Subject: ACS 547, Noise Control Applications - Module 2 Assignment

Date: February 24, 2025 (Submitted)

Problem 1 - Modal Behaviour of a Cylindrical Room

The Matlab code for this problem is listed in Appendix 1.

Problem 1a

Table 1 lists the ten lowest resonance mode orders for the room and the respective frequency.

Index	$\mathbf{Mode} \; (\mathbf{n}_{\mathrm{x}},\mathbf{n}_{\vartheta},\mathbf{n}_{\mathrm{r}})$	Frequency [Hz]
0	0, 0, 0	0
1	1, 0, 0	17.2
2	0, 1, 0	33.5
3	2,0,0	34.3
4	1, 1, 0	37.6
5	2,1,0	48.0
6	3, 0, 0	51.5
7	0, 2, 0	55.6
8	1, 2, 0	58.2
9	3, 1, 0	61.4
10	2,2,0	65.3

Table 1: Resonant modes of the cylindrical room.

Problem 1b

The two closest modes are (3, 0, 0) and (0, 2, 0) with frequencies of 51.5 Hz and 55.6 Hz, respectively.

Problem 1c

Figure 1 illustrates the (3, 0, 0) and (0, 2, 0) modes. The white lines in each figure show the modal lines for that mode. The machine can be placed where the modal lines for each mode overlap. The figures were produced using the Room Eigenmode Simulator Version 1.1 software package.

The pink rings in Figure 1b indicate 3 possible places where the machine could be placed. These points coincide with the three modal planes shown in Figure 1a. Theoretically, there are an infinite number of places where the machine could be placed. However, placement would take into account practical considerations such as accessibility, etc.

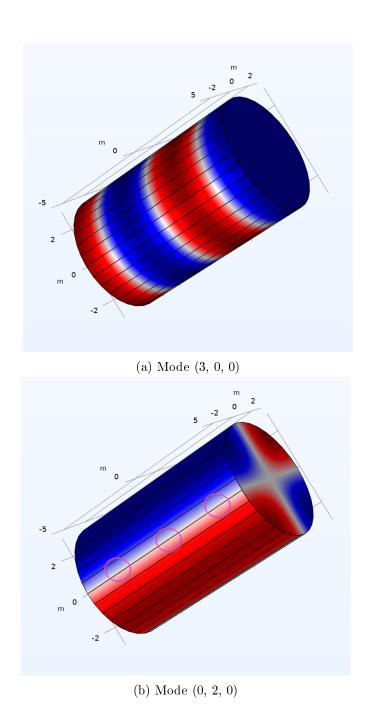


Figure 1: Visualization of modes. (a.) Mode (3, 0, 0). (b.) Model (0, 2, 0). The pink circles in 1b illustrate a few modal line intersections where the machine could be placed.

Problem 2 - Sabine Room

The Matlab code for this problem is listed in Appendix 2.

Problem 2a

The reverberant field sound pressure level is approximately 98.3 dB SPL.

Problem 2b

Figure 2 shows the direct, reverberant, and total sound pressure levels for a 25 mW, 125 Hz, broadband, omnidirectional source placed centrally in the room (i.e. the directivity factor is 1).

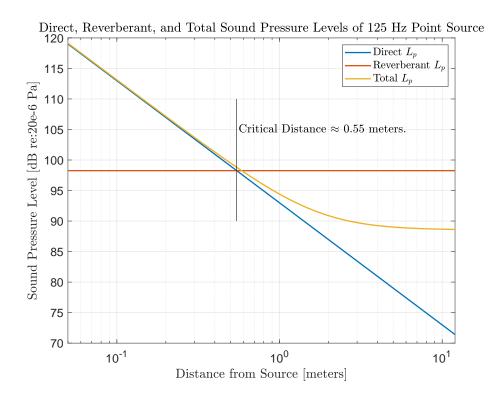


Figure 2: Sound levels for the room produced by a 25 mW, 125 Hz omnidirectional, broadband source.

Problem 3 - Transmission Loss Measurement

The Matlab code for this problem is listed in Appendix 3.

Figure 3 shows the average absorption per octave band based on the T60 data. The calibration plate isolates the receiver room and the absorption calculation does not consider the calibration plate.

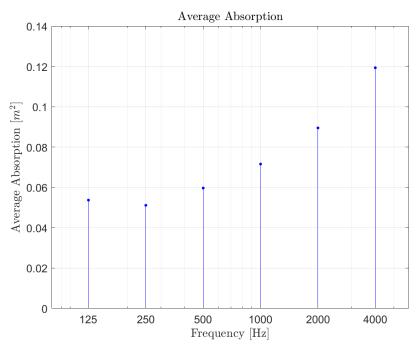


Figure 3: Average absorption per octave band.

Figure 4 shows the transmission loss per octave band.

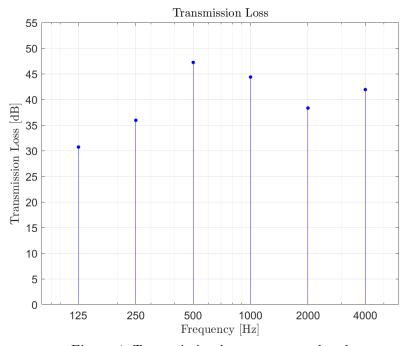


Figure 4: Transmission loss per octave band.

Problem 4 - Panel Transmission Loss

The Matlab code for this problem is listed in Appendix 4.

Problem 4a

The resonance frequency, f_0 , of the galvanized steel panel is 4 Hz or 22.6 $\frac{\text{radians}}{\text{s}}$.

Problem 4b

i - Critical Frequency and Coincidence Frequency at 75°

The critical frequency is 10,216 Hz and the coincidence frequency at 75° is 10,494 Hz.

ii - Transmission Loss at Angle of Incidence of 75°

Figure 5 shows the transmission loss for an angle of incidence of 75°.

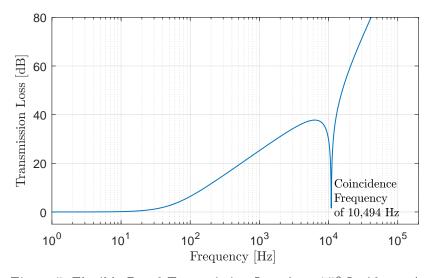


Figure 5: Flexible Panel Transmission Loss for a 75° Incidence Angle

iii - Transmission Loss for Angles of Incidence between $0-90^{\circ}$

Figure 6 shows the transmission loss angles of incidence from 0 to 90° in steps of 10°.

iv - Diffuse Transmission Loss

See the Matlab code in the Appendix 4

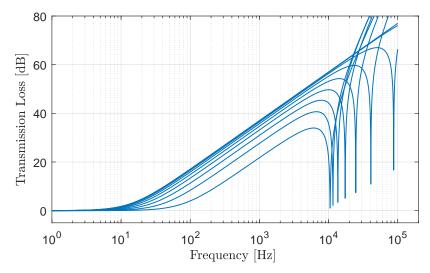


Figure 6: Flexible Panel Transmission Loss for angles of incidence between 0 and 90°.

