

Signals & Systems

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Chapter 8 Communication Systems

Sect. 8.1 Complex Exponential and Sinusoidal Amplitude Modulation

Sect. 8.2 Demodulation for Sinusoidal AM

Sect. 8.3 Frequency Division Multiplexing

Sect. 8.4 Single-Sideband Sinusoidal Amplitude Modulation

Sect. 8.5 Amplitude Modulation with a Pulse-Train Carrier

Sect. 8.6 Pulse Amplitude Modulation

Sect. 8.7 Sinusoidal Frequency Modulation

Sect. 8.8 Discrete-Time Modulation

Sect. 8.9 Frequency-Shift Keying, Phase-Shift Keying,
and Quadrature Amplitude Modulation

Communication:

Transmission / receiving a signal

Modulation:

The general process of embedding an information-bearing signal into a second signal.

Amplitude modulation (AM):

Info of the input signal is embedded in the **amplitude** of the modulation output

Frequency modulation (FM):

Info of the input signal is embedded in the **frequency** of the modulation output.

Demodulation:

Extracting the information-bearing signal from the modulation output.

Multiplexing:

Making possible the simultaneous transmission of more than one signal.

Sect. 8.1 Complex Exponential & Sinusoidal Amplitude Modulation & Demodulation

- Amplitude Modulation

$$y(t) = x(t)c(t)$$

$x(t)$: modulating signal (the input of modulation)

$c(t)$: carrier signal with carrier frequency ω_c

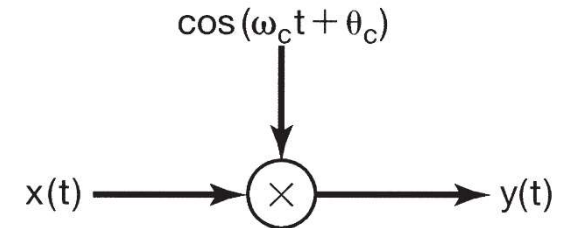
$y(t)$: modulated signal (the output of modulation)

$$c(t) = e^{j(\omega_c t + \theta_c)} \text{ or } c(t) = \cos(\omega_c t + \theta_c).$$

choose $\theta_c = 0$, so that the modulated signal is $y(t) = x(t)e^{j\omega_c t}$.

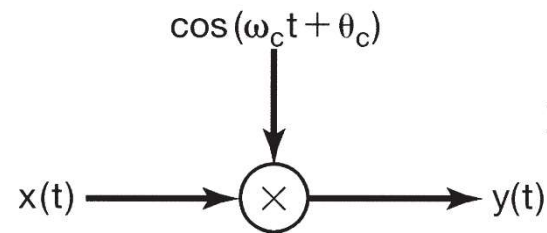
denoting the Fourier transforms of $x(t)$, $y(t)$, and $c(t)$, respectively,

$$Y(j\omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta)C(j(\omega - \theta))d\theta.$$



- Amplitude Modulation (cont'd)

$$C(j\omega) = \pi[\delta(\omega - \omega_c) + \delta(\omega + \omega_c)], \quad \theta_c = 0$$



$$Y(j\omega) = \frac{1}{2}[X(j\omega - j\omega_c) + X(j\omega + j\omega_c)].$$

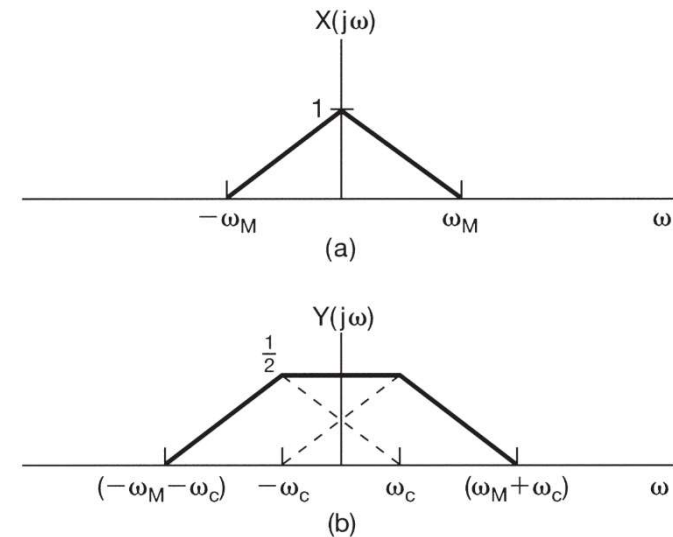
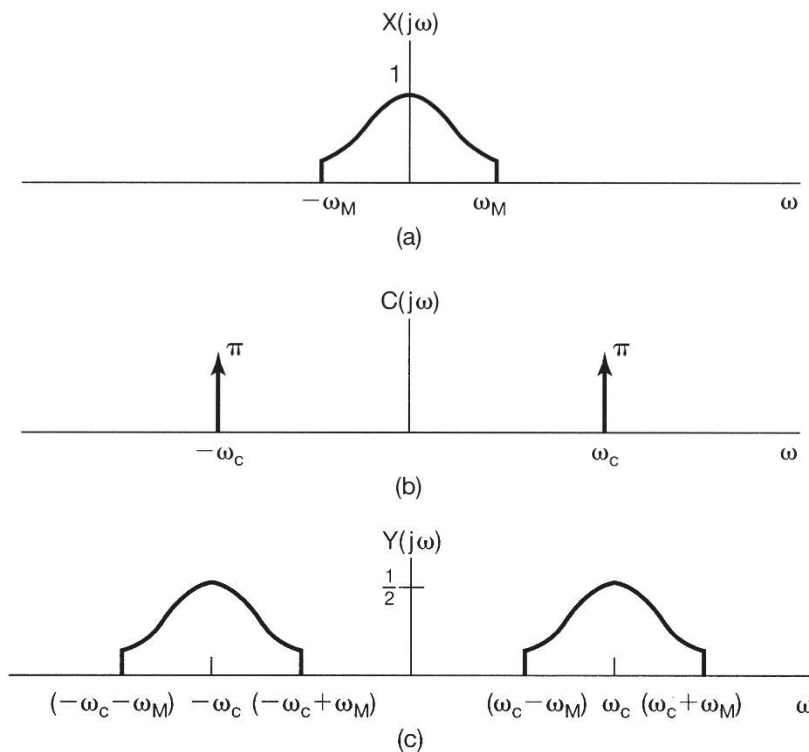
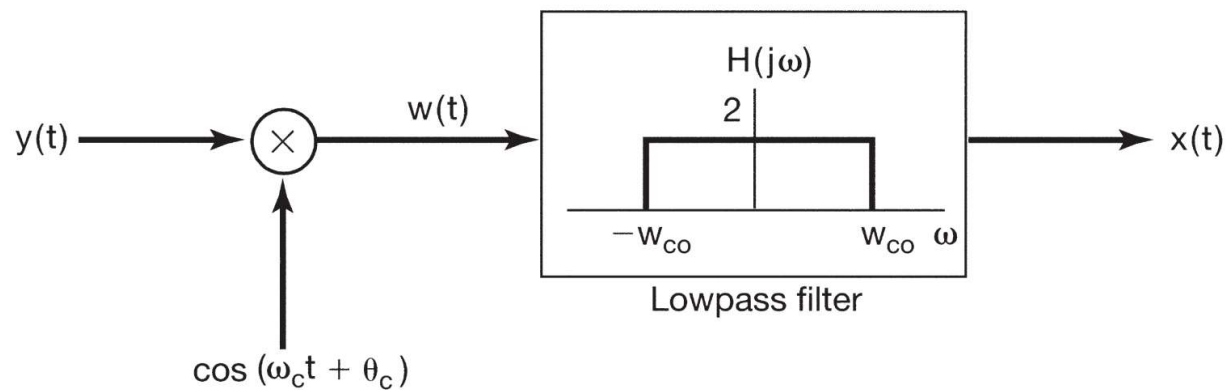
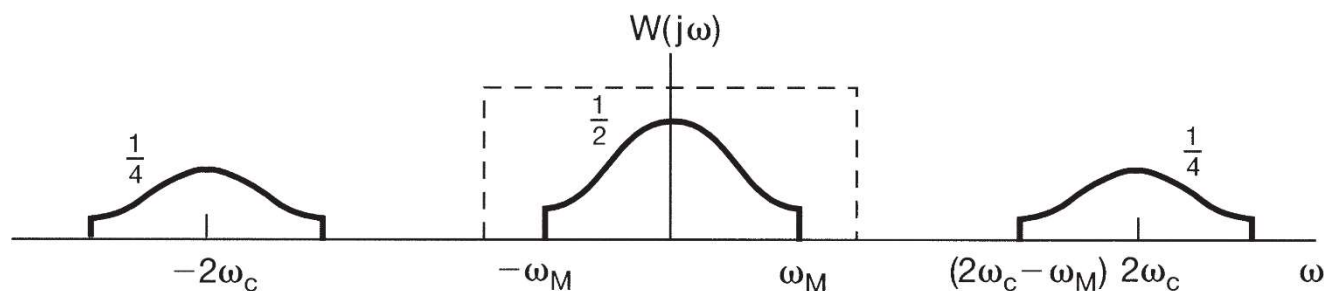
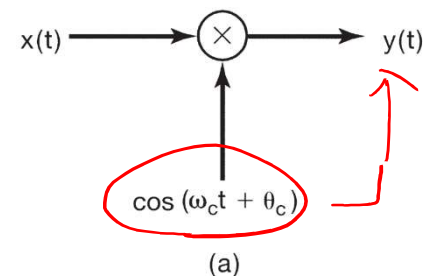


Figure 8.5 Sinusoidal amplitude modulation with carrier $\cos \omega_c t$ for which $\omega_c = \omega_M/2$: (a) spectrum of modulating signal; (b) spectrum of modulated signal.

