Subject: ACS 547, Noise Control Applications - Module 2 Assignment

Date: February 23, 2025 (Submitted)

# Problem 1 - Modal Behaviour of a Cylindrical Room

The Matlab code for this problem is listed in Appendix 1.

#### Problem 1a

Table 1 lists the ten lowest resonance mode orders for the room and the respective frequency.

Index	$\mathbf{Mode}  (\mathbf{n}_{\mathrm{x}},  \mathbf{n}_{\vartheta},  \mathbf{n}_{\mathrm{r}})$	Frequency [Hz]
0	0, 0, 0	0
1	1, 0, 0	17.2
2	0, 1, 0	33.5
3	2, 0, 0	34.3
4	1, 1, 0	37.6
5	2, 1, 0	48.0
6	3, 0, 0	51.5
7	0, 2, 0	55.6
8	1, 2, 0	58.2
9	3, 1, 0	61.4
10	2, 2, 0	65.3

Table 1: Resonant modes of the cylindrical room.

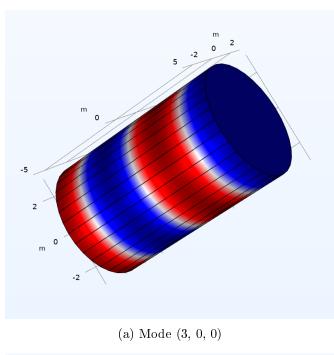
#### Problem 1b

The two closest modes are (3, 0, 0) and (0, 2, 0) with frequencies of 51.5 Hz and 55.6 Hz, respectively.

#### Problem 1c

Figure 1 illustrates the (3, 0, 0) and (0, 2, 0) modes. The white lines in each figure show the modal lines for that mode. The machine can be placed where the modal lines for each mode overlap. The figures were produced using the Room Eigenmode Simulator Version 1.1 software package.

The pink rings in Figure 1b indicate 3 possible places where the machine could be placed. These points coincide with the three modal planes shown in Figure 1a. Theoretically, there are an infinite number of places where the machine could be placed. However, placement would take into account practical considerations such as accessibility, etc.



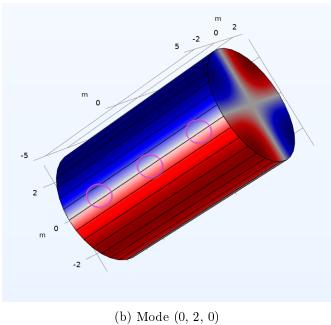


Figure 1: Visualization of modes. (a.) Mode (3, 0, 0). (b.) Model (0, 2, 0). The pink circles in 1b illustrate a few modal line intersections where the machine could be placed.

# Problem 2 - Sabine Room

The Matlab code for this problem is listed in Appendix 2.

#### Problem 2a

The reverberant field sound pressure level is approximately 98.3 dB SPL.

#### Problem 2b

Figure 2 shows the direct, reverberant, and total sound pressure levels for a 25 mW, 125 Hz, broadband, omnidirectional source placed centrally in the room (i.e. the directivity factor is 1).

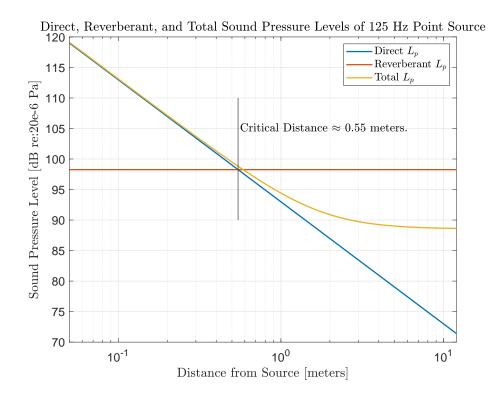


Figure 2: Sound levels for the room produced by a 25 mW, 125 Hz omnidirectional, broadband source.

# Problem 3 - Transmission Loss Measurement

The Matlab code for this problem is listed in Appendix 3.

Figure 3 shows the average absorption per octave band based on the T60 data. The calibration plate isolates the receiver room and the absorption calculation does not consider the calibration plate.

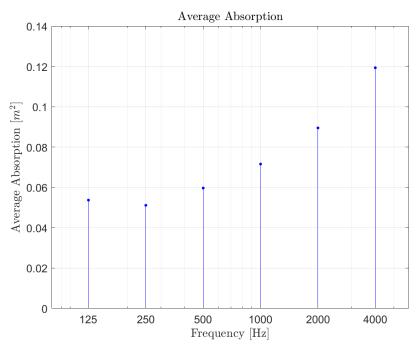


Figure 3: Average absorption per octave band.

Figure 4 shows the transmission loss per octave band.

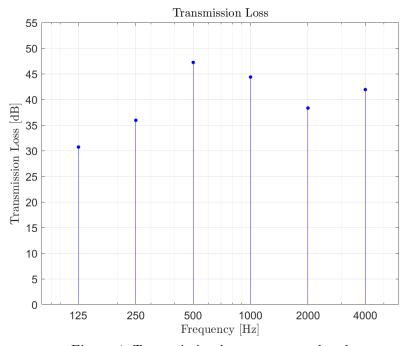


Figure 4: Transmission loss per octave band.

# Problem 4 - Panel Transmission Loss

The Matlab code for this problem is listed in Appendix 4.

#### Problem 4a

Table 2 lists the Mach numbers for each pipe section. The flow rate is  $0.017462 \frac{\text{m}^3}{\text{s}}$ .

Pipe	Area [m <sup>2</sup> ]	Mach Number [unitless]
Inlet	0.000507	-0.10047
Outlet	0.00811	-0.0062795

Table 2: Calculated Mach numbers.

#### Problem 4b

Figure ?? shows the transmission loss profiles.

The addition of flow to the intake system introduces a slight phase delay, a lower overall level of loss (approximately 22 dB), and greater loss at the dips. The phase delay is easier to see at respective dips in the loss profile.

i - Critical Frequency and Coincidence Frequency at  $75^{\circ}$ 

ph

ii - Transmission Loss at Angle of Incidence of  $75^{\circ}$ 

ph

iii - Transmission Loss for Angles of Incidence between  $0-90^\circ$ 

ph

iv - Diffuse Transmission Loss

ph

# Problem 4c Problem 4d i - Critical Frequency and Coincidence Frequency at 75° ph ii - Transmission Loss at Angle of Incidence of 75° ph vspace0.25cm iii - Transmission Loss for Angles of Incidence between 0-90° ph

