

Problem 1 - Modal Behaviour of a Cylindrical Room

The Matlab code for this problem is listed in Appendix 1.

Problem 1a

Table 1 lists the ten lowest resonance mode orders for the room and the respective frequency.

Index	Mode (n_x, n_θ, n_r)	Frequency [Hz]
0	0, 0, 0	0
1	1, 0, 0	17.2
2	0, 1, 0	33.5
3	2, 0, 0	34.3
4	1, 1, 0	37.6
5	2, 1, 0	48.0
6	3, 0, 0	51.5
7	0, 2, 0	55.6
8	1, 2, 0	58.2
9	3, 1, 0	61.4
10	2, 2, 0	65.3

Table 1: Resonant modes of the cylindrical room.

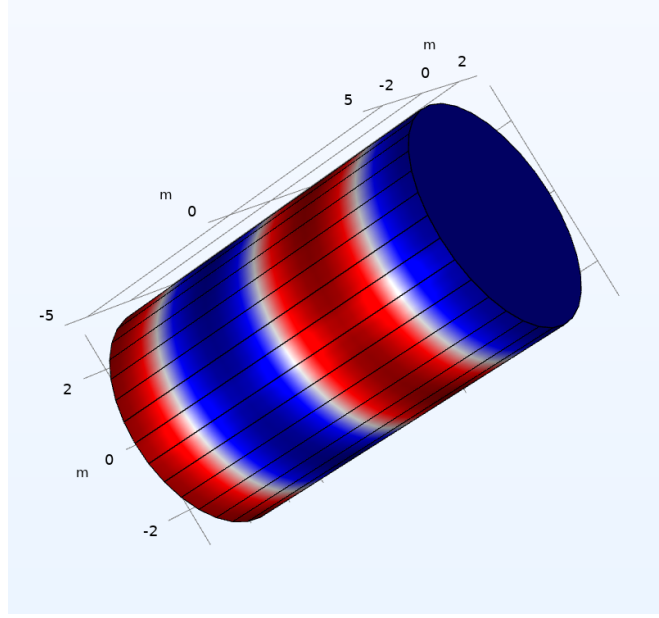
Problem 1b

The two closest modes are (3, 0, 0) and (0, 2, 0) with frequencies of 51.5 Hz and 55.6 Hz, respectively.

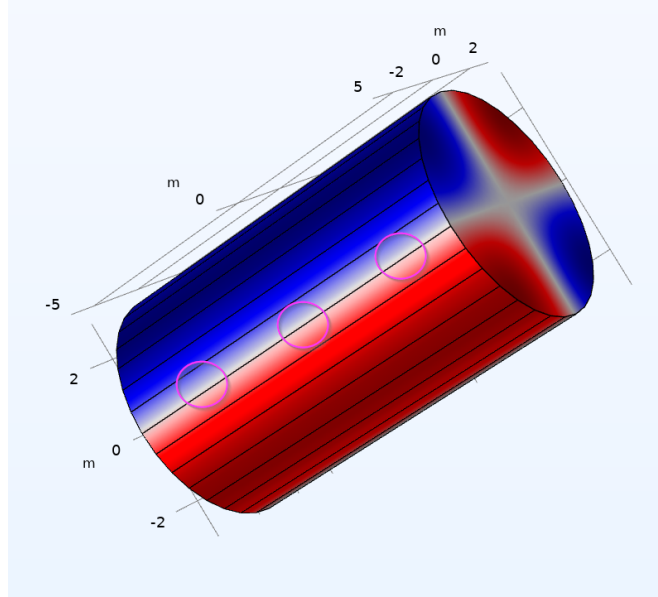
Problem 1c

Figure 1 illustrates the (3, 0, 0) and (0, 2, 0) modes. The white lines in each figure show the modal lines for that mode. **The machine can be placed where the modal lines for each mode overlap.** The figures were produced using the Room Eigenmode Simulator Version 1.1 software package.

The pink rings in Figure 1b indicate 3 possible places where the machine could be placed. These points coincide with the three modal planes shown in Figure 1a. Theoretically, there are an infinite number of places where the machine could be placed. However, placement would take into account practical considerations such as accessibility, etc.



(a) Mode (3, 0, 0)



(b) Mode (0, 2, 0)

Figure 1: Visualization of modes. (a.) Mode (3, 0, 0). (b.) Model (0, 2, 0). The pink circles in [1b](#) illustrate a few modal line intersections where the machine could be placed.

Problem 2 - Sabine Room

The Matlab code for this problem is listed in Appendix 2.

Problem 2a

The reverberant field sound pressure level is approximately 98.3 dB SPL.

Problem 2b

Figure 2 shows the direct, reverberant, and total sound pressure levels for a 25 mW, 125 Hz, broadband, omnidirectional source placed centrally in the room (i.e. the directivity factor is 1).

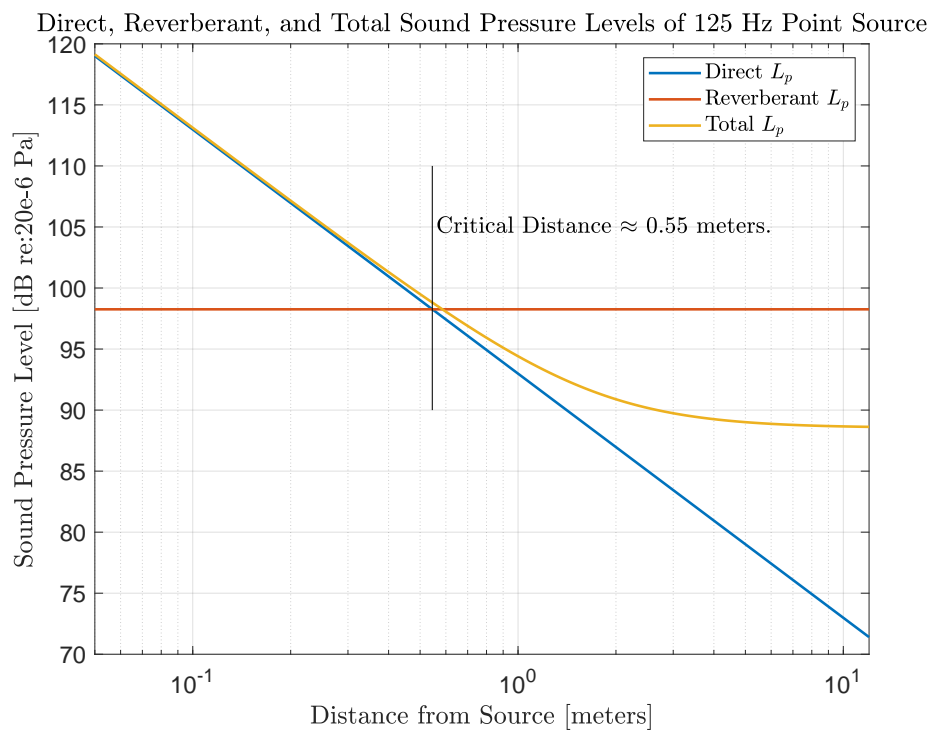


Figure 2: Sound levels for the room produced by a 25 mW, 125 Hz omnidirectional, broadband source.

Problem 3 - Transmission Loss Measurement

The Matlab code for this problem is listed in Appendix 3.

Figure 3 shows the average absorption per octave band based on the T60 data. The calibration plate isolates the receiver room and the absorption calculation does not consider the calibration plate.

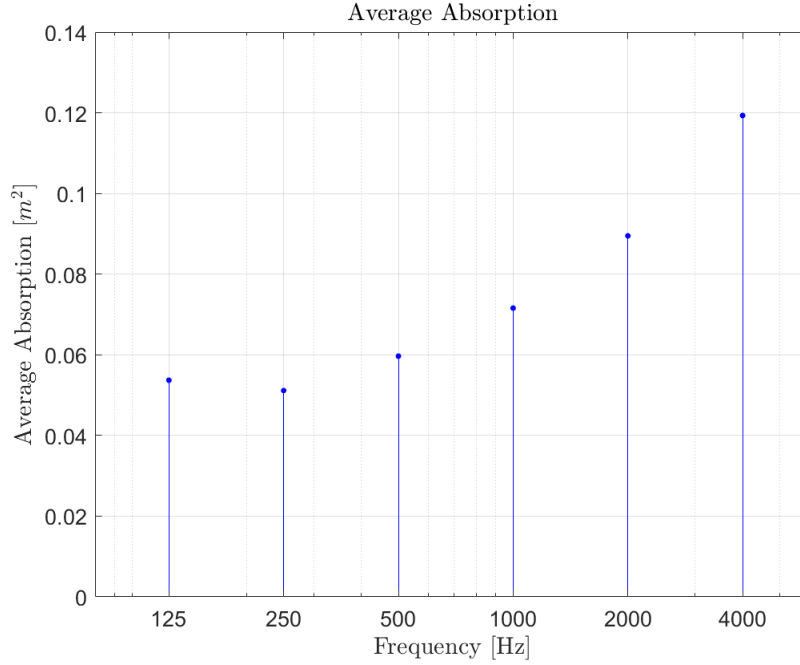


Figure 3: Average absorption per octave band.