Sect. 8.2 Demodulation for Sinusoidal AM

- Synchronous Demodulation of $y(t) = x(t) \cos \omega_c t$.

$$w(t) = \frac{1}{2}x(t) + \frac{1}{2}x(t) \cos 2\omega_c t.$$



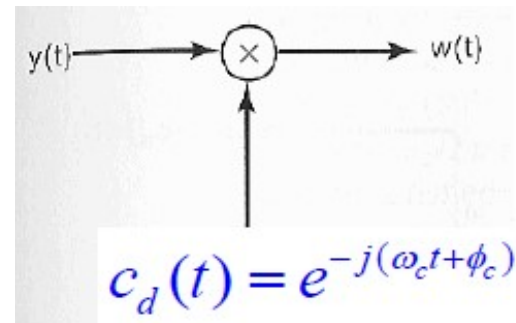
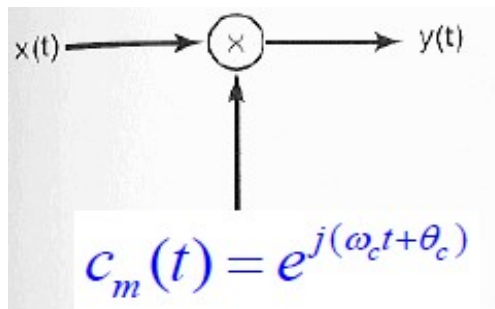
Sect. 8.2 Demodulation for Sinusoidal AM

- Synchronous or Asynchronous Demodulation

$$y(t) = e^{j(\omega_c t + \theta_c)} x(t),$$

$$w(t) = e^{-j(\omega_c t + \phi_c)} y(t),$$

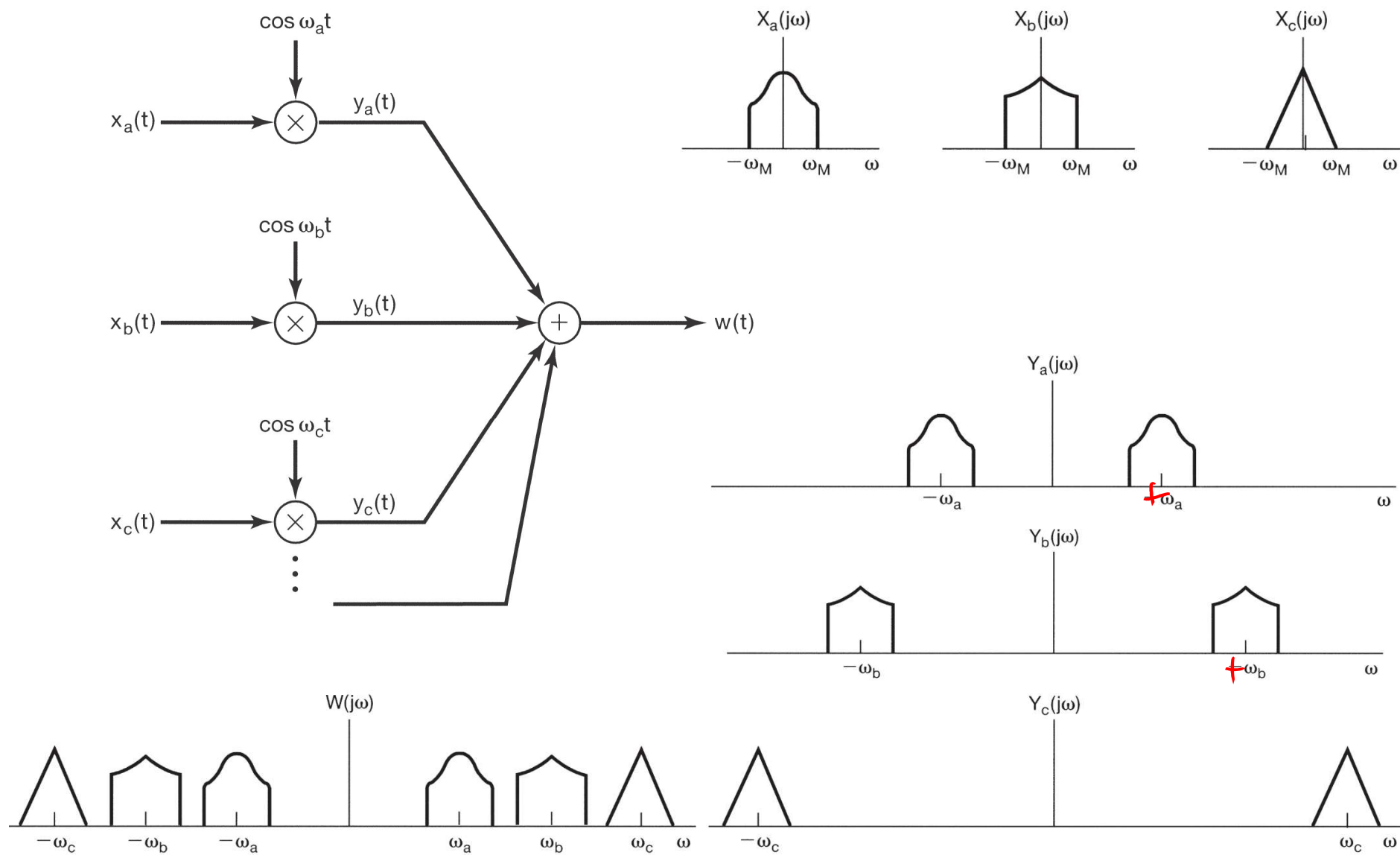
$$w(t) = e^{j(\theta_c - \phi_c)} x(t).$$



\Rightarrow Only ensure $|x(t)| = |\omega(t)|$

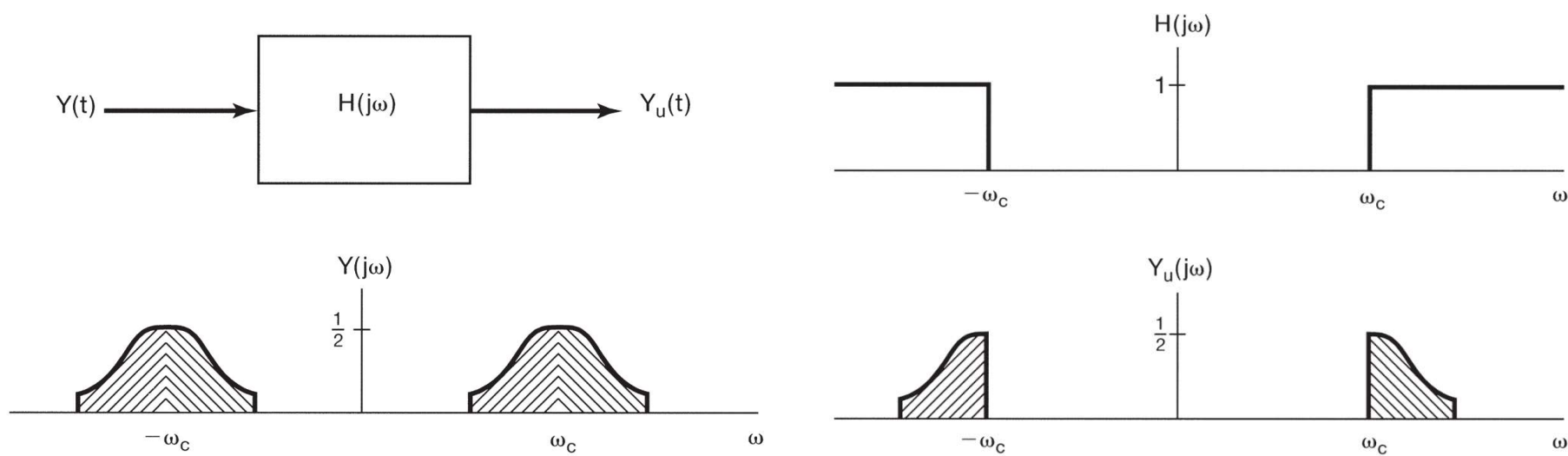
\Rightarrow If $x(t) > 0$, we get $x(t) = |\omega(t)|$