Problem 4c

See the Matlab code in the Appendix 4

Problem 4d

Figure 7 shows the transmission loss angles of incidence from 0 to 90° in steps of 10° .

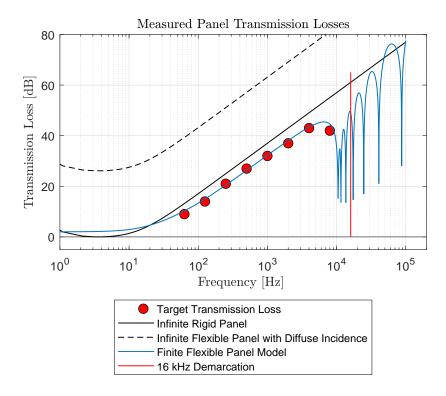


Figure 7: Measured data and the modeled responses.

The finite flexible panel appears to be the most appropriate model. As noted in class, the measured transmission loss at 8 kHz is smaller than the loss a 4 kHz. This indicates that the loss at 16 kHz should be less than the response of the infinite rigid panel at 16 kHz.

Problem 5 - Large Enclosure Design

The Matlab code for this problem is listed in Appendix $\pmb{6}.$

ph

Problem 6 - Close-fitting Enclosure Design

The Matlab code for this problem is listed in Appendix 6.

ACOUSTICAL DATA:

The most effective noise reduction products combine both sound absorption and noise barrier properties. Tested under strict compliance to appropriate ASTM standards, we offer the following results:

Sound Transmission Loss (dB) per Octave Band Frequency									
NetWell Model #	THK.	WT.	125	250	500	1000	2000	4000	STC
QBV-1	1"	1.3	11 ,	16	24	30	35	35	27
QBV-2	2"	1.5	13	20	29	40	50	55	32
QBV-3	2.5"	2	19	25	33	46	53	58	37
QBS-1	2"	1.5	12	16	27	40	44	43	29
QBS-2	2"	2.5	19	22	28	40	56	61	33
Roof Panel	2"	2	18	24	28	37	45	46	31

Per ASTM E 90

Sound Absorption Data – Absorber Component Random Incident Sound Absorption Octave Band Center Frequencies (Hz)									
Product	тнк.	125	250	500	1000	2000	4000	NRC	
QBV-1	1"	.12	.47	.85	.84	.64	.62	.70	
QBV-2	2"	.07	.27	.96	1.13	1.08	.99	.85	
QBS-1 & 2	2"	.45	.96	.87	.66	.47	.30	.75	
QB-4	4"	.21	.89	1.09	1.17	1.13	1.07	1.05	

Product Descriptor Flame Spread Developed

Vinyl faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced loaded vinyl barrier septum

QBS-HT Silicone faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced loaded vinyl barrier septum

QBS-HT Vinyl faced 2" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced loaded vinyl noise barrier septum

Vinyl faced 2" quilt on one side of a 1 lb. reinforced loaded vinyl noise barrier along the product of the policy of th

Above table shows flame spread and smoke developed ratings per ASTM Designation E&F Surface Burning Characteristics of Building Materials. Note: Class A rating applies to products with a flame spread index of 25 or less, and a smoke developed index of 450 or less. The spread is the spread index of 450 or less.

Figure 8: Measured data and modeled responses.

QBS 2 - https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf $44.008\ 15.983\ 28.025\ 54.008\ 27.271\ 26.737\ 45.008\ 39.396\ 5.6122\ 47.008\ 55.395\ -8.3873\ 58.008\ 60.395\ -2.3873$

with the alpha correction to 0.99

QBS 2 - https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf $44.008\ 24.279\ 19.729\ 54.008\ 31.843\ 22.165\ 45.008\ 43.657\ 1.3507\ 47.008\ 49.21\ -2.2021\ 58.008\ 52.314\ 5.6942$

```
2
   % Synopsis
4
   % Problem 1 - Modal Behaviour of a Cylindrical Room
9
10 % Environment
   close all; clear; clc;
13
   % restored efault path;
   % addpath( genpath( '' ), '-begin' );
addpath( genpath( './00 Support' ), '-begin' );
16
   % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineWidth', 1.5);
18
19
   set( 0, 'DefaultTextInterpreter', 'Latex' );
24
   format ShortG;
26
   pause ( 1 );
28
29
30 %% Define Room
   room.radius = 3; % m
   room.length = 10; \% m
   7% Test Circular Mode Function
38
   40
41
   7% Define Anonymous Function for the Natural Frequencies
45
   46
        .^2);
47
50 % Calculate the Natural Frequencies
   % The maximum number of radial modes is 5 (indexed from 0 to 4).
52
   % The maximum number of angular modes is 8 (indexed from 0 to 7).
54
   NX SIZE = 20;
   \overline{NTHETA}_{SIZE} = 7;
   NR SIZE = 4;
58
        natural frequencies = nan( NX SIZE, NTHETA SIZE, NR SIZE );
59
60
   for nx = 0:1:NX SIZE
        for ntheta = 0:1:NTHETA SIZE
61
62
            \begin{array}{lll} \textbf{for} & \textbf{nr} = 0:1: NR\_SIZE \end{array}
                natural\_frequencies (\ nx+1,\ ntheta+1,\ nr+1\ ) \ = \ h\_natural\_frequencies (\ 343\,,\ nx\,,\ ntheta\,,
                     nr, 10, 3, false);
        end
   end
68
70
   % Part a - Find 10 Lowest Resonance Frequencies
   NUMBER OF LOWEST FREQUENCIES = 11;
```

```
73
          mode indices = ( 1:1:NUMBER OF LOWEST FREQUENCIES ).';
 74
     [ sortedValues, sortedIndices ] = sort ( natural frequencies (:) ); % 21-by-8-by-5 -> 840 elements
 76
 77
     smallest Values = sorted Values ( 1:NUMBER\_OF\_LOWEST\_FREQUENCIES );\\
 78
         % [ mode indices
                               round (smallest Values, 1)
         %
 79
         \% 1
         % 2
                       17.2
 81
         % 3
 82
                       33.5
         % 4
 83
                       34.3
         % 5
 84
                       37.6
         % 6
 85
                       47.9
 86
         % 7
                       51.5
 87
         % 8
                       55.6
         % 9
                       58.2
 89
         % 10
                         61.4
         % 11
                        65.3
     smallestIndices = sortedIndices( 1:NUMBER OF LOWEST FREQUENCIES);
 94
     [ x, y, z ] = ind2sub( size(natural_frequencies), smallestIndices );
         % ( [ x y z ] - 1 )
 95
 97
    % Verify the calculated mode indices.
98
    h_natural_frequencies( 343, 0, 0, 0, 10, 3, false );
                                                                   % 0 Hz
    h_natural_frequencies( 343, 1, 0, 0, 10, 3, false );
                                                                   % 17.2 Hz
    h_natural_frequencies( 343, 0, 1, 0, 10, 3, false );
h_natural_frequencies( 343, 2, 0, 0 , 10, 3, false );
                                                                    % 34.3 Hz
    h_natural_frequencies( 343, 1, 1, 0 , 10, 3, false
                                                                    \% 37.6 Hz
    % 48.0 Hz
                                                                );
                                                                    \% 51.5 Hz
    h\_natural\_frequencies (\ 343\,,\ 0\,,\ 2\,,\ 0\ ,\ 10\,,\ 3\,,\ false
                                                                    % 55.6 Hz
                                                                );
    h_natural_frequencies( 343, 1, 2, 0 , 10, 3, false
h_natural_frequencies( 343, 3, 1, 0 , 10, 3, false
                                                                    % 58.2 Hz
                                                                );
                                                                    \% 61.4 Hz
    h natural frequencies (343, 2, 2, 0, 10, 3, false);
108
110
112 %% Part b — Two
114
    \% [ (1:11). abs(smallest Values - 53)]
    temp = [x y z] - 1; temp(7:8, :, :)
116
118
     h\_natural\_frequencies ( \ 343, \ 3, \ 0, \ 0, \ 10, \ 3, \ false \ ); \\ \ \% \ 51.5 \ Hz, \ (3, \ 0, \ 0) 
119
     h natural frequencies ( 343, 0, 2, 0, 10, 3, false ); \% 55.6 Hz, (0, 2, 0)
    %% Part c
124
    % See the report.
126
128
129
    % Clean-up
     if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
              if ( size( monitors, 1 ) == 1 )
              \begin{array}{c} \texttt{autoArrangeFigures(2,2,1);} \\ \texttt{elseif (1 < size(monitors,1))} \end{array}
                   autoArrangeFigures(2, 2, 1);
              end
138
    end
     fprintf(1, '\n\n*** Processing Complete ***\n\n');
    % Reference(s)
146
```

