specification sheet.
            TL = 70; % From specification sheet.
                 \begin{array}{ll} {\rm IL\_estimates\,(5\,)} \ = \ h\_{\rm IL\_large\,(\ enclosure.area\,,\ alpha\_w\,,\ machine.area\,,\ machine.} \\ {\rm absorption\,\,,\ TL\,\,)} \ ; \end{array} 
178
179
        case 4
180
181
            % HTL-4 from specification sheet shown in class.
182
            \% 250 Hz
183
184
            \% alpha w = 1.13; \% From specification sheet.
            alpha_w = 0.99;
185
            	ext{TL} = 	extbf{3}	ext{9}; % From specification sheet.
                IL\_estimates\,(1)\ =\ h\_IL\_large\,(\ enclosure.area\,,\ alpha\ w\,,\ machine.area\,,\ machine.
187
                    absorption, TL);
188
189
            \% 500 Hz
            \% alpha_w = 1.12; \% From specification sheet.
            alpha w = 0.99;
            TL = 59; % From specification sheet.
                IL\_estimates\left(2\right) \ = \ h\_IL\_large\left( \ enclosure.area \, , \ alpha\_w \, , \ machine.area \, , \ machine.
                     absorption, TL );
            \% 1 kHz
            \%~alpha\_w=1.09\,;~\%~From~specification~sheet.~alpha\_w=0.99\,;
            TL = 68; % From specification sheet.
                199
            \% 2 kHz
            \% alpha_w = 1.03; \% From specification sheet.
            alpha \ w = 0.99;
            \mathrm{TL} = \mathbf{67}; % From specification sheet.
                IL estimates (4) = h IL large (enclosure.area, alpha w, machine.area, machine.
                    absorption, TL;
            \% 4 kHz
            alpha w=0.91; % From specification sheet.
            TL = 72; % From specification sheet.
```

```
IL estimates (5) = h IL large (enclosure.area, alpha w, machine.area, machine.
                                      absorption, TL);
        end
214
216 % Calculate the Differences
218
                                           IL_estimates.'
                                                                               (octave_band_IL - IL_estimates.') ]
        [ octave_band_IL
        data = [ \dots ]
                                            28.0
                                                           19.7
                                                                         10.6
               250
                                                                                        5.6; ...
                                44
                                                                                        -4.4; ...
                500
                                54
                                            26.7
                                                           22.2
                                                                          6.6
                1\,0\,0\,0
                               45
                                          5.6
                                                        1.4
                                                                     -15.4
                                                                                      -22.4; \dots
                                                         -2.2
               2000
                               47
                                           -8.4
                                                                        -18.4
                                                                                          -19.4; ...
                4\,0\,0\,0
                                           -2.4
                                                         5.7
                                                                         -11.0
                                                                                          -13.0 ];
        figure(); ...
                h1 = plot( data(:, 1 ), data(:, 3 ), 'LineStyle', '-', 'Color', 'k', 'Marker', '+', '
                      MarkerSize', 8); hold on;
                MarkerSize', 8);
                h3 = plot(data(:, 1), data(:, 5), 'LineStyle', ':', 'Color', 'k', 'Marker', '+', '
                       MarkerSize', 8);
                h4 = plot(data(:, 1), data(:, 6), 'LineStyle', '-.', 'Color', 'k', 'Marker', '+', 'LineStyle', '-.', 'Color', 'k', 'Marker', '-.', 'Color', 'LineStyle', '-.', 'Color', 'k', 'Marker', '-.', 'Color', '
               MarkerSize', 8 ); grid on; line( [200 5500], [0 0 ], 'Color', 'r' ); legend( [ h1 h2 h3 h4 ], { 'Case 1 - Control Noise QBV 2', 'Case 2 - Control Noise QBV 3', '