Sect. 8.3 Frequency Division Multiplexing



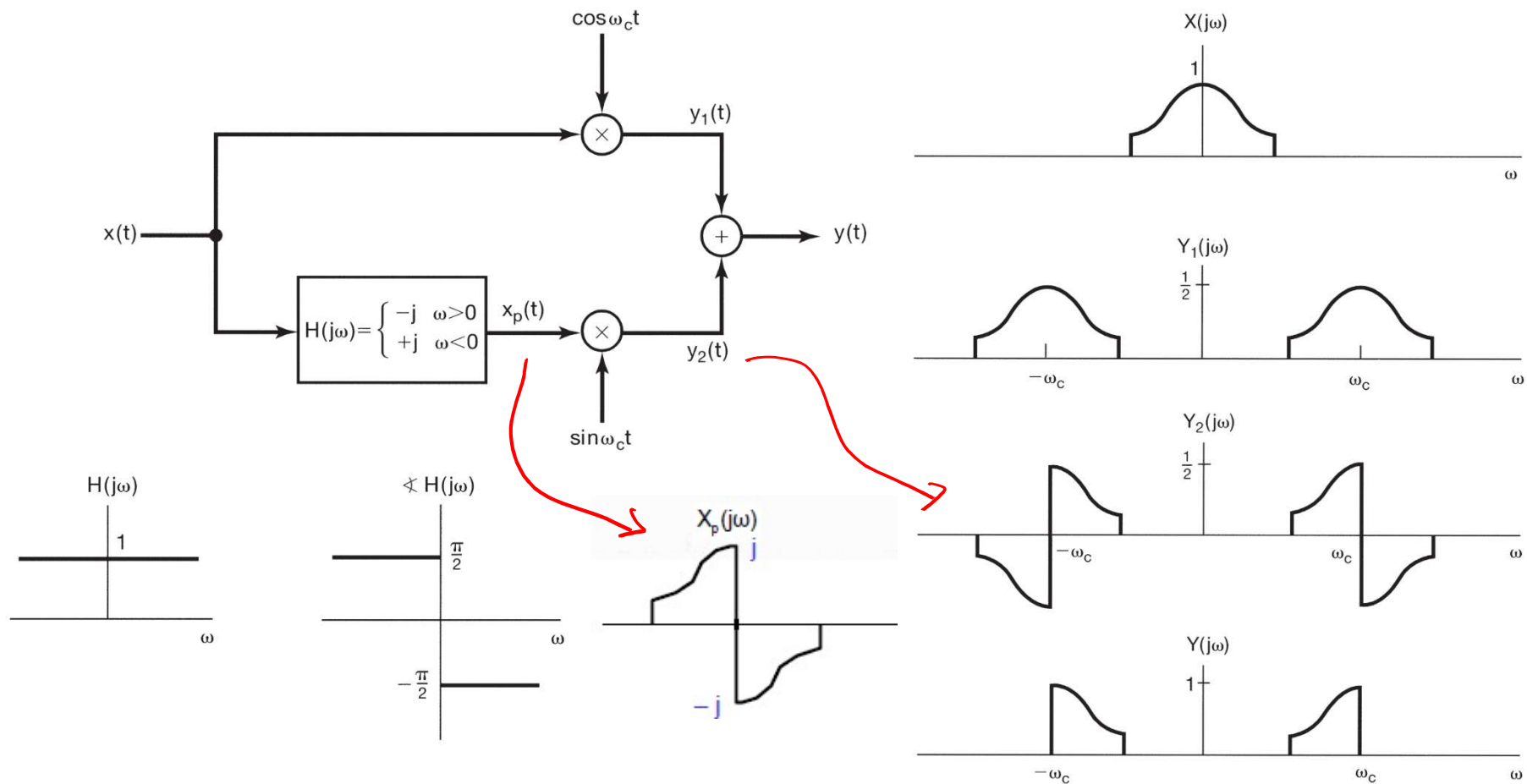
Sect. 8.4 Single-Sideband Sinusoidal AM

- Generating Sidebands Using **Ideal HPF**

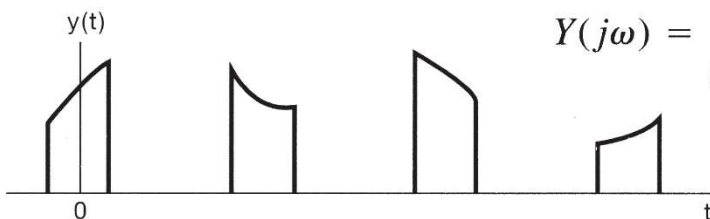
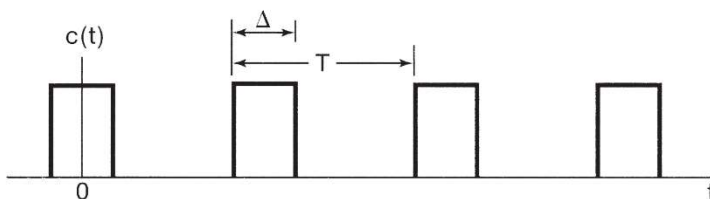
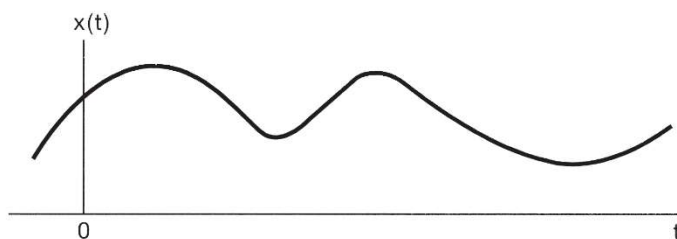
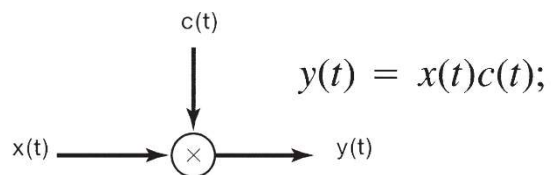


Sect. 8.4 Single-Sideband Sinusoidal AM

- Generating Sidebands Using **Phase Shifting**



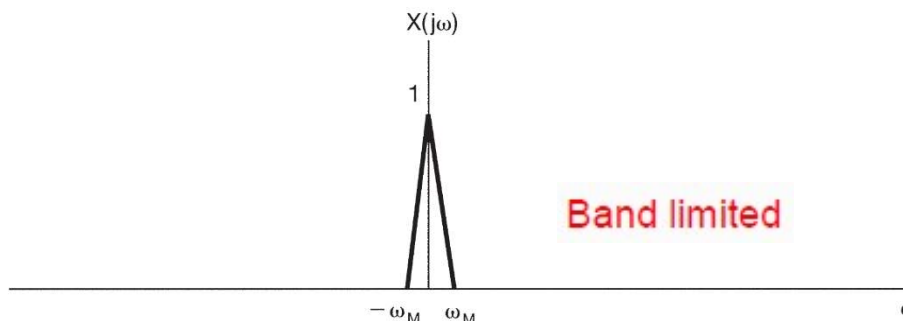
Sect. 8.5 AM with a Pulse-Train Carrier



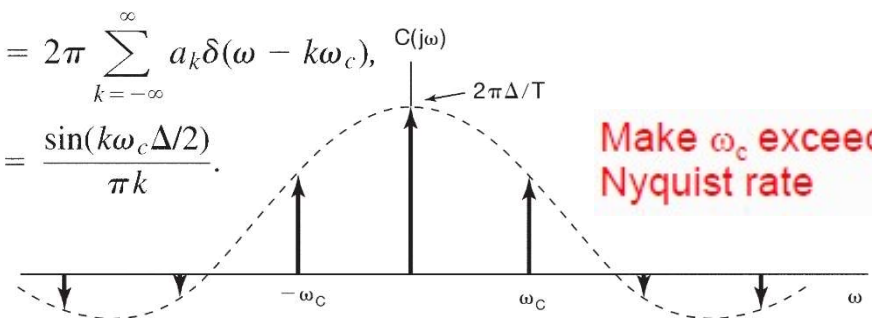
$$Y(j\omega) = \sum_{k=-\infty}^{+\infty} a_k X(j(\omega - k\omega_c)).$$

$$C(j\omega) = 2\pi \sum_{k=-\infty}^{\infty} a_k \delta(\omega - k\omega_c),$$

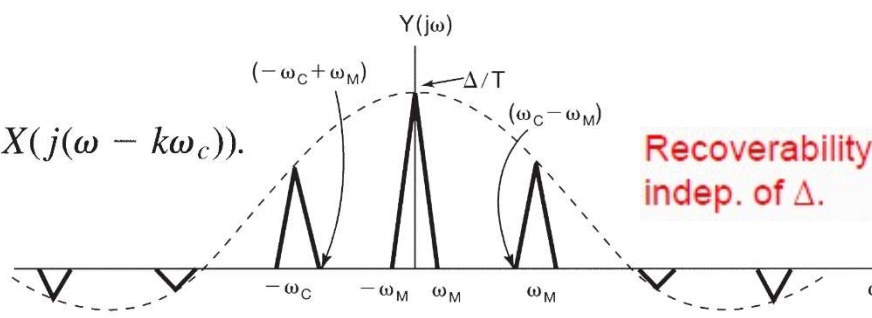
$$a_k = \frac{\sin(k\omega_c \Delta/2)}{\pi k}.$$



(a)

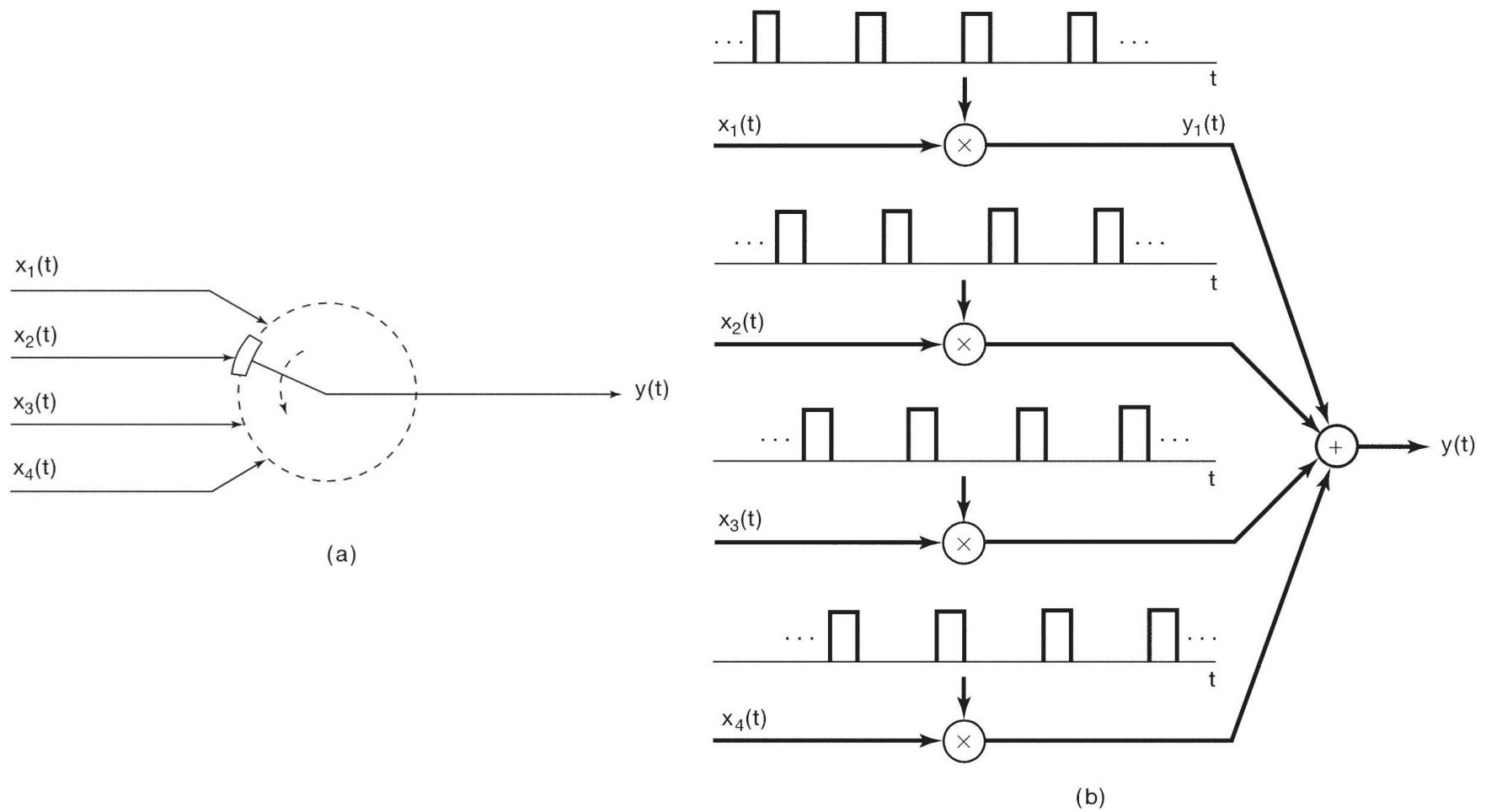


(b)



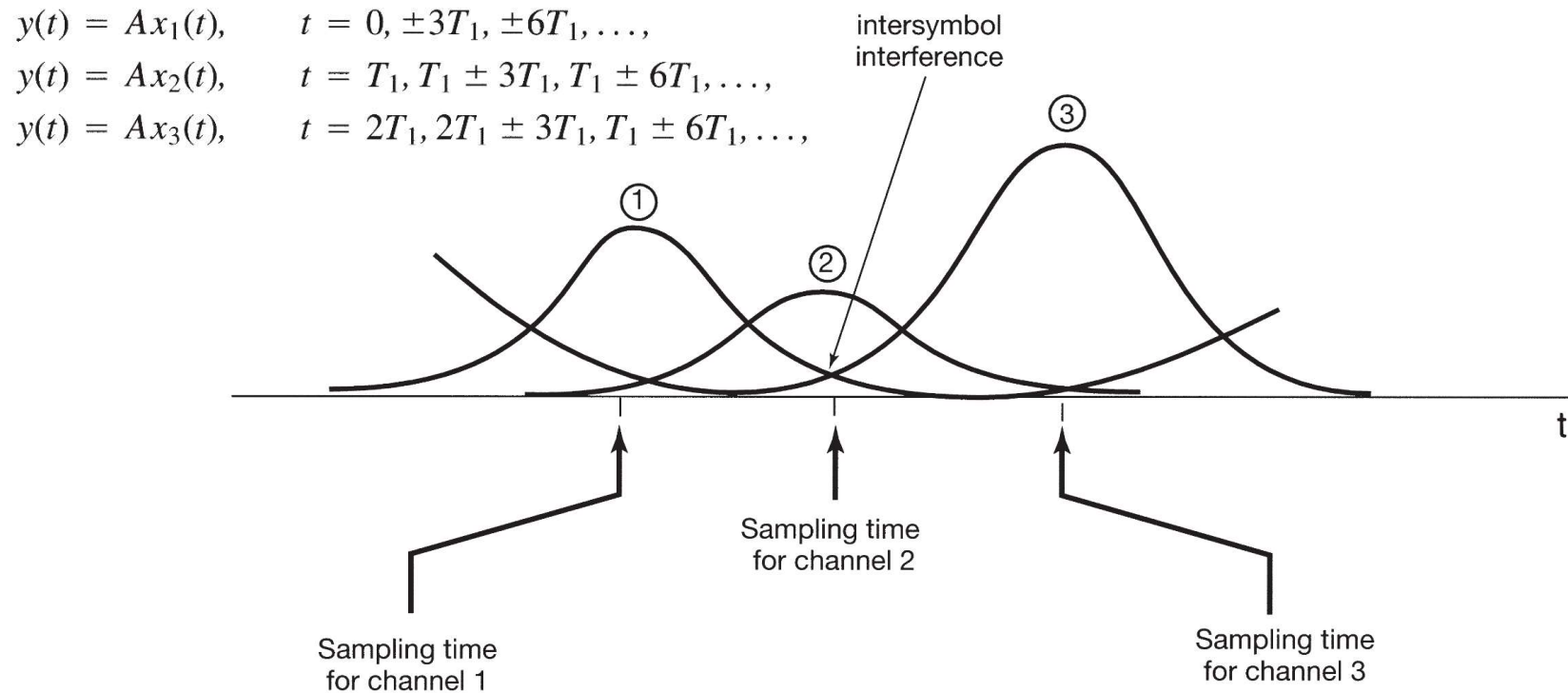
(c)

