Subject: Noise Control Applications - Module 1 Assignement

Date: February 3, 2025 (Submitted)

Problem 1 - Cut-on Frequencies in Ducts and Pipes

The Matlab code for this problem is listed in Appendix 1.

Problem 1a

The lowest cut-on frequency for a rectangular duct with air flow is given by equation,

$$f_{\text{cut-on}} = 0.5 \cdot \frac{c}{L} \tag{1}$$

where c is the speed of sound in air, 343 $\frac{m}{s}$, and L is the largest side of the rectangular cross-section.

With cross-sectional dimensions of $L_x = 12$ cm and $L_y = 20$ cm, the lowest cut-on frequency for this rectangular duct is,

$$f_{
m cut-on} = 0.5 \cdot rac{343 \ rac{m}{s}}{0.20 \ m} =$$
857.5 Hz

Problem 1b

The lowest cut-on frequency for a circular duct with air flow with the same cross-sectional area as the rectangular duct in part (a.) can be calculated using equation,

$$f_{\text{cut-on}} = 0.568 \cdot \frac{c}{d} \tag{2}$$

where c is the speed of sound in air, $343 \frac{m}{s}$, and d is diameter of the circular duct.

The cross-sectional area of the rectangular duct is,

Area
$$_{\rm rectangular\ duct} = 0.12\ {\rm m}\ \cdot 0.20\ {\rm m} = 0.024\ {\rm m}$$

The corresponding diameter for this area is,

$$diameter = \sqrt{\frac{0.24 \text{ m}^2}{\pi}} \cdot 2 = 0.17 \text{ m}$$

Using Eq. 2, the lowest cut-on frequency for this circular duct with air flow is,

$$f_{cut-on} = 0.568 \cdot \frac{1,500 \frac{m}{s}}{0.17 m} = 1,114.5 \text{ Hz}$$

Problem 1c

The lowest cut-on frequency for this circular duct with water flow can be calculated using Eq. 2,

$$f_{\rm cut-on} = 0.568 \cdot \frac{1,500 \frac{m}{s}}{0.17 m} = 4,873.9 \; Hz$$

The lowest cut-on frequency for water is considerable larger than it is for air flow.

Problem 1d

The speed of sound in air is calculated by,

$$c = \sqrt{\gamma \cdot R \cdot T_K} \tag{3}$$

where $\gamma=1.4$ is the ratio of specific heats, $R=287~\frac{J}{kg\cdot K}$ is the gas constant, and T_K is the absolute temperature in Kelvin.

Figure 1 illustrates how the lowest cut-on frequency changes as the air heats from 0° to 500° Celsius.

The square-root relationship between temperature and the speed of sound in air is apparent and governs the behaviour of the cut-on frequency.

Lowest Cut-on Frequency for a Circular Pipe with Air Flow Versus Air Temperature

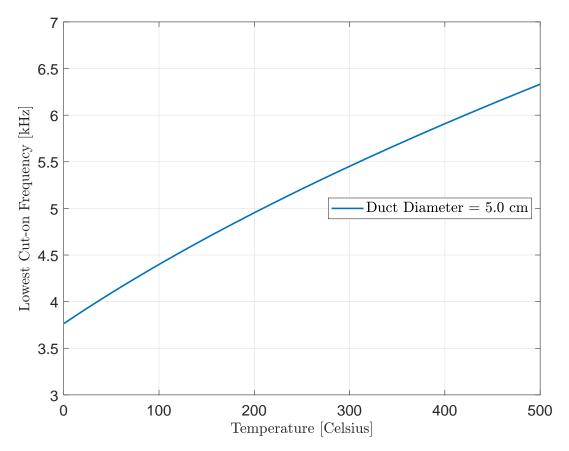


Figure 1: Lowest cut-on frequency for a circular 5 cm diameter duct versus air temperature.

Problem 1e

Question: Are cut-on frequencies higher for a circular or rectangular duct for a given cross-sectional area?

