

Asynchronous Sliding Mode Control of Two-Dimensional Markov Jump Systems

Yue-Yue Tao, Zheng-Guang Wu, and Peng Shi

Abstract—In this paper, asynchronous sliding mode control (SMC) is investigated for two-dimensional (2D) discrete-time Markov jump systems. As the system modes are not always accessible to the controller, the hidden Markov model is employed to describe the asynchronization between the system models and controller. A new 2D sliding surface is constructed and the corresponding asynchronous SMC is designed under the framework of hidden Markov model. By Lyapunov function and linear matrix inequality (LMI) approaches, sufficient conditions are presented to guarantee the underlying 2D system is asymptotically mean square stable (AMSS) with an H_∞ disturbance attenuation performance. Then, an algorithm is provided to derive the asynchronous 2D-SMC law. Finally, an example is given to verify the validity and effectiveness of the new SMC law design algorithm.

Index Terms—Markov jump systems, 2D systems, sliding mode control, hidden Markov model

I. INTRODUCTION

Markov jump systems (MJSs), a special class of stochastic switching systems, have received considerable attentions for its powerful ability in modeling systems with sudden changes in parameters or system structures, for instance, environmental disturbances, actuator failures, and interconnection variations in subsystems, etc. Over the past decades, a large number of results on system stability analysis and design of controllers/filters have been reported in [1]–[5].

However, the aforementioned works are generally based on the implicit assumption that the information of system modes are always fully available for the controller/filter, so that the controller/filter modes can run synchronously with system modes. Unfortunately, in practical applications, it is rather difficult to satisfy this ideal assumption because of some unexpected factors, such as, time delays, data dropouts and quantization in networked control systems. To overcome the strict limitation, two research approaches were proposed, namely, mode-independent and asynchronous methods. In mode-independent methods, see [6]–[8], the controller/filter modes are independent of system modes, which means the information of system modes is not fully utilized and may result in some conservativeness. In [9], Wu proposed the hidden Markov model, a united asynchronous framework that covers synchronous and mode-independent cases. A similar

description of this model can also be found in earlier works [1] and [10]. The hidden Markov model supposes that the controller/filter modes can be detected via a hidden Markov chain, such that controllers/filters can utilize more information of the origin system modes. Based on this model, many problems of asynchronous control/filtering for MJSs have been studied in recent years [11]–[13].

Moreover, SMC, an effective control technique for its strong robustness against parameter variations, exogenous disturbances and model uncertainties, has been successfully applied to a large variety of practical systems [14]–[16]. The prime idea of SMC is to design a discontinuous control law to drive the system state trajectories toward a predefined sliding surface and stay within a neighbourhood of the sliding surface after reaching it [17]. In the last few decades, the SMC design problems have been extensively studied, and a large number of research results for MJSs have been published [18]–[20]. Recently, some researchers have investigated the asynchronous SMC design methods for one-dimensional (1D) MJSs based on hidden Markov model [21]–[23].

On the other hand, 2D systems, a special class of multi-dimensional systems dating back to 1970s, have been used to represent a large variety of practical applications, such as digital image processing, partial differential equations modeling and signal filtering [24]–[26], etc. Different from 1D systems, the prime feature of 2D systems lie in the system information propagates along two different directions and the information in each direction will have effects on the other, which brings much complexity and difficulty in system analysis and synthesis. To describe the special properties of 2D systems, several mathematical models presented in state-space framework have been proposed, for example Roesser model [24] and Fornasini-Marchesini model [27]. In Roesser model, the system state is composed of two independent states, horizontal state and vertical state, which are denoted by sub-vectors, the next horizontal state and vertical state in different directions can be deduced from current state, respectively. Unlike the Roesser model, the system state in Fornasini-Marchesini model is represented by a vector which is a function with two independent variables, and the current system state is derived from the last two adjacent states in different directions. In most circumstances, Roesser model can be regarded as particular case of Fornasini-Marchesini model, but is much simpler and more intelligible than the latter. Based on 2D bounded real lemma, the H_∞ control theory for 2D systems was established by Du and Xie in [28] and [29]. This result was extended to control and filtering problems for 2D systems with time-varying delays [30], multiplicative noise