iv - Diffuse Transmission Loss

# Problem 5 - Large Enclosure Design

The Matlab code for this problem is listed in Appendix  $\pmb{6}.$ 

ph

# Problem 6 - Close-fitting Enclosure Design

The Matlab code for this problem is listed in Appendix  $\pmb{6}.$ 

 $\rm ph$ 

```
2
   % Synopsis
4
   % Problem 1 - Modal Behaviour of a Cylindrical Room
9
10 % Environment
   close all; clear; clc;
13
   % restored efault path;
   % addpath( genpath( '' ), '-begin' );
addpath( genpath( './00 Support' ), '-begin' );
16
   % set(0, 'DefaultFigurePosition', [400 400 900 400]); % [left bottom width height] set(0, 'DefaultFigurePaperPositionMode', 'manual'); set(0, 'DefaultFigureWindowStyle', 'normal'); set(0, 'DefaultLineWidth', 1.5);
18
19
   set( 0, 'DefaultTextInterpreter', 'Latex' );
24
   format ShortG;
26
   pause ( 1 );
28
29
30 %% Define Room
   room.radius = 3; % m
   room.length = 10; \% m
   7% Test Circular Mode Function
38
   40
41
   7% Define Anonymous Function for the Natural Frequencies
45
   46
        .^2);
47
50 % Calculate the Natural Frequencies
   % The maximum number of radial modes is 5 (indexed from 0 to 4).
52
   % The maximum number of angular modes is 8 (indexed from 0 to 7).
54
   NX SIZE = 20;
   \overline{NTHETA}_{SIZE} = 7;
   NR SIZE = 4;
58
        natural frequencies = nan( NX SIZE, NTHETA SIZE, NR SIZE );
59
60
   for nx = 0:1:NX SIZE
        for ntheta = 0:1:NTHETA SIZE
61
62
            \begin{array}{lll} \textbf{for} & \textbf{nr} = 0:1: NR\_SIZE \end{array}
                natural\_frequencies (\ nx+1,\ ntheta+1,\ nr+1\ ) \ = \ h\_natural\_frequencies (\ 343\,,\ nx\,,\ ntheta\,,
                     nr, 10, 3, false);
        end
   end
68
70
   % Part a - Find 10 Lowest Resonance Frequencies
   NUMBER OF LOWEST FREQUENCIES = 11;
```

```
73
          mode indices = ( 1:1:NUMBER OF LOWEST FREQUENCIES ).';
 74
     [ sortedValues, sortedIndices ] = sort ( natural frequencies (:) ); % 21-by-8-by-5 -> 840 elements
 76
 77
     smallest Values = sorted Values ( 1:NUMBER\_OF\_LOWEST\_FREQUENCIES ); \\
 78
         % [ mode indices
                                round (smallest Values, 1)
         %
 79
         \% 1
         % 2
                        17.2
 81
         % 3
 82
                        33.5
         % 4
 83
                        34.3
         % 5
 84
                        37.6
         % 6
 85
                        47.9
 86
         % 7
                        51.5
 87
         % 8
                        55.6
         % 9
                        58.2
 89
         % 10
                         61.4
         % 11
                         65.3
     smallestIndices = sortedIndices( 1:NUMBER OF LOWEST FREQUENCIES);
 94
     [ x, y, z ] = ind2sub( size(natural_frequencies), smallestIndices );
         % ( [ x y z ] - 1 )
 95
 97
    % Verify the calculated mode indices.
98
    h_natural_frequencies( 343, 0, 0, 0, 10, 3, false );
                                                                    % 0 Hz
    h_natural_frequencies( 343, 1, 0, 0, 10, 3, false );
                                                                    % 17.2 Hz
     h_natural_frequencies( 343, 0, 1, 0, 10, 3, false );
h_natural_frequencies( 343, 2, 0, 0 , 10, 3, false );
                                                                     % 34.3 Hz
     h_natural_frequencies( 343, 1, 1, 0 , 10, 3, false
                                                                     \% 37.6 Hz
     % 48.0 Hz
                                                                 );
                                                                     \% 51.5 Hz
     h\_natural\_frequencies (\ 343\,,\ 0\,,\ 2\,,\ 0\ ,\ 10\,,\ 3\,,\ false
                                                                      % 55.6 Hz
                                                                 );
     h_natural_frequencies( 343, 1, 2, 0 , 10, 3, false
h_natural_frequencies( 343, 3, 1, 0 , 10, 3, false
                                                                      % 58.2 Hz
                                                                 );
                                                                     \% 61.4 Hz
     h natural frequencies (343, 2, 2, 0, 10, 3, false);
108
110
112 %% Part b — Two
114
    \% [ (1:11). abs(smallest Values - 53)]
     temp = [x y z] - 1; temp(7:8, :, :)
116
118
      h\_natural\_frequencies (\ 343,\ 3,\ 0,\ 0,\ 10,\ 3,\ false\ ); \ \%\ 51.5\ Hz,\ (3,\ 0,\ 0) 
119
     h natural frequencies ( 343, 0, 2, 0, 10, 3, false ); \% 55.6 Hz, (0, 2, 0)
    %% Part c
124
    % See the report.
126
128
129
    % Clean-up
     if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
              if ( size( monitors, 1 ) == 1 )
               \begin{array}{c} \texttt{autoArrangeFigures(2,2,1);} \\ \texttt{elseif (1 < size(monitors,1))} \end{array}
                   autoArrangeFigures (\phantom{-}2\,,\phantom{-}2\,,\phantom{-}1\phantom{-})\,;
               end
138
     end
     fprintf(1, '\n\n*** Processing Complete ***\n\n');
    % Reference(s)
146
```

10

 $\% \ \ https://www.mathworks.com/matlabcentral/answers/1883747-how-to-find-the-5-minimum-values-in-a-find-the-$ 