The lowest cut-on frequency is higher for a circular duct than for a rectangular duct for a given cross-sectional area.

For the dimensions given in class, the rectangular duct is not square. This produces a larger dimension and thus a smaller, lowest cut-on frequency. If the rectangular duct is square dimensions on the order of the circular duct diameter with the same cross-sectional area, the cut-on frequencies are approximately equal.

Question: What about in air versus water?

The lowest cut-on frequency is larger for water than for air. The cut-on frequency is proportional to the speed of sound and the speed of sound in water is greater than the speed of sound in air.

Question: What about cold versus hot air?

The lowest cut-on frequency is higher for warm air than it is for cold air.

Problem 2 - Muffler Design Comparison

The Matlab code for this problem is listed in Appendix 2.

For these muffler comparisons, it is assumed that there is no resistive terms (i.e., damping) and no flow. Since transmission losses are plotted, the end corrections (i.e., load impedance at outlet of the system) have no physical meaning and are not accounted for in the computations.

Problem 2a

Figure 2 shows the transmission loss profile for the simple expansion chamber (red, dashed line).

Peak occur at a quarter wavelength; extension tube at outlet.

Extension tube aids quarter wavelenths.

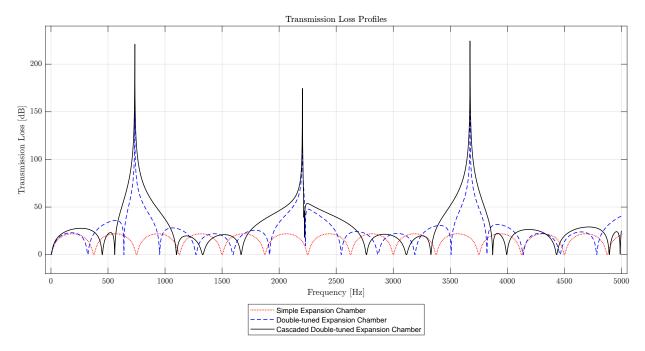


Figure 2: Transmission loss profiles for a simple expansion chamber, a double-tuned expansion chamber, and a cascaded double-tuned expansion chamber mufflers.

Problem 2b

There is no damping in the system; resonances will be artificially high.

Problem 2c

There is no damping in the system; resonances will be artificially high.

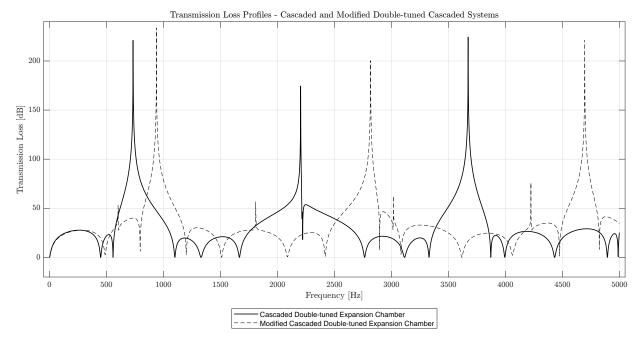


Figure 3: Transmission loss profiles for a cascaded double-tuned expansion chamber muffler and a modified, cascaded double-tuned expansion chamber mufflers.

Problem 3 - Bugle Recorder

Diameters of holes should be smaller than a wavelength.

 R_A is neglected (energy loss).