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[31] and uncertainty parameters [32]. Anh has studied the dissipative control and filtering problems for 2D systems in [33] by utilizing linear matrix inequalities technique. A large number of preliminary results on SMC of discrete-time 2D systems have been established [34]–[36]. In recent years, 2D systems with Markov jump parameters have attracted more interests of researchers. For example, the H_∞ control, H_∞ filtering, H_∞ mode reduction and fault detection problems for 2D-MJSs have been investigated in [37]–[41], respectively. However, we have to notice that, the issue of SMC for 2D-MJSs has not been studied yet, which motivates us for current work.

Based on the aforementioned considerations, we will investigate the problem of asynchronous SMC for 2D-MJSs in this paper. The primary contributions of this paper are shown as following aspects:

- 1) Based on the properties of 2D systems, a novel 2D sliding surface is constructed, and the corresponding asynchronous 2D-SMC law is designed under the framework of hidden Markov model, which means it is more practical and flexible than the synchronous or mode-independent ones.
- 2) A sufficient condition that can guarantee the concerned 2D system is AMSS with an H_∞ disturbance attenuation performance is established. Moreover, this condition can simultaneously ensure the reachability of the sliding mode dynamics. Finally, the design procedures of SMC law are summarized into an algorithm.
- 3) It is the first time that the asynchronous SMC is investigated for 2D-MJSs, which shows the feasibility and effectiveness of SMC for 2D-MJSs. However, Considering the complexity and difficulty in system analysis and synthesis of 2D systems over 1D systems, our work Though asynchronous SMC schemes for 1D-MJSs have been extensively studied in preview works, such as [21]–[23] etc. However, as

II. PRELIMINARIES

Considering the following discrete-time 2D-MJS in Roesser model:

$$\begin{cases} \mathbf{x}(i, j) = A_{r(i, j)}x(i, j) + E_{r(i, j)}w(i, j) \\ \quad + B_{r(i, j)}[u(i, j) + f(x(i, j), r(i, j))] \\ y(i, j) = C_{r(i, j)}x(i, j) + D_{r(i, j)}w(i, j) \end{cases} \quad (1)$$

where

$$\mathbf{x}(i, j) = \begin{bmatrix} x^h(i+1, j) \\ x^v(i, j+1) \end{bmatrix}, \quad x(i, j) = \begin{bmatrix} x^h(i, j) \\ x^v(i, j) \end{bmatrix}$$

$x^h(i, j) \in \mathbb{R}^{n_h}$ and $x^v(i, j) \in \mathbb{R}^{n_v}$ represent horizontal and vertical sub-states respectively, $u(i, j) \in \mathbb{R}^{n_u}$ and $y(i, j) \in \mathbb{R}^{n_y}$ represent the control input and controlled output respectively, and $w(i, j) \in \mathbb{R}^{n_w}$ represents the exogenous disturbance which belongs to $\ell_2\{[0, \infty), [0, \infty)\}$. $A_{r(i, j)}$, $B_{r(i, j)}$, $C_{r(i, j)}$, $D_{r(i, j)}$ and $E_{r(i, j)}$ represent the time-varying system matrices, all of which are real known with appropriate dimensions. Besides, we assume that the matrix $B_{r(i, j)}$ is full column rank for each $r(i, j) \in \mathcal{N}_1$, that is,