10

 $\% \ \ https://www.mathworks.com/matlabcentral/answers/1883747-how-to-find-the-5-minimum-values-in-a-find-the-$

multidimensional-matrix-and-the-indices-to-which-these-entries

```
2
               % Synopsis
   4
               % Problem 2 - Sabine Room
10 % Environment
                 close all; clear; clc;
13 % restored efault path;
                % addpath( genpath( '' ), '-begin' );
addpath( genpath( '../00 Support' ), '-begin' );
16
               % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
18
               set(0, 'DefaultFigurePaperPositionMode', 'manual');
set(0, 'DefaultFigureWindowStyle', 'normal');
set(0, 'DefaultLineLineWidth', 1.5);
set(0, 'DefaultTextInterpreter', 'Latex');
19
24
                 format ShortG;
26
                 pause ( 1 );
28
29
30 % Define Room
              room.width = 8; % m
                room.length = 6; \% m

room.height = 3; \% m
                                      room.volume = room.width * room.length * room.height; % 144 m^3
                                      {\tt room.area} \ = \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.length*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.height}) \ + \ 2*(
                                                         length); \% 180 m<sup>2</sup>
                 alpha\_average\_walls\_and\_floor = \ 0.05; \ \% \ For \ the \ walls \ and \ the \ floor \, .
38
                  alpha_average_ceiling = 0.15; % For the ceiling.
39
                % For the 125 Hz octave band.
41
44
                %% Part a - Estimate the Reverberant Sound Pressure Level
45
47
                Lw = 10 * log 10 ( 25e-3 / 1e-12 ); \% 103.98 dB
48
                  average\_absorption\_coefficient = (\ (room.width*room.length)*alpha\_average \ ceiling \ + \ (room.width*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*ro
                                      *room.length + 2*(room.width*room.height) + 2*(room.length*room.height))*
alpha_average_walls_and_floor) / room.area; % 0.076667 unitless
                  room constant = room.area * average absorption coefficient / ( 1 - average absorption coefficient
                                          ); % 14.9 m<sup>2</sup> or Sabin
                  sound pressure level = Lw + 10*log10 (4 / room constant); % 98.3 dB
56
58 % Part b - Calculate the Critical Distance
59
60 \quad D0 = 1;
61
                 r = 0:0.05:12; % m
                 h Lp direct = @(Lw, D0, r) Lw + 10*log10(D0./(4.*pi.*r.^2));
                 h Lp reverberant = @( Lw, room constant ) Lw + 10*log10( 4 ./ room constant );
66 %
                 h\_Lp\_net = @( \ Lw, \ D0, \ r \,, \ room\_constant \ ) \\ Lw + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \,
67
                                       10*\log 10 (343*1.2/400);
68
                 figure ( ); ...
```

```
h1 = plot(r, h_Lp_direct(Lw, D0, r)); hold on;
          h1 = plot( r, h_bp_alrect( bw, bo, r) ), hold on, h2 = plot( r, ones( size(r) ).*h_Lp_reverberant( Lw, room_constant) ); h3 = plot( r, h_Lp_net( Lw, D0, r, room.volume )); grid on; legend( [ h1, h2 h3 ], { 'Direct $L_p$', 'Reverberant $L_p$', 'Total $L_p$' }, 'Interpreter', 'Latex' );
 73
 74
 76
          text( 0.56, 105, 'Critical Distance $\approx$ 0.55 meters.', 'Interpreter', 'Latex' );
               line([0.545 0.545], [90 110], 'Color', 'k', 'LineWidth', 0.6);
 78
          xlabel( 'Distance from Source [meters]' ); ylabel( 'Sound Pressure Level [dB re:20e-6 Pa]' )
 79
          title ( 'Direct, Reverberant, and Total Sound Pressure Levels of 125 Hz Point Source' );
 80
          %
 81
 82
          set ( gca, 'XScale', 'log');
 83
 84
 85 % Estimate the critical distance (see page 84 of "06-Indoors.pdf" notes for ACS 537).
 86
     rc = 0.141 * sqrt ( D0 * room_constant ); % 0.5451 meters
 87
 88
     return
 89
90 % Clean—up
91
     if ( ~isempty( findobj( 'Type', 'figure') ) )
   monitors = get( 0, 'MonitorPositions');
   if ( size( monitors, 1 ) == 1 )
92
93
94
                autoArrangeFigures(2,2,1);
elseif (1 < size(monitors,1))
96
                    autoArrangeFigures(2,2,1);
97
98
99
     end
     104
106 % Reference(s)
```

```
2
   % Synopsis
4
   % Question 3 - Transmission Loss Measurement
9
  % Note(s):
10 %
       1.) Lp1 depends on the transmission loss.
12 %
13 %
            If the transmission loss is low, then more energy goes to room 2 (i.e., the receiver room
   %
14
15 %
           The noise reduction from the source room to the receiver room.
16 %
17
   %
            Adding the barrier will change the level in the source room. Typically making the sound
       level higher in the source room.
18
19
21 % Environment
   close all; clear; clc;
24 % restored efault path;
  % addpath( genpath( '' ), '-begin' );
26
   addpath ( genpath ( '../00 Support'), '-begin');
28
   % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
29
   set(0, DefaultFigurePaperPositionMode', 'manual');
30
   set( 0, 'DefaultFigureWindowStyle', 'n
set( 0, 'DefaultLineLineWidth', 1.2 );
            'DefaultFigureWindowStyle', 'normal');
   38
   format ShortG;
40
   pause ( 1 );
41
43
   % Dimensions of Rooms and Panel
44
46 \operatorname{room.length} = 4; % m
47
   room.width = 4; \% m
   room.height = 4; \% m
48
       room.volume = room.length * room.width * room.height; % 64 m^3
       {\tt room.area} = 2*({\tt room.length} \ * \ {\tt room.width}) \ + \ 2*({\tt room.length} \ * \ {\tt room.height}) \ + \ 2*({\tt room.width}) \ *
           room.height); % 96 m^2
   \begin{array}{lll} panel.width &=& 0.8\,; & \%~m \\ panel.height &=& 0.8\,; & \%~m \end{array}
53
       panel.area = panel.width * panel.height; % 0.64 m^2
56
   c = 343; \% m/s
58
59
60 % Measurement Data
61
   1000 2000 4000 ].'; % Hz
                                          spl.source room spl.receiver room (spl.source room - spl.
           receiver_room) ]
68
```