Problem 3a

Problem 3b

Problem 4 - Intake Duct

Problem 4a

Problem 4b

Problem 4c

Problem 4d

Problem 5 - Intake Duct Silencer

Problem 5a
Problem 5b
Problem 5c
Problem 5d
Problem 5e

1 Appendix - Matlab Code for Problem 1

```
% Synopsis
% Question 1 - Cut-on Frequencies in Ducts and Pipes
% Environment
close all; clear; clc;
% restoredefault path;
% addpath( genpath( '' ), '-begin' );
addpath( genpath( '../40 Assignments/00 Support'), '-begin');
\% set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); \% [ left bottom width
    height ]
set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
set( 0, 'DefaultFigureWindowStyle', 'normal' );
set( 0, 'DefaultLineLineWidth', 1.5 );
set( 0, 'DefaultTextInterpreter', 'Latex' );
format ShortG;
pause ( 1 );
PRINT_FIGURES = 0;
% Define Constants and Anonymous Functions
c~air\,=\,3\,43\,;~\% The speed of sound in air (meters per second).
c water = 1500; % The speed of sound in water (meters per second).
gamma = 1.4; % The ratio of specific heats [unitless].
R = 287; % The gas constant [Joules per (kilogram * Kelvin)].
h_f_{cut\_on\_rectangular\_duct} = @(c, L) = 0.5 .* c./ L;
\% c — The speed of sound.
% L - The largest cross-section dimension of the rectangular duct.
h_f_{cut}_{on}_{circular}_{duct} = @(c, d) = 0.568 .* c./ d;
\% c — The speec of sound.
\% L - The diameter of the circular duct.
h speed of sound in air = @(gamma, R, temperature Kelvin) sqrt(gamma .* R .*
    temperature Kelvin );
% Problem 1a
\% The cross-sectional dimensions for the rectangular duct are: Lx = 12 cm and Ly = 20 cm
% The largest dimension is Ly = 20 cm or 0.2 m.
% The cut—on frequency is,
h f cut on rectangular duct( c air, 0.2 ); % 857.5 Hz (shown in class 858 Hz)
```

```
% Problem 1b
\% The cross-sectional dimensions for the rectangular duct are: Lx = 12 cm and Ly = 20 cm
\% The cross-sectional area of the rectangular duct is 12 cm * 20 cm = 240 cm<sup>2</sup> or 0.024 m
rectangular duct cross sectional area = 0.12 * 0.20; % 0.024 \text{ m}^2
% The diameter of the circulat pipe is,
circular\_duct\_diameter = sqrt(0.024 / pi) * 2; % 0.17481 meters
% Check:
        \% pi * ( circular_duct diameter / 2 )^2 CHECKED
% The cut-on frequency for the circular duct is,
h\_f\_cut\_on\_circular\_duct (\ c\_air\ ,\ circular\_duct\_diameter\ )\ ; \ \%\ 1\ , 114.5\ Hz
          fprintf( 1, '\n Problem 1b: The lowest cut-on frequency for the circular pipe (of
         equal area) with air is \%3.1f~Hz.\n',~h\_f\_cut\_on\_circular\_duct(~c\_air\,,
        circular duct diameter ) );
% Problem 1c
% The cut-on frequency for the circular duct with water is,
h_f_{\text{cut\_on\_circular\_duct(}} c_{\text{water,}} c_{\text{ircular\_duct\_diameter.}}); \% 4,873.9 Hz
          fprintf( 1, '\n Problem 1c: The lowest cut—on frequency for the circular pipe (of
         equal area) with water is \%3.1f Hz.\n', h_f_cut_on_circular_duct( c_water,