multidimensional-matrix-and-the-indices-to-which-these-entries

```
2
               % Synopsis
   4
               % Problem 2 - Sabine Room
10 % Environment
                 close all; clear; clc;
13 % restored efault path;
                % addpath( genpath( '' ), '-begin' );
addpath( genpath( '../00 Support' ), '-begin' );
16
               % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
18
               set(0, 'DefaultFigurePaperPositionMode', 'manual');
set(0, 'DefaultFigureWindowStyle', 'normal');
set(0, 'DefaultLineLineWidth', 1.5);
set(0, 'DefaultTextInterpreter', 'Latex');
19
24
                 format ShortG;
26
                 pause ( 1 );
28
29
30 % Define Room
              room.width = 8; % m
                room.length = 6; \% m

room.height = 3; \% m
                                      room.volume = room.width * room.length * room.height; % 144 m^3
                                      {\tt room.area} \ = \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.length*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.width*room.height}) \ + \ 2*({\tt room.height}) \ + \ 2*(
                                                         length); \% 180 m<sup>2</sup>
                 alpha\_average\_walls\_and\_floor = \ 0.05; \ \% \ For \ the \ walls \ and \ the \ floor \, .
38
                  alpha_average_ceiling = 0.15; % For the ceiling.
39
                % For the 125 Hz octave band.
41
44
                %% Part a - Estimate the Reverberant Sound Pressure Level
45
47
                Lw = 10 * log 10 ( 25e-3 / 1e-12 ); \% 103.98 dB
48
                  average\_absorption\_coefficient = (\ (room.width*room.length)*alpha\_average \ ceiling \ + \ (room.width*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*room.length*ro
                                      *room.length + 2*(room.width*room.height) + 2*(room.length*room.height))*
alpha_average_walls_and_floor) / room.area; % 0.076667 unitless
                  room constant = room.area * average absorption coefficient / ( 1 - average absorption coefficient
                                          ); % 14.9 m<sup>2</sup> or Sabin
                  sound pressure level = Lw + 10*log10 ( 4 / room constant ); % 98.3 dB
56
58 % Part b - Calculate the Critical Distance
59
60 \quad D0 = 1;
61
                 r = 0:0.05:12; % m
                 h Lp direct = @(Lw, D0, r) Lw + 10*log10(D0./(4.*pi.*r.^2));
                 h Lp reverberant = @( Lw, room constant ) Lw + 10*log10( 4 ./ room constant );
66 %
                 h\_Lp\_net = @( \ Lw, \ D0, \ r \,, \ room\_constant \ ) \\ Lw + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \, + \, 4/room \ constant \ ) \\ + 10*log10 \, ( \ D0./(4.*pi.*r.^2) \,
67
                                       10*\log 10 (343*1.2/400);
68
                 figure ( ); ...
```

```
h1 = plot(r, h_Lp_direct(Lw, D0, r)); hold on;
          h1 = plot( r, h_bp_alrect( bw, bo, r) ), hold on, h2 = plot( r, ones( size(r) ).*h_Lp_reverberant( Lw, room_constant) ); h3 = plot( r, h_Lp_net( Lw, D0, r, room.volume )); grid on; legend( [ h1, h2 h3 ], { 'Direct $L_p$', 'Reverberant $L_p$', 'Total $L_p$' }, 'Interpreter', 'Latex' );
 73
 74
 76
          text( 0.56, 105, 'Critical Distance $\approx$ 0.55 meters.', 'Interpreter', 'Latex' );
               line([0.545 0.545], [90 110], 'Color', 'k', 'LineWidth', 0.6);
 78
          xlabel( 'Distance from Source [meters]' ); ylabel( 'Sound Pressure Level [dB re:20e-6 Pa]' )
 79
          title ( 'Direct, Reverberant, and Total Sound Pressure Levels of 125 Hz Point Source' );
 80
          %
 81
 82
          set ( gca, 'XScale', 'log');
 83
 84
 85 % Estimate the critical distance (see page 84 of "06-Indoors.pdf" notes for ACS 537).
 86
     rc = 0.141 * sqrt(D0 * room\_constant); % 0.5451 meters
 87
 88
     return
 89
90 % Clean—up
91
     if ( ~isempty( findobj( 'Type', 'figure') ) )
   monitors = get( 0, 'MonitorPositions');
   if ( size( monitors, 1 ) == 1 )
92
93
94
                autoArrangeFigures(2,2,1);
elseif (1 < size(monitors,1))
96
                    autoArrangeFigures(2,2,1);
97
98
99
     end
     104
106 % Reference(s)
```

```
2
   % Synopsis
4
   % Question 3 - Transmission Loss Measurement
9
  % Note(s):
10 %
       1.) Lp1 depends on the transmission loss.
12 %
13 %
            If the transmission loss is low, then more energy goes to room 2 (i.e., the receiver room
   %
14
15 %
           The noise reduction from the source room to the receiver room.
16 %
17
   %
            Adding the barrier will change the level in the source room. Typically making the sound
       level higher in the source room.
18
19
21 % Environment
   close all; clear; clc;
24 % restored efault path;
  % addpath( genpath( '' ), '-begin' );
26
   addpath ( genpath ( '../00 Support'), '-begin');
28
   % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ]
29
   set(0, DefaultFigurePaperPositionMode', 'manual');
30
   set( 0, 'DefaultFigureWindowStyle', 'n
set( 0, 'DefaultLineLineWidth', 1.2 );
            'DefaultFigureWindowStyle', 'normal');
   38
   format ShortG;
40
   pause ( 1 );
41
43
   % Dimensions of Rooms and Panel
44
46 \operatorname{room.length} = 4; % m
47
   room.width = 4; \% m
   room.height = 4; \% m
48
       room.volume = room.length * room.width * room.height; % 64 m^3
       {\tt room.area} = 2*({\tt room.length} \ * \ {\tt room.width}) \ + \ 2*({\tt room.length} \ * \ {\tt room.height}) \ + \ 2*({\tt room.width}) \ *
           room.height); % 96 m^2
   \begin{array}{lll} panel.width &=& 0.8\,; &\%~m\\ panel.height &=& 0.8\,; &\%~m \end{array}
53
       panel.area = panel.width * panel.height; % 0.64 m^2
56
   c = 343; \% m/s
58
59
60 % Measurement Data
61
   1000 2000 4000 ].'; % Hz
                                          spl.source room spl.receiver room (spl.source room - spl.
           receiver_room) ]
68
```

70 %% Calculate Average Absorption in the Receiver Room using Reverberation Time Measurements

```
average absorption = @( volume, area, c, T60 ) ( 55.25 .* volume ) ./ ( area .* c .* T60 );
 73
 74
         receiver room.average absorption = average absorption (room.volume, room.area, c, T60);
 76
        % Assumption: Calibration panel has very high transmission loss.
 78
          figure(); ...
                  stem (\ octave\_band\_frequencies \,,\ receiver\_room.\, average\_absorption \,,\ 'Marker' \,,\ '.\,',\ 'MarkerSize' \,,
 79
                  12, 'Color', 'b'); grid on; xlabel( 'Frequency [Hz]'); ylabel( 'Average Absorption [$m^2$]'); title( 'Average Absorption');
 80
 81
 82
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) ); set( gca, 'XScale', 'log'); xlim( [ 80 6e3 ] ); ylim( [ 0 0.14 ] );
 83
 84
 85
 87
 88
 89 % Calculate the Receiver Room Constant
 91 % The calibration plate isolates the receiver room.
 93
        % The receiver room does not consider the calibration plate.
         \label{eq:constant} \begin{array}{lll} room\_constant = @(\ average\_absorption\ ,\ area\ ) & (\ average\_absorption\ )\ ; & \% \ Unitless \\ \end{array}
 97
         receiver room.room constant = room constant ( receiver room.average absorption, room.area );
 98
        % Calculate the Transmission Loss in Each Octave Band
         transmission\_coefficient = @(\ receiver\_room\_pressure \,,\ source\_room\_pressure \,,\ panel\_area \,,
                  receiver_room_constant ) ( ( receiver_room_pressure ./ source_room_pressure ) .*
                  receiver room constant ) / panel_area;
         tau = transmission\_coefficient ( 10.^(spl.receiver\_room./10)*20e-6, 10.^(spl.source\_room/10)*20e-6, 10.^(spl.source\_room/10)
                  -6, panel.area, receiver room.room constant);
         TL = -10*log10 (tau);
108
         figure( ); ...
                  stem (octave band frequencies, TL, '.', 'MarkerSize', 15, 'Color', 'b'); grid on;
110
                  xlabel( 'Frequency [Hz]'); ylabel( 'Transmission Loss [dB]');
                  title ( Transmission Loss );
                  xticks( octave_band_frequencies ); xticklabels( num2cell( octave_band_frequencies ) );
114
                  set ( gca, 'XScale', 'log');
                  xlim( [ 80 6e3 ] ); ylim( [ 0 55 ] );
116
118
         return
119
120 % Clean—up
          if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
                           if (size(monitors, 1) == 1)
                                    autoArrangeFigures(2,2,1);
126
                            elseif (1 < size (monitors, 1))
                                   autoArrangeFigures(2,2,1);
128
                           end
129
         end
         fprintf( 1, \n\n\n*** Processing Complete ***\n\n\n');
```