                        Case 3- Acoustics World HTL (100 MM)', 'Case 4- HTL 4 (class table)' \}, 'Location',
                       SouthOutside ');
                xlabel( 'Frequency [Hz]'); ylabel( 'Insertion Loss Difference [dB]');
               axis( [ 150 6e3 -30 30 ] );
set( gca, 'XScale', 'log' );
238
               \% Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
               %
               pos(4)]);
                                          print(gcf, 'Q5 IL Plot', '-dpdf', '-r0');
               %
       \% \ \text{https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex}
247
248
250 % Clean—up
       253 %
       %
                           if ( size(monitors, 1) == 1 )
       %
                                   autoArrangeFigures (2, 2, 1);
      %
256
                            elseif (1 < size (monitors, 1))
       %
                                  autoArrangeFigures(2,2,1);
258
       %
                           end
259
       % end
        fprintf( 1, \n\n\n*** Processing Complete ***\n\n\n');
266 % Reference(s)
267
269
               % Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
               %
               , pos(4) | );
                                          print (gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0');
       \% \ \text{https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex}
```

```
2
          % Synopsis
  4
           % Problem 6 - Close-fitting Enclosure Design
10 % Environment
             close all; clear; clc;
         % restored efault path;
           \% addpath( genpath( ^{-++} ), ^{+}-begin \,^{+-});
16
           addpath (genpath ('../40 Assignments/00 Support'), '-begin');
          % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ] set ( 0, 'DefaultFigurePaperPositionMode', 'manual' );
18
19
            set( 0, 'DefaultFigureWindowStyle', 'normal' );
set( 0, 'DefaultLineLineWidth', 0.8 );
            set( 0, 'DefaultTextInterpreter', 'Latex' );
24
            format ShortG;
26
            pause ( 1 );
28
29
30 % Define Compressor
            compressor.width = 1; \% m
            compressor.depth = 1; \% m
             compressor.height = 2; % m
                           compressor.area = 2*(compressor.width * compressor.depth) + 2*(compressor.width * compressor.
                                        height) + 2*(compressor.depth * compressor.height); % 3 m^2
36
                           compressor.volume = compressor.width * compressor.depth * compressor.height; % m^3
             {\tt compressor.power\_level} = 105; \quad \% \ {\tt dB} \ {\tt re:} \ 1e{-}12 \ {\tt Watts}
38
39
             compressor.frequency = 50; % Hz
41
            c = 343; \% m/s
           rho0 = 1.21; \% kg/m^3
44
45
47
          %% Sound Level Target
48
             sound level target = 82; % dB re: 20e-6 Pascals
53 % Define Workshop
54
          R = 40; % m^2 or Sabins
58
59
          % Define Anonymous Functions
           61
                          (7 + 100 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 + 10) + (7 
62
            h_RA_{term_2} = @( \ rho0 \ , \ c \ , \ S, \ k \ , \ delta_mu \ , \ D, \ w, \ h \ ) \\ \ ( \ rho0*c/S \ ) \\ \ * \quad 0.288*k*3.178e-5*log10((4*k+1.5)e-5*log10) + (4*k+1.5)e-5*log10((4*k+1.5)e-5*log10) + (4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10((4*k+1.5)e-5*log10
                          S)/(pi*h^2));
            h RA term 3 = @(\text{rho0}, \text{c}, \text{S}, \text{k}, \text{delta mu}, \text{D}, \text{w}, \text{h}) (\text{rho0*c/S}) * (0.5*S*k^2)/(2*pi);
67 % Define Close-fitting Enclosure
68
69
            helmholtz_factor = (2 * pi * compressor.frequency) / c; \% 0.92 m^-1
70
                       For a small enclosure, k*d << 1. Therefore d << 1.1.
```

```
73 enclosure.width = compressor.width + 0.25; % m
    enclosure.depth \ = \ compressor.depth \ + \ 0.5; \quad \% \ m
74
    enclosure.height = 3; % m; compression height is 2 m
76
         enclosure.area = 2*(enclosure.width * enclosure.depth) + 2*(enclosure.width * enclosure.
             height) + 2*(enclosure.depth * enclosure.height);
         enclosure.volume = enclosure.width * enclosure.depth * enclosure.height;
78
    enclosure.E = 3.6\,e9; % Pascals
79
    enclosure.thickness = 3.81e-2; % m
80
    enclosure.density = 800; % kg/m^3
81
82
    enclosure.poisson_ratio = 0.25; % Unitless
83
84
    % Clamped boundary conditions.