Figure 4 shows the transmission loss per octave band.

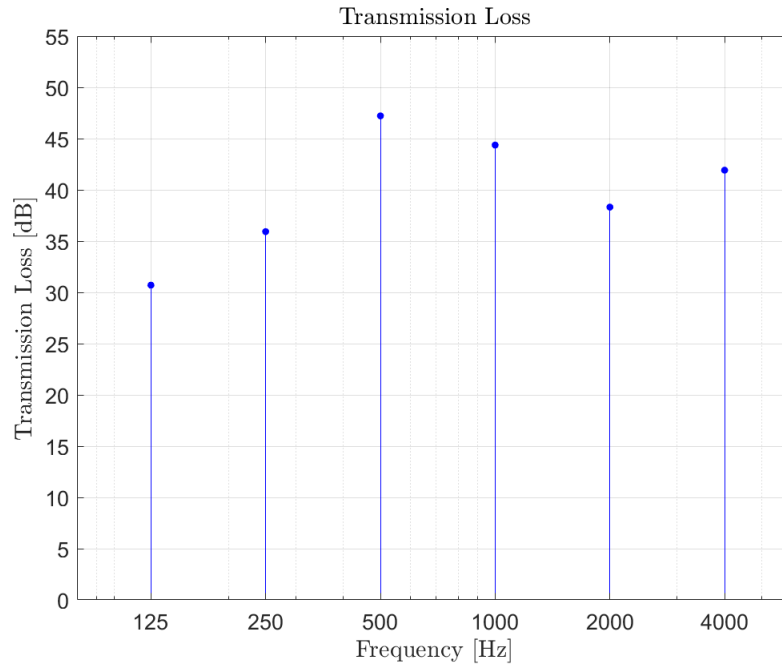


Figure 4: Transmission loss per octave band.

Problem 4 - Panel Transmission Loss

The Matlab code for this problem is listed in Appendix 4.

Problem 4a

The resonance frequency, f_o , of the galvanized steel panel is 4 Hz or $22.6 \frac{\text{radians}}{\text{s}}$.

Problem 4b

i - Critical Frequency and Coincidence Frequency at 75°

The critical frequency is 10,216 Hz and the coincidence frequency at 75° is 10,494 Hz.

ii - Transmission Loss at Angle of Incidence of 75°

Figure 5 shows the transmission loss for an angle of incidence of 75° .

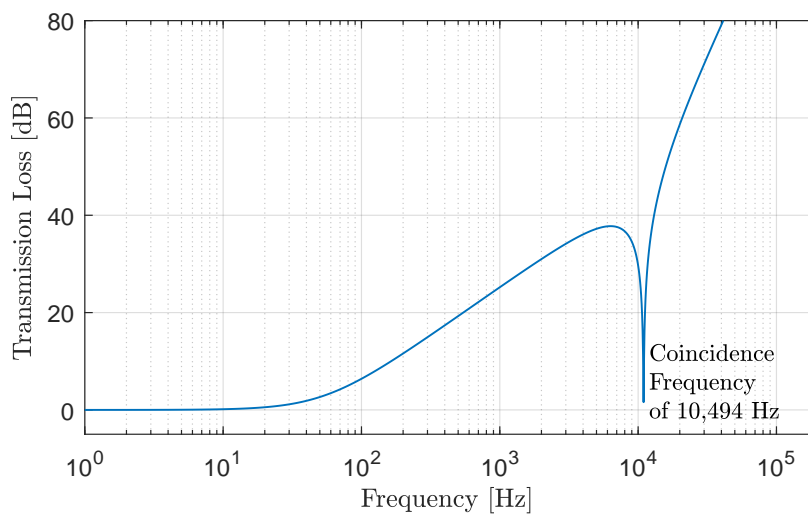


Figure 5: Flexible Panel Transmission Loss for a 75° Incidence Angle

iii - Transmission Loss for Angles of Incidence between $0-90^\circ$

Figure 6 shows the transmission loss angles of incidence from 0 to 90° in steps of 10° .

iv - Diffuse Transmission Loss

See the Matlab code in the Appendix 4

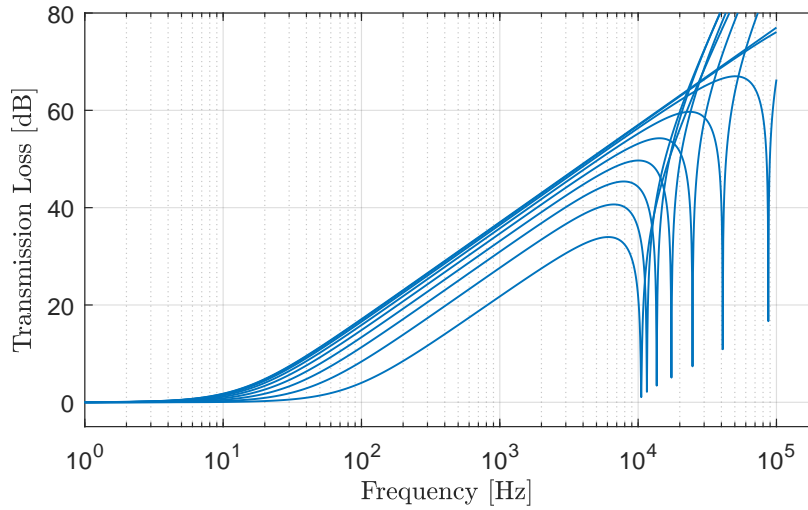


Figure 6: Flexible Panel Transmission Loss for angles of incidence between 0 and 90°.

Problem 4c

See the Matlab code in the Appendix 4

Problem 4d

Figure 7 shows the transmission loss angles of incidence from 0 to 90° in steps of 10°.

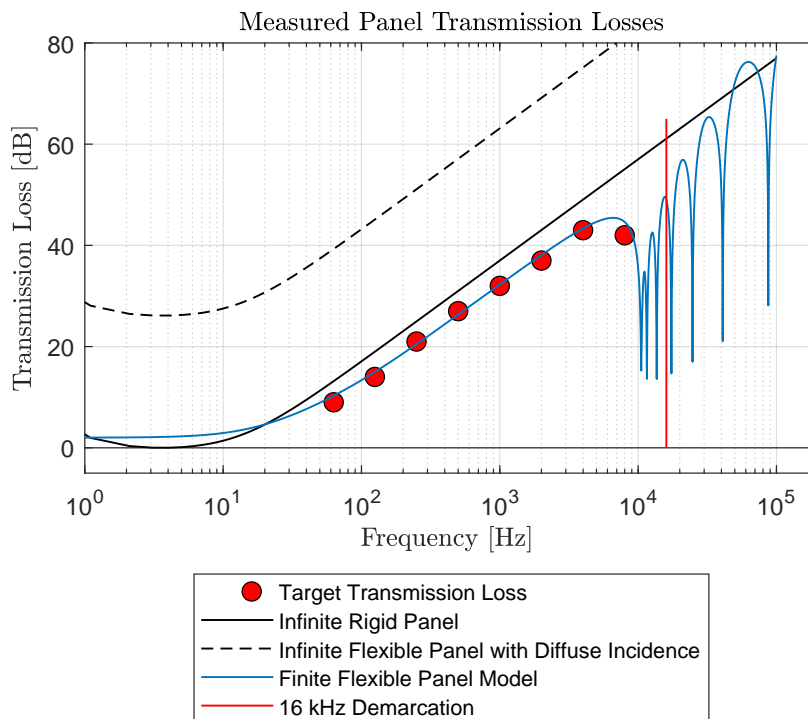


Figure 7: Measured data and the modeled responses.

The finite flexible panel appears to be the most appropriate model. As noted in class, the measured transmission loss at 8 kHz is smaller than the loss at 4 kHz. This indicates that the loss at 16 kHz should be less than the response of the infinite rigid panel at 16 kHz.

Problem 5 - Large Enclosure Design

The Matlab code for this problem is listed in Appendix 5.

My enclosure is a 2 m cube that sits on the ground (5 sides of enclosure material) over the machine. The machine is suspended above the pad (directivity factor of unity). It is assumed that there is no noise transmission through the ground.

Table 2 lists the target insertion losses, the calculated insertion losses for four materials, and the loss difference between the target and each type of material. *A positive value indicates that the target insertion loss for the given octave band was not met.*

Figure 8 shows calculated insertion loss differences for the data in Table 2.

Octave Band [Hz]	Target IL [dB]	QBV 2 [dB]	QBV 3 [dB]	HTL (100MM) [dB]	HTL 4 [dB]
250	44	28.0	19.7	10.6	5.6
500	54	26.7	22.2	6.6	-4.4
1,000	45	5.6	1.4	-15.4	-22.4
2,000	47	-8.4	-2.2	-18.4	-19.4
4,000	58	-2.4	5.7	-11.0	-13.0

Table 2: Calculated insertion losses for the 4 enclosure materials.