8.5.2 Time-Division Multiplexing (TDM)



Sect. 8.6 Pulse Amplitude Modulation

- Intersymbol Interference in PAM Systems



Filtering due to non-ideal frequency response of the channel causes a smearing of the pulses, which can cause the received pulses to overlap in time. This is referred to as **intersymbol interference**.

Sect. 8.7 Sinusoidal Frequency Modulation

- Frequency Modulation
 - Modulating signal controls the **frequency** of a sinusoidal carrier.
 - For AM, the peak **amplitude** of the envelope of the modulated signal can have a large dynamic range.
 - For FM, a constant envelope is generated for the modulated signal. This means that an FM transmitter can always have a better quality than AM reception.
 - But, the price to pay...the **bandwidth**!

Sect. 8.7 Sinusoidal Frequency Modulation

- **Angle Modulation** $c(t) = A \cos(\omega_c t + \theta_c) = A \cos \theta(t),$

- **Phase Modulation**

Use the modulating signal $x(t)$ to vary the **phase** θ_c

$$y(t) = A \cos \theta(t) = A \cos[\omega_c t + \theta_c(t)]$$

$$\theta_c(t) = \theta_0 + k_p x(t)$$

$$\frac{d\theta(t)}{dt} = \omega_c + k_p \frac{dx(t)}{dt}$$

$$\theta(t) = \omega_c t + \theta_0 + k_p x(t),$$

- **Frequency Modulation**

Use the modulating signal $x(t)$ to vary the **derivative of the angle**

$$y(t) = A \cos(\theta(t))$$

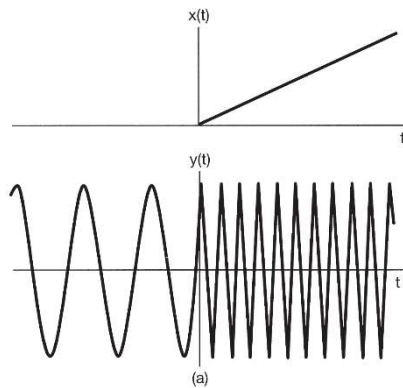
$$\frac{d\theta(t)}{dt} = \omega_c + k_f x(t)$$

$$\theta(t) = \omega_c t + \theta_0 + k_f \int x(t)$$

Sect. 8.7 Sinusoidal Frequency Modulation

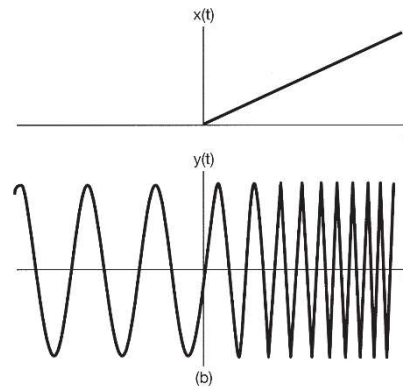
- Phase & Frequency Modulation

Phase
modulation



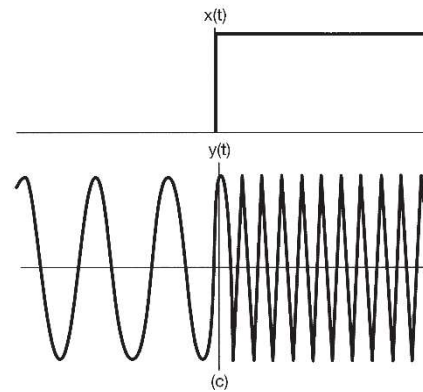
$$\theta(t) = \omega_c t + \theta_0 + k_p x(t),$$

Frequency
modulation

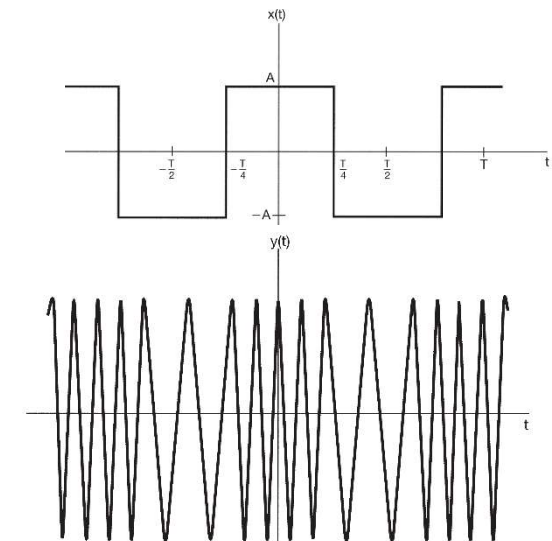


$$\theta(t) = \omega_c t + \theta_0 + k_f \int x(t)$$

Frequency
modulation



Frequency
modulation



$$y(t) = r(t) \cos[(\omega_c + \Delta\omega)t] + r\left(t - \frac{T}{2}\right) \cos[(\omega_c - \Delta\omega)t],$$

Sect. 8.7 Sinusoidal Frequency Modulation

- Instantaneous Frequency

$$y(t) = A \cos \theta(t),$$

$$\omega_i(t) = \frac{d\theta(t)}{dt}.$$

- Phase Modulation:

$$\omega_i = \frac{d\theta(t)}{dt} = \omega_c + k_p \frac{dx(t)}{dt}$$

- Frequency Modulation:

$$\omega_i = \frac{d\theta(t)}{dt} = \omega_c + k_f x(t)$$

Sect. 8.7 Sinusoidal Frequency Modulation

- Narrowband FM

$$x(t) = A \cos \omega_m t.$$



$$\omega_i(t) = \omega_c + k_f A \cos \omega_m t,$$

$$\omega_i(t) = \frac{d\theta(t)}{dt}$$

$$= \omega_c + k_f A \cos \omega_m t$$

$$= \omega_c + \Delta\omega \cos(\omega_m t)$$

$$\Delta\omega \triangleq k_f A$$

$$y(t) = \cos \omega_c t + k_f \int x(t) dt$$

$$= \cos \left(\omega_c t + \frac{\Delta\omega}{\omega_m} \sin \omega_m t + \theta_0 \right)$$

$$= \cos \left(\omega_c t + \frac{\Delta\omega}{\omega_m} \sin \omega_m t \right)$$

$$\text{let } \theta_0 = 0$$

Sect. 8.7 Sinusoidal Frequency Modulation

- Narrowband FM (cont'd) $y(t) = \cos \left[\omega_c t + \frac{\Delta\omega}{\omega_m} \sin \omega_m t \right]$.

$$y(t) = \cos(\omega_c t + m \sin \omega_m t) \quad m: \text{modulation index}$$

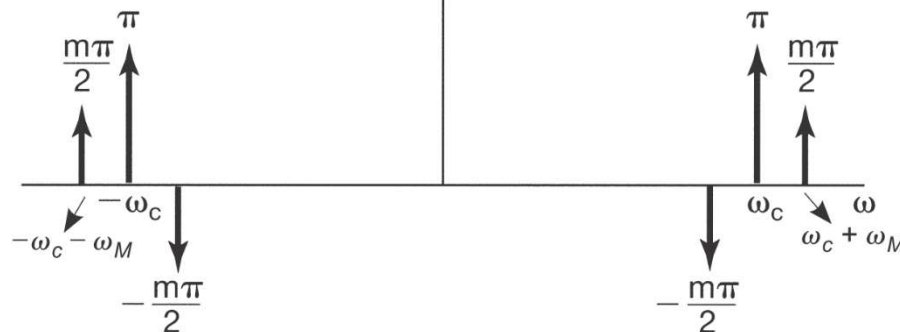
$$y(t) = \cos \omega_c t \cos(m \sin \omega_m t) - \sin \omega_c t \sin(m \sin \omega_m t).$$

