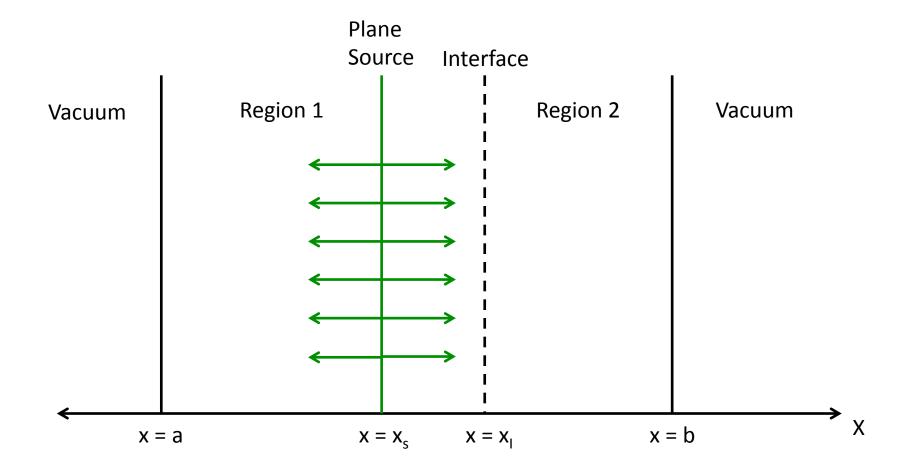
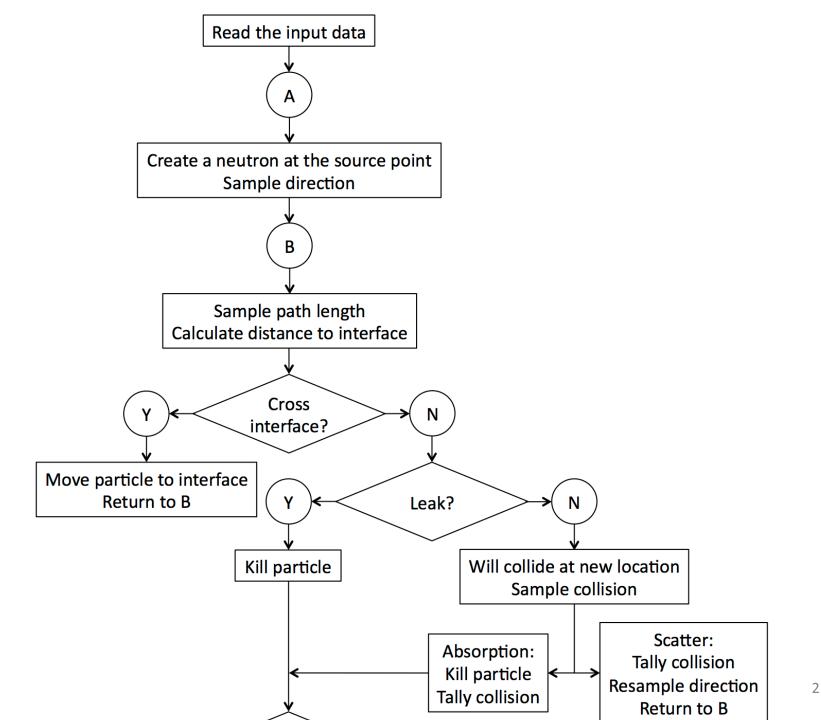
Problem Description and Geometry





Sampling Routines

Sampling direction

- Generate a random number ξ on the uniform distribution [0, 1).
- If ξ < 0.5, direction = left (-)
- else, direction = right (+)

Sampling path length

- Generate a random number ξ on the uniform distribution [0, 1).
- Plug into inverted CDF for path length:

$$s = -\log\left(\frac{\xi}{\sum_{t}}\right)$$

Sampling angle

Isotropic source and scattering; angle can range from $[0, 2\pi]$. Interested in cosine of angle [-1, 1]. Direction covers half of angle space; reduce sampling of cosine of angle to [0, 1].