136 **% Reference(s)** 

```
2
   % Synopsis
   % Slide 8 - Noise Reduction and Transmission Loss
10 % Environment
   % close all; clear; clc;
13 % restored efault path;
   \% addpath( genpath( ^{-++} ), ^{+}-begin \,^{+-});
   addpath ( genpath ( '../40 Assignments/00 Support'), '-begin');
16
   % set ( 0, 'DefaultFigurePosition', [ 400 400 900 400 ] ); % [ left bottom width height ] set ( 0, 'DefaultFigurePaperPositionMode', 'manual' );
18
19
   set( 0, 'DefaultFigureWindowStyle', 'normal' );
set( 0, 'DefaultLineLineWidth', 0.8 );
    set( 0, 'DefaultTextInterpreter', 'Latex' );
24
    format ShortG;
26
   pause ( 1 );
28
   PRINT FIGURES = 0;
29
32 % Parameters
34
    c = 343; \% m/s
35 \quad \text{rho0} = 1.21; \% \text{ kg}
    panel.length = 80e-2; % meters
38 %
   panel.E = 200e9; % Pascals
40
    panel.density = 7800; % kg / m<sup>3</sup>
   panel.v = 0.29; % Poisson's Ratio (unitless)
41
   panel.thickness = 1.2e-3; % m
43
    panel.eta = 0.001; % Loss factor (unitless)
45
46
47 % Panel Data
48
   49
                                                        1000 2000 4000 8000 ].'; % Hz
53 % figure(); ...
        stem( octave_band_frequencies, TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); grid on; xlabel( 'Frequency [Hz] '); ylabel( 'Transmission Loss [dB]');
54
           title ( 'Measured Panel Transmission Losses ');
56 %
           set ( gca, 'XScale', 'log');
   %
58
           axis([40 12e3 -5 45]);
59
61
62 % Problem 4a - Infinite, Rigid Panel Model with Normal Incidence
63
64 D = ( panel.E * panel.thickness.^3 ) / ( 12 * (1 - panel.v^2) ); % 31.4
   % From lecture 9 on Wednesday, February 12, 2025, the equivalent bending
   \% moment of the panel is a half-wavelength.
68 %
   wavelength = 2 * panel.length; % 1.6 meters
70
   ms = panel.density * panel.thickness;
73
    wo = pi^2 / panel.length * sqrt(D / ms);
        s = wo^2 * ms;
```

```
76
   78
               pi.*f*ms - s./(2*pi.*f) ./ (rho0*c) + (wo*ms*eta) ./ (rho0*c) + n + 1 ).^2 );
   79
   81
              1 Problem 4b - Infinite, Flexible Panel Model with Random Incidence
   82
   83
   84
              % Panel has bending waves.
   85
   86
   87
               \label{eq:h_tau_term1} h\_tau\_term1 \, = \, @(\ rho0 \; , \ c \; , \ phi \; ) \quad (\ 2*rho0*c*secd (phi) \; ) \, . \, \hat{\ } 2 \; ; \quad \% \; \ Checked
               h\_tau\_term2 = @( rho0, c, phi, D, eta, f ) ( 2*rho0*c*secd(phi) + (D*eta*(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c).^4)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c)./(2*pi.*f./c).
   88
                             .*f) .* sind(phi).^4).^2; % Checked
               89
   91
                h\_tau\_infinite\_flexible\_panel = @( f, rho0, c, phi, D, eta ) ( 2*rho0.*c*secd(phi)).^2 ./ ( (2*rho0.*c*secd(phi)).^2 ./ ( (2*rho0.*c*secd(phi))... ( (2*rho0.*c*secd(phi
   92
                             (2*pi.*f*ms - D*(2*pi.*f./c).^4./(2*pi.*f)*sind(phi)^4).^2);
              % return
              7% Plot Data and Model - Air on Both Sides
  98
  99
             % 75 degrees from normal to panel.
               h_c_bending_wave = @(D, f, ms) ((D*(2*pi.*f).^2) ./ ms).^0.25;
             %
              %
                              Proportional to the square-root of frequency.
              %
             %
                                             Small wavelenths (high frequencies; arrive first) travel faster than long wavelength (
                             low frequencies; arrive later).
                phi = 75;
                               \label{eq:h_coincidence_frequency}  \mbox{$h$\_coincidence\_frequency} = \mbox{$@($ ms, D, c, phi )$} \mbox{$1./(2*pi) * sqrt($ ms/D ) .* ($ c./ sind(phi) ... ) ... ] } 
                                               )).^2; % 10,949 Hz
                              h coincidence frequency (ms, D, c, phi); % 10,949 Hz
                               [ \ (0:15:90).' \ h\_coincidence\_frequency ( \ ms, \ D, \ c \,, \ [ \ 0:15:90 \ ] \ ) \,.' \ ]; 
113
114
                              critical\_frequency = 1./(2*pi) .* sqrt(ms/D) .* (c/sind(90)).^2 % 10,216 Hz
                                             critical frequency verify 1 = c^2 / (2*pi) * sqrt(ms / D); % lowest coincidence
                                                          frequency
                                             critical\_frequency\_verify\_2 \ = \ c^2 \ / \ ( \ 1.8 \ * \ panel.thickness \ * \ sqrt \ ( \ panel.E \ / \ ) \ ( \ panel.E \ / \ ) \ )
                                                           density * (1 - panel.v^2));
118
              \% \text{ f} = 1 \text{ e} - 2:1 \text{ e} - 2:40 \text{ e} 3;
              f = 1e - 2:1:100 e3;
               eta = panel.eta;
128
               phi set = 0:10:90;
              [ phi set.' h coincidence frequency (ms, D, c, phi set ).' ]
               t_set = [ ];
               h1 = figure(); ...
                              hold on;
                            % stem(octave_band_frequencies./(wo/(2*pi)), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on; stem(octave_band_frequencies, TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on; line([16e3 16e3], [0 65], 'Color', 'c');
138
141
                             %
```

```
 \% \ plot( \ f \ ./ \ (wo \ / \ (2*pi) \ ) \ , \ -10*log10 \ ( \ h \_ tau \_infinite \_rigid \_panel( \ f \ , \ wo, \ ms, \ s \ , \ rho0 \ , \ c \ , \ panel. \ eta \ ) \ ) \ , \ 'LineStyle' \ , \ '-' \ ) \ ; 
                 plot(f, -10*log10(h_tau_infinite_rigid_panel(f, wo, ms, s, rho0, c, panel.eta)),
                         LineStyle', '-');
                 for phi = phi_set
146
                        % plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_term1( rho0, c, phi ) ./ ( h_tau_term2(
                                 {\tt rho0}\;,\;\; {\tt c}\;,\;\; {\tt phi}\;,\;\; {\tt D}\;,\;\; {\tt eta}\;,\;\; {\tt f}\;\;\;)\;\;+\;\; {\tt h\_tau\_term3}\left(\;\; {\tt f}\;,\;\; {\tt ms}\;\;, {\tt D}\;,\;\; {\tt phi}\;\;\;\right)\;\;)\;\;,\;\;\; {\tt 'Color'}\;,