When m is small ($\ll \pi/2$), it becomes **narrowband FM** and

$$\cos(m \sin \omega_m t) \approx 1,$$

$$\sin(m \sin \omega_m t) \approx m \sin \omega_m t,$$

$$y(t) \approx \cos \omega_c t - m(\sin \omega_m t)(\sin \omega_c t).$$

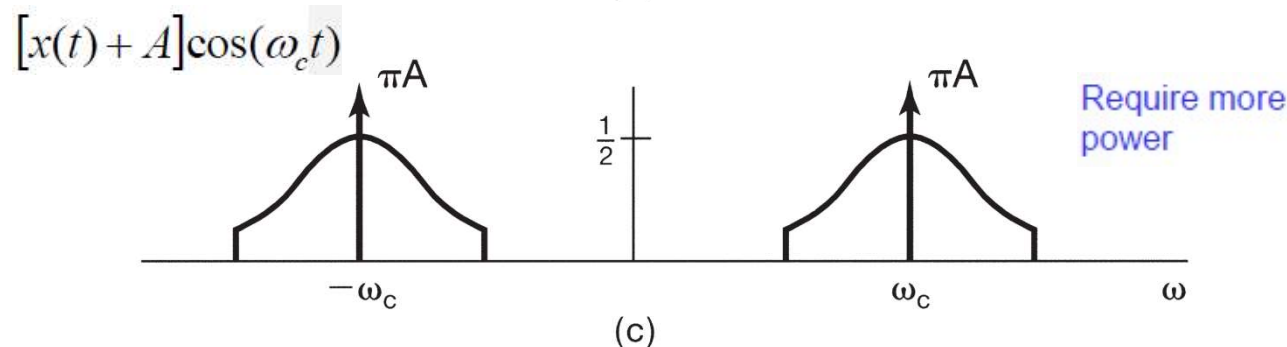
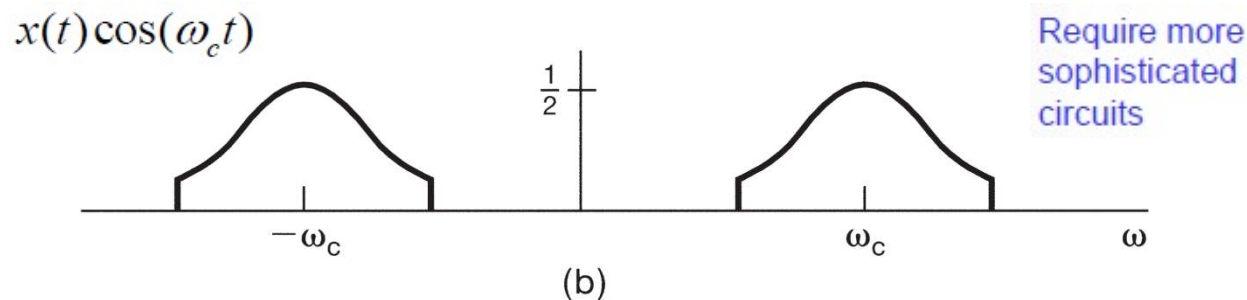
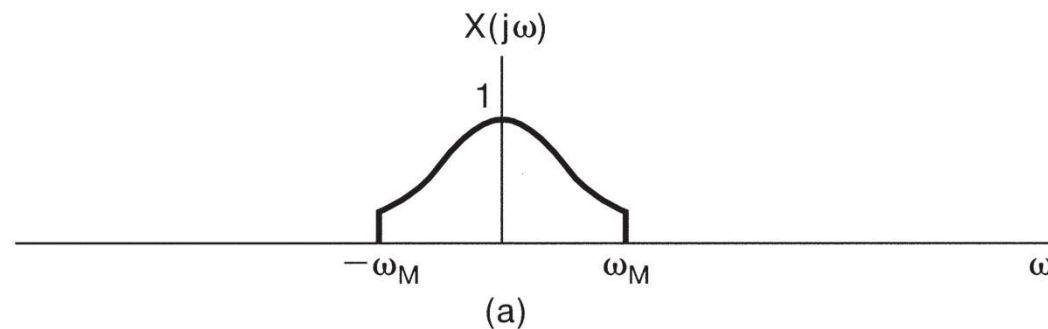


For narrowband FM, the BW of the sideband equals the BW ω_m of the modulating signal. And, the spectrum is similar to **AM-DSB/WC**.

Figure 8.36 Approximate spectrum for narrowband FM.

Recall that Demodulation for Sinusoidal AM

- Comparisons of Sync & Async Demodulation



Refer to Figs. 8.12 - 8.14, pp. 592-593.

$$\begin{aligned}
 y(t) &= (A + x(t)) \cos \omega_c t \\
 &= (1 + m \cos \omega_m t) \cos \omega_c t \\
 &= \cos \omega_c t + m \cos \omega_m t \cos \omega_c t
 \end{aligned}$$

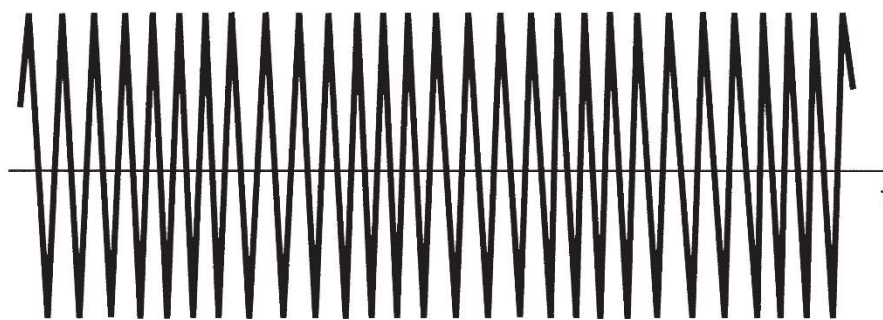
Figure 8.14 Comparison of spectra for synchronous and asynchronous sinusoidal amplitude modulation systems: (a) spectrum of modulating signal; (b) spectrum of $x(t) \cos \omega_c t$ representing modulated signal in a synchronous system; (c) spectrum of $[x(t) + A] \cos \omega_c t$ representing modulated signal in an asynchronous system.

Sect. 8.7 Sinusoidal Frequency Modulation

- Comparison of narrowband FM and AM-DSB/WC

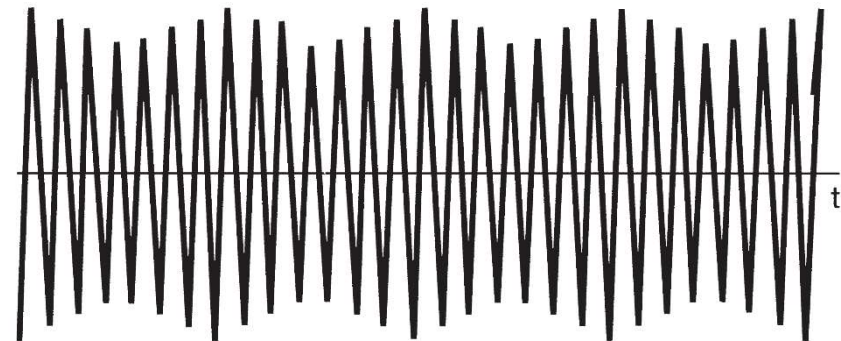
Refer to Figs. 8.12 - 8.14, pp. 592-593.

$$\begin{aligned}y(t) &= (A + x(t))\cos\omega_c t \\&= (1 + m\cos\omega_m t)\cos\omega_c t \\&= \cos\omega_c t + m\cos\omega_m t\cos\omega_c t\end{aligned}$$



(a)

$$y(t) \approx \cos\omega_c t - m\sin\omega_m t\sin\omega_c t$$



(b)

$$y_2(t) = \cos\omega_c t + m\cos\omega_m t\cos\omega_c t$$

Figure 8.37 Comparison of narrowband FM and AM-DSB/WC: (a) narrowband FM; (b) AM-DSB/WC.

Sect. 8.7 Sinusoidal Frequency Modulation

- Wideband FM $y(t) = \cos \left[\omega_c t + \frac{\Delta \omega}{\omega_m} \sin \omega_m t \right].$

$$y(t) = \cos(\omega_c t + m \sin \omega_m t) \quad m: \text{modulation index}$$

$$y(t) = \cos \omega_c t \underbrace{\cos(m \sin \omega_m t)} - \sin \omega_c t \underbrace{\sin(m \sin \omega_m t)}.$$

- Both are periodic signals with fundamental frequency ω_m .
- Thus the FT of each signal is an impulse train with impulses at integer multiples of ω_m and amplitudes proportional to the Fourier series coefficients.
- The first [second] term corresponds to a carrier amplitude modulated by the periodic signal $\cos(m \sin \omega_m t)$ [$\sin(m \sin \omega_m t)$].

If the period of $\cos(m \sin \omega_m t)$ is T , then
 $\cos(m \sin \omega_m t) = \cos(m \sin \omega_m (t + T))$
 $= \cos(m \sin \omega_m t \cos \omega_m T + m \cos \omega_m t \sin \omega_m T)$
 $\Rightarrow \cos \omega_m T = \pm 1$ and $\sin \omega_m T = 0 \Rightarrow T = \pi / \omega_m$
 \Rightarrow Fundamental frequency of $\cos(m \sin \omega_m t)$ is $2\omega_m$.

If the period of $\sin(m \sin \omega_m t)$ is T , then
 $\sin(m \sin \omega_m t) = \sin(m \sin \omega_m (t + T))$
 $= \sin(m \sin \omega_m t \cos \omega_m T + m \cos \omega_m t \sin \omega_m T)$
 $\Rightarrow \cos \omega_m T = 1$ and $\sin \omega_m T = 0 \Rightarrow T = 2\pi / \omega_m$
 \Rightarrow Fundamental frequency of $\sin(m \sin \omega_m t)$ is ω_m .

Sect. 8.7 Sinusoidal Frequency Modulation

- Periodic Square-Wave Modulating Signal

$$y(t) = r(t) \cos[(\omega_c + \Delta\omega)t] + r\left(t - \frac{T}{2}\right) \cos[(\omega_c - \Delta\omega)t],$$

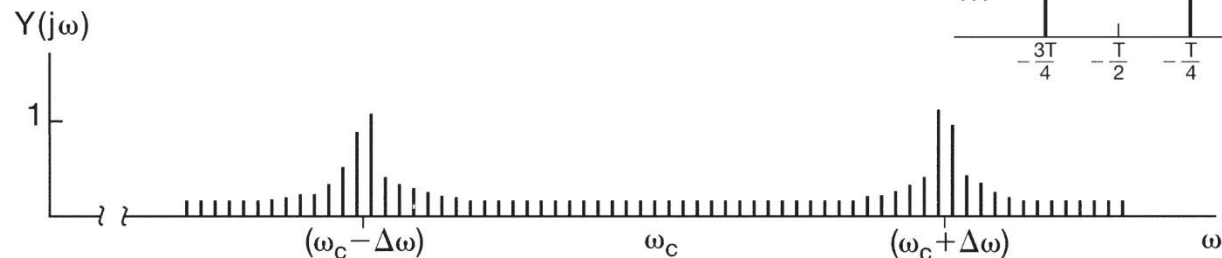
$$Y(j\omega) = \frac{1}{2}[R(j\omega + j\omega_c + j\Delta\omega) + R(j\omega - j\omega_c - j\Delta\omega)] \\ + \frac{1}{2}[R_T(j\omega + j\omega_c - j\Delta\omega) + R_T(j\omega - j\omega_c + j\Delta\omega)],$$

where $R(j\omega)$ is the Fourier transform of the periodic square wave $r(t)$ and $R_T(j\omega)$ is the Fourier transform of $r(t - T/2)$.