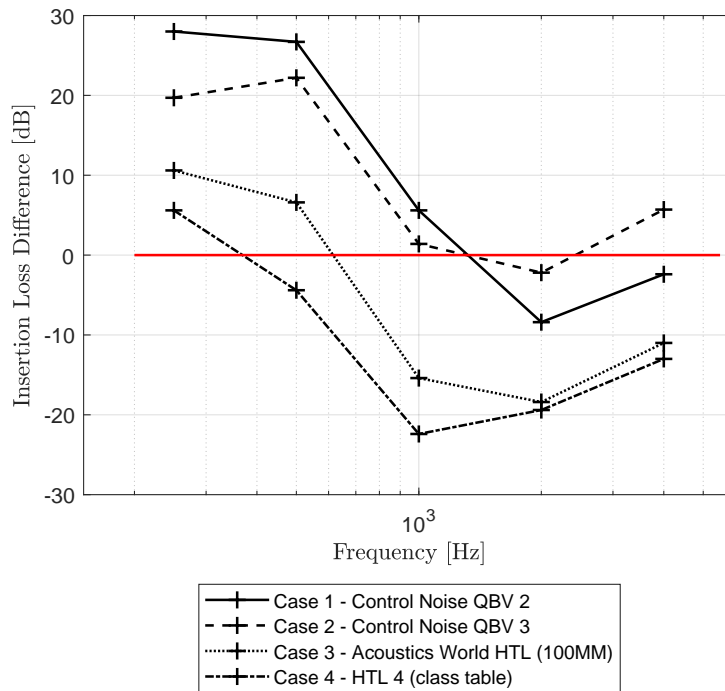


Figure 8: Insertion loss differences.

The most restrictive case given the 2 cubic-meter, 5-sided enclosure, is the HTL 4 material, Case 4, which was presented in class. The target insertion loss was reached by all of the octave bands except the 250 Hz band.

With the same enclosure dimensions and machine orientation, the HTL (100MM) material, Case 3, was found to be the second best material, not meeting the 250 Hz and 500 Hz targets. Figure 9 shows the transmission loss and absorption coefficient data for the material selected from [Acoustics World](#).

The QBV-2 and QBV-3 , Case 1 and Case 2, respectively, had the poorest performance. Figure 10 shows the transmission loss and absorption coefficient data for these material from **Control Noise**.

Using the HTL 4 material from class, a cube with 2 m sides appeared to produce the optimal insertion loss for the 250 Hz octave band. Making the size of the enclosure larger does not reduce this insertion loss and does not seem to be practical. A supplementary approach for this octave band should be considered.

NRC Rating								
Sound Absorption Coefficients (ASTM C423)								
Acoustic Panel Type	Panel Construction	125 Hz	250Hz	500Hz	1000 Hz	2000 Hz	4000 Hz	NRC
STL (100MM)	18 ga. solid / 22 ga. perforated	0.60	1.13	1.12	1.09	1.03	0.91	1.00
STL (100MM)	16 ga. solid / 22 ga. perforated	0.60	1.13	1.12	1.09	1.03	0.91	1.00
HTL (100MM)	16 ga. solid / 22 ga. perforated with HD Soundbloc Layer	0.60	1.13	1.12	1.09	1.03	0.91	1.00

STC Rating								
Sound Transmission Class								
Acoustic Panel Type	Panel Construction	125 Hz	250Hz	500Hz	1000 Hz	2000 Hz	4000 Hz	STC
STL (100MM)	18 ga. solid / 22 ga. perforated	21	28	39	48	56	58	40
STL (100MM)	16 ga. solid / 22 ga. perforated	24	32	41	51	60	66	43
HTL (100MM)	16 ga. solid / 22 ga. perforated with HD Soundbloc Layer	27	34	48	61	66	70	48

Figure 9: HTL (100MM) data from Acoustics World.

ACOUSTICAL DATA:

The **most effective** noise reduction products combine **both sound absorption and noise barrier properties**. Tested under strict compliance to appropriate ASTM standards, we offer the following results:

Sound Transmission Loss (dB) per Octave Band Frequency									
NetWell Model #	THK.	WT.	125	250	500	1000	2000	4000	STC
QBV-1	1"	1.3	11	16	24	30	35	35	27
QBV-2	2"	1.5	13	20	29	40	50	55	32
QBV-3	2.5"	2	19	25	33	46	53	58	37
QBS-1	2"	1.5	12	16	27	40	44	43	29
QBS-2	2"	2.5	19	22	28	40	56	61	33
Roof Panel	2"	2	18	24	28	37	45	46	31

Per ASTM E 90

Sound Absorption Data – Absorber Component Random Incident Sound Absorption Octave Band Center Frequencies (Hz)								
Product	THK.	125	250	500	1000	2000	4000	NRC
QBV-1	1"	.12	.47	.85	.84	.64	.62	.70
QBV-2	2"	.07	.27	.96	1.13	1.08	.99	.85
QBS-1 & 2	2"	.45	.96	.87	.66	.47	.30	.75
QB-4	4"	.21	.89	1.09	1.17	1.13	1.07	1.05

Per ASTM C 423

Flammability Ratings			
Product	Descriptor	Flame Spread	Smoke Developed
QBS-1	Vinyl faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced loaded vinyl barrier septum	23	30
QBS-HT	Silicone faced 1" quilted fiberglass on both sides of a 1 lb. PSF non-reinforced noise barrier septum	4	19
QBV-2	Vinyl faced 2" quilt on one side of a 1 lb. reinforced loaded vinyl noise barrier	23	12
QBV-1	Vinyl faced 1" quilt on one side of a 1lb. reinforced loaded vinyl noise barrier	23	30

Above table shows flame spread and smoke developed ratings per ASTM Designation E84; Surface Burning Characteristics of Building Materials. Note: Class A rating applies to products with a flame spread index of 25 or less, and a smoke developed index of 450 or less. Additional products tested to ASTM E 162 and ASTM E 662; test reports available on request.

Figure 10: QBV-2 and QBV-3 data from Control Noise.

Problem 6 - Close-fitting Enclosure Design

The Matlab code for this problem is listed in Appendix 6.

The required target insertion loss is 13 dB. This is estimated with the given data and the assumption that the sound measurement distance is beyond the critical distance (i.e., in the diffuse field).

Table 3 lists the dimensions of the designed enclosure.

Octave Band [Hz]	Target IL [dB]	QBV 2 [dB]	QBV 3 [dB]	HTL (100MM) [dB]	HTL 4 [dB]
250	44	28.0	19.7	10.6	5.6
500	54	26.7	22.2	6.6	-4.4
1,000	45	5.6	1.4	-15.4	-22.4
2,000	47	-8.4	-2.2	-18.4	-19.4
4,000	58	-2.4	5.7	-11.0	-13.0

Table 3: Dimensions of the designed enclosure.

Table 4 lists the design parameters for the design enclosure.

Octave Band [Hz]	Target IL [dB]	QBV 2 [dB]	QBV 3 [dB]	HTL (100MM) [dB]	HTL 4 [dB]
250	44	28.0	19.7	10.6	5.6
500	54	26.7	22.2	6.6	-4.4
1,000	45	5.6	1.4	-15.4	-22.4
2,000	47	-8.4	-2.2	-18.4	-19.4
4,000	58	-2.4	5.7	-11.0	-13.0

Table 4: Enclosure design summary.

The estimated insertion loss without the hole is 14.2 dB, which exceeds the target loss of 13.

The estimated insertion loss with the hole is 11.8 dB, based on the hole depth correction of Deng (1998). The hole reduces the required insertion loss. The intake silencer needs to provide 1.2 dB of insertion loss.