$\text{rank}(B_{r(i, j)}) = n_u$. The nonlinear function $f(x(i, j), r(i, j))$ satisfies the following property:

$$\|f(x(i, j), r(i, j))\| \leq \delta_{r(i, j)}\|x(i, j)\| \quad (2)$$

where $\delta_{r(i, j)}$ is a known scalar, $\|\cdot\|$ denotes the Euclidean norm of a vector. The parameter $r(i, j)$ takes values in a finite set $\mathcal{N}_1 = \{1, 2, \dots, N_1\}$ with transition probability matrix $\Lambda = [\lambda_{kp}]$, and the related transition probability in both directions satisfies (see [38], [39])

$$\lambda_{kp} = \begin{cases} \Pr\{r(i+1, j) = p | r(i, j) = k\}, & \forall k, p \in \mathcal{N}_1 \\ \Pr\{r(i, j+1) = p | r(i, j) = k\}, & \end{cases} \quad (3)$$

where $\lambda_{kp} \in [0, 1]$, for all $k, p \in \mathcal{N}_1$, and $\sum_{p=1}^{N_1} \lambda_{kp} = 1$ for every mode k . We define the boundary condition (X_0, Γ_0) of the 2D-MJS (1), as follows:

$$\begin{cases} X_0 = \{x^h(0, j), x^v(i, 0) | i, j = 0, 1, 2, \dots\} \\ \Gamma_0 = \{r(0, j), r(i, 0) | i, j = 0, 1, 2, \dots\} \end{cases} \quad (4)$$

And the corresponding zero boundary condition is assumed as $x^h(0, j) = 0, x^v(i, 0) = 0$, for every nonnegative integer i, j . Besides, the following assumption is imposed on X_0 :

Assumption 1. The boundary condition X_0 satisfies:

$$\lim_{Z \rightarrow \infty} \mathbb{E} \left\{ \sum_{z=0}^Z (\|x^h(0, z)\|^2 + \|x^v(z, 0)\|^2) \right\} < \infty \quad (5)$$

Here $\mathbb{E}\{\cdot\}$ represents the mathematical expectation.

In practical applications, the complete information of $r(i, j)$ can not always be available to the controller. Hence, in this paper, the hidden Markov model $(r(i, j), \sigma(i, j), \Lambda, \Psi)$ as in [9] is introduced to characterize the asynchronous phenomenon between the controller and the original system. The parameter $\sigma(i, j)$, refers to controller mode, takes values in another finite set $\mathcal{N}_2 = \{1, 2, \dots, N_2\}$, and satisfies the conditional probability matrix $\Psi = [\mu_{k\tau}]$ with conditional mode transition probabilities

$$\Pr\{\sigma(i, j) = \tau | r(i, j) = k\} = \mu_{k\tau} \quad (6)$$

where $\mu_{k\tau} \in [0, 1]$ for all $k \in \mathcal{N}_1, \tau \in \mathcal{N}_2$, and $\sum_{\tau=1}^{N_2} \mu_{k\tau} = 1$ for any mode k .

Remark 1. Two strict assumptions are required to guarantee the controller modes run synchronously with original system modes all the time. First, all system modes should be detected accurately by the controller in time. Second, the controller should switch to the corresponding mode in time. However, the first assumption might be impaired by failures or delays of communication devices, and the second assumption might be impaired by failures or low efficiency of mode switching devices. In other words, the synchronous controller has high requirements on the reliability and efficiency of the physical equipment, which are rather difficult to be guaranteed. Therefore, the mismatched modes between controller and system are more practical in real applications. The hidden Markov model can flexibly handle the mismatched modes between controller and system through statistical methods, which will reduce requirements for physical devices.

Remark 2. The hidden Markov model is a united framework that covers synchronous, asynchronous and mode-independent cases. In this model, system modes are governed by the Markov chain $\{r(i, j), i, j = 1, 2 \dots\}$, and controller modes are derived by the conditional mode transition probability $u_{k\tau}$. That is, the conditional probability matrix Ψ establishes a connection between the modes of controller and original system. Which case the controller belongs to depends on the conditional probability matrix Ψ . The controller becomes a synchronous one when Ψ is a unit matrix, or becomes a mode-independent one when $\mathcal{N}_2 = \{1\}$. Thus, the established results can be readily extended to synchronous or mode-independent cases by adjusting the conditional probability matrix Ψ .