85
86
87
   % Calculate Diffuse Sound Pressure Level
88
89
    % Assume distance is beyond the critical distance, so the distance value is
91
    % large and its associated term is not relevant.
    sound pressure level = 105 + 10*\log 10(4/R); % 95 dB SPL
97
    % Calculate the Required Insertion Loss
9.8
99
    target insertion loss = sound pressure level - 82 % 13 dB
    % Insertion Loss
    bending_stiffness = ( enclosure.E * enclosure.thickness^3 ) / ( 12*(1 - enclosure.poisson_ratio^2 ) );
         h wall compliance = @( wall area, correction factor ) ( 0.001 * wall area^3 *
             correction factor ) / bending stiffness;
108
    Ca = enclosure.volume / (rho0 * c^2);
    % Top
112 top.area = enclosure.width * enclosure.depth;
    top.aspect \quad ratio = max(\ enclosure.width \, , \ enclosure.depth \, ) \ / \ min(\ enclosure.width \, , \ enclosure.
        depth );
114
    top.correction factor = 3.8;
        top.compliance = h wall compliance( top.area, top.correction factor );
    % Side 1
118
    side 1.area = enclosure.depth * enclosure.height;
119
    side\_1.aspect\_ratio = max(\ enclosure.width\,,\ enclosure.height\ )\ /\ min(\ enclosure.width\,,\ enclosure.width).
        height);
    side_1.correction_factor = 0.6;
        side\_1.compliance = h\_wall\_compliance(side\_1.area, side\_1.correction\_factor);
    % Side 2
124
    side 2.compliance = side_1.compliance;
128 % Side 3
    side_3.area = enclosure.width * enclosure.height;
         _3.aspect_ratio = max( enclosure.width, enclosure.height ) / min( enclosure.width, enclosure.
        height);
    side 3.correction factor = 0.5;
        side 3.compliance = h wall compliance (side 3.area, side 3.correction factor);
    % Side 4
    side\_4.compliance = side 3.compliance;\\
    estimated\_insertion\_loss = 20*log10 ( \ 1 + Ca \ / \ ( \ top.compliance + \ 2*side\_1.compliance + \ 2* \ side\_3.
138
         compliance ));
         13 - estimated insertion loss
```

143 % Compliance of the Air Intake

```
144
           air_intake_frequency = 50; \% Hz
148
                      air intake angular frequency = 2*pi*air intake frequency; % radians/s
149
           viscosity = 1.5 e-5; \% m^2/s
           h = 0.3;
154
           f = 50:
                     term 2 = h RA term 2 ( rho0, c, pi*(air intake radius*2)^2/4, 2*pi*f/c, sqrt ( (2 * 3.178e-5)
156
                     / ( 2*pi*f*rho0 ) ), pi*0.1, 2*pi*f, \overline{0}.3 ); term_3 = h_RA_term_3( rho0, c, pi*(0.1)^2/4, 2*pi*f/c, sqrt((2*3.178e-5)) / ( 2*pi*f*pi*f/c)
                               rho0 ) ), pi * 0.1, 2*pi*f, 0.3 );
                                impedance.real = term_1 + term_2 + term_3;
158
          % Deng (1998)
162
           epsilon = 1;
163
                     L\_o = air\_intake\_radius * ( 1.27 / (1 + 1.92*epsilon) - 0.086 );
           L e = enclosure.thickness + 2*L o;
                     impedance.imaginary = 1 j * r\overline{ho0} * (2 * pi * f) * L_e / ( pi*0.1^2/4 );
168
169
           impedance.net = impedance.real + impedance.imaginary;
170
                      {\tt compliance\_of\_hole} \ = \ 1 \ / \ impedance.net \ ;
                               Cl = a\overline{b}s(\overline{compliance\_of\_hole});
173
           estimated\_insertion\_loss\_with\_hole = 20*log10 ( (Cl + Ca) \ / \ (Cl + (top.compliance + 2*side\_1.) \\
                      compliance + 2* side_3.compliance ) ) );
13 - estimated_insertion_loss_with_hole
174
176
           critical\_frequency = c^2/(2*pi)*sqrt (\ enclosure.density * enclosure.thickness / bending\_stiffness | frequency 
                       ); <sup>-</sup>% 777.1 Hz
178
179
180
         % Clean-up
181
182
           fprintf(1, '\n\n*** Processing Complete ***\n\n');
183
184
185
187 % Reference(s)
```