70 %% Calculate Average Absorption in the Receiver Room using Reverberation Time Measurements

```
average absorption = @( volume, area, c, T60 ) ( 55.25 .* volume ) ./ ( area .* c .* T60 );
 73
 74
         receiver room.average absorption = average absorption (room.volume, room.area, c, T60);
 76
        % Assumption: Calibration panel has very high transmission loss.
 78
          figure(); ...
                  stem (\ octave\_band\_frequencies \,,\ receiver\_room.\, average\_absorption \,,\ 'Marker' \,,\ '.\,',\ 'MarkerSize' \,,
 79
                  12, 'Color', 'b'); grid on; xlabel( 'Frequency [Hz]'); ylabel( 'Average Absorption [$m^2$]'); title( 'Average Absorption');
 80
 81
 82
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) ); set( gca, 'XScale', 'log'); xlim( [ 80 6e3 ] ); ylim( [ 0 0.14 ] );
 83
 84
 85
 87
 88
 89 % Calculate the Receiver Room Constant
 91 % The calibration plate isolates the receiver room.
 93
        % The receiver room does not consider the calibration plate.
         \label{eq:constant} \begin{array}{lll} room\_constant = @(\ average\_absorption\ ,\ area\ ) & (\ average\_absorption\ )\ ; & \% \ Unitless \\ \end{array}
 97
         receiver room.room constant = room constant ( receiver room.average absorption, room.area );
 98
        % Calculate the Transmission Loss in Each Octave Band
         transmission\_coefficient = @( \ receiver\_room\_pressure \,, \ source\_room\_pressure \,, \ panel\_area \,,
                  receiver_room_constant ) ( ( receiver_room_pressure ./ source_room_pressure ) .*
                  receiver room constant ) / panel_area;
         tau = transmission\_coefficient ( 10.^(spl.receiver\_room./10)*20e-6, 10.^(spl.source\_room/10)*20e-6, 10.^(spl.source\_room/10)
                  -6, panel.area, receiver room.room constant);
         TL = -10*log10 (tau);
108
         figure( ); ...
                  stem (octave band frequencies, TL, '.', 'MarkerSize', 15, 'Color', 'b'); grid on;
110
                  xlabel( 'Frequency [Hz]'); ylabel( 'Transmission Loss [dB]');
                  title ( Transmission Loss );
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) );
114
                  set ( gca, 'XScale', 'log');
                  xlim( [ 80 6e3 ] ); ylim( [ 0 55 ] );
116
118
119
120 % Clean—up
          if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
                           if (size(monitors, 1) == 1)
                                    autoArrangeFigures(2,2,1);
126
                            elseif (1 < size (monitors, 1))
                                   autoArrangeFigures(2,2,1);
128
                           end
129
         end
         fprintf( 1, \n\n\n*** Processing Complete ***\n\n\n');
```