In the following, the definitions of AMSS and H_∞ disturbance attenuation performance for 2D systems will be given in Definition 1 and Definition 2, respectively.

Definition 1. For $w(i, j) \equiv 0$, the 2D-MJS (1) under Assumption 1 is said to be AMSS, if the following formulation holds:

$$\lim_{i+j \rightarrow \infty} \mathbb{E}\{\|x(i, j)\|^2\} = 0 \quad (7)$$

for any boundary condition X_0 .

Definition 2. Given a scalar $\gamma > 0$, the 2D-MJS (1) under zero boundary condition with $w(i, j) \in \ell_2\{[0, \infty), [0, \infty)\}$ is said to be AMSS with an H_∞ disturbance attenuation performance γ , if (7) and following formulation hold:

$$\sum_{i=0}^{\infty} \sum_{j=0}^{\infty} \{\|y(i, j)\|^2\} < \gamma^2 \sum_{i=0}^{\infty} \sum_{j=0}^{\infty} \{\|w(i, j)\|^2\}. \quad (8)$$

Now, we will make some notational simplification for convenience. The parameter $r(i, j)$ will be represented by k , and $\sigma(i, j)$ will be represented by τ .

The objective of this work is to design an asynchronous 2D-SMC law, such that the 2D-MJS (1) is AMSS with an H_∞ disturbance attenuation performance γ .

III. MAIN RESULT

In this section, we first construct a novel 2D sliding surface based on the properties of 2D systems, and design an corresponding asynchronous 2D-SMC law under hidden Markov model. Then, we will analyze the asymptotic mean square stability for the concerned 2D-MJS and the reachability of the sliding mode dynamics.

A. Sliding Surface and Asynchronous SMC Law Design

In this work, we construct a novel 2D sliding surface as follows:

$$s(i, j) = \begin{bmatrix} s^h(i, j) \\ s^v(i, j) \end{bmatrix} = Gx(i, j) \quad (9)$$

where $s^h(i, j)$ and $s^v(i, j)$ represent horizontal and vertical sub-sliding surface respectively, the matrix $G = \sum_{k=1}^{N_1} \beta_k B_k^T$, and scalars β_k should be chosen properly such that GB_k is nonsingular for any $k \in \mathcal{N}_1$. Based on the assumption that B_k is full column rank for any $k \in \mathcal{N}_1$, we can find that the above condition can be guaranteed easily with properly selected parameter β_k .

Considering that modes of original system can not be accessed directly to the controller, thus, we design an asynchronous 2D-SMC law as follows:

$$u(i, j) = K_\tau x(i, j) - \rho(i, j) \frac{s(i, j)}{\|s(i, j)\|} \quad (10)$$

where the matrix $K_\tau \in \mathbb{R}^{n_u \times n_x}$ with $n_x = n_h + n_v$ will be determined later, and the parameter $\rho(i, j)$ is set to

$$\rho(i, j) = \varrho_1 \|x(i, j)\| + \varrho_2 \|w(i, j)\| \quad (11)$$

with $\varrho_1 = \max_{k \in \mathcal{N}_1} \{\delta_k\}$, $\varrho_2 = \max_{k \in \mathcal{N}_1} \{\|(GB_k)^{-1}GE_k\|\}$, and the parameter δ_k is given in (2).

Considering system (1) with asynchronous 2D-SMC law (10), we can derive the following closed-loop 2D system

$$\mathbf{x}(i, j) = \bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j) + E_k w(i, j) \quad (12)$$

where $\bar{A}_{k\tau} = A_k + B_k K_\tau$, and $\bar{\rho}_k(i, j)$ as follows:

$$\bar{\rho}_k(i, j) = f_k(x(i, j)) - (\varrho_1 \|x(i, j)\| + \varrho_2 \|w(i, j)\|) \cdot \frac{s(i, j)}{\|s(i, j)\|}.$$