                        LineStyle', '-', 'Marker', 'none');
% plot(f./(wo/(2*pi)), -10*log10(h_tau_infinite_flexible_panel(f, rho0, c, phi, D
                         , panel.eta ) ), 'LineStyle', '--', 'Marker', 'none' );
plot( f, -10*log10( h_tau_term1( rho0, c, phi ) ./ ( h_tau_term2( rho0, c, phi, D, eta, f
                                   ) + h tau term3(f, ms, D, phi))), 'Color', 'r', 'LineStyle', '-', 'Marker',
                                 none ');
                        \% plot(f, -10*log10(h_tau_infinite_flexible_panel(f, rho0, c, phi, D, panel.eta)), '
                                 LineStyle', '--', 'Marker', 'none');
                         t set = [ t set; h tau infinite flexible panel(f, rho0, c, phi, D, panel.eta)];
                end
156
                 grid on;
                 set ( gca, 'XScale', 'log');
                 axis([2e-3 100e3 -5 70]);
163
                 close (h1);
164
        N \text{ phi} = \text{size}(t \text{ set}, 1);
168
        temp1 = t set;
        temp2 = \overline{\sin} d (2*phi set).';
169
        \% \text{ temp2} = \text{sind}( \text{phi\_set}).';
        temp3 = t set .* repmat(temp2, 1, size(temp1, 2));
174
        tau d = 1/N phi .* nansum( temp3, 1 );
176
       tau d verify = nanmean( t set .* temp2, 1 );
178
179
180
        h2 = figure(); ...
181
182
                 hold on:
183
                stem (\ octave\_band\_frequencies\ ,\ TL,\ 'LineWidth'\ ,\ 0.5\ ,\ 'Marker'\ ,\ 'o'\ ,\ 'MarkerSize'\ ,\ 8\ ,\ 'burner'\ ,\ 'o'\ ,\ 'MarkerSize'\ ,\ 8\ ,\ 'burner'\ ,\ 'burne
184
                         MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
185
                 line( [ 16e3 16e3 ], [ 0 65 ], 'Color', 'b', 'LineWidth', 1.5 );
187
                 plot(f, -10*log10(h_tau_infinite_rigid_panel(f, wo, ms, s, rho0, c, panel.eta)),
                         LineStyle', '-'
                                                       );
                 for phi = phi set
                         plot(f, -10*log10(h_tau_term1(rho0, c, phi)./(h_tau_term2(rho0, c, phi, D, eta, f) + h_tau_term3(f, ms, D, phi))), 'Color', 'r', 'LineStyle', '-', 'Marker', '
191
                                 none ');
                        \% plot( f, -10*log10( h_tau_infinite_flexible_panel( f, rho0, c, phi, D, panel.eta ) ), '
                                 LineStyle', '--', '\overline{M}arker', 'none');
194
                 plot( f, -10*log10( tau_d ), 'LineStyle', '-', 'Marker', 'none', 'Color', 'm', 'LineWidth',
                         1.2 );
                 plot( f, -10*log10( tau_d_verify ), 'LineStyle', '-', 'Marker', 'none', 'Color', 'k', '
                         LineWidth + , 1.2 );
                 plot(f, -10*log10(h tau infinite rigid panel(f, wo, ms, s, rho0, c, panel.eta)./panel.
                         eta * ( 4*panel.length / ( panel.length^2 * critical_frequency ) ) ), 'LineStyle', '-',
                         Marker', 'none', 'Color', 'k', 'LineWidth', 1.2 );
                 grid on;
```

```
xlabel( 'Frequency [\$\{nc\{nega\}\{nega_o\}\}]'); ylabel( 'Transmission Loss [dB]'); \\
                    title ( 'Measured Panel Transmission Losses'
                    set ( gca, 'XScale', 'log');
                   axis([2e-3 200e3 -5 90]);
208
                    close (h2);
210 \% return
212 % Final Plot
214
         figure(); ...
216
                   hold on;
                   stem (\ octave\_band\_frequencies\ ,\ TL,\ 'LineWidth'\ ,\ 0.5\ ,\ 'Marker'\ ,\ 'o'\ ,\ 'MarkerSize'\ ,\ 8\ ,\ 'burner'\ ,\ 'o'\ ,\ 'MarkerSize'\ ,\ 8\ ,\ 'burner'\ ,\ 'burne
218
                            MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r'); hold on;
                    plot(f, -10*log10(h_tau_infinite_rigid_panel(f, wo, ms, s, rho0, c, panel.eta)),
                             LineStyle', '-');
                   plot(\ f,\ -10*log10(\ tau\_d\ ),\ 'LineStyle',\ '-',\ 'Marker',\ 'none',\ 'Color',\ 'm',\ 'LineWidth',
                            1.2 );
                   % plot( f, -10*log10( tau_d_verify ), 'LineStyle', '-', 'Marker', 'none', 'Color', 'k', '
                            LineWidth, 1.2);
                   line( [ 16e3 \ 16e3 ], [ 0 \ 65 ], 'Color', 'b', 'LineWidth', 1.5 );
228
229
                   grid on;
                   legend ( ...
                             'Target Transmission Loss', ...
                              'Infinite Rigid Panel', ...
                              'Infinite Flexible Panel with Diffuse Incidence', ...
                             'Finite Flexible Panel Model');
                   xlabel( 'Frequency [$\frac{\omega}{\omega o}$| '); ylabel( 'Transmission Loss [dB]');
                   title ( 'Measured Panel Transmission Losses'); set ( gca, 'XScale', 'log');
238
                    axis ( [2e-3 \ 200e3 \ -5 \ 90] );
244 % Plot Data and Model - Different Side Materials
245
         \% \text{ f} = 1 \text{ e} - 2:1 \text{ e} - 2:20 \text{ e} 3;
248 \% \text{ phi} = 15;
249 \quad \% \ \text{eta} = \text{panel.eta} \, ;
         %
        %
         % figure(); ...
                     plot (f./ (wo / (2*pi) ), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1)), 'LineStyle', '-'); hold on; plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 1/3600)), 'LineStyle', '-'); plot (f./ (wo / (2*pi)), -10*log10 (h_tau_infinite_rigid_panel_side_materials (f, wo, ms, s, rho0, c, panel.eta, 3600)), 'LineStyle', '-'); grid on;
253
         %
        %
254
255 %
        %
257 %
                                 legend ( ...
258 %
                                           'Same Fluid',
                                           Water to Air', ...
259
        %
261 %
                                          'Location', 'North');
        %
                       %
                        %
        %
                        set ( gca, 'XScale', 'log');
        %
         %
                        \% axis ( [ 40 12e3 -5 45] );
267
```