136 **% Reference(s)**

```
2
   % Synopsis
4
   % Problem 4 - Panel Tramission Loss
10 % Environment
   close all; clear; clc;
13 % restored efault path;
   \% addpath( genpath( ^{-++} ), ^{+}-b\,\mathrm{egin}^{+-});
   addpath ( genpath ( '../40 Assignments/00 Support'), '-begin');
16
   % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineLineWidth', 0.8); set(0, 'DefaultTextInterpreter', 'Latex');
18
19
24
   format ShortG;
26
   pause ( 1 );
28
29
30 %% Define Panel
   panel.length = 80e-2; % m
   panel.E = 200e9; % Pa
panel.density = 7800; % kg/m^3
34
35 panel.v = 0.29; % Poisson's Ratio (unitless)
   \mathtt{panel.thickness} \ = \ 1.2\,\mathrm{e}\!-\!3\,; \quad \% \ \mathrm{m}
   panel.eta = 0.001; % Loss factor (unitless)
38
   c = 343; \% m/s
39
40
   rho0 = 1.21; \% kg/m^3
41
44 % Measured Panel Data
45
   46
47
48
49
   7 Problem 4a - Infinite, Rigid Panel Model with Normal Incidence
   D = (panel.E * panel.thickness.^3) / (12 * (1 - panel.v^2)); % 31.4
54
55 \quad ms = panel.density * panel.thickness; \ \% \ 9.4 \ kg/m^2
56
   wo = pi^2 / panel.length * sqrt(D / ms); % 22.6 radians/s
58
        s = wo^2 * ms; % 4,785.9 kg radians / m^2s^2
59
   fo = wo / (2*pi); \% 4 Hz
61
62
   \% Define an Anonymous function for the rigid panel with normal incidence.
64
   h_{tau}_{infinite}_{rigid}_{panel} = @(f, wo, ms, s, rho0, c, eta) + 4 ./ ((2*pi.*f*ms - s./(2*pi.*f))
         ./ (rho0 * c) ).^2 + ((wo*ms*eta) ./ (rho0*c) + 2 ).^2);
66
68 % Problem 4b - Infinite, Flexible Panel Model with Random Incidence
70 % The panel has bending waves.
   % Part (i.)
73
```

```
75 % The critical frequency.
     critical frequency = c^2 / (2*pi) * sqrt(ms / D); \% 10.22 kHz
76
   \% Verify the critical frequency using a 90 degree angle of incidence.
79
    critical frequency verify 1 = 1./(2*pi) .* sqrt( ms / D ) .* ( c / sind( 90 )).^2; \% 10.22 kHz
80
81
   % Verify the critical frequency using the properties of the panel.
    critical\_frequency\_verify\_2 = c^2 \ / \ (\ 1.8 \ * \ panel.thickness \ * \ sqrt \ (\ panel.E \ / \ (\ panel.density \ * \ (
82
        1 - panel.v^2) )); % 10.3 kHz
83
84
   % Coincidence frequency for a 75 degree angle of incidence.
85
        h coincidence frequency = @( ms, D, c, phi ) 1./(2*pi) * sqrt( ms / D ) .* ( c ./ sind( phi
87
            )).^2;
            h\_coincidence\_frequency(ms, D, c, phi); % 10,949 Hz
89
   \% Define an Anonymous function for the flexible panel with random incidence.
    (2*pi.*f*ms - D*(2*pi.*f./c).^4./(2*pi.*f)*sind(phi)^4).^2);
   \% Part (ii.) - Transmission loss for a 75 degree angle of incidence.
9.8
   f = 0.1:1:100 e3;
    figure( ); ...
        LineStyle', '-', 'Marker', 'none', 'Color', [0.00, 0.45, 0.74]'); grid on; text( 12e3, 5, sprintf( 'Coincidence\nFrequency\nof 10,494 Hz'));
        xlabel( 'Frequency [Hz] '); ylabel( 'Transmission Loss [dB]'); set( gca, 'XScale', 'log'); avis( [1,20062, 7,00])
        axis( [ 1 200e3 -5 80 ] );
       % Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
       %
       % set ( gcf, 'units', 'point', 'pos', [ 200 200 
% pos = get ( gcf, 'Position');
                                                      493*0.8 744*0.3 );
                 set ( gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3)
       %
            , pos(4)]);
       %
                     print (gcf, 'Q4 TL for 75 AOI', '-dpdf', '-r0');
   %
114
   \% \ \text{https://tex.stackexchange.com/questions/} 179382/\text{best-practices-for-using-matlab-images-in-latex}
116
118 % Part (iii.)
119
   f = 0.1:1:100 e3:
    eta = panel.eta; phi set = 0:10:90; t set = [];
    figure(); ...
        hold on;
        for phi = phi_set
           128
        end
       %
        grid on; box on;
xlabel( 'Frequency [Hz] ' ); ylabel( 'Transmission Loss [dB]' );
set( gca, 'XScale', 'log' );
        axis([1 200e3 -5 80]);
134
       %
       \% Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
       %
       , pos(4)]);
       %
                     print (gcf, 'Q4iii TL for 75 AOI', '-dpdf', '-r0');
141
   %
   \%\ https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
145
    tau_d = nanmean(t_set .* sind(2*phi_set).', 1);
```

```
148
           % Combined Transmission Loss Plot
149
                         h1 = stem(\ octave\_band\_frequencies\ ,\ TL,\ 'LineStyle',\ 'none',\ 'Marker',\ 'o',\ 'MarkerSize',\ 8,
                                     'MarkerFaceColor', 'r', 'MarkerEdgeColor', 'k'); hold on;
                         h2 = plot(f, -10*log10(h tau infinite rigid panel(f, wo, ms, s, rho0, c, panel.eta)),
                         \begin{array}{l} LineStyle', \ '-', \ 'Color', \ '\overline{k}' \ ); \\ h3 = plot(\ f, \ -10*log10(\ h\_tau\_infinite\_rigid\_panel(\ f, \ wo, \ ms, \ s, \ rho0, \ c, \ panel.eta \ ) \end{array}
                         0.74]);
                         h5 = line([16e3\ 16e3\ ], [0\ 65\ ], "Color", "r"); grid on; <math>\%\ 16\ kHz Demarcation
                         legend ( ...
158
                                     [ h1, h2, h3, h4, h5 ], ...
                                        Target Transmission Loss', ...
                                     'Infinite Rigid Panel', ...
                                      'Infinite Flexible Panel with Diffuse Incidence', ...
                                      'Finite Flexible Panel Model', ...
                                     116 kHz Demarcation , ...
                                      'Location', 'SouthOutside');
                         xlabel( 'Frequency [Hz] '); ylabel( 'Transmission Loss [dB]');
title( 'Measured Panel Transmission Losses');
                         set ( gca, 'XScale', 'log');