Then, based on (2) and the properties of norm, following condition can be obtained

$$\|\bar{\rho}_k(i, j)\| \leq (\varrho_1 + \delta_k) \|x(i, j)\| + \varrho_2 \|w(i, j)\|, \quad (13)$$

which further implies

$$\|\bar{\rho}_k(i, j)\|^2 \leq 2(\varrho_1 + \delta_k)^2 \|x(i, j)\|^2 + 2\varrho_2^2 \|w(i, j)\|^2. \quad (14)$$

Remark 3. As mentioned in introduction, asynchronous SMC schemes for 1D-MJSs have been extensively studied in previous works, and a large number of excellent results have been achieved, such as [21]–[23] etc. For 2D-MJSs, both its system states and system modes will propagate along two different directions, thus results of those works can not directly extend to 2D-MJSs because of its complex structural properties. In this paper, following the idea of Roesser model, a new 2D sliding surface $s(i, j)$ which is consisted of horizontal sub-sliding surface $s^h(i, j)$ and vertical sub-sliding surface $s^v(i, j)$ is constructed, and the corresponding asynchronous SMC law is designed under the framework of hidden Markov model. It is obvious that 2D structures $x(i, j)$ and $s(i, j)$ are included in SMC law (10), which is the reason we name it as 2D-SMC law.

B. Analysis of Stability and H_∞ Attenuation Performance

In this subsection, we focus on the stability and H_∞ disturbance attenuation performance analysis for the concerned closed-loop 2D system (12). A sufficient condition will be established to guarantee the concerned 2D system is AMSS with an H_∞ attenuation performance γ .

Theorem 1. Consider the 2D-MJS (1) under Assumption (1) and with the asynchronous 2D-SMC law (10). For a given scalar $\gamma > 0$, if there exist matrices $K_\tau \in \mathbb{R}^{n_u \times n_x}$, $R_k = \text{diag}\{R_k^h, R_k^v\} > 0$, $Q_{k\tau} > 0$, $T_{k\tau} > 0$ and scalars $\epsilon_k > 0$, for any $k \in \mathcal{N}_1, \tau \in \mathcal{N}_2$, such that the following inequalities hold:

$$B_k^T \mathcal{R}_k B_k - \epsilon_k I \leq 0 \quad (15)$$

$$\mathcal{A}_k + 2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} \text{diag}\{Q_{k\tau}, T_{k\tau}\} \right) < 0 \quad (16)$$

$$\hat{A}_{k\tau}^T \mathcal{R}_k \hat{A}_{k\tau} - \text{diag}\{Q_{k\tau}, T_{k\tau}\} < 0 \quad (17)$$

where

$$\mathcal{A}_k = \begin{bmatrix} \Pi_1 & \Pi_3 \\ * & \Pi_2 \end{bmatrix}$$

with

$$\begin{cases} \Pi_1 = -R_k + 4(\delta_k + \varrho_1)^2 \epsilon_k I + C_k^T C_k \\ \Pi_2 = -\gamma^2 I + D_k^T D_k + 4\varrho_2^2 \epsilon_k I \\ \Pi_3 = C_k^T D_k \end{cases}$$

and $\mathcal{R}_k = \sum_{p=1}^{N_1} \lambda_{kp} R_p$, $\hat{A}_{k\tau} = [\bar{A}_{k\tau} \ E_k]$, then the closed-loop system (12) is AMSS with an H_∞ disturbance attenuation performance γ .

Proof. Let's start the proof with the stability of system. Selecting the Lyapunov candidate as $V_1(i, j) = x^T(i, j) R_{\tau(i, j)} x(i, j)$, and define

$$\Delta V_1(i, j) = \mathbf{x}(i, j)^T R^*(i, j) \mathbf{x}(i, j) - x^T(i, j) R_k x(i, j) \quad (18)$$

where $R^*(i, j) = \text{diag}\{R_{\tau(i+1, j)}^h, R_{\tau(i, j+1)}^v\}$.