From Example 4.6, with $T = 4T_1$,

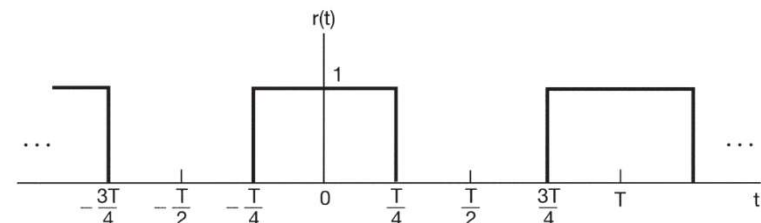
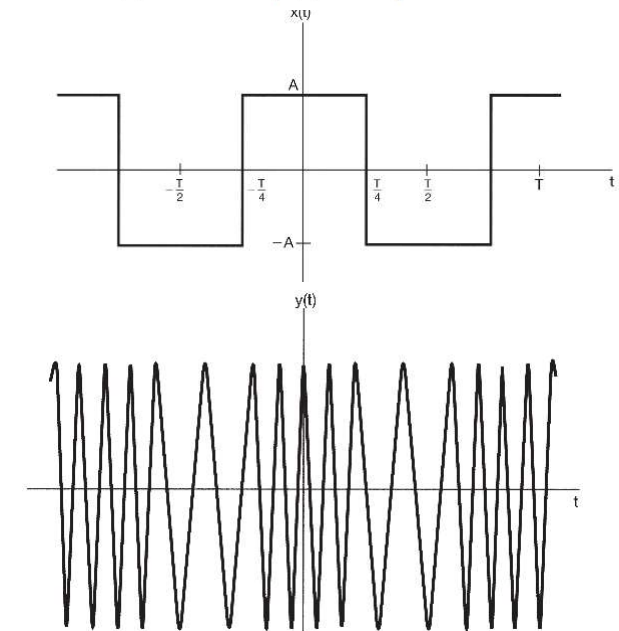
$$R(j\omega) = \sum_{k=-\infty}^{\infty} \frac{2}{2k+1} (-1)^k \delta\left[\omega - \frac{2\pi(2k+1)}{T}\right] + \pi\delta(\omega)$$

$$R_T(j\omega) = R(j\omega)e^{-j\omega T/2}.$$

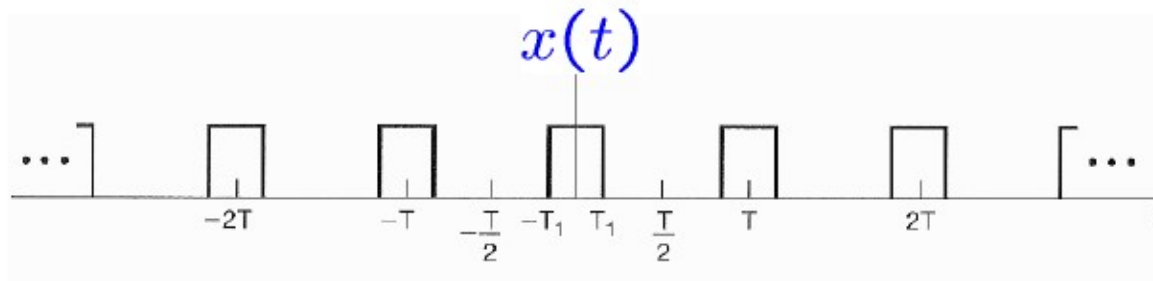


$$\omega_i(t) = \omega_c + k_f x(t) \quad k_f = 1 \Rightarrow \Delta\omega = A$$

- When $x(t) > 0$, $\omega_i(t) = \omega_c + \Delta\omega$
- When $x(t) < 0$, $\omega_i(t) = \omega_c - \Delta\omega$



- Example 4.6

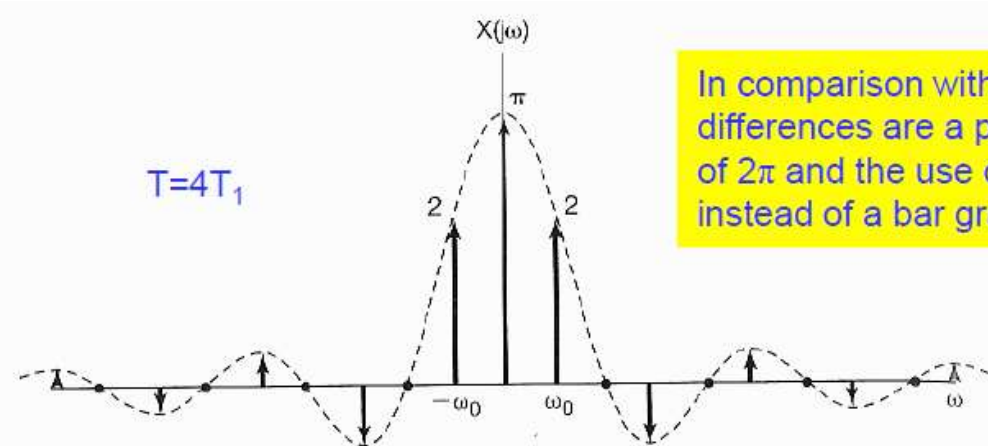


$$x(t) = \sum_{k=-\infty}^{+\infty} a_k e^{jk\omega_0 t}$$

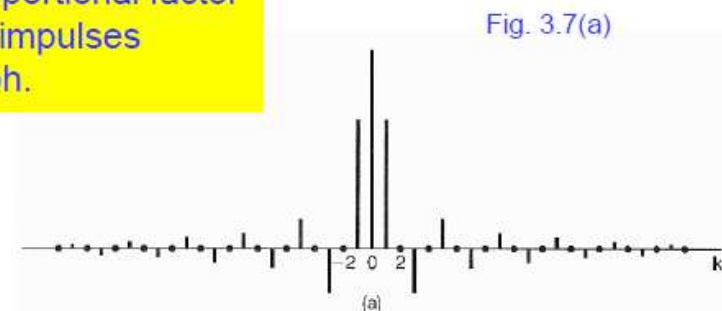
$$a_k = \frac{\sin(k\omega_0 T_1)}{\pi k}$$

$$\Rightarrow X(j\omega) = \sum_{k=-\infty}^{+\infty} 2\pi a_k \delta(\omega - k\omega_0)$$

$$= \sum_{k=-\infty}^{+\infty} \frac{2 \sin(k\omega_0 T_1)}{k} \delta(\omega - k\omega_0)$$



In comparison with Fig. 3.7(a), the differences are a proportional factor of 2π and the use of impulses instead of a bar graph.

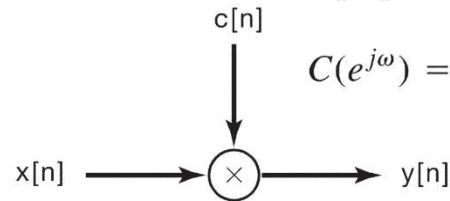


Sect. 8.9 DT Modulation

- DT Sinusoidal AM & Demodulation

$$c[n] = e^{j\omega_c n}.$$

$$C(e^{j\omega}) = \sum_{k=-\infty}^{+\infty} 2\pi\delta(\omega - \omega_c + k2\pi),$$

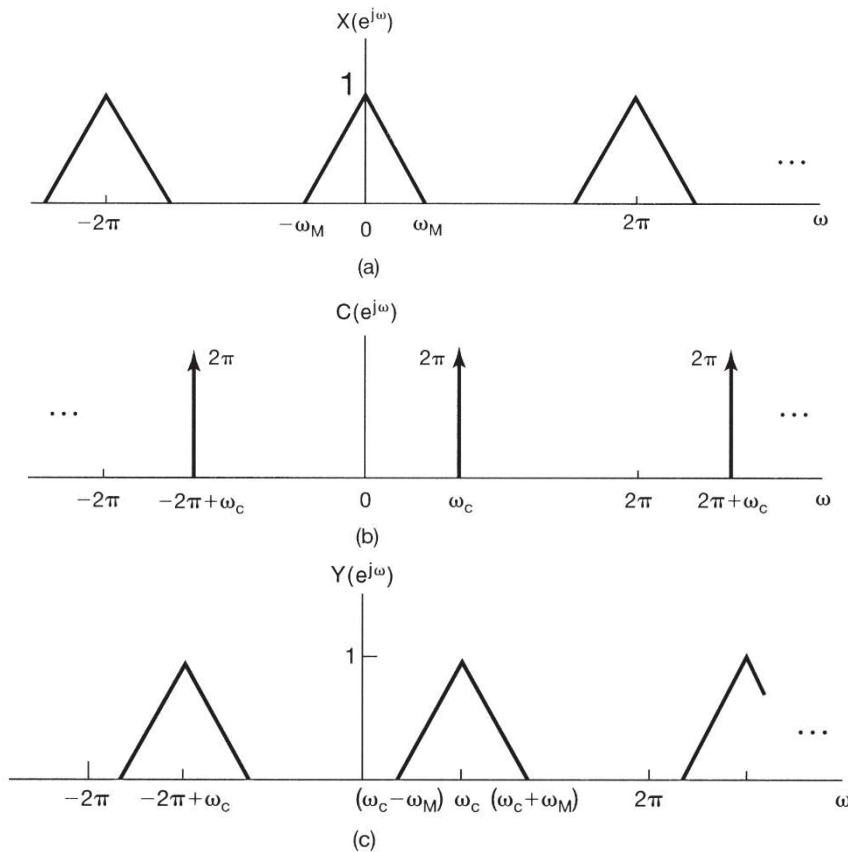


$$y[n] = x[n]c[n].$$

$$Y(e^{j\omega}) = \frac{1}{2\pi} \int_{2\pi} X(e^{j\theta}) C(e^{j(\omega-\theta)}) d\theta.$$

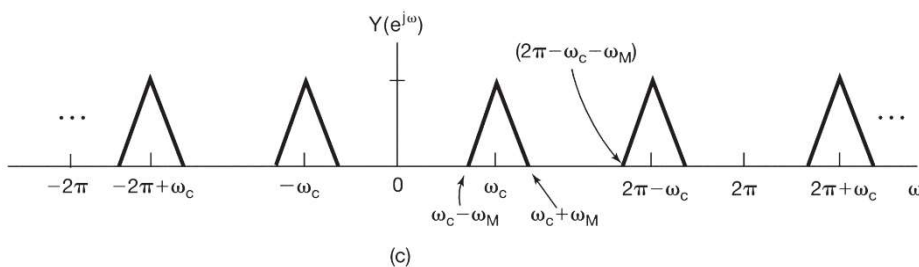
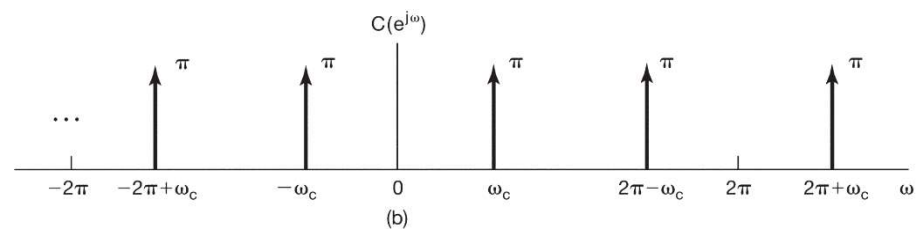
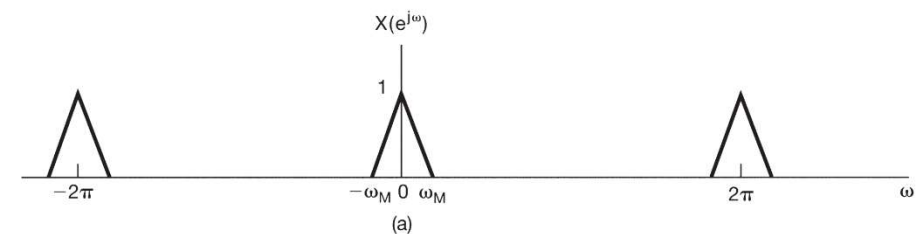
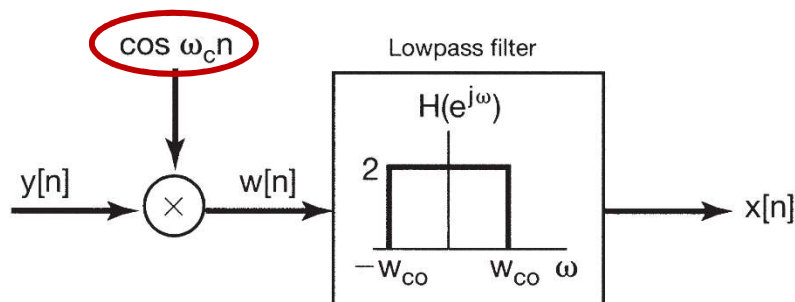