        circular duct diameter ) );
% The cut-on frequency should be higher because it is proportional to the
% speed of sound in a given medium.
% Problem 1d
 fprintf( 1, '\n Problem 1d: See the figure.\n' );
temperature range celsius = 0:0.1:500; % Celsius
          temperature_range_kelvin = temperature_range_celsius + 273.15; % Kelvin
FONT_SIZE = 14;
 figure(); ...
          plot (\ temperature\_range\_celsius\ ,\ h\_f\_cut\_on\_circular\_duct (\ h\_speed\_of\_sound\_in\_air (\ h\_speed
        gamma, R, temperature_range_kelvin ), 0.05 ) ./ 1e3 ); grid on; legend( 'Duct Diameter = 5.0 cm', 'Location', 'East', 'FontSize', FONT_SIZE, '
         Interpreter', 'Latex');
                   set ( gca, 'FontSize', FONT_SIZE );
         pxl(2);
                  %
                                set ( xl, 'position', pxl);
          ylabel( 'Lowest Cut-on Frequency [kHz]', 'FontSize', FONT SIZE );
                 \% yl = get(gca, 'ylabel'); pyl = get(yl, 'position'); pyl(1) = 1.2 * pyl(
           1);
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```
set (yl, 'position', pyl);
    caption = sprintf( 'Lowest Cut-on Frequency for a Circular Pipe with Air Flow Versus
    Air Temperature\n');
        title ( caption , 'FontSize', FONT SIZE );
    ylim([3 7]);
% Problem 1e
fprintf( 1, '\n Problem 1e: See Section Problem 1e of the Matlab script for the answers
    . \ n \ n \ );
% Question: Are cut—on frequencies higher for a circular or rectangular duct for a given
     cross-sectional area?
% The lowest cut-on frequency is higher for a circular duct than for a
% rectangular duct for a given cross-sectional area.
% For the dimensions given in class, the rectangular duct is not square.
% This produces a larger dimension and thus a smaller, lowest cut-on
% frequency.
% If the rectangular duct is square dimensions on the order of the circular
\% duct diameter with the same cross—sectional area, the the cut—on
% frequencies are approximately equal.
% Question: What about in air versus water?
\% The lowest cut—on frequency is larger with water than air. This due to
\% the fact that the cut—on frequency is proportional to the speed of sound
\% and the speed of sound in water is greater than it is in air.
% Question: What about cold versus hot air?
% For a circular pipe, the cut-on frequency is higher in warm air than cold
% air.
% Clean-up
if ( ~isempty( findobj( 'Type', 'figure' ) ) )
    monitors = get(0, 'MonitorPositions');
        if ( size( monitors, 1 ) == 1 )
            autoArrangeFigures( 2, 2, 1 );
        elseif (1 < size(monitors, 1))
            autoArrangeFigures( 2, 2, 1 );
        end
end
if ( PRINT FIGURES == 1 )
    saveas (gcf, 'Cut-on Frequency Versus Temperature - Sunday, January 19, 2025.pdf');
end
fprintf(1, '\n\n*** Processing Complete ***\n\n');
```