Based on the closed-loop system equation (12) with $w(i, j) = 0$, we have

$$\begin{aligned} & \mathbb{E}\{\Delta V_1(i, j)\} \\ &= \mathbb{E}\{\mathbf{x}(i, j)^T \mathcal{R}_k \mathbf{x}(i, j) - x^T(i, j) R_k x(i, j)\} \\ &= \sum_{\tau=1}^{N_2} \mu_{k\tau} \left\{ [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j)]^T \mathcal{R}_k \right. \\ &\quad \times [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j)] \left. \right\} \\ &\quad - x^T(i, j) R_k x(i, j) \\ &\leq x^T(i, j) \left\{ 2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T \mathcal{R}_k \bar{A}_{k\tau} \right) \right\} x(i, j) \\ &\quad + 2 \bar{\rho}_k^T(i, j) B_k^T \mathcal{R}_k B_k \bar{\rho}_k(i, j) \\ &\quad - x^T(i, j) R_k x(i, j) \end{aligned} \quad (19)$$

Recalling the conditions given in (13) and (15), the following inequality can be further obtained

$$\mathbb{E}\{\Delta V_1(i, j)\} \leq x^T(i, j) \mathcal{G}_{k\tau} x(i, j) \quad (20)$$

where $\mathcal{G}_{k\tau} = 2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T \mathcal{R}_k \bar{A}_{k\tau} \right) + 2\epsilon_k (\delta_k + \varrho_1)^2 I - R_k$. The following inequality can be deduced from (16) based on the property of positive definite matrix

$$2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} Q_{k\tau} \right) + 4\epsilon_k (\delta_k + \varrho_1)^2 I + C_k^T C_k - R_k < 0 \quad (21)$$

which further implies

$$2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} Q_{k\tau} \right) + 2\epsilon_k (\delta_k + \varrho_1)^2 I - R_k < 0 \quad (22)$$

The following inequality can be derived directly from condition (17)

$$\bar{A}_{k\tau}^T \mathcal{R}_k \bar{A}_{k\tau} - Q_{k\tau} < 0 \quad (23)$$

Combining (22) and (23), we can infer that $\mathcal{G}_{k\tau} < 0$, which is equivalent to

$$\mathcal{G}_{k\tau} \leq -\alpha I \quad (24)$$

with scalar $\alpha > 0$. Recalling (20), we can further infer that

$$\mathbb{E}\{\Delta V_1(i, j)\} \leq -\alpha \mathbb{E}\{\|x(i, j)\|^2\} \quad (25)$$

Summing up on the both sides of (25), we have

$$\mathbb{E}\left\{ \sum_{i=0}^{\hat{\kappa}_1} \sum_{j=0}^{\hat{\kappa}_2} \|x(i, j)\|^2 \right\} \leq -\frac{1}{\alpha} \mathbb{E}\left\{ \sum_{i=0}^{\hat{\kappa}_1} \sum_{j=0}^{\hat{\kappa}_2} \Delta V_1(i, j) \right\} \quad (26)$$

where parameters $\hat{\kappa}_1, \hat{\kappa}_2$ are any positive integers. By substituting ΔV_1 with (18) and let $R_k = \text{diag}\{R_k^h, R_k^v\}$ (see Theorem 1), we obtain

$$\begin{aligned} & \sum_{i=0}^{\hat{\kappa}_1} \sum_{j=0}^{\hat{\kappa}_2} \Delta V_1(i, j) \\ &= \sum_{i=0}^{\hat{\kappa}_1} \{V_1^v(i, \hat{\kappa}_2 + 1) - V_1^v(i, 0)\} \\ &\quad + \sum_{j=0}^{\hat{\kappa}_2} \{V_1^h(\hat{\kappa}_1 + 1, j) - V_1^h(0, j)\} \\ &\leq - \left(\sum_{i=0}^{\hat{\kappa}_1} V_1^v(i, 0) + \sum_{j=0}^{\hat{\kappa}_2} V_1^h(0, j) \right) \end{aligned} \quad (27)$$

where $V_1^h(i, j)$ and $V_1^v(i, j)$ are defined as

$$\begin{cases} V_1^h(i, j) = x^{hT}(i, j) R_{\tau(i, j)}^h x^h(i, j) \\ V_1^v(i, j) = x^{vT}(i, j) R_{\tau(i, j)}^v x^v(i, j) \end{cases}$$