1 Appendix - Matlab Code for Problem 1

```
1
2
3
4 %% Synopsis
5
6 % Problem 1 – Modal Behaviour of a Cylindrical Room
7
8
9
10 %% Environment
11
12 close all; clear; clc;
13 % restoredefaultpath;
14
15 % addpath( genpath( '' ), '-begin' );
16 addpath( genpath( './00 Support' ), '-begin' );
17
18 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
19 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
20 set( 0, 'DefaultFigureWindowStyle', 'normal' );
21 set( 0, 'DefaultLineWidth', 1.5 );
22 set( 0, 'DefaultTextInterpreter', 'Latex' );
23
24 format ShortG;
25
26 pause( 1 );
27
28
29
30 %% Define Room
31
32 room.radius = 3; % m
33 room.length = 10; % m
34
35
36
37 %% Test Circular Mode Function
38
39 % psi = circular_mode_shape( 3, 1, 2, false ); % 3.7261 – CHECKED FROM CLASS (PLOT NOT CREATED)
40 % psi = circular_mode_shape( 3, 1, 2, true ); % 3.7261 – CHECKED FROM CLASS (PLOT CREATED)
41
42
43
44 %% Define Anonymous Function for the Natural Frequencies
45
46 h_natural_frequencies = @( c, nx, ntheta, nr, Lx, cylinder_radius, plot_flag ) (c/2) .* sqrt( (
    nx/Lx).^2 + (circular_mode_shape(nr, ntheta, cylinder_radius, plot_flag)/cylinder_radius)
    .^2 );
47
48
49
50 %% Calculate the Natural Frequencies
51
52 % The maximum number of radial modes is 5 (indexed from 0 to 4).
53 % The maximum number of angular modes is 8 (indexed from 0 to 7).
54
55 NX_SIZE = 20;
56 NTHETA_SIZE = 7;
57 NR_SIZE = 4;
58 natural_frequencies = nan( NX_SIZE, NTHETA_SIZE, NR_SIZE );
59
60 for nx = 0:1:NX_SIZE
61     for ntheta = 0:1:NTHETA_SIZE
62         for nr = 0:1:NR_SIZE
63             natural_frequencies( nx+1, ntheta+1, nr+1 ) = h_natural_frequencies( 343, nx, ntheta,
                nr, 10, 3, false );
64         end
65     end
66 end
67
68
69
70 %% Part a – Find 10 Lowest Resonance Frequencies
71
72 NUMBER_OF_LOWEST_FREQUENCIES = 11;
```

```

73     mode_indices = ( 1:1:NUMBER_OF_LOWEST_FREQUENCIES ).';
74
75 [ sortedValues, sortedIndices ] = sort( natural_frequencies(:) ); % 21-by-8-by-5 -> 840 elements
76
77 smallestValues = sortedValues( 1:NUMBER_OF_LOWEST_FREQUENCIES );
78 % [ mode_indices    round( smallestValues, 1 ) ]
79 %
80 % 1            0
81 % 2           17.2
82 % 3           33.5
83 % 4           34.3
84 % 5           37.6
85 % 6           47.9
86 % 7           51.5
87 % 8           55.6
88 % 9           58.2
89 % 10          61.4
90 % 11          65.3
91
92 smallestIndices = sortedIndices( 1:NUMBER_OF_LOWEST_FREQUENCIES );
93
94 [ x, y, z ] = ind2sub( size(natural_frequencies), smallestIndices );
95 % ( [ x y z ] - 1 )
96
97 % Verify the calculated mode indices.
98 h_natural_frequencies( 343, 0, 0, 0, 10, 3, false ); % 0 Hz
99 h_natural_frequencies( 343, 1, 0, 0, 10, 3, false ); % 17.2 Hz
100 h_natural_frequencies( 343, 0, 1, 0, 10, 3, false ); % 33.5 Hz
101 h_natural_frequencies( 343, 2, 0, 0, 10, 3, false ); % 34.3 Hz
102 h_natural_frequencies( 343, 1, 1, 0, 10, 3, false ); % 37.6 Hz
103 h_natural_frequencies( 343, 2, 1, 0, 10, 3, false ); % 48.0 Hz
104 h_natural_frequencies( 343, 3, 0, 0, 10, 3, false ); % 51.5 Hz
105 h_natural_frequencies( 343, 0, 2, 0, 10, 3, false ); % 55.6 Hz
106 h_natural_frequencies( 343, 1, 2, 0, 10, 3, false ); % 58.2 Hz
107 h_natural_frequencies( 343, 3, 1, 0, 10, 3, false ); % 61.4 Hz
108 h_natural_frequencies( 343, 2, 2, 0, 10, 3, false ); % 65.3 Hz
109
110
111
112 %% Part b – Two
113
114 % [ (1:11).' abs( smallestValues - 53 ) ]
115
116 temp = [ x y z ] - 1; temp( 7:8, :, : )
117
118 h_natural_frequencies( 343, 3, 0, 0, 10, 3, false ); % 51.5 Hz, (3, 0, 0)
119 h_natural_frequencies( 343, 0, 2, 0, 10, 3, false ); % 55.6 Hz, (0, 2, 0)
120
121
122
123 %% Part c
124
125 % See the report.
126
127
128
129 %% Clean-up
130
131 fprintf( 1, '\n\n*** Processing Complete ***\n\n' );
132
133
134
135 %% Reference(s)
136
137 % https://www.mathworks.com/matlabcentral/answers/1883747-how-to-find-the-5-minimum-values-in-a-multidimensional-matrix-and-the-indices-to-which-these-entries

```

2 Appendix - Matlab Code for Problem 2

```
1
2
3
4 %% Synopsis
5
6 % Problem 2 — Sabine Room
7
8
9
10 %% Environment
11
12 close all; clear; clc;
13 % restoredefaultpath;
14
15 % addpath( genpath( '' ), '-begin' );
16 addpath( genpath( '../00 Support' ), '-begin' );
17
18 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
19 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
20 set( 0, 'DefaultFigureWindowStyle', 'normal' );
21 set( 0, 'DefaultLineLineWidth', 1.5 );
22 set( 0, 'DefaultTextInterpreter', 'Latex' );
23
24 format ShortG;
25
26 pause( 1 );
27
28
29
30 %% Define Room
31
32 room.width = 8; % m
33 room.length = 6; % m
34 room.height = 3; % m
35 room.volume = room.width * room.length * room.height; % 144 m^3
36 room.area = 2*(room.width*room.height) + 2*(room.length*room.height) + 2*(room.width*room.
    length); % 180 m^2
37
38 alpha_average_walls_and_floor = 0.05; % For the walls and the floor.
39 alpha_average_ceiling = 0.15; % For the ceiling.
40
41 % For the 125 Hz octave band.
42
43
44
45 %% Part a — Estimate the Reverberant Sound Pressure Level
46
47 Lw = 10*log10( 25e-3 / 1e-12 ); % 103.98 dB
48
49 average_absorption_coefficient = ( (room.width*room.length)*alpha_average_ceiling + (room.width
    *room.length + 2*(room.width*room.height) + 2*(room.length*room.height) ) *
    alpha_average_walls_and_floor ) / room.area; % 0.076667 unitless
50
51 room_constant = room.area * average_absorption_coefficient / ( 1 - average_absorption_coefficient
    ); % 14.9 m^2 or Sabin
52
53
54 sound_pressure_level = Lw + 10*log10( 4 / room_constant ); % 98.3 dB
55
56
57
58 %% Part b — Calculate the Critical Distance
59
60 D0 = 1;
61
62 r = 0:0.05:12; % m
63
64 h_Lp_direct = @( Lw, D0, r ) Lw + 10*log10( D0./(4.*pi.*r.^2) );
65 h_Lp_reverberant = @( Lw, room_constant ) Lw + 10*log10( 4 ./ room_constant );
66 %
67 h_Lp_net = @( Lw, D0, r, room_constant ) Lw + 10*log10( D0./(4.*pi.*r.^2) + 4/room_constant ) +
    10*log10( 343*1.2/400 );
68
69
70 figure( ); ...
```

```

71     h1 = plot( r, h_Lp_direct( Lw, D0, r ) ); hold on;
72     h2 = plot( r, ones( size(r) ).*h_Lp_reverberant( Lw, room_constant ) );
73     h3 = plot( r, h_Lp_net( Lw, D0, r, room.volume ) ); grid on;
74     legend( [ h1, h2 h3 ], { 'Direct $L_p$', 'Reverberant $L_p$', 'Total $L_p$' }, '
        Interpreter', 'Latex' );
75
76     %
77     text( 0.56, 105, 'Critical Distance $\approx$ 0.55 meters.', 'Interpreter', 'Latex' );
78     line( [ 0.545 0.545 ], [ 90 110 ], 'Color', 'k', 'LineWidth', 0.6 );
79
80     xlabel( 'Distance from Source [meters]' ); ylabel( 'Sound Pressure Level [dB re:20e-6 Pa]' )
81     ;
82     title( 'Direct, Reverberant, and Total Sound Pressure Levels of 125 Hz Point Source' );
83     %
84     set( gca, 'XScale', 'log' );
85
86 % Estimate the critical distance (see page 84 of "06-Indoors.pdf" notes for ACS 537).
87 rc = 0.141 * sqrt( D0 * room_constant ); % 0.5451 meters
88
89 return
90 %% Clean-up
91
92 if ( ~isempty( findobj( 'Type', 'figure' ) ) )
93     monitors = get( 0, 'MonitorPositions' );
94     if ( size( monitors, 1 ) == 1 )
95         autoArrangeFigures( 2, 2, 1 );
96     elseif ( 1 < size( monitors, 1 ) )
97         autoArrangeFigures( 2, 2, 1 );
98     end
99 end
100
101 fprintf( 1, '\n\n*** Processing Complete ***\n\n' );
102
103
104
105
106 %% Reference(s)