- Generate a random number ξ on the uniform distribution [0, 1).
- ξ multiplied by the direction is the cosine of angle

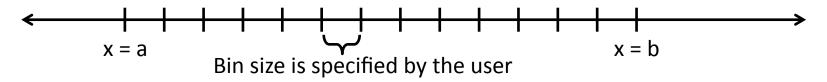
Sampling reaction

Two reactions possible: scattering (s) and absorption (a). Probability of reaction *i*:

$$p_i = \frac{\sum_i}{\sum_t}$$

- Generate a random number ξ on the uniform distribution [0, 1).
- If $\xi \ge P_s$, neutron is absorbed.
- Else, it scatters

To resolve a collision tally over space, a spatial tally mesh is used for scoring and statistics.



For each neutron history *i*, a score vector is initialized corresponding to this spatial binning. Each score corresponds to a collision of particle *i*.

Once the history is complete (the particle is terminated):

 The score is added to a cumulative score (a vector of equal size representing the sum of all previous histories). Each entry is given by:

$$T^{\in 1xJ} = \sum_{i} x_{ij}$$

• The score in each bin of the score vector is squared and added to a vector containing the cumulative sum of the squares of the scores.

$$Q^{\in 1xJ} = \sum_{i} x_{ij}^2$$

After N histories, sum of the scores and squares of scores in each bin are used to calculate the flux and statistics in each bin.

$$\frac{\mathsf{Flux}}{\overline{\phi}_j} \approx \frac{1}{V} \overline{x}_j = \frac{1}{L_i} \frac{1}{N} \sum_{i=1}^N x_{ij}$$

Statistics:

Sample Variance

$$S_{x,j}^{2} = \frac{1}{N-1} \sum_{i=1}^{N} \left(x_{ij} - \overline{x}_{j} \right)^{2} = \frac{1}{N-1} \left(\sum_{i=1}^{N} x_{ij}^{2} - 2\overline{x}_{j} \sum_{i=1}^{N} x_{ij} + \overline{x}_{j}^{2} \sum_{i=1}^{N} 1 \right)$$

Estimated Variance of Mean

$$S_{\overline{x},j}^2 = \frac{S_{xj}^2}{N}$$

Relative Error

$$R_j = \frac{S_{\overline{x},j}}{\overline{x}_j}$$

The method can be validated by solving the diffusion equation for a simplified system (finite slab, plane source).

$$\frac{1}{v}\frac{\partial \phi}{\partial t} - D(x)\phi(x,t) - \Sigma_a \phi(x,t) = S(x,t)$$

Two solution are required for flux on each side of the plane source.

Assume steady state, homogeneous material properties

Boundary conditions for each region are:

(1) Vacuum at slab boundaries (a and b)

$$\phi(\tilde{a}) = \phi(\tilde{b}) = 0$$

(2) Constant current at the source

$$\lim_{x \to 0} J(x) = \lim_{x \to 0} \frac{d\phi}{dx} = \frac{S}{2}$$

$$\phi(x) = \frac{SL}{2D} \left(1 + e^{\frac{-2\tilde{a}}{L}} \right)^{-1} \left(e^{\frac{-x}{L}} - e^{\frac{-2\tilde{a}}{L}} e^{\frac{x}{L}} \right) \qquad \tilde{a} \le x < 0$$

This solution can be adjusted to allow for the source to be anywhere in(a,b)

$$\phi(x) = \frac{SL}{2D} \left(1 + e^{\frac{-2\tilde{b}}{L}} \right)^{-1} \left(e^{\frac{-x}{L}} - e^{\frac{-2\tilde{b}}{L}} e^{\frac{x}{L}} \right) \qquad 0 < x \le \tilde{b}$$

Comparison of the analytical diffusion and MC solutions for the flux

 $x_{\text{source}} = 0$

Cross-sections equal in each region:

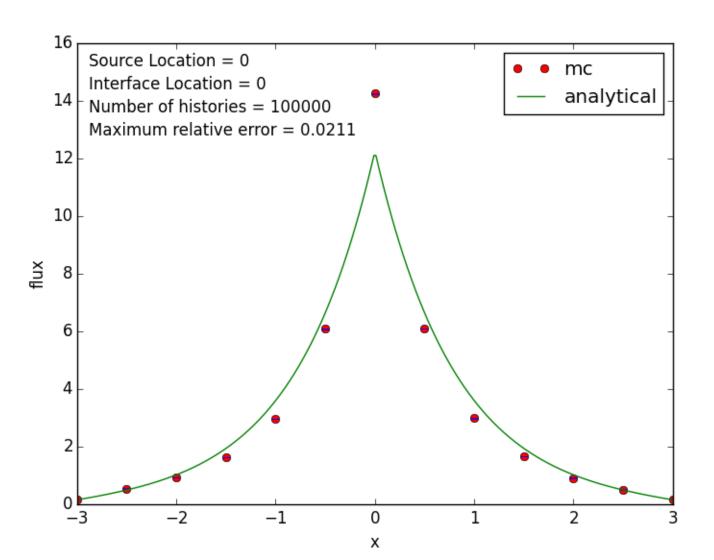
 $x_{interface} = 0$

 $\Sigma_{\rm t}(1) = \Sigma_{\rm t}(2)$

a = 3, b = -3

 $\Sigma_s(1) = \Sigma_s(2)$

S = 10



Comparison of the analytical diffusion and MC solutions for the flux

 $x_{\text{source}} = 1$

Cross-sections equal in each region:

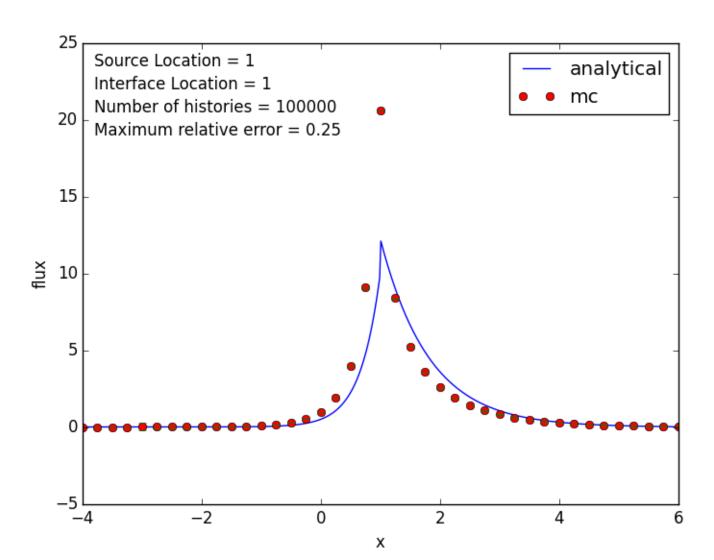
 $x_{interface} = 1$

 $\Sigma_{\rm t}(1) \neq \Sigma_{\rm t}(2)$

a = -4, b = 6

 $\Sigma_s(1) \neq \Sigma_s(2)$

S = 10



Comparison of the analytical diffusion and MC solutions for the flux

 $x_{\text{source}} = 0$

Cross-sections equal in each region:

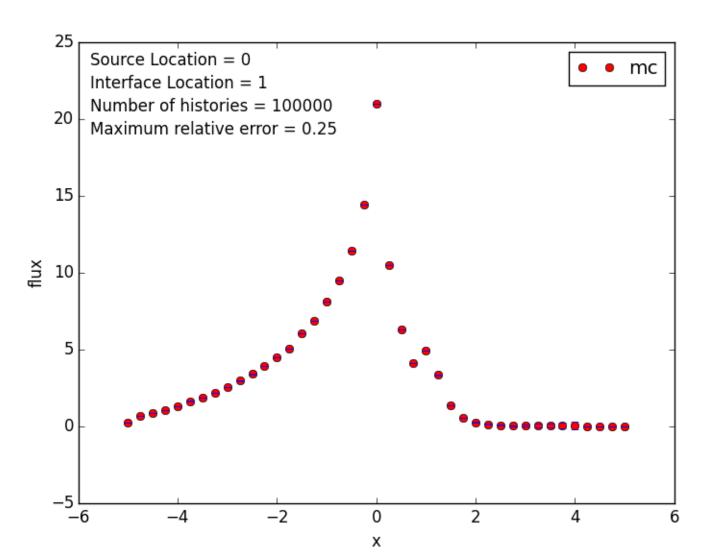
 $x_{interface} = 1$

 $\Sigma_{\rm t}(1) < \Sigma_{\rm t}(2)$

$$a = -6, b = 6$$

 $\Sigma_{s}(1) = \Sigma_{s}(2)$

S = 10



<u>References</u>

[1] MCNP5 - A General Monte Carlo N-Particle Transport Code, Version 5. Volume 1: Overview and Theory. X-5 Monte Carlo Team, Los Alamos National Laboratory (rev. 2008).

[2] J. J. Duderstadt, L. J. Hamilton. *Nuclear Reactor Analysis*. John Wiley & Sons, Inc. 1976.