% Change is Stiffness

```
272 % figure(); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
    %
274
         %
276
    %
         %
    %
278
                %
    %
279
                 legend ( ...
    %
                      'Target TL Values', ...
                      'Infinite Rigid Panel with Normal Incidence Sound', ...
281
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
282
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s / 100) ^{\shortmid}, \ldots
                      'Location',
284 %
                                   'North');
285
    %
            xlabel( \ 'Frequency \ [\$\frac{\omega}{\omega_o}\$] \ ' \ ); \ ylabel( \ 'Transmission \ Loss \ [dB]' \ );
    %
            title ( 'Measured Panel Transmission Losses - Change in Stiffness ');
    %
287
            set ( gca , 'XScale', 'log' );
    %
288
289
    %
            \% axis ( [ 40 12e3 -5 45] );
    % Change in Mass
    % figure(); ...
          stem( octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
         plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*100, s, rho0, c, panel.eta )), 'LineStyle', '-');
plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms, s, rho0, c, panel.eta )), 'LineStyle', '-');
plot( f ./ (wo / (2*pi) ), -10*log10( h_tau_infinite_rigid_panel( f, wo, ms*1e-2, s, rho0, c, panel.eta )), 'LineStyle', '-');
    %
    %
    %
          c, panel.eta)), 'LineStyle', '-');
    %
                %
    %
                 legend ( ...
303 %
                      'Target TL Values', ...
                      'Infinite Rigid Panel with Normal Incidence Sound', ...
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s * 100)', ...
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (s / 100)', ...
306 %
    %
                      'Location', 'North');
    %
308
            xlabel( 'Frequency [\$\frac{\omega_0}^{}] ' ); ylabel( 'Transmission Loss [dB]' ); \\
    %
            title ( 'Measured Panel Transmission Losses - Change in Mass');
    %
    %
            set ( gca, 'XScale', 'log');
    %
            \% axis( [ 40 12e3 -5 45] );
314
316 %% Change in Loss Factor
318
    % figure( ); ...
          stem('octave_band_frequencies ./ (wo / (2*pi) ), TL, 'LineWidth', 0.5, 'Marker', 'o', 'MarkerSize', 8, 'MarkerEdgeColor', 'b', 'MarkerFaceColor', 'r' ); hold on;
319
         322 %
         plot( i ./ (wo / (2*pl) ), -lo*log10( i _tau_infinite_rigid_panel( i, wo, ins, s, rhoo, c, panel.eta*1e2 )), 'LineStyle', ':');

plot( f ./ (wo / (2*pl) ), -lo*log10( i _tau_infinite_rigid_panel( f, wo, ms, s, rhoo, c, panel.eta*1e-2 )), 'LineStyle', ':');
    %
324
    %
                %
    %
                 legend ( ...
326 %
                      'Target TL Values', ...
327 %
                      'Infinite Rigid Panel with Normal Incidence Sound', ...
    %
328
                      'Infinite Rigid Panel with Normal Incidence Sound (eta * 100)', ...
    %
                      'Infinite Rigid Panel with Normal Incidence Sound (eta / 100)', ...
    %
                     'Location', 'North');
    %
            %
            xlabel( 'Frequency [$\frac{\omega}{\omega o}$] ' ); ylabel( 'Transmission Loss [dB]' );
332
    %
333 %
            title ( 'Measured Panel Transmission Losses - Change in Loss Factor');
            set ( gca, 'XScale', 'log', 'YScale', 'log');
334 %
            \% axis( [ 40 12e3 -5 45] );
    %
```

```
338
339 % Clean—up
340
       % return
342
       if ( ~isempty( findobj( 'Type', 'figure') ) )
  monitors = get( 0, 'MonitorPositions');
  if ( size( monitors, 1 ) == 1 )
     autoArrangeFigures( 2, 2, 1 );
  elseif ( 1 < size( monitors, 1 ) )
     autoArrangeFigures( 2, 2, 1 );
end</pre>
343
344
345
346
348
349
        end \\
351
352
353
        fprintf(\ 1,\ '\ \ \ );
354
356
357 % Reference(s)
```

```
2
    % Synopsis
4
   % Slide 8 - Noise Reduction and Transmission Loss
    % Volume of the enclosure is much bigger than the machine. Diffuse sound field in the enclosure.
9
10
   % Environment
    % close all; clear; clc;
14
    % restoredefaultpath;
16
    \% addpath( genpath( '' ), '-begin' ); addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
18
20~\% set ( 0, 'DefaultFigurePosition', [ 400~400~900~400~] ); % [ left bottom width height ] 21~ set ( 0, 'DefaultFigurePaperPositionMode', 'manual' );
    set( 0, DefaultFigureVindowStyle', 'normal');
set( 0, 'DefaultLineLineWidth', 0.8 );
set( 0, 'DefaultTextInterpreter', 'Latex');
24
26
   format ShortG;
28
   pause(1);
29
   PRINT FIGURES = 0;
   % Define Machine
34
    machine.area = 3; \% m<sup>2</sup>
    machine.absorption = 0.07; % Sabine
    machine D = 1; % Unitless - In air.
38
40
    machine.distance = 10; % m
41
42
44 %% Data
45
    \begin{array}{l} octave\_band\_frequencies = [\ 250\ 500\ 1000\ 2000\ 4000\ ].\,\,^{'}; \quad \% \ Hz \\ Lw = [\ 105\ 115\ 106\ 108\ 119\ ].\,\,^{'}; \quad \% \ dB \ re: \ 1 \ pW \end{array}
46
47
         % [ octave_band_frequencies Lw ]
48
49
   % figure(); ...
           h1 = stem( octave band frequencies, Lw, 'Marker', '.', 'MarkerSize', 12, 'Color', 'r');
         hold on;
           h2 = line( [ 2e2 5e3 ], [ 30 30 ] ); grid on; legend( [ h1 h2 ], 'Current Sound Pressure Levels', 'Target Sound Pressure Level', '
52 %
53 %
         Location ', 'North');
                     'Frequency [Hz]'); ylabel('Sound Pressure Level [dB re: 20e-6 Pa]');
54
            title ( 'Sound Power Level Versus Octave Band Center Frequency ');
55 %
56 %
            axis( [ 150 6e3 0 140 ] );
set( gca, 'XScale', 'log');
    %
    %
58
59
60
61
62 % Per Octave Band Insertion Loss
    Lp 10 meters = Lw + 10*log10 ( machine.D /( 4*pi* machine.distance^2 ) ); % dB re: 20e-6 Pa
         % octave band frequencies Lp 10 meters
66
67
       The value of R is infinite. The machine is outside in open air.
68
    octave\_band\_IL \ = \ Lp\_10\_meters \ - \ 30\,;
70
         % [ octave_band_frequencies octave_band_IL ]
```

```
74 % Anonymous Function for Insertion Loss
    h_{IL\_large} = @(Sw, alpha_w, Si, alpha_i, TL) \\ 10*log10(1 + (Sw*alpha_w + Si*alpha_i)./(Sw*alpha_w, Si, alpha_i).
76
          + Si)*10^(TL/10) );
77
78
79
80 % Find Values of TL and Aborption that will Meet the Target Insertion Loss — Ground Reflecting
81
82 % Assumption(s):
83 %
    %
84
         1.)
              The ground is a hard reflecting survice
   %
         2.)
              The enclosure is a cube.
8.5
86
    %
             There is no noise transmission through the ground.
87
    enclosure.dimension = 2; % m
88