```

3 Appendix - Matlab Code for Problem 3

```
1
2
3
4 %% Synopsis
5
6 % Question 3 – Transmission Loss Measurement
7
8
9 % Note(s):
10 %
11 %     1.) Lp1 depends on the transmission loss.
12 %
13 %         If the transmission loss is low, then more energy goes to room 2 (i.e., the receiver room
14 %         ).
15 %
16 %         The noise reduction from the source room to the receiver room.
17 %
18 %         Adding the barrier will change the level in the source room. Typically making the sound
19 %         level higher in the source room.
20
21 %% Environment
22
23 close all; clear; clc;
24 % restoredefaultpath;
25
26 % addpath( genpath( '' ), '-begin' );
27 addpath( genpath( '../00 Support' ), '-begin' );
28
29 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
30 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
31 set( 0, 'DefaultFigureWindowStyle', 'normal' );
32 set( 0, 'DefaultLineLineWidth', 1.2 );
33 set( 0, 'DefaultLineMarker', 'x' );
34 set( 0, 'DefaultLineMarkerSize', 15 );
35 % set( 0, 'DefaultAxesLineStyleOrder', { '-' '--o' '+' } );
36 set( 0, 'DefaultTextInterpreter', 'Latex' );
37
38 format ShortG;
39
40 pause( 1 );
41
42
43
44 %% Dimensions of Rooms and Panel
45
46 room.length = 4; % m
47 room.width = 4; % m
48 room.height = 4; % m
49 room.volume = room.length * room.width * room.height; % 64 m^3
50 room.area = 2*(room.length * room.width) + 2*(room.length * room.height) + 2*(room.width *
51     room.height); % 96 m^2
52
53 panel.width = 0.8; % m
54 panel.height = 0.8; % m
55 panel.area = panel.width * panel.height; % 0.64 m^2
56
57 c = 343; % m/s
58
59
60 %% Measurement Data
61
62 octave_band_frequencies = [ 125 250 500 1000 2000 4000 ].'; % Hz
63 T60 = [ 2.0 2.1 1.8 1.5 1.2 0.9 ].'; % seconds
64 spl.source_room = [ 90 95 103 105 100 93 ].'; % dB re: 20e-6 Pa
65 spl.receiver_room = [ 50 50 46 50 50 38 ].'; % dB re: 20e-6 Pa
66 % [ octave_band_frequencies T60 spl.source_room spl.receiver_room (spl.source_room - spl.
67     receiver_room) ]
68
69
70 %% Calculate Average Absorption in the Receiver Room using Reverberation Time Measurements
71
```

```

72 average_absorption = @( volume, area, c, T60 ) ( 55.25 .* volume ) ./ ( area .* c .* T60 );
73
74 receiver_room.average_absorption = average_absorption( room.volume, room.area, c, T60 );
75
76 % Assumption: Calibration panel has very high transmission loss.
77
78 figure( ); ...
79 stem( octave_band_frequencies, receiver_room.average_absorption, 'Marker', '.', 'MarkerSize',
      12, 'Color', 'b' ); grid on;
80 xlabel( 'Frequency [Hz]' ); ylabel( 'Average Absorption [m^2]' );
81 title( 'Average Absorption' );
82 %
83 xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) );
84 set( gca, 'XScale', 'log' );
85 xlim( [ 80 6e3 ] ); ylim( [ 0 0.14 ] );
86
87
88


---


89 %% Calculate the Receiver Room Constant
90
91 % The calibration plate isolates the receiver room.
92
93 % The receiver room does not consider the calibration plate.
94
95 room_constant = @( average_absorption, area ) ( average_absorption * area ) ./ ( 1 -
      average_absorption ); % Unitless
96
97 receiver_room.room_constant = room_constant( receiver_room.average_absorption, room.area );
98
99
100


---


101 %% Calculate the Transmission Loss in Each Octave Band
102
103 transmission_coefficient = @( receiver_room_pressure, source_room_pressure, panel_area,
      receiver_room_constant ) ( ( receiver_room_pressure ./ source_room_pressure ) .*
      receiver_room_constant ) ./ panel_area;
104
105 tau = transmission_coefficient( 10.^(spl.receiver_room./10)*20e-6, 10.^(spl.source_room./10)*20e
      -6, panel.area, receiver_room.room_constant );
106
107 TL = -10*log10( tau );
108
109 figure( ); ...
110 stem( octave_band_frequencies, TL, '.', 'MarkerSize', 15, 'Color', 'b' ); grid on;
111 xlabel( 'Frequency [Hz]' ); ylabel( 'Transmission Loss [dB]' );
112 title( 'Transmission Loss' );
113 %
114 xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) );
115 set( gca, 'XScale', 'log' );
116 xlim( [ 80 6e3 ] ); ylim( [ 0 55 ] );
117
118
119


---


120 %% Clean-up
121
122 if ( ~isempty( findobj( 'Type', 'figure' ) ) )
123     monitors = get( 0, 'MonitorPositions' );
124     if ( size( monitors, 1 ) == 1 )
125         autoArrangeFigures( 2, 2, 1 );
126     elseif ( 1 < size( monitors, 1 ) )
127         autoArrangeFigures( 2, 2, 1 );
128     end
129 end
130
131
132 fprintf( 1, '\n\n\n*** Processing Complete ***\n\n\n' );
133
134
135


---


136 %% Reference(s)

```

4 Appendix - Matlab Code for Problem 4

```
1
2
3
4 %% Synopsis
5
6 % Problem 4 — Panel Transmission Loss
7
8
9
10 %% Environment
11
12 close all; clear; clc;
13 % restoredefaultpath;
14
15 % addpath( genpath( '' ), '-begin' );
16 addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
17
18 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
19 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
20 set( 0, 'DefaultFigureWindowStyle', 'normal' );
21 set( 0, 'DefaultLineLineWidth', 0.8 );
22 set( 0, 'DefaultTextInterpreter', 'Latex' );
23
24 format ShortG;
25
26 pause( 1 );
27
28
29
30 %% Define Panel
31
32 panel.length = 80e-2; % m
33 panel.E = 200e9; % Pa
34 panel.density = 7800; % kg/m^3
35 panel.v = 0.29; % Poisson's Ratio (unitless)
36 panel.thickness = 1.2e-3; % m
37 panel.eta = 0.001; % Loss factor (unitless)
38
39 c = 343; % m/s
40 rho0 = 1.21; % kg/m^3
41
42
43
44 %% Measured Panel Data
45
46 octave_band_frequencies = [ 63 125 250 500 1000 2000 4000 8000 ].'; % Hz
47 TL = [ 9 14 21 27 32 37 43 42 ].'; % dB
48
49
50
51 %% Problem 4a — Infinite, Rigid Panel Model with Normal Incidence
52
53 D = ( panel.E * panel.thickness.^3 ) / ( 12 * ( 1 - panel.v^2 ) ); % 31.4
54
55 ms = panel.density * panel.thickness; % 9.4 kg/m^2
56
57 wo = pi^2 / panel.length * sqrt( D / ms ); % 22.6 radians/s
58 s = wo^2 * ms; % 4,785.9 kg radians / m^2s^2
59
60 fo = wo / (2*pi); % 4 Hz
61
62
63 % Define an Anonymous function for the rigid panel with normal incidence.
64 h_tau_infinite_rigid_panel = @( f, wo, ms, s, rho0, c, eta) 4 ./ ( ( (2*pi.*f*ms - s./(2*pi.*f))
65     ./ (rho0 * c) ).^2 + ( (wo*ms*eta) ./ (rho0*c) + 2 ).^2 );
66
67
68 %% Problem 4b — Infinite, Flexible Panel Model with Random Incidence
69
70 % The panel has bending waves.
71
72
73 % Part (i.)
74
```



```

75 % The critical frequency.
76 critical_frequency = c^2 / (2*pi) * sqrt( ms / D ); % 10.22 kHz
77
78 % Verify the critical frequency using a 90 degree angle of incidence.
79 critical_frequency_verify_1 = 1./(2*pi) .* sqrt( ms / D ) .* ( c / sind( 90 ) ).^2; % 10.22 kHz
80
81 % Verify the critical frequency using the properties of the panel.
82 critical_frequency_verify_2 = c^2 / ( 1.8 * panel.thickness * sqrt( panel.E / ( panel.density * (
    1 - panel.v^2) ) ) ); % 10.3 kHz
83
84
85 % Coincidence frequency for a 75 degree angle of incidence.
86 phi = 75;
87 h_coincidence_frequency = @( ms, D, c, phi ) 1./(2*pi) * sqrt( ms / D ) .* ( c ./ sind( phi
    ) ).^2;
88 h_coincidence_frequency( ms, D, c, phi ); % 10,949 Hz
89
90
91 % Define an Anonymous function for the flexible panel with random incidence.
92 h_tau_infinite_flexible_panel = @( f, rho0, c, phi, D, eta ) ( 2*rho0.*c*secd(phi)).^2 ./ ( (2*
    rho0.*c*secd(phi) + D*eta*(2*pi.*f./c).^4./(2*pi.*f)*sind(phi)^4).^2 + ...
93 (2*pi.*f*ms - D*(2*pi.*f./c).^4./(2*pi.*f)*sind(phi)^4).^2 );
94
95
96
97 % Part (ii.) - Transmission loss for a 75 degree angle of incidence.
98 f = 0.1:1:100 e3;
99
100 figure( ); ...
101 plot( f, -10*log10( h_tau_infinite_flexible_panel( f, rho0, c, phi, D, panel.eta ) ), '
    LineStyle', '-', 'Marker', 'none', 'Color', [0.00, 0.45, 0.74] ); grid on;
102 text( 12e3, 5, sprintf( 'Coincidence\nFrequency\nof 10,494 Hz' ) );
103 xlabel( 'Frequency [Hz]' ); ylabel( 'Transmission Loss [dB]' );
104 set( gca, 'XScale', 'log' );
105 axis( [ 1 200e3 -5 80 ] );
106 %
107 % Textheight: 744 pt. and Textwidth: 493 pt. from LaTeX document
108 %
109 % set( gcf, 'units', 'point', 'pos', [ 200 200 493*0.8 744*0.3 ] );
110 % pos = get( gcf, 'Position' );
111 % set( gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3)
    , pos(4)] );
112 % print(gcf, 'Q4 TL for 75 AOI', '-dpdf', '-r0' );
113 %
114 % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
115
116
117
118 % Part (iii.)
119 f = 0.1:1:100 e3;
120
121 eta = panel.eta; phi_set = 0:10:90; t_set = [ ];
122
123 figure( ); ...
124 hold on;
125 for phi = phi_set
126     plot( f, -10*log10( h_tau_infinite_flexible_panel( f, rho0, c, phi, D, panel.eta ) ), '
        LineStyle', '-', 'Marker', 'none', 'Color', [0.00, 0.45, 0.74] );
127     t_set = [ t_set; h_tau_infinite_flexible_panel( f, rho0, c, phi, D, panel.eta ) ];
128 end
129 %
130 grid on; box on;
131 xlabel( 'Frequency [Hz]' ); ylabel( 'Transmission Loss [dB]' );
132 set( gca, 'XScale', 'log' );
133 axis( [ 1 200e3 -5 80 ] );
134 %
135 % Textheight: 744 pt. and Textwidth: 493 pt. from LaTeX document
136 %
137 % set( gcf, 'units', 'point', 'pos', [ 200 200 493*0.8 744*0.3 ] );
138 % pos = get( gcf, 'Position' );
139 % set( gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3)
    , pos(4)] );
140 % print(gcf, 'Q4iii TL for 75 AOI', '-dpdf', '-r0' );
141 %
142 % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
143
144
145 tau_d = nanmean( t_set .* sind( 2*phi_set ).', 1 );