$$x[n] = y[n]e^{-j\omega_c n}.$$



Sect. 8.9 DT Modulation

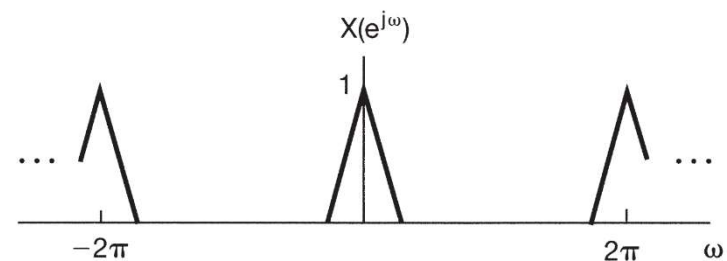
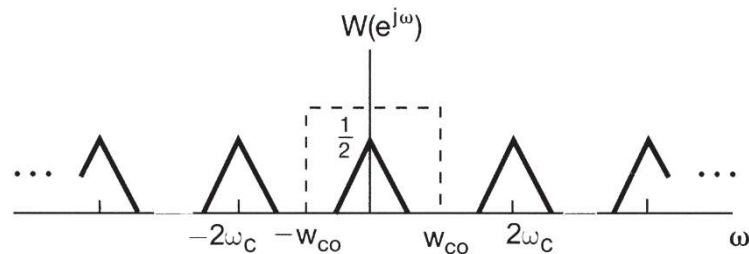
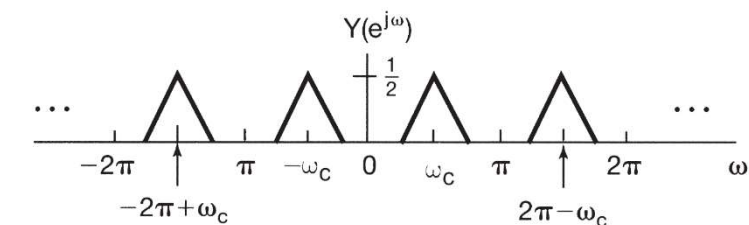
- DT Sinusoidal AM & Demodulation



$$\omega_c > \omega_M$$

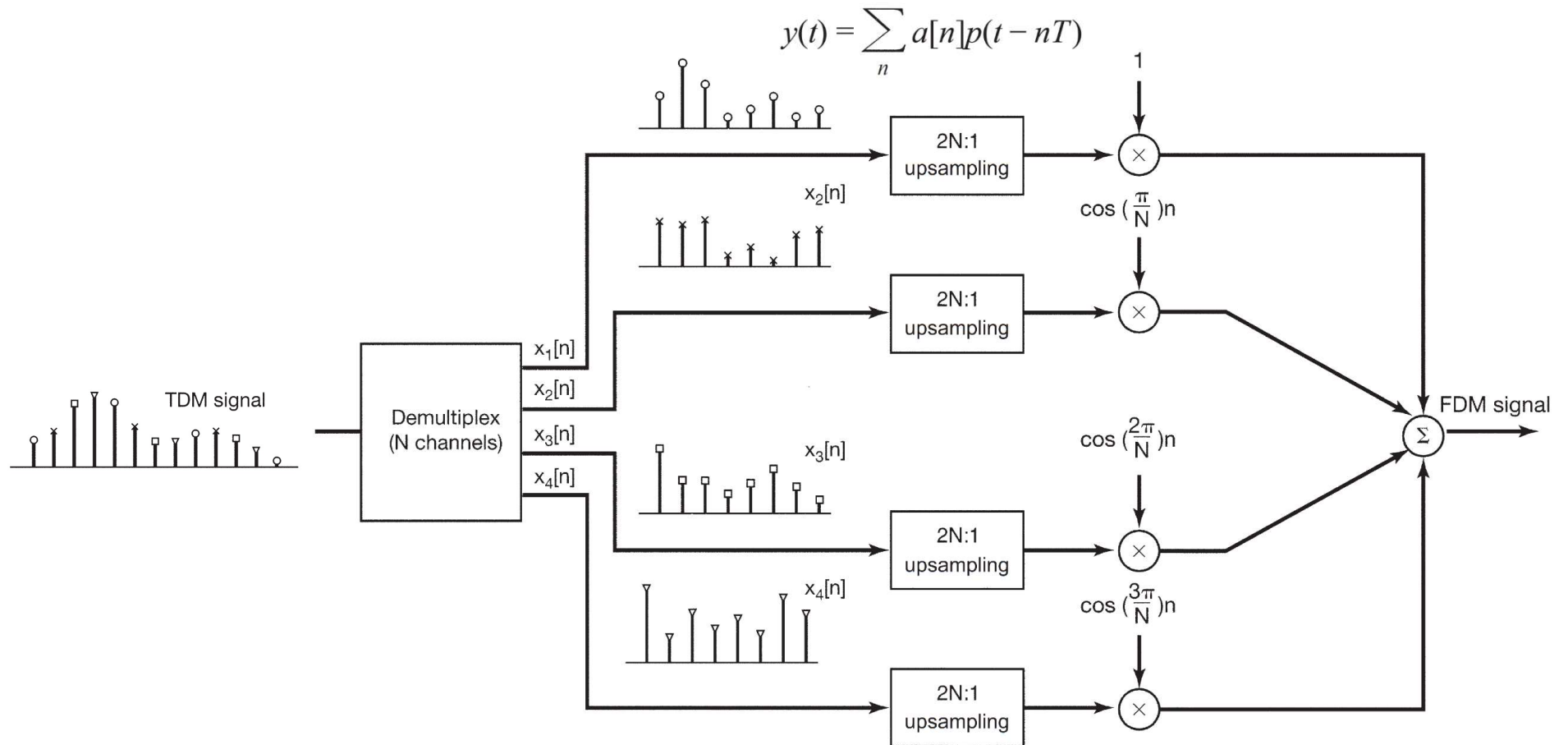
$$2\pi - \omega_c - \omega_M > \omega_c + \omega_M$$

$$\omega_M < \omega_c < \pi - \omega_M.$$



Sect. 8.9 DT Modulation

- DT Transmodulation or Transmultiplexing: TDM to FDM



$$s(t) = \sum_n a[n]p(t - nT)\cos(\omega_c t + \theta_c)$$

Sect. 8.9 DT Modulation

- Frequency-Shift Keying (FSK)

In phase-shift keying, PAM $y(t)$ with a sinusoidal carrier takes the form

$$s(t) = \sum_n a[n]p(t - nT)\cos(\omega_c t + \theta_n).$$

With FSK

$$s(t) = \sum_n a[n]p(t - nT)\cos((\omega_0 + \Delta_n)t + \theta_c)$$

With PSK, in each symbol interval, information can now be incorporated in both the pulse amplitude $a[n]$ and the carrier phase ϑ_n .

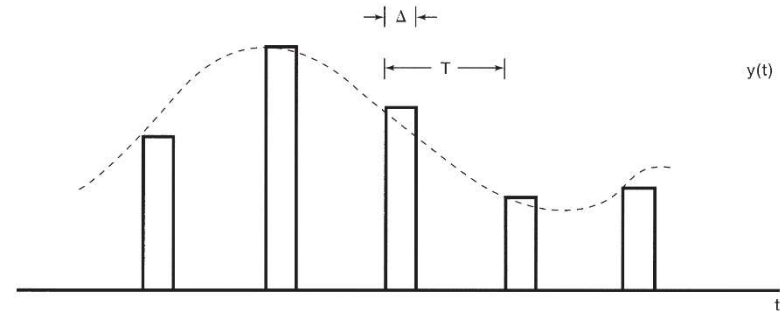
$$s(t) = \sum_n ap(t - nT)\cos(\omega_c t + \theta_n).$$

For example, choosing

$$\theta_n = \frac{2\pi b_n}{M} \quad ; \quad 0 \leq b_n \leq M-1$$

$$y(t) = \sum_n a[n]p(t - nT) \quad \text{where} \quad a[n] = x(nT).$$

where $p(t) = 1$ for $|t| < \Delta/2$, $p(t) = 0$ otherwise.



Sect. 8.9 DT Modulation

- Phase-Shift Keying (PSK) $s(t) = \sum_n a p(t - nT) \cos(\omega_c t + \theta_n)$. $\theta_n = \frac{2\pi b_n}{M}$; $0 \leq b_n \leq M-1$

Suppose that $x[n]$ is a binary discrete-time signal.