         enclosure.area = 6 * enclosure.dimension^2; % 20 m^2
89
   % https://www.controlnoise.com/wp-content/uploads/2022/02/Acoustic-Enclosures-Datasheet.pdf
    % https://www.cecoenviro.com/wp-content/uploads/2023/12/Acoustic-Enclosures-8pp-A4-web.pdf
94
    \% \ \ https://www.controlnoise.com/product/acoustic-enclosures/
97
    switch (3)
98
         case 1
             \% 250 Hz - QBV-2
             alpha\_w = 0.27; % From specification sheet.
             TL = 20; % From specification sheet.
                 IL_{estimates}(1) = h_{IL_{arge}(enclosure.area, alpha_w, machine.area, machine.
                     absorption, TL);
             \% 500 Hz - QBV-2
             alpha\_w = 0.96; % From specification sheet.
             \overline{TL} = 29; % From specification sheet.
                 IL\_estimates(2) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                     absorption, TL );
             \% 1 kHz - QBV–2
             \% alpha w = 1.13; \% From specification sheet.
             alpha\_w = 0.99; \ \% \ From \ specification \ sheet. \ See \ comment \ on \ slide \ 28 \ of \ Lecture \ 10.
             TL = 40; % From specification sheet.
                 IL\_estimates\left(3\right) \ = \ h\_IL\_large\left( \ enclosure.area \, , \ alpha\_w \, , \ machine.area \, , \ machine.
                     absorption, TL);
116
             \% 2 kHz - QBV-2
118
             \% alpha w = 1.08; \% From specification sheet.
             alpha\_w = 0.99; ~\% \ \text{From specification sheet}. ~~\text{See comment on slide 28 of Lecture 10}.
119
             TL = 50; % From specification sheet.
                 IL\_estimates\left(4\right) \ = \ h\_IL\_large\left(\ enclosure.area \, , \ alpha \ w \, , \ machine.area \, , \ machine.
                     absorption, TL);
             \% 4 kHz - QBV-2
             alpha\_w\,=\,\,0.99\,;\quad\%\,\, \text{From specification sheet}\,.
                  55; % From specification sheet.
                 IL estimates (5) = h IL large (enclosure.area, alpha w, machine.area, machine.
                     absorption, TL );
128
         case 2
             \% Note: Aboseption values are carried over from QBV-2.
             \% 250 Hz - QBV-3
             alpha_w = 0.27; % From specification sheet.
             TL = 25; % From specification sheet.
                 138
             \% 500 Hz - QBV-2
             alpha w = 0.96; % From specification sheet.
139
             TL = 33; % From specification sheet.
                 IL\_estimates\,(2\,) \ = \ h\_IL\_large\,(\ enclosure.area\,,\ alpha\_w\,,\ machine.area\,,\ machine.
                      absorption, TL);
             \% 1 kHz - QBV-2
```

```
\% alpha w = 1.13; \% From specification sheet.
            alpha\_w = 0.99; ~\% \ \text{From specification sheet}. ~~\text{See comment on slide 28 of Lecture 10}.
            TL = 46; % From specification sheet.
                IL\_estimates\left(3\right) \ = \ h\_IL\_large\left( \ enclosure.area\ , \ alpha\_w\ , \ machine.area\ , \ machine.
                    absorption, TL);
148
149
            \% 2 kHz - QBV-2
            \% alpha_w = 1.08; \% From specification sheet.
            alpha\_w = 0.99; \quad \% \ \text{From specification sheet.} \quad \text{See comment on slide 28 of Lecture 10.}
            TL = 53; % From specification sheet.
                IL\_estimates (4) = h\_IL\_large( \ enclosure.area \, , \ alpha\_w \, , \ machine.area \, , \ machine.
                    absorption, TL );
            \% 4 kHz - QBV-2
            alpha\_w = \stackrel{.}{0}.99; \quad \% \ From \ specification \ sheet \, .
156
            TL = 58; % From specification sheet.
                IL\_estimates(5) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                    absorption, TL );
        case 3
163
            % Note: Aboseption values are carried over from QBV-2.
            \% 250 Hz - QBV–3
            alpha\_w \, = \, 0.99\,; \quad \% \ From \ specification \ sheet \, .
            TL = 39; % From specification sheet.
                \% 500 Hz - QBV-2
            alpha_w = 0.96; % From specification sheet.
            TL = 59; % From specification sheet.
172
                174
            \% 1 kHz - QBV-2
            \% alpha_w = 1.13; \% From specification sheet.
            alpha \overline{w}=0.99; % From specification sheet. See comment on slide 28 of Lecture 10.
            TL = 68; % From specification sheet.
178
                179
            \% 2 kHz - QBV–2
181
            \% alpha_w = 1.08; \% From specification sheet.   
alpha_w = 0.99; \% From specification sheet. See comment on slide 28 of Lecture 10.
182
183
184
            TL = 67; % From specification sheet.
185
                IL\_estimates (4) = h\_IL\_large( enclosure.area, alpha\_w, machine.area, machine.
                    absorption, TL);
186
            \% 4 kHz - QBV-2
187
            alpha w = 0.91; % From specification sheet.
188
            TL = 72; % From specification sheet.
189
                IL\_estimates(5) = h\_IL\_large(enclosure.area, alpha\_w, machine.area, machine.
                    absorption, TL);
192
    end
195
                                           (octave band IL - IL estimates.')
    [ octave band IL
                        IL estimates.'
198
    % What is the most restrictive case?
   5% Find Values of TL and Aborption that will Meet the Target Insertion Loss - Ground with Cover
    % Assumption(s):
    %
    %
             The ground is covered with the absorption material.
        2.)
             The enclosure is a cube.
208
209
    % Clean-up
    if ( ~isempty ( findobj ( 'Type', 'figure' ) )
```

```
2
   % Synopsis
4
   % Lecture 11, Wednesday, February 19, 2025
   % The compressor elevated above the ground.
9
10
  % Environment
13
   close all; clear; clc;
14
   % restoredefaultpath;
16
   \% addpath( genpath( '' ), '-begin' ); addpath( genpath( '../40 Assignments/00 Support' ), '-begin' );
18
19
20~\% set ( 0, 'DefaultFigurePosition', [ 400~400~900~400~] ); % [ left bottom width height ] 21~ set ( 0, 'DefaultFigurePaperPositionMode', 'manual' );
   set( 0, DefaultFigureVindowStyle', 'normal');
set( 0, 'DefaultLineLineWidth', 0.8 );
set( 0, 'DefaultTextInterpreter', 'Latex');
24
26
   format ShortG;
28
  pause( 1 );
29
30 PRINT FIGURES = 0;
   %% Define Anonymous Functions
34
  \overline{S})/(\overline{p}i*h^2);
   39
  % Define Compressor
43
44
   compressor.width = 1; \% m
   \mathtt{compressor.depth} \ = \ 1\,; \quad \% \ \mathrm{m}
46