                         axis( [ 1 200e3 -5 80 ] );
170
                        \% Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
                        %
                       , pos(4)]);
                                                                  print(gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0');
176
178
           % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
180
181
182 % Plot Data and Model - Different Side Materials
183
            \% \ h\_tau\_infinite\_rigid\_panel\_side\_materials = @( \ f, \ wo, \ ms, \ s, \ rho0 \,, \ c \,, \ eta \,, \ n \ ) \quad (4*n) \ ./ \ ( \ (4*n) \,, \ (4*n
184
                         (2*pi.*f*ms - s./(2*pi.*f)). / (rho0 * c) ). ^2 + ( (wo*ms*eta) . / (rho0*c) + n + 1 ). ^2 );
185
           \% f = 1e-2:1e-2:20e3:
187
188
           \% \text{ phi} = 15;
           \% eta = panel.eta;
          %
           %
            % figure();
                           plot (f./ (wo / (2*pi) ), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1)), 'LineStyle', '-'); hold on; plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1/3600)), 'LineStyle', '-'); plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy and panel_side_materials (f, wo, ms, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy are grid_energy and panel_side_materials (f, wo, ms, rho0, c, panel.eta, 2600)), 'LineStyle', '-'); grid_energy are grid_ene
194
           %
           %
                            s, rho0, c, panel.eta, 3600 ) ), 'LineStyle', '-' ); grid on;
                                          %
          %
                                           legend ( ...
                                                      Same Fluid', ...
Water to Air', ...
Air to Water', ...
           %
198
          %
200 %
                                                       'Location', 'North');
           %
203 %
                               xlabel( 'Frequency [\$ frac \{omega\} \{omega o\} \$] ' ); ylabel( 'Transmission Loss [dB]' );
           %
                               title ( 'Measured Panel Transmission Losses');
                              set ( gca, 'XScale', 'log');
% axis([ 40 12e3 -5 45]);
           %
           %
208
210 % Change is Stiffness
           % figure(); ...
                              stem( octave band frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', '
```

```
MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
    %
214
          plot(\ f\ ./\ (wo\ /\ (2*pi)\ )\ ,\ -10*log10(\ h\_tau\_infinite\_rigid\_panel(\ f\ ,\ wo,\ ms,\ s\ ,\ rho0\ ,\ c\ ,\ panel.\ eta\ )\ )\ ,\ 'LineStyle'\ ,\ '-'\ );
    %
         216 %
217
219 %
                 legend ( ...
                      'Target TL Values', ...
220 %
    %
                      'Infinite Rigid Panel with Normal Incidence Sound', ...
222 %
                      'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
                     'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
223 %
224
                      'Location', 'North');
    %
226 %
            xlabel( 'Frequency [$\frac{\omega}{\omega o}$] '); ylabel( 'Transmission Loss [dB]');
            title ( 'Measured Panel Transmission Losses - Change in Stiffness ');
    %
            set ( gca, 'XScale', 'log');
    %
228
229 %
            \% \text{ axis} ( [40 \ 12 \text{ e}3 \ -5 \ 45] );
233 % Change in Mass
    % figure(); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
    %
          \begin{array}{c} \text{plot( f ./ (wo / (2*pi) ), } -10*log10( \ h\_tau\_infinite\_rigid\_panel( f , wo, ms*100, s, rho0, c , panel.eta ) ), 'LineStyle', '-' ); \\ \text{plot( f ./ (wo / (2*pi) ), } -10*log10( \ h\_tau\_infinite\_rigid\_panel( f , wo, ms, s, rho0, c , panel.eta ) ), 'LineStyle', '-' ); \\ \text{panel.eta ) ), 'LineStyle', '-' ); \\ \end{array} 
    %
238
    %
          plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*le-2, s, rho0, c, panel.eta ) ), 'LineStyle', '-');
240 %
241 %
                %
242 %
                 legend ( ...
243 %
                      'Target TL Values', ...
244 %
                     'Infinite Rigid Panel with Normal Incidence Sound', ...
245 %
                      'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
247 %
                     Location,
                                    North );
248 %
            %
            xlabel( \ 'Frequency \ [\$\frac{\omega}{\omega_o}\$] \ ' \ ); \ ylabel( \ 'Transmission \ Loss \ [dB]' \ );
249
    %
            title ( 'Measured Panel Transmission Losses - Change in Mass' );
    %
    %
            set ( gca, 'XScale', 'log' );
    %
            % axis( [40 \ 12e3 \ -5 \ 45]);
254
256 %% Change in Loss Factor
258
    % figure( ); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
    %
    %
         %
    %
          panel.eta*1e2 ) ), 'LineStyle', ':' ); plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rhoo, c,
263 %
          panel.eta*1e-2 ) ), 'LineStyle', ':' );
265 %
                 legend ( ...
266 %
                      'Target TL Values', ...
267
                      'Infinite Rigid Panel with Normal Incidence Sound', ...
                      'Infinite Rigid Panel with Normal Incidence Sound (eta * 100)', ...
    %
268
269 %
                     'Infinite Rigid Panel with Normal Incidence Sound (eta / 100)', ...
    %
                      'Location', 'North');
    %
    %
            xlabel( 'Frequency [$\frac{\omega}{\omega o}$] '); ylabel( 'Transmission Loss [dB]');
            title ( 'Measured Panel Transmission Losses - Change in Loss Factor ');
273 %
274
    %
            set ( gca, 'XScale', 'log', 'YScale', 'log');
            \% \text{ axis} ( [40 \ 12 \, e3 \ -5 \ 45] );
```