11

% Reference(s)

2 Appendix - Matlab Code for Problem 2

```
% Synopsis
% Question 2 - Muffler Design Comparison
% Environment
close all; clear; clc;
% restoredefault path;
% addpath( genpath( '' ), '-begin' );
addpath( genpath( '../00 Support' ), '-begin' );
\% set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ]); \% [ left bottom width
    height ]
set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
set( 0, 'DefaultFigureWindowStyle', 'normal' );
set( 0, 'DefaultLineLineWidth', 1.5 );
set( 0, 'DefaultTextInterpreter', 'Latex' );
format ShortG;
pause ( 1 );
PRINT FIGURES = 0;
% Constants
rho0 = 1.21; % Ratio of specific heats (unitless).
c = 343; % Speed of sound in air (meters per second).
frequency set = 0:1:5e3; % Hertz
% Dimensions
convert.inches to meters = 0.0254;
convert.foot to meters = 0.3048;
dimensions.inlet_diameter_meters = 2 * convert.inches_to_meters; % 0.0508 meters
dimensions inlet length meters = 6 * convert foot to meters; % 1.82 meters
dimensions.muffler_diameter_meters = 10 * convert.inches_to_meters; % 0.254 meters
dimensions.muffler length meters = 18 * convert.inches to meters; % 0.4572 meters
dimensions.outlet_diameter_meters = 2 * convert.inches_to_meters; % 0.0508 meters
dimensions.outlet length meters = 1 * convert.foot to meters; % 0.3048 meters
outlet flanged = false;
dimensions.overhang = 3 *convert.inches to meters; % 0.0762 meters
segment\_diameters = [ ... ]
    {\tt dimensions.outlet\_diameter\_meters}\;,\;\; ...
    dimensions.muffler diameter meters, ...
    dimensions.inlet diameter meters, ...
%
h area from diameter = @(d) pi .* d^2 ./ 4;
```

```
segment areas = h area from diameter ( segment diameters );
segment\_lengths = [ ... ]
    {\tt dimensions.outlet\_length\_meters}\;,\;\;\dots
     dimensions. muffler length meters, ...
    dimensions.inlet_length_meters, ...
    dimensions.overhang, ...
    ].';
% Part a — Simple Expansion Chamber
nFreq = length( frequency_set );
    {
m TL} = {
m z} \, {
m er} \, {
m o} \, {
m s} \, ( {
m nFreq} \, , {
m 1} \, ) \, ;
for frequency index = 1:1:nFreq
    f = frequency_set( frequency_index );
    T \text{ total} = [1 0; 0 1];
    T outlet = duct segment transfer matrix (f, rho0, c, segment lengths (1),
    segment_areas ( 1 ) );
     T\_muffler = duct\_segment\_transfer\_matrix(\ f\ ,\ rho0\ ,\ c\ ,\ segment\_lengths(\ 2\ )\ ,
    segment_areas(2);
    T_inlet = duct_segment_transfer_matrix( f, rho0, c, segment_lengths( 3 ),
    segment_areas(3);
    T net = T inlet * T muffler * T outlet * T total;
    T11 = T \text{ net}(1, 1); \quad T12 = T \text{ net}(1, 2); \quad T21 = T \text{ net}(2, 1); \quad T22 = T \text{ net}(2, 2);
    % Z = open_end_impedance( f, rho0, c, segment_lengths( 1 ), segment_areas( 1 ),
    outlet flanged);
        TL(frequency index) = 10 * log10(abs(T11 + segment areas(3)*T12/(rho0*c))
     + (rho0*c)*T21/segment_areas(1) + T22)/2)^2;
end
TL parta = TL;
% Part b - Double-tuned Expansion Chamber
annulus\_area\_squared\_meters = pi/4 * ( segment\_diameters(2)^2 - segment\_diameters(1)^2 );
    branch_diameter = sqrt( 4 * annulus_area_squared_meters / pi );
        a = branch_diameter / 2;
epsilon = branch_diameter / segment_diameters(2); % 0.9787
    L_o = a * (0.9326 - 0.6196*epsilon); % Using Ji (2005) - Slide 11, Lecture 3 notes
nFreq = length( frequency_set );
    TL = zeros(nFreq, 1);
for frequency\_index = 1:1:nFreq