   compressor.height = 2; % m
47
       compressor.area = 2*(compressor.width * compressor.depth) + 2*(compressor.width * compressor.
           height) + 2*(compressor.depth * compressor.height); \% 3 m^2
48
       compressor.volume = compressor.width * compressor.depth * compressor.height; % m^3
49
   compressor.power level = 105; % dB re: 1e-12 Watts
   compressor frequency = 50; % Hz
53
   c = 343; \% m/s
   rho0 = 1.2; % kg/m^3 CHECK
56
58
59 % Sound Level Target
   sound_level_target = 82; % dB re: 20e-6 Pascals
61
62
65 % Define Workshop
66
  R = 40; % m^2 or Sabins
68
   7% Define Close-fitting Enclosure
```

```
73 helmholtz factor = (2 * pi * compressor.frequency) / c; % 0.92 m
 74
 75 % For a small enclosure, k*d \ll 1. Therefore d \ll 1.1.
 76 	 d = 0.75:
      d = 0.25;
 78
       % d = 1;
 79
               \% helmholtz factor * d; \% 0.69
 80
 81
       enclosure.width = compressor.width + d;
       enclosure.depth \ = \ compressor.depth \ + \ d\,; \quad \% \ m
 82
 8.3
       enclosure.height = 3; \% m; compression height is 2 m
 84
       % enclosure.height = compressor.height + d;
                enclosure.area \,=\, 2*(\,enclosure.width \,\,*\,\,enclosure.depth\,) \,\,+\,\, 2*(\,enclosure.width \,\,*\,\,enclosure\,.
 85
                       height) + 2*(enclosure.depth * enclosure.height);
 86
                enclosure.volume = enclosure.width * enclosure.depth * enclosure.height;
 87
 88
       enclosure.E = 3.6e9; % Pascals
        enclosure.thickness = 3.81e-2; % m
 8.9
       enclosure.density = 800; % kg/m<sup>3</sup>
       enclosure.poisson ratio = 0.25; % Unitless
 91
 93 % Clamped boundary conditions.
 97
       % Calculate Diffuse Sound Pressure Level
 9.8
 99
       % Assume distance is beyond the critical distance, so the distance value is
       % large and its associated term is not relevant.
        sound pressure level = 105 + 10*log10(4/R); % 95 dB SPL
106 % Calculate the Required Insertion Loss
108
       target insertion loss = sound pressure level - 82 \% 13 dB
112 % Insertion Loss
114 % For the insertion loss to be high, we need:
116 %
                        Compliance of the air to be high; volume of enclosure must be large.
               1.)
      %
               2.) Compliance of each enclosure wall to be low; low area, high stiffness, edges clamped).
118
                              AREA IS THE DOMINATE FACTOR OVER VOLUME.
       \% The correction factor for clamped walls. See Figure 12.4 on slide 9 of the Lecture 11 notes.
        aspect ratio = enclosure.height / enclosure.width; % 1.7
                correction factor = 2; % Approximate value read from the Figure 12.4.
124
        bending\_stiffness = (enclosure.E * enclosure.thickness \^{3}) / (12*(1-enclosure.poisson\_ration)) / (
                ^{2} ) ; % 1.78 e7
               h_{\text{wall\_compliance}} = @(\text{wall\_area}, \text{correction\_factor}) (0.001 * \text{wall\_area}^3 *
                       correction factor ) / bending stiffness;
128 Ca = enclosure.volume / (rho0 * c^2);
129
131 % Top
       top.area = enclosure.width * enclosure.depth;
       top.aspect ratio = max( enclosure.width, enclosure.depth ) / min( enclosure.width, enclosure.
               depth );
134
       top.correction factor = 3.8;
               top.compliance = h_wall_compliance( top.area, top.correction_factor );
136
138 % Side 1
139
        side 1.area = enclosure.depth * enclosure.height;
        side\_1.aspect\_ratio = max(\ enclosure.width\,,\ enclosure.height\ )\ /\ min(\ enclosure.width\,,\ enclosure.width).
               height);
141
        side 1.correction factor = 2;
               __side_1.compliance = h_wall_compliance( side_1.area, side_1.correction_factor );
145
       side 2.compliance = side 1.compliance;
```

```
148
            % Side 3
             side 3.area = enclosure.width * enclosure.height;
                           _3.aspect_ratio = max( enclosure.width, enclosure.height ) / min( enclosure.width, enclosure.
                          height);
              side 3. correction factor = 2;
                          side_3.compliance = h_wall_compliance( side_3.area, side_3.correction_factor );
154
            % Side 4
              side 4.compliance = side 3.compliance;
158
              estimated insertion loss = 20*\log 10 ( 1 + \mathrm{Ca} / (top.compliance + 2*\mathrm{side} 1.compliance + 2* side 3.
                          compliance)); -\% 59.2 dB
            % Compliance of the Air Intake
             \begin{array}{l} air\_intake\_radius = 10\,e-2; \quad \% \ m \\ air\_intake\_thickness = enclosure.thickness; \quad \% \ m \\ air\_intake\_frequency = 50; \quad \% \ Hz \end{array}
165
166
                          air_intake_angular_frequency = 2*pi*air_intake_frequency; % radians/s
             viscosity = 1.5 e-5; \% m^2/s
            h = 0.3; % CHECK
173
            f = 50;
                         174
                          term\_2 = h\_RA\_term\_2 ( rho0 , c , pi*(air\_intake\_radius*2)^2/4 , 2*pi*f/c , sqrt( (2*3.178e-5)) + (2*3.178e-5) + (2*3.178e-5
                          [-rho0], [-pi * 0.1, 2*pi*f, 0.3];
                                      impedance.real = term 1 + term 2 + term 3;
178
           % Deng (1998)
181
             epsilon = 1;
182
                         L o = air intake radius * (1.27 / (1 + 1.92 * epsilon) - 0.086);
184
             L e = enclosure.thickness + 2*L o;
185
                         impedance.imaginary = 1j * rho0 * (2 * pi * f) * L_e / ( pi*0.1^2/4 );
186
187
             impedance.net \ = \ impedance.real \ + \ impedance.imaginary \, ;
188
189
                          compliance_of_hole = 1 / impedance.net;
                                      Cl = a\overline{b}s(\overline{compliance\_of\_hole});
              estimated\_insertion\_loss
             196
             13 - estimated insertion loss with hole;
198
199
              critical\_frequency = c^2/(2*pi)*sqrt (\ enclosure.density * enclosure.thickness / bending\_stiffness | \ density = critical\_frequency | \ density = critical\_frequen
            \% The critical frequency is 25 Hz.
204
            % The frequency of the compressor is 50 Hz.
206
210 % Clean—up
211
              if ( ~isempty( findobj( 'Type', 'figure')))
    monitors = get( 0, 'MonitorPositions');
                                      if (size(monitors, 1) == 1)
                                                  autoArrangeFigures(2,2,1);
216
                                       elseif (1 < size (monitors, 1))
```