279 **%% Clean—up**

```
280
281 % if (~isempty( findobj( 'Type', 'figure' ) ) )
282 % monitors = get( 0, 'MonitorPositions' );
283 % if ( size( monitors, 1 ) == 1 )
284 % autoArrangeFigures( 2, 2, 1 );
285 % elseif ( 1 < size( monitors, 1 ) )
286 % autoArrangeFigures( 2, 2, 1 );
287 % end
288 % end
289
290
291 fprintf( 1, '\n\n\n*** Processing Complete ***\n\n\n' );
292
293
294
295 %% Reference(s)
```

```
2
      % Synopsis
 4
      % Problem 5 - Large Enclosure Design
10 % Environment
       close all; clear; clc;
13 % restored efault path;
       \% addpath( genpath( ^{-++} ), ^{+}-b\,\mathrm{egin}^{+-});
       addpath ( genpath ( '../40 Assignments/00 Support'), '-begin');
16
      % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ] set ( 0, 'DefaultFigurePaperPositionMode', 'manual');
18
19
       set( 0, 'DefaultFigureWindowStyle', 'normal' );
set( 0, 'DefaultLineLineWidth', 0.8 );
       set( 0, 'DefaultTextInterpreter', 'Latex' );
24
       format ShortG;
26
       pause ( 1 );
28
29
30 %% Define Machine
       machine.area = 3; \% m^2
       machine.absorption = 0.07; % m<sup>2</sup> or Sabin
        machine.D = 1; % Unitless - In air.
       machine.distance = 10; % m
38
40 % Measurement Data
41
       42
43 Lw = \begin{bmatrix} -105 & \overline{1}15 & 106 & 108 \end{bmatrix}
45 % figure(); ...
                    h1 = stem (octave band frequencies, Lw, 'Marker', '.', 'MarkerSize', 12, 'Color', 'r');
46
      %
47
                     h2 = line([2e2 5e3], [30 30]); grid on;
48
      %
                             legend ([ h1 h2 ], 'Current Sound Pressure Level', 'Target Sound Pressure Level', '
                 Location', 'North');
xlabel('Frequency [Hz]'); ylabel('Sound Pressure Level [dB re: 20e-6 Pa]');
49
      %
                      title ( 'Sound Power Level Versus Octave Band Center Frequency ');
       %
      %
52 %
                     axis( [ 150 6e3 0 140 ] );
       %
                      set ( gca, 'XScale', 'log');
54
      % Per Octave Band Insertion Loss
58
       Lp 10 meters = Lw + 10*log10( machine.D /( 4 * pi * machine.distance^2 ) ); % dB re: 20e-6 Pa
59
60
       \% The value of R is infinite. The machine is outside in open air.
62
       octave band IL = Lp 10 meters - 30;
67 % Define Anonymous Function for Insertion Loss
68
        \label{eq:h_IL_large} $$ h_IL_large = @(Sw, alpha_w, Si, alpha_i, TL) $$ 10*log10(1 + (Sw*alpha_w + Si*alpha_i)./(Sw*alpha_w, Si, alpha_i). $$ (Sw*alpha_w, Si, alpha_i) $$ (Sw*alpha_i) $$ (Sw*al
                   + Si)*10^(TL/10);
```

```
73 % Find Values of TL and Aborption that will Meet the Target Insertion Loss - Ground Reflecting
 75 % Assumption(s):
 76 %
 77
       %
                        The enclosure is a cube.
               1.)
 78
       %
                        The machine sits on the ground.
               2.)
 79
               2.)
                       There is no noise transmission through the ground.
 80
 81
        enclosure.dimension = 2; % m
 82
               enclosure.area = 5 * enclosure.dimension^2; % 20 m^2
 8.3
 84
       \%\ https://www.\ control noise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf
 8.5
 86 % https://www.cecoenviro.com/wp-content/uploads/2023/12/Acoustic-Enclosures-8pp-A4-web.pdf
 87
       % https://www.controlnoise.com/product/acoustic-enclosures/
 88
 89
       % Volume of the enclosure is much bigger than the machine. Diffuse sound field in the enclosure.
 91
       switch (2)
 93
 94
               case 1
 97
                      \% 250 Hz - QBV–2
                      alpha\_w \, = \, 0.27; \quad \% \ From \ specification \ sheet \, .
 98
                      TL = 22; % From specification sheet.
                             \% 500 Hz - QBV-2
                      alpha_w = 0.96; % From specification sheet.
                      TL = 28; % From specification sheet.
                             \% 1 kHz - QBV-2
                      \% alpha_w = 1.13; \% From specification sheet.
108
                      alpha \overline{w}=0.99; % From specification sheet. See comment on slide 28 of Lecture 10.
                      TL = 40; % From specification sheet.
                              \% 2 kHz - QBV-2
                      \% alpha_w = 1.08; \% From specification sheet.   
alpha_w = 0.99; \% From specification sheet. See comment on slide 28 of Lecture 10.
114
116
                      TL = 56; % From specification sheet.
                             IL_{estimates}(4) = h_{IL_{estimates}}(4) = h_{IL_{e
                                     absorption, TL);
118
                      \% 4 kHz - QBV-2
                      alpha \ w = 0.99; % From specification sheet.
                      \overline{TL} = 61; % From specification sheet.
                              IL\_estimates(5) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                                     absorption, TL );
               case 2
                      \% Note: Aboseption values are carried over from QBV-2.
128
                      \% 250 Hz - QBV-3
                      \begin{array}{lll} alpha\_w = 0.96\,; & \% \ From \ specification \ sheet\,. \\ TL = 25\,; & \% \ From \ specification \ sheet\,. \end{array}
                              IL estimates (1) = h IL large (enclosure.area, alpha w, machine.area, machine.
                                     absorption, TL );
                      \% 500 Hz - QBV-3
                       alpha\_w \, = \, 0.87\,; \quad \% \ \text{From specification sheet} \, .
                                33; % From specification sheet.
                              IL\_estimates(2) \ = \ h\_IL\_large(\ enclosure.area\ ,\ alpha\_w\ ,\ machine.area\ ,\ machine.
                                     absorption, TL );
139
                      \% 1 kHz - QBV-3
                      \% \ alpha\_w = \ 1.13\,; \quad \% \ From \ specification \ sheet \,.
                      alpha w=0.66; % From specification sheet. See comment on slide 28 of Lecture 10.
                      \overline{TL} = \overline{46}; % From specification sheet.
                              IL_{estimates}(3) = h_{IL_{arge}(enclosure.area, alpha_w, machine.area, machine.
```

```
absorption, TL);
              \% 2 kHz - QBV–3
              \% alpha w = 1.08; \% From specification sheet.
              \overline{\text{alpha w}} = 0.47; % From specification sheet. See comment on slide 28 of Lecture 10.
                    53; % From specification sheet.
148
149
                   IL estimates (4) = h IL large (enclosure.area, alpha w, machine.area, machine.
                       absorption, TL );
             \% 4 kHz - QBV-3
              \begin{array}{lll} alpha\_w = \stackrel{\circ}{0}.30\,; & \% \ \ \text{From specification sheet}\,. \\ TL = 58\,; & \% \ \ \text{From specification sheet}\,. \end{array}
                  IL\_estimates\left(5\right) \ = \ h\_IL\_large\left(\ enclosure.area\,,\ alpha\_w\,,\ machine.area\,,\ machine.
                       absorption, TL );
         case 3
158
             \% Note: Aboseption values are carried over from QBV-2.
              \% 250 Hz - QBV-3
              alpha\_w = 0.99; % From specification sheet.
162
              TL = 39; % From specification sheet.
163
                  IL\_estimates(1) \ = \ h\_IL\_large(\ enclosure.area\ ,\ alpha\_w\ ,\ machine.area\ ,\ machine.
                       absorption, TL);
             \% 500 Hz - QBV–2
              alpha \ w = 0.96; \ \% \ From \ specification \ sheet.
              \overline{TL} = 59; % From specification sheet.
                  IL\_estimates(2) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                       absorption, TL);
              \% 1 kHz - QBV-2
             \% alpha_w = 1.13; \% From specification sheet. 
 alpha_w = 0.99; \% From specification sheet. See comment on slide 28 of Lecture 10.
174
              TL = 68; % From specification sheet.
                  IL_estimates(3) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.absorption, TL);
176
              \% 2 kHz - QBV-2
             \% alpha_w = 1.08; \% From specification sheet. 
 alpha_w = 0.99; \% From specification sheet. See comment on slide 28 of Lecture 10.
178
179
              TL = 67; % From specification sheet.
                  IL estimates (4) = h IL large (enclosure.area, alpha w, machine.area, machine.
181
                       absorption, TL );
182
183
              \% 4 kHz - QBV-2
              alpha_w = 0.91; % From specification sheet.
184
185
              TL = 72; % From specification sheet.
                  186
187
188
     end
     octave band IL
                          IL estimates.' (octave band IL - IL estimates.')
192
194 % What is the most restrictive case?
195