    f = frequency_set( frequency_index );
    T \text{ total} = [1 0; 0 1];
    T outlet = duct segment transfer matrix (f, rho0, c, segment lengths (1),
    segment_areas ( 1 ) );
     T_muffler = duct_segment_transfer_matrix( f, rho0, c, segment_lengths(2) - 2*
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```
segment lengths(4), segment areas(2));
    T inlet = duct segment transfer matrix (f, rho0, c, segment lengths (3),
    segment_areas(3);
    k = 2 * p i * f / c;
         Z_A = -1j*rho0*c/annulus_area_squared_meters*cot(k*(dimensions.overhang+L_o)
    ) );
              T\_branch\_1 \; = \; \left[ \begin{array}{ccc} 1 & 0 \, ; & 1/Z\_A & 1 \end{array} \right];
              T branch_2 = [1 0; 1/Z_A 1];
     T \ \ net = \ T \ \ inlet \ * \ T \ \ branch \ 2 \ * \ T \ \ muffler \ * \ T \ \ branch \ 1 \ * \ T \ \_outlet \ * \ T \ \_total; 
         T11 = T \text{ net}(1, 1); \quad T12 = T \text{ net}(1, 2); \quad T21 = T \text{ net}(2, 1); \quad T22 = T \text{ net}(2, 2);
    % Z = open end impedance (f, rhoo, c, segment lengths (1), segment areas (1),
    outlet flanged);
         TL(frequency\_index) = 10 * log10(abs((T11 + segment\_areas(3)*T12/(rho0*c)))
        (rho0*c)*T21/segment_areas(1) + T22)/2)^2;
end
TL partb = TL;
M Part c - Cascaded, Double-tuned Expansion Chamber
nFreq = length ( frequency_set );
    TL = zeros(nFreq, 1);
for frequency index = 1:1:nFreq
     f = frequency set ( frequency index );
     T \text{ total} = [1 0; 0 1];
     T outlet = duct segment transfer matrix (f, rho0, c, segment lengths (1),
    segment_areas ( 1 ) );
     T_muffler_1 = duct_segment_transfer_matrix(\ f,\ rho0\,,\ c\,,\ (\ segment_lengths(2)\,-\,4*) 
    segment_lengths(4))/2, segment_areas(2));
    T muffler 2 = duct segment transfer matrix (f, rho0, c, (segment lengths (2) - 4*
    segment lengths (4) ) /2, segment areas (2) );
    T inlet = duct segment transfer matrix (f, rho0, c, segment lengths (3),
    segment areas (3);
    k \; = \; 2*p\,i*f\,/\,c\;;
         Z A = -1j*rho0*c/annulus area squared meters*cot(k * ( dimensions.overhang + L o
    ) );
              {\tt T\_branch\_1} \; = \; \left[ \begin{array}{ccc} 1 & 0 \, ; & 1/Z\_A & 1 \end{array} \right];
              T_branch_2 = [1 0; 1/Z_A 1];
              T_branch_3 = [1 0;
                                       1/Z_A \quad 1 ];
              T branch 4 = [1 0; 1/Z A 1];
     T \ \ net = \ T \ \ inlet \ * \ T \ \ branch \ \ 4 \ * \ T \ \ muffler \ \ 2 \ * \ T \ \ branch \ \ 3 \ * \ T \ \ branch \ \ 2 \ * \ T \ \ muffler \ \ 1 \ * 
    T_branch_1 * T_outlet * T_total;
         T11 = T_{net}(1, 1); \quad \overline{T12} = T_{net}(1, 2); \quad T21 = T_{net}(2, 1); \quad T22 = T_{net}(2, 2);
    \% Z = open_end_impedance( f, rho0, c, segment_lengths( 1 ), segment_areas( 1 ),
    outlet flanged );
         TL(frequency index) = 10 * log10(abs(T11 + segment areas(3)*T12/(rho0*c))
     + (rho0*c)*T21/segment_areas(1) + T22)/2)^2;
end
TL partc = TL;
```

```
M Part d - Cascaded, Double-tuned Expansion Chamber
nFreq = length ( frequency_set );
    TL = zeros(nFreq, 1);
for frequency index = 1:1:nFreq
    f = frequency set(frequency index);
    T \text{ total} = [1 0; 0 1];
    T outlet = duct segment transfer matrix (f, rho0, c, segment lengths (1),
    segment_areas ( 1 ) );
    T muffler 1 = duct segment transfer matrix (f, rho0, c, 0.1016, segment areas (2));
     % Changed to 4 inches.