```

```

146
147
148
149 %% Combined Transmission Loss Plot
150
151 figure( ); ...
152 h1 = stem( octave_band_frequencies, TL, 'LineStyle', 'none', 'Marker', 'o', 'MarkerSize', 8,
153           'MarkerFaceColor', 'r', 'MarkerEdgeColor', 'k' ); hold on;
154 h2 = plot( f, -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c, panel.eta ) ), '
155           'LineStyle', '-', 'Color', 'k' );
156 h3 = plot( f, -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c, panel.eta )
157           ./ (200*panel.eta) * ( 4*panel.length / ( panel.length^2 * critical_frequency ) ) ), '
158           'LineStyle', '-', 'Marker', 'none', 'Color', 'k' );
159 h4 = plot( f, -10*log10( tau_d ), 'LineStyle', '-', 'Marker', 'none', 'Color', [0.00, 0.45,
160           0.74] );
161 h5 = line( [ 16e3 16e3 ], [ 0 65 ], 'Color', 'r' ); grid on; % 16 kHz Demarcation
162 legend( ...
163         [ h1, h2, h3, h4, h5 ], ...
164         'Target Transmission Loss', ...
165         'Infinite Rigid Panel', ...
166         'Infinite Flexible Panel with Diffuse Incidence', ...
167         'Finite Flexible Panel Model', ...
168         '16 kHz Demarcation', ...
169         'Location', 'SouthOutside' );
170
171 xlabel( 'Frequency [Hz]' ); ylabel( 'Transmission Loss [dB]' );
172 title( 'Measured Panel Transmission Losses' );
173 set( gca, 'XScale', 'log' );
174 axis( [ 1 200e3 -5 80 ] );
175 %
176 % Textheight: 744 pt. and Textwidth: 493 pt. from LaTeX document
177 %
178 % set( gcf, 'units', 'point', 'pos', [ 200 200 493*0.8 744*0.45 ] );
179 % pos = get( gcf, 'Position' );
180 % set( gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [ pos(3)
181 % , pos(4) ] );
182 % print(gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0' );
183 %
184 % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
185
186
187 %% Plot Data and Model – Different Side Materials
188
189 % h_tau_infinite_rigid_panel_side_materials = @( f, wo, ms, s, rho0, c, eta, n ) (4*n) ./ ( (
190 % (2*pi.*f*ms - s./(2*pi.*f)) ./ (rho0 * c) ).^2 + ( (wo*ms*eta) ./ (rho0*c) + n + 1 ).^2 );
191
192 % f = 1e-2:1e-2:20e3;
193 %
194 % phi = 15;
195 % eta = panel.eta;
196 %
197 % figure( ); ...
198 % plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel_side_materials( f, wo, ms,
199 % s, rho0, c, panel.eta, 1 ) ), 'LineStyle', '-' ); hold on;
200 % plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel_side_materials( f, wo, ms,
201 % s, rho0, c, panel.eta, 1/3600 ) ), 'LineStyle', '-' );
202 % plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel_side_materials( f, wo, ms,
203 % s, rho0, c, panel.eta, 3600 ) ), 'LineStyle', '-' ); grid on;
204 %
205 % legend( ...
206 %         'Same Fluid', ...
207 %         'Water to Air', ...
208 %         'Air to Water', ...
209 %         'Location', 'North' );
210 %
211 % xlabel( 'Frequency [ $\frac{\omega}{\omega_o}$ ]' ); ylabel( 'Transmission Loss [dB]' );
212 % title( 'Measured Panel Transmission Losses' );
213 % set( gca, 'XScale', 'log' );
214 % axis( [ 40 12e3 -5 45 ] );
215
216
217 %% Change in Stiffness
218
219 % figure( ); ...
220 % stem( octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', '

```

```

MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
214 %
215 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c,
panel.eta ) ), 'LineStyle', '-' );
216 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s*100, rho0, c
, panel.eta ) ), 'LineStyle', '--' );
217 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s*1e-2, rho0,
c, panel.eta ) ), 'LineStyle', '-.-' );
218 %
219 %     legend( ...
220 %         'Target TL Values', ...
221 %         'Infinite Rigid Panel with Normal Incidence Sound', ...
222 %         'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
223 %         'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
224 %         'Location', 'North' );
225 %
226 %     xlabel( 'Frequency [ $\frac{\omega}{\omega_o}$ ]' ); ylabel( 'Transmission Loss [dB]' );
227 %     title( 'Measured Panel Transmission Losses - Change in Stiffness' );
228 %     set( gca, 'XScale', 'log' );
229 %     % axis( [ 40 12e3 -5 45] );
230
231
232


---


233 %% Change in Mass
234
235 % figure( ); ...
236 %     stem( octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', '
MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
237 %
238 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*100, s, rho0, c
, panel.eta ) ), 'LineStyle', '-' );
239 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c,
panel.eta ) ), 'LineStyle', '-' );
240 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*1e-2, s, rho0,
c, panel.eta ) ), 'LineStyle', '-.-' );
241 %
242 %     legend( ...
243 %         'Target TL Values', ...
244 %         'Infinite Rigid Panel with Normal Incidence Sound', ...
245 %         'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
246 %         'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
247 %         'Location', 'North' );
248 %
249 %     xlabel( 'Frequency [ $\frac{\omega}{\omega_o}$ ]' ); ylabel( 'Transmission Loss [dB]' );
250 %     title( 'Measured Panel Transmission Losses - Change in Mass' );
251 %     set( gca, 'XScale', 'log' );
252 %     % axis( [ 40 12e3 -5 45] );
253
254
255


---


256 %% Change in Loss Factor
257
258 % figure( ); ...
259 %     stem( octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', '
MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
260 %
261 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c,
panel.eta ) ), 'LineStyle', '-' );
262 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c,
panel.eta*1e2 ) ), 'LineStyle', ':' );
263 %     plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c,
panel.eta*1e-2 ) ), 'LineStyle', ':' );
264 %
265 %     legend( ...
266 %         'Target TL Values', ...
267 %         'Infinite Rigid Panel with Normal Incidence Sound', ...
268 %         'Infinite Rigid Panel with Normal Incidence Sound (eta * 100)', ...
269 %         'Infinite Rigid Panel with Normal Incidence Sound (eta / 100)', ...
270 %         'Location', 'North' );
271 %
272 %     xlabel( 'Frequency [ $\frac{\omega}{\omega_o}$ ]' ); ylabel( 'Transmission Loss [dB]' );
273 %     title( 'Measured Panel Transmission Losses - Change in Loss Factor' );
274 %     set( gca, 'XScale', 'log', 'YScale', 'log' );
275 %     % axis( [ 40 12e3 -5 45] );
276
277
278


---


279 %% Clean-up

```

```

280
281 % if ( ~isempty( findobj( 'Type', 'figure' ) ) )
282 %     monitors = get( 0, 'MonitorPositions' );
283 %     if ( size( monitors, 1 ) == 1 )
284 %         autoArrangeFigures( 2, 2, 1 );
285 %     elseif ( 1 < size( monitors, 1 ) )
286 %         autoArrangeFigures( 2, 2, 1 );
287 %     end
288 % end
289
290
291 fprintf( 1, '\n\n\n*** Processing Complete ***\n\n\n' );
292
293
294
295 %% Reference(s)