    5% Find Values of TL and Aborption that will Meet the Target Insertion Loss - Ground with Cover
198
    % Assumption(s):
    %
               The ground is covered with the absorption material.
    %
         2.) The enclosure is a cube.
    % Clean-up
208
     if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
209
              if (size(monitors, 1) == 1)
                  autoArrangeFigures(2,2,1);
              elseif (1 < size (monitors, 1))
```

```
214
           autoArrangeFigures(2,2,1);
        end
216
  end
218
  219
223 % Reference(s)
224
     % Textheight: 744 pt. and Textwidth: 493 pt. from LaTex document
228
     %
     229
     %
              print (gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0');
  %
  \%\ https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
234
```

```
2
        % Synopsis
 4
       % Lecture 11, Wednesday, February 19, 2025
        % The compressor elevated above the ground.
 9
10
       % Environment
13
14
        close all; clear; clc;
        % restoredefaultpath;
16
        \% addpath( genpath( '' ), '-begin' ); addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
18
19
20~\% set ( 0, 'DefaultFigurePosition', [ 400~400~900~400~] ); % [ left bottom width height ] 21~ set ( 0, 'DefaultFigurePaperPositionMode', 'manual' );
        set( 0, DefaultFigureVindowStyle', 'normal');
set( 0, 'DefaultLineLineWidth', 0.8 );
set( 0, 'DefaultTextInterpreter', 'Latex');
24
26
       format ShortG;
28
       pause( 1 );
29
30 PRINT FIGURES = 0;
       %% Define Anonymous Functions
34
       h_RA_term_2 = @( \ rho0 \ , \ c \ , \ \dot{S}, \ \dot{k}, \ delta_mu \ , \ D, \ w, \ h \ ) \\ \ ( \ rho0*c/S \ ) \\ \ * \\ \ 0.288*k*3.178e-5*log10((4*k+3).178e-5*log10) + (4*k+3).178e-5*log10((4*k+3).178e-5*log10) + (4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log10((4*k+3).178e-5*log
                  \overline{S})/(\overline{p}i*h^2);
         h_RA_term_3 = @( \ rho0 \ , \ c \ , \ S, \ k \ , \ delta_mu \ , \ D, \ w, \ h \ ) \\  \  ( \ rho0*c/S \ ) \\  \  * \\  \  (0.5*S*k^2)/(2*pi); 
39
       % Define Compressor
43
44
        compressor.width = 1; \% m
         \mathtt{compressor.depth} \ = \ 1\,; \quad \% \ \mathrm{m}
46
         compressor.height = 2; % m
47
                  compressor.area = 2*(compressor.width * compressor.depth) + 2*(compressor.width * compressor.
                             height) + 2*(compressor.depth * compressor.height); \% 3 m^2
48
                   compressor.volume = compressor.width * compressor.depth * compressor.height; % m^3
49
         compressor.power level = 105; % dB re: 1e-12 Watts
         compressor frequency = 50; % Hz
53
        c = 343; \% m/s
        rho0 = 1.2; % kg/m^3 CHECK
56
58
59 % Sound Level Target
         sound_level_target = 82; % dB re: 20e-6 Pascals
61
62
65 % Define Workshop
66
       R = 40; % m^2 or Sabins
68
        7% Define Close-fitting Enclosure
```

```
73 helmholtz factor = (2 * pi * compressor.frequency) / c; % 0.92 m
 74
 75 % For a small enclosure, k*d \ll 1. Therefore d \ll 1.1.
 76 	 d = 0.75:
      d = 0.25;
 78
       % d = 1;
 79
               \% helmholtz factor * d; \% 0.69
 80
 81
       enclosure.width = compressor.width + d;
       enclosure.depth \ = \ compressor.depth \ + \ d\,; \quad \% \ m
 82
 8.3
       enclosure.height = 3; \% m; compression height is 2 m
 84
       % enclosure.height = compressor.height + d;
                enclosure.area \,=\, 2*(\,enclosure.width \,\,*\,\,enclosure.depth\,) \,\,+\,\, 2*(\,enclosure.width \,\,*\,\,enclosure\,.
 85
                       height) + 2*(enclosure.depth * enclosure.height);
 86
                enclosure.volume = enclosure.width * enclosure.depth * enclosure.height;
 87
 88
       enclosure.E = 3.6e9; % Pascals
        enclosure.thickness = 3.81e-2; % m
 8.9
       enclosure.density = 800; % kg/m<sup>3</sup>
       enclosure.poisson ratio = 0.25; % Unitless
 91
 93 % Clamped boundary conditions.
 97
       % Calculate Diffuse Sound Pressure Level
 9.8
 99
       % Assume distance is beyond the critical distance, so the distance value is
       % large and its associated term is not relevant.
        sound pressure level = 105 + 10*log10(4/R); % 95 dB SPL
106 % Calculate the Required Insertion Loss
108
       target insertion loss = sound pressure level - 82 \% 13 dB
112 % Insertion Loss
114 % For the insertion loss to be high, we need:
116 %
                        Compliance of the air to be high; volume of enclosure must be large.
               1.)
      %
               2.) Compliance of each enclosure wall to be low; low area, high stiffness, edges clamped).
118
                              AREA IS THE DOMINATE FACTOR OVER VOLUME.
       \% The correction factor for clamped walls. See Figure 12.4 on slide 9 of the Lecture 11 notes.
        aspect ratio = enclosure.height / enclosure.width; % 1.7
                correction factor = 2; % Approximate value read from the Figure 12.4.
124
        bending\_stiffness = (enclosure.E * enclosure.thickness \^{3}) / (12*(1-enclosure.poisson\_ration)) / (
                ^{2} ) ; % 1.78 e7
               h_{\text{wall\_compliance}} = @(\text{wall\_area}, \text{correction\_factor}) (0.001 * \text{wall\_area}^3 *
                       correction factor ) / bending stiffness;
128 Ca = enclosure.volume / (rho0 * c^2);
129
131 % Top
       top.area = enclosure.width * enclosure.depth;
       top.aspect ratio = max( enclosure.width, enclosure.depth ) / min( enclosure.width, enclosure.
               depth );
134
       top.correction factor = 3.8;
               top.compliance = h_wall_compliance( top.area, top.correction_factor );
136
138 % Side 1
139
        side 1.area = enclosure.depth * enclosure.height;
        side\_1.aspect\_ratio = max(\ enclosure.width\,,\ enclosure.height\ )\ /\ min(\ enclosure.width\,,\ enclosure.width).
               height);
141
        side 1.correction factor = 2;
               __side_1.compliance = h_wall_compliance( side_1.area, side_1.correction_factor );
145
       side 2.compliance = side 1.compliance;
```

```
148
            % Side 3
             side 3.area = enclosure.width * enclosure.height;
                           _3.aspect_ratio = max( enclosure.width, enclosure.height ) / min( enclosure.width, enclosure.
                          height);
              side 3. correction factor = 2;
                          side_3.compliance = h_wall_compliance( side_3.area, side_3.correction_factor );
154
            % Side 4
              side 4.compliance = side 3.compliance;
158
              estimated insertion loss = 20*log10 ( 1 + Ca / (top.compliance + 2*side 1.compliance + 2*side 3.
                         compliance)); -\% 59.2 dB
            % Compliance of the Air Intake
             \begin{array}{l} air\_intake\_radius = 10\,e-2; \quad \% \ m \\ air\_intake\_thickness = enclosure.thickness; \quad \% \ m \\ air\_intake\_frequency = 50; \quad \% \ Hz \end{array}
165
166
                          air_intake_angular_frequency = 2*pi*air_intake_frequency; % radians/s
             viscosity = 1.5 e-5; \% m^2/s
            h = 0.3; % CHECK
173
            f = 50;
                         174
                          term\_2 = h\_RA\_term\_2 ( rho0 , c , pi*(air\_intake\_radius*2)^2/4 , 2*pi*f/c , sqrt( (2*3.178e-5)) + (2*3.178e-5) + (2*3.178e-5
                         [-rho0], [-pi * 0.1, 2*pi*f, 0.3];
                                      impedance.real = term 1 + term 2 + term 3;
178
           % Deng (1998)
181
             epsilon = 1;
182
                         L o = air intake radius * (1.27 / (1 + 1.92 * epsilon) - 0.086);
184
             L e = enclosure.thickness + 2*L o;
185
                         impedance.imaginary = 1j * rho0 * (2 * pi * f) * L_e / ( pi*0.1^2/4 );
186
187
             impedance.net \ = \ impedance.real \ + \ impedance.imaginary \, ;
188
189
                          compliance_of_hole = 1 / impedance.net;
                                      Cl = a\overline{b}s(\overline{compliance\_of\_hole});
              estimated\_insertion\_loss
             196
             13 - estimated insertion loss with hole;
198
199
              critical\_frequency = c^2/(2*pi)*sqrt (\ enclosure.density * enclosure.thickness / bending\_stiffness | \ density = critical\_frequency | \ density = critical\_frequen
            \% The critical frequency is 25 Hz.
204
            % The frequency of the compressor is 50 Hz.
206
210 % Clean—up
211
              if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
                                      if (size(monitors, 1) == 1)
                                                  autoArrangeFigures(2,2,1);
216
                                       elseif (1 < size (monitors, 1))
```