    T\_muffler\_2 = duct\_segment\_transfer\_matrix(\ f\ ,\ rho0\ ,\ c\ ,\ 0.0508\ ,\ segment\ areas(\ 2\ )\ )\ ;
     % Changed to 2 inches.
    T inlet = duct segment transfer matrix (f, rho0, c, segment lengths (3),
    segment areas (3);
    k = 2 * pi * f / c;
        Z A = -1j*rho0*c/annulus area squared meters*cot(k * ( 0.0508 + L o )); %
    Changed to 2 inches.
            T_branch_1 = [1 0; 1/Z_A 1];
            T_branch_2 = [1 0; 1/Z_A 1];
            T_branch_4 = [1 0; 1/Z_A 1];
        Z3 = -1j*rho0*c/annulus area squared meters*cot(k * ( 0.1016 + L o ) ); %
   Changed to 4 inches.
            T branch 3 = [1 0; 1/Z3 1];
    T net = T inlet * T branch 4 * T muffler 2 * T branch 3 * T branch 2 * T muffler 1 *
   T branch 1 * T outlet * T total;
        T11 = T_net(1, 1); T12 = T_net(1, 2); T21 = T_net(2, 1); T22 = T_net(2, 2);
    \% Z = open_end_impedance( f, rho0, c, segment_lengths( 1 ), segment_areas( 1 ),
    outlet flanged );
        TL(frequency index) = 10 * log10(abs(T11 + segment areas(3)*T12/(rho0*c))
    + (rho0*c)*T21/segment_areas(1) + T22)/2)^2;
end
TL partd = TL;
% Plot Transmission Loss Profiles
Y LIMITS = [-20 \ 240];
h_figure_1 = figure(); ...
    plot (frequency set, TL parta, 'LineWidth', 1.0, 'LineStyle', ':', 'Color', 'r');
    plot ( frequency set , TL partc, 'LineWidth', 0.9, 'LineStyle', '-', 'Color', 'k' );
    grid on;
        legend ( ...
            'Simple Expansion Chamber', ...
            'Double-tuned Expansion Chamber', ...
            'Cascaded Double-tuned Expansion Chamber', ...
    'Location', 'SouthOutside');
xlabel( 'Frequency [Hz]'); ylabel( 'Transmission Loss [dB]');
    title ( 'Transmission Loss Profiles');
    %
    Ax = gca;
        Ax. XAxis. TickLabelInterpreter = 'latex';
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```
Ax. YAxis. TickLabelInterpreter = 'latex';
    %
     axis ( \begin{bmatrix} -50 & 5e3+50 & Y_LIMITS \end{bmatrix} );
Y_LIMITS = \begin{bmatrix} -20 & 240 \end{bmatrix};
h \quad figure\_2 \ = \ figure(\ ) \ ; \ \dots
     plot( frequency_set , TL_partc, 'LineWidth', 1.0, 'LineStyle', '-', 'Color', 'k');
     plot (frequency set, TL partd, 'LineWidth', 0.6, 'LineStyle', '--', 'Color', 'k');
    grid on;
         legend ( ...
              'Cascaded Double-tuned Expansion Chamber', ...
              'Modified Cascaded Double-tuned Expansion Chamber', ...
              'Location', 'SouthOutside');
     xlabel( 'Frequency [Hz]' ); ylabel( 'Transmission Loss [dB]' );
     title ( 'Transmission Loss Profiles - Cascaded and Modified Double-tuned Cascaded
    Systems ');
    %
    Ax = gca;
         Ax. XAxis. TickLabelInterpreter = 'latex';
         Ax. YAxis. TickLabelInterpreter = 'latex';
     axis ( \begin{bmatrix} -50 & 5\,\mathrm{e}3 + 50 & \mathrm{Y\_LIMITS} \end{bmatrix} );
% Clean-up
if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
         if ( size( monitors, 1 ) == 1 )
              autoArrangeFigures(2, 2, 1);
         elseif (1 < size(monitors, 1))
              autoArrangeFigures(2, 2, 1);
         end
end
if ( PRINT FIGURES == 1 )
         exportgraphics (h figure 1, 'Assignment 1 - Question 2 Figure All TL Profiles.pdf
    ', 'Append', true );
         exportgraphics ( h figure 2, 'Assignment 1 - Question 2 Figure Comparison TL Plot
    For Cascaded Systems.pdf', 'Append', true );
end
fprintf(1, '\n\n*** Processing Complete ***\n\n');
% Reference(s)
```