If PSK with $M = 4$ is adopted to encode $x[n]$, then we can set

$$\begin{aligned} \theta_n &= 0 & \text{if } x[2n] = x[2n+1] = 0, \\ \theta_n &= \pi/2 & \text{if } x[2n] = 0 \text{ and } x[2n+1] = 1, \\ \theta_n &= \pi & \text{if } x[2n] = 1 \text{ and } x[2n+1] = 0, \\ \theta_n &= 3\pi/2 & \text{if } x[2n] = x[2n+1] = 1, \end{aligned}$$

Using the identity

$$\cos(\omega_c t + \theta_n) = \cos(\theta_n) \cos(\omega_c t) - \sin(\theta_n) \sin(\omega_c t),$$

we can write with

$$s(t) = I(t) \cos(\omega_c t) - Q(t) \sin(\omega_c t),$$

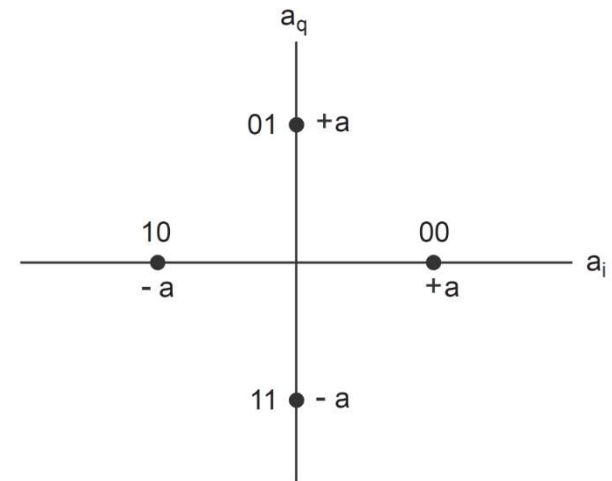
with

$$I(t) = \sum_n a_i[n] p(t - nT) \quad Q(t) = \sum_n a_q[n] p(t - nT)$$

and

$$a_i[n] = a \cos(\theta_n)$$

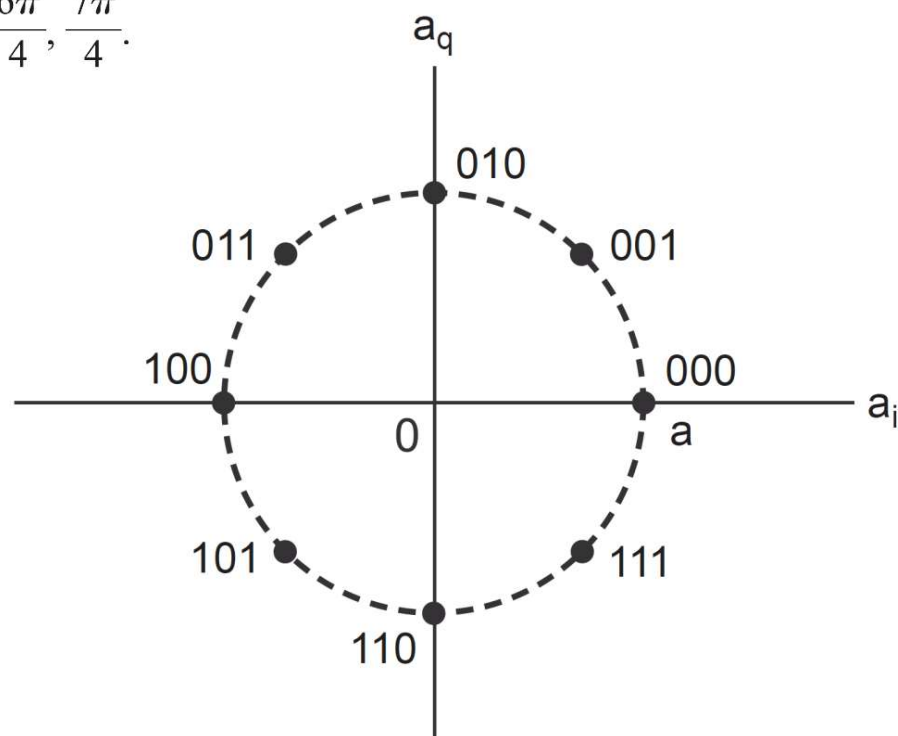
$$a_q[n] = a \sin(\theta_n).$$



Sect. 8.9 DT Modulation

- Quadrature Amplitude Modulation (QAM)

$$0, \frac{\pi}{4}, \frac{\pi}{2}, \frac{3\pi}{4}, \pi, \frac{5\pi}{4}, \frac{6\pi}{4}, \frac{7\pi}{4}.$$



Sect. 8.9 DT Modulation

- Demodulation

The input signal $r_i(t)$ in Figure 8.51 is

$$\begin{aligned} r_i(t) &= I(t)\cos^2(\omega_c t) - Q(t)\sin(\omega_c t)\cos(\omega_c t) \\ &= \frac{1}{2}I(t) - \frac{1}{2}I(t)\cos(2\omega_c t) - \frac{1}{2}Q(t)\sin(2\omega_c t). \end{aligned}$$

Similarly,

$$\begin{aligned} r_q(t) &= I(t)\cos(\omega_c t)\sin(\omega_c t) - Q(t)\sin^2(\omega_c t) \\ &= \frac{1}{2}I(t)\sin(2\omega_c t) + \frac{1}{2}Q(t) - \frac{1}{2}Q(t)\cos(2\omega_c t). \end{aligned}$$

From Figure 8.52,

$$a_i[n] = 3a \text{ and } a_q^2[n] = -a.$$

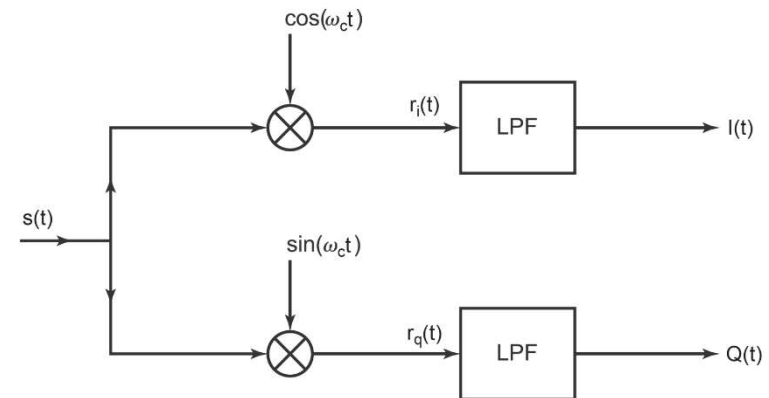


Figure 8.51 Demodulation scheme for a quadrature modulated PAM signal.

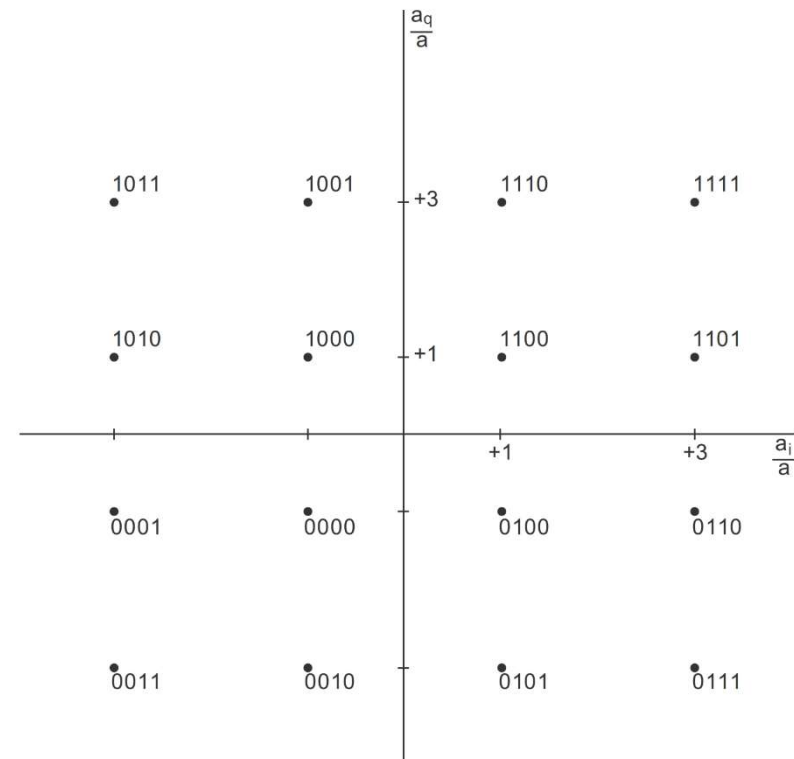
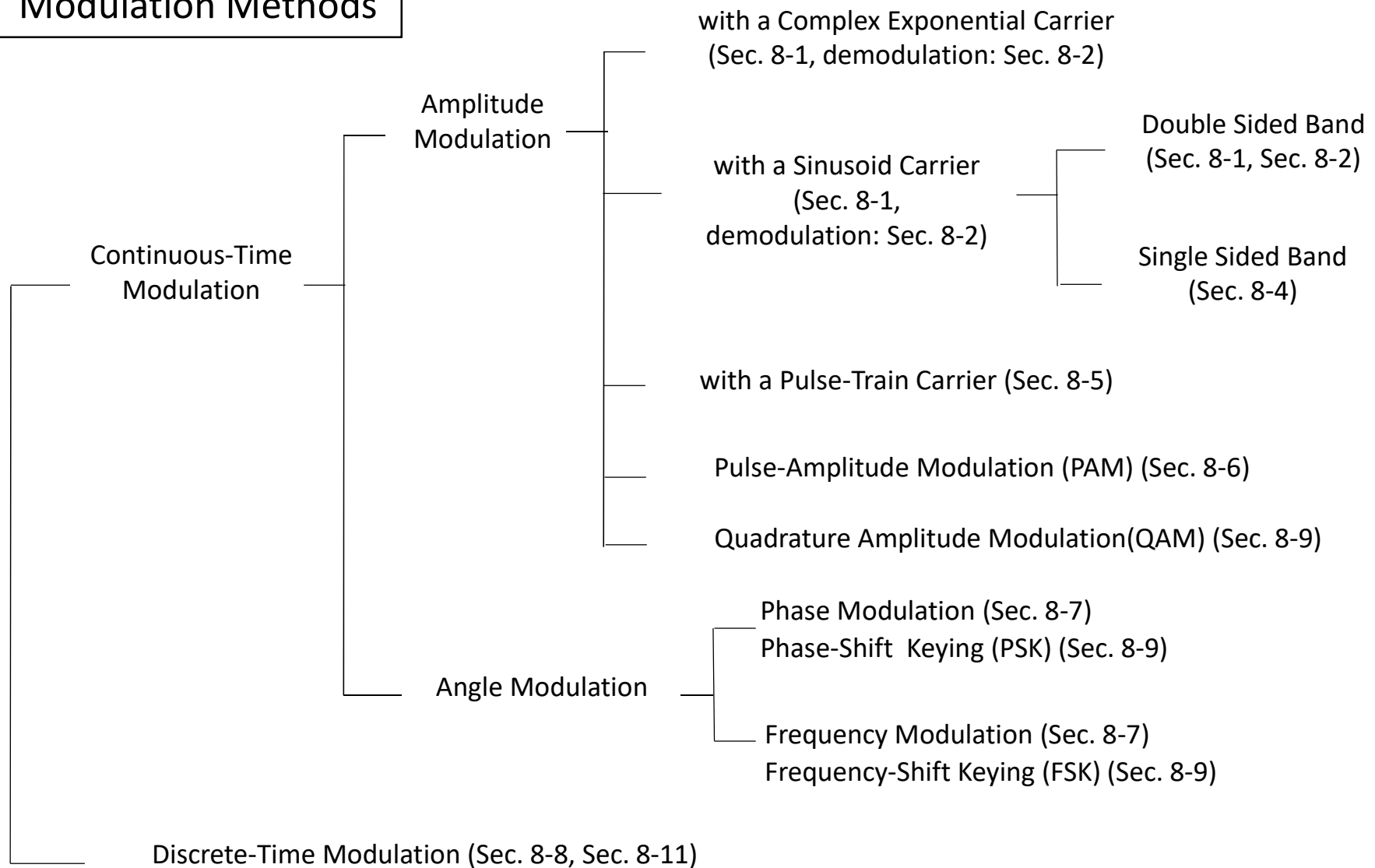


Figure 8.52 A 16-point QAM constellation.

Modulation Methods



Multiplexing Methods