```

5 Appendix - Matlab Code for Problem 5

```
1
2
3
4 %% Synopsis
5
6 % Problem 5 — Large Enclosure Design
7
8
9
10 %% Environment
11
12 close all; clear; clc;
13 % restoredefaultpath;
14
15 % addpath( genpath( '' ), '-begin' );
16 addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
17
18 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
19 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
20 set( 0, 'DefaultFigureWindowStyle', 'normal' );
21 set( 0, 'DefaultLineLineWidth', 1.2 );
22 set( 0, 'DefaultTextInterpreter', 'Latex' );
23
24 format ShortG;
25
26 pause( 1 );
27
28
29
30 %% Define Machine
31
32 machine.area = 3; % m^2
33 machine.absorption = 0.07; % m^2 or Sabine
34 machine.D = 1; % Unitless — In air.
35
36 machine.distance = 10; % m
37
38
39
40 %% Measurement Data
41
42 octave_band_frequencies = [ 250 500 1000 2000 4000 ].'; % Hz
43 Lw = [ 105 115 106 108 119 ].'; % dB re: 1 pW
44
45
46
47 %% Per Octave Band Insertion Loss
48
49 Lp_10_meters = Lw + 10*log10( machine.D / ( 4 * pi * machine.distance^2 ) ); % dB re: 20e-6 Pa
50 %
51 % The value of R is infinite. The machine is outside in open air.
52
53 octave_band_IL = Lp_10_meters - 30;
54
55
56
57 %% Define Anonymous Function for Insertion Loss
58
59 h_IL_large = @( Sw, alpha_w, Si, alpha_i, TL ) 10*log10( 1 + (Sw*alpha_w + Si*alpha_i)./(Sw
+ Si)*10^(TL/10) );
60
61
62
63 %% Find Values of TL and Aborption that will Meet the Target Insertion Loss — Ground Reflecting
64
65 % Assumption(s):
66 %
67 % 1.) The enclosure is a cube.
68 % 2.) The machine sits on the ground.
69 % 2.) There is no noise transmission through the ground.
70
71 enclosure.dimension = 2.0; % m
72 enclosure.area = 5 * enclosure.dimension^2; % 20 m^2
73
74 % Volume of the enclosure is much bigger than the machine Diffuse sound field in the enclosure.
```

```

75
76
77 switch ( 4 )
78
79     case 1
80
81         % https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf
82
83         % 250 Hz – QBV-2
84         alpha_w = 0.27; % From specification sheet.
85         TL = 22; % From specification sheet.
86         IL_estimates(1) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
87
88         % 500 Hz – QBV-2
89         alpha_w = 0.96; % From specification sheet.
90         TL = 28; % From specification sheet.
91         IL_estimates(2) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
92
93         % 1 kHz – QBV-2
94         % alpha_w = 1.13; % From specification sheet.
95         alpha_w = 0.99; % From specification sheet. See comment on slide 28 of Lecture 10.
96         TL = 40; % From specification sheet.
97         IL_estimates(3) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
98
99         % 2 kHz – QBV-2
100        % alpha_w = 1.08; % From specification sheet.
101        alpha_w = 0.99; % From specification sheet. See comment on slide 28 of Lecture 10.
102        TL = 56; % From specification sheet.
103        IL_estimates(4) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
104
105        % 4 kHz – QBV-2
106        alpha_w = 0.99; % From specification sheet.
107        TL = 61; % From specification sheet.
108        IL_estimates(5) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
109
110
111    case 2
112
113        % https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf
114
115        % Note: Absorption values are carried over from QBV-2.
116
117        % 250 Hz – QBV-3
118        alpha_w = 0.96; % From specification sheet.
119        TL = 25; % From specification sheet.
120        IL_estimates(1) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
121
122        % 500 Hz – QBV-3
123        alpha_w = 0.87; % From specification sheet.
124        TL = 33; % From specification sheet.
125        IL_estimates(2) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
126
127        % 1 kHz – QBV-3
128        % alpha_w = 1.13; % From specification sheet.
129        alpha_w = 0.66; % From specification sheet. See comment on slide 28 of Lecture 10.
130        TL = 46; % From specification sheet.
131        IL_estimates(3) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
132
133        % 2 kHz – QBV-3
134        % alpha_w = 1.08; % From specification sheet.
135        alpha_w = 0.47; % From specification sheet. See comment on slide 28 of Lecture 10.
136        TL = 53; % From specification sheet.
137        IL_estimates(4) = h_IL_large( enclosure.area, alpha_w, machine.area, machine.
            absorption, TL );
138
139        % 4 kHz – QBV-3
140        alpha_w = 0.30; % From specification sheet.
141        TL = 58; % From specification sheet.

```

```

142         IL_estimates(5) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
143             absorption , TL );
144
145 case 3
146
147     % https://www.acousticworld.com/machine-acoustic-enclosures/
148
149     % 250 Hz
150     % alpha_w = 1.13; % From specification sheet.
151     alpha_w = 0.99;
152     TL = 34; % From specification sheet.
153     IL_estimates(1) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
154         absorption , TL );
155
156     % 500 Hz
157     % alpha_w = 1.12; % From specification sheet.
158     alpha_w = 0.99;
159     TL = 48; % From specification sheet.
160     IL_estimates(2) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
161         absorption , TL );
162
163     % 1 kHz
164     % alpha_w = 1.09; % From specification sheet.
165     alpha_w = 0.99;
166     TL = 61; % From specification sheet.
167     IL_estimates(3) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
168         absorption , TL );
169
170     % 2 kHz
171     % alpha_w = 1.03; % From specification sheet.
172     alpha_w = 0.99;
173     TL = 66; % From specification sheet.
174     IL_estimates(4) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
175         absorption , TL );
176
177     % 4 kHz
178     % alpha_w = 0.91; % From specification sheet.
179     TL = 70; % From specification sheet.
180     IL_estimates(5) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
181         absorption , TL );
182
183 case 4
184
185     % HTL-4 from specification sheet shown in class.
186
187     % 250 Hz
188     % alpha_w = 1.13; % From specification sheet.
189     alpha_w = 0.99;
190     TL = 39; % From specification sheet.
191     IL_estimates(1) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
192         absorption , TL );
193
194     % 500 Hz
195     % alpha_w = 1.12; % From specification sheet.
196     alpha_w = 0.99;
197     TL = 59; % From specification sheet.
198     IL_estimates(2) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
199         absorption , TL );
200
201     % 1 kHz
202     % alpha_w = 1.09; % From specification sheet.
203     alpha_w = 0.99;
204     TL = 68; % From specification sheet.
205     IL_estimates(3) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
206         absorption , TL );
207
208     % 2 kHz
209     % alpha_w = 1.03; % From specification sheet.
210     alpha_w = 0.99;
211     TL = 67; % From specification sheet.
212     IL_estimates(4) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
213         absorption , TL );
214
215     % 4 kHz
216     % alpha_w = 0.91; % From specification sheet.
217     TL = 72; % From specification sheet.

```

```

210         IL_estimates(5) = h_IL_large( enclosure.area , alpha_w , machine.area , machine.
211             absorption , TL );
212     end
213
214
215
216 %% Calculate the Differences
217
218 [ octave_band_IL      IL_estimates.'      (octave_band_IL - IL_estimates.') ]
219
220 data = [ ...
221     250      44      28.0      19.7      10.6      5.6; ...
222     500      54      26.7      22.2      6.6      -4.4; ...
223     1000     45      5.6      1.4     -15.4     -22.4; ...
224     2000     47     -8.4     -2.2     -18.4     -19.4; ...
225     4000     58     -2.4      5.7     -11.0     -13.0 ];
226
227 figure( ); ...
228 h1 = plot( data(:, 1) , data(:, 3) , 'LineStyle', '-', 'Color', 'k', 'Marker', '+', '
229     MarkerSize', 8 ); hold on;
230 h2 = plot( data(:, 1) , data(:, 4) , 'LineStyle', '-', 'Color', 'k', 'Marker', '+', '
231     MarkerSize', 8 );
232 h3 = plot( data(:, 1) , data(:, 5) , 'LineStyle', ':', 'Color', 'k', 'Marker', '+', '
233     MarkerSize', 8 );
234 h4 = plot( data(:, 1) , data(:, 6) , 'LineStyle', '-', 'Color', 'k', 'Marker', '+', '
235     MarkerSize', 8 ); grid on;
236 line( [200 5500], [0 0] , 'Color', 'r' );
237 legend( [ h1 h2 h3 h4 ] , { 'Case 1 - Control Noise QBV 2', 'Case 2 - Control Noise QBV 3', '
238     Case 3 - Acoustics World HTL (100MM)', 'Case 4 - HTL 4 (class table)' }, 'Location', '
239     SouthOutside' );
240 xlabel( 'Frequency [Hz]' ); ylabel( 'Insertion Loss Difference [dB]' );
241 %
242 axis( [ 150 6e3 -30 30 ] );
243 set( gca, 'XScale', 'log' );
244 %
245 % Textheight: 744 pt. and Textwidth: 493 pt. from LaTeX document
246 %
247 set((gcf, 'units', 'point', 'pos', [ 200 200 493*0.8 744*0.5 ] );
248 pos = get((gcf, 'Position' );
249 set((gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3),
250     pos(4)] );
251 %
252 print(gcf, 'Q5 IL Plot', '-dpdf', '-r0' );
253 %
254 % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex
255
256
257 %% Clean-up
258
259 % if ( ~isempty( findobj( 'Type', 'figure' ) ) )
260 %     monitors = get( 0, 'MonitorPositions' );
261 %     if ( size( monitors, 1 ) == 1 )
262 %         autoArrangeFigures( 2, 2, 1 );
263 %     elseif ( 1 < size( monitors, 1 ) )
264 %         autoArrangeFigures( 2, 2, 1 );
265 %     end
266 % end
267
268 fprintf( 1, '\n\n\n*** Processing Complete ***\n\n\n' );
269
270
271
272 %% Reference(s)
273
274 %
275 % Textheight: 744 pt. and Textwidth: 493 pt. from LaTeX document
276 %
277 set((gcf, 'units', 'point', 'pos', [ 200 200 493*0.8 744*0.45 ] );
278 pos = get((gcf, 'Position' );
279 set((gcf, 'PaperPositionMode', 'Auto', 'PaperUnits', 'points', 'PaperSize', [pos(3),
280     pos(4)] );
281 %
282 print(gcf, 'Q4d TL for 75 AOI', '-dpdf', '-r0' );
283 %
284 % https://tex.stackexchange.com/questions/179382/best-practices-for-using-matlab-images-in-latex

```


6 Appendix - Matlab Code for Problem 6

```

1
2
3
4 %% Synopsis
5
6 % Problem 6 — Close-fitting Enclosure Design
7
8
9
10 %% Environment
11
12 close all; clear; clc;
13 % restoredefaultpath;
14
15 % addpath( genpath( '' ), '-begin' );
16 addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
17
18 % set( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
19 set( 0, 'DefaultFigurePaperPositionMode', 'manual' );
20 set( 0, 'DefaultFigureWindowStyle', 'normal' );
21 set( 0, 'DefaultLineLineWidth', 0.8 );
22 set( 0, 'DefaultTextInterpreter', 'Latex' );
23
24 format ShortG;
25
26 pause( 1 );
27
28
29
30 %% Define Compressor
31
32 compressor.width = 1; % m
33 compressor.depth = 1; % m
34 compressor.height = 2; % m
35 compressor.area = 2*(compressor.width * compressor.depth) + 2*(compressor.width * compressor.
    height) + 2*(compressor.depth * compressor.height); % 3 m^2
36 compressor.volume = compressor.width * compressor.depth * compressor.height; % m^3
37
38 compressor.power_level = 105; % dB re: 1e-12 Watts
39 compressor.frequency = 50; % Hz
40
41 c = 343; % m/s
42
43 rho0 = 1.21; % kg/m^3
44
45
46
47 %% Sound Level Target
48
49 sound_level_target = 82; % dB re: 20e-6 Pascals
50
51
52
53 %% Define Workshop
54
55 R = 40; % m^2 or Sabins
56
57
58
59 %% Define Anonymous Functions
60
61 h_RA_term_1 = @( rho0, c, S, k, delta_mu, D, w ) ( rho0*c/S ) * ( ( k * sqrt( (2*3.178e-5) / (
    rho0*w) ) * D * 0.004 ) / (2*S) * 1.4364 );
62 h_RA_term_2 = @( rho0, c, S, k, delta_mu, D, w, h ) ( rho0*c/S ) * 0.288*k*3.178e-5*log10((4*
    S)/(pi*h^2));
63 h_RA_term_3 = @( rho0, c, S, k, delta_mu, D, w, h ) ( rho0*c/S ) * (0.5*S*k^2)/(2*pi);
64
65
66
67 %% Define Close-fitting Enclosure
68
69 helmholtz_factor = (2 * pi * compressor.frequency) / c; % 0.92 m^-1
70 %
71 % For a small enclosure, k*d << 1. Therefore d << 1.1.
72

```

```

73 enclosure.width = compressor.width + 0.25; % m
74 enclosure.depth = compressor.depth + 0.5; % m
75 enclosure.height = 3; % m; compression height is 2 m
76     enclosure.area = 2*(enclosure.width * enclosure.depth) + 2*(enclosure.width * enclosure.
77         height) + 2*(enclosure.depth * enclosure.height);
78     enclosure.volume = enclosure.width * enclosure.depth * enclosure.height;
79 enclosure.E = 3.6e9; % Pascals
80 enclosure.thickness = 3.81e-2; % m
81 enclosure.density = 800; % kg/m^3
82 enclosure.poisson_ratio = 0.25; % Unitless
83
84 % Clamped boundary conditions.
85
86
87
88 %% Calculate Diffuse Sound Pressure Level
89
90 % Assume distance is beyond the critical distance, so the distance value is
91 % large and its associated term is not relevant.
92
93 sound_pressure_level = 105 + 10*log10( 4/R ); % 95 dB SPL
94
95
96
97 %% Calculate the Required Insertion Loss
98
99 target_insertion_loss = sound_pressure_level - 82 % 13 dB
100
101
102
103 %% Insertion Loss
104
105 bending_stiffness = ( enclosure.E * enclosure.thickness^3 ) / ( 12*( 1 - enclosure.poisson_ratio
106     ^2 ) );
107 h_wall_compliance = @( wall_area, correction_factor ) ( 0.001 * wall_area^3 *
108     correction_factor ) / bending_stiffness;
109
110 Ca = enclosure.volume / ( rho0 * c^2 );
111
112 % Top
113 top.area = enclosure.width * enclosure.depth;
114 top.aspect_ratio = max( enclosure.width, enclosure.depth ) / min( enclosure.width, enclosure.
115     depth );
116 top.correction_factor = 3.8;
117 top.compliance = h_wall_compliance( top.area, top.correction_factor );
118
119 % Side 1
120 side_1.area = enclosure.depth * enclosure.height;
121 side_1.aspect_ratio = max( enclosure.width, enclosure.height ) / min( enclosure.width, enclosure.
122     height );
123 side_1.correction_factor = 0.5;
124 side_1.compliance = h_wall_compliance( side_1.area, side_1.correction_factor );
125
126 % Side 2
127 side_2.compliance = side_1.compliance;
128
129 % Side 3
130 side_3.area = enclosure.width * enclosure.height;
131 side_3.aspect_ratio = max( enclosure.width, enclosure.height ) / min( enclosure.width, enclosure.
132     height );
133 side_3.correction_factor = 0.5;
134 side_3.compliance = h_wall_compliance( side_3.area, side_3.correction_factor );
135
136 % Side 4
137 side_4.compliance = side_3.compliance;
138
139 estimated_insertion_loss = 20*log10( 1 + Ca / ( top.compliance + 2*side_1.compliance + 2* side_3.
140     compliance ) );
141 13 - estimated_insertion_loss
142
143 %% Compliance of the Air Intake

```

```

144
145 air_intake_radius = 10e-2; % m
146 air_intake_thickness = enclosure.thickness; % m
147 air_intake_frequency = 50; % Hz
148     air_intake_angular_frequency = 2*pi*air_intake_frequency; % radians/s
149
150 viscosity = 1.5e-5; % m^2/s
151
152 h = 0.3;
153
154 f = 50;
155 term_1 = h_RA_term_1( rho0, c, pi*(air_intake_radius^2)^2/4, 2*pi*f/c, sqrt( (2 * 3.178e-5 )
156     / ( 2*pi*f * rho0 ) ), pi * 0.1, 2*pi*f );
157 term_2 = h_RA_term_2( rho0, c, pi*(air_intake_radius^2)^2/4, 2*pi*f/c, sqrt( (2 * 3.178e-5 )
158     / ( 2*pi*f * rho0 ) ), pi * 0.1, 2*pi*f, 0.3 );
159 term_3 = h_RA_term_3( rho0, c, pi*(0.1)^2/4, 2*pi*f/c, sqrt( (2 * 3.178e-5 ) / ( 2*pi*f *
160     rho0 ) ), pi * 0.1, 2*pi*f, 0.3 );
161 impedance.real = term_1 + term_2 + term_3;
162
163 % Deng (1998)
164 epsilon = 1;
165 L_o = air_intake_radius * ( 1.27 / (1 + 1.92*epsilon) - 0.086 );
166 L_e = enclosure.thickness + 2*L_o;
167 impedance.imaginary = 1j * rho0 * (2 * pi * f) * L_e / ( pi*0.1^2/4 );
168
169 impedance.net = impedance.real + impedance.imaginary;
170 compliance_of_hole = 1 / impedance.net;
171 Cl = abs( compliance_of_hole );
172
173 estimated_insertion_loss_with_hole = 20*log10( (Cl + Ca) / ( Cl + ( top.compliance + 2*side_1.
174     compliance + 2* side_3.compliance ) ) );
175 13 - estimated_insertion_loss_with_hole
176
177 critical_frequency = c^2/(2*pi)*sqrt( enclosure.density * enclosure.thickness / bending_stiffness
178     ); % 777.1 Hz
179
180
181 %% Clean-up
182
183 fprintf( 1, '\n\n*** Processing Complete ***\n\n' );
184
185
186
187 %% Reference(s)

```