Recalling the boundary condition in Assumption 1, and let $\hat{\kappa}_1, \hat{\kappa}_2$ tend to infinity, it follows from (26) and (27) that

$$\begin{aligned} & \mathbb{E}\left\{ \sum_{i=0}^{\infty} \sum_{j=0}^{\infty} \|x(i, j)\|^2 \right\} \\ &\leq \frac{\beta}{\alpha} \sum_{\ell=0}^{\infty} (\|x^v(\ell, 0)\|^2 + \|x^h(0, \ell)\|^2) \\ &< \infty \end{aligned} \quad (28)$$

where $\beta > 0$ is the maximum eigenvalue of $R_{\tau(0, \ell)}^h$ and $R_{\tau(\ell, 0)}^v$, for any $\ell = 0, 1, 2, \dots$, which indicates that (7) holds. Therefore, the asymptotic mean square stability of the concerned closed-loop 2D system is proved.

Next, let's focus on the H_∞ disturbance attenuation performance when the system is under zero boundary condition.

Based on the closed-loop system equation (12), it is easy to find that

$$\begin{aligned}
& \mathbb{E}\{\Delta V_1(i, j)\} \\
&= \sum_{\tau=1}^{N_2} \mu_{k\tau} \left\{ [\bar{A}_{k\tau}x(i, j) + B_k\bar{\rho}_k(i, j) + E_kw(i, j)]^T \right. \\
&\quad \times \mathcal{R}_k[\bar{A}_{k\tau}x(i, j) + B_k\bar{\rho}_k(i, j) + E_kw(i, j)] \left. \right\} \\
&\quad - x^T(i, j)R_kx(i, j) \\
&\leq \hat{x}^T(i, j) \left\{ 2 \left(\sum_{\tau=1}^{N_2} \mu_{k\tau} \hat{A}_{k\tau}^T \mathcal{R}_k \hat{A}_{k\tau} \right) \hat{x}(i, j) \right. \\
&\quad + 2\bar{\rho}_k^T(i, j)B_k^T \mathcal{R}_k B_k \bar{\rho}_k(i, j) \\
&\quad \left. - x^T(i, j)R_kx(i, j) \right\}
\end{aligned} \tag{29}$$

where

$$\hat{x}(i, j) = \begin{bmatrix} x(i, j) \\ w(i, j) \end{bmatrix}, \quad \hat{A}_{k\tau}(i, j) = [\bar{A}_{k\tau} \quad E_k]$$

Notice that from (14) and (15), we have

$$\begin{aligned}
& \bar{\rho}_k^T(i, j)B_k^T \mathcal{R}_k B_k \bar{\rho}_k(i, j) \\
&\leq \|B_k^T \mathcal{R}_k B_k\| \|\bar{\rho}_k\|^2 \\
&\leq 2\epsilon_k((\delta_k + \varrho_1)^2 \|x(i, j)\|^2 + \varrho_2^2 \|w(i, j)\|^2)
\end{aligned} \tag{30}$$

The following condition can be deduced easily from (16) and (17)

$$\Xi_{k\tau} < 0 \tag{31}$$

where $\Xi_{k\tau} \equiv \mathcal{A}_k + 2 \sum_{\tau=1}^{N_2} \mu_{k\tau} \hat{A}_{k\tau}^T \mathcal{R}_k \hat{A}_{k\tau}$. Recalling the system (1), and substituting (30) into (29) yields

$$\begin{aligned}
& \mathbb{E}\{\Delta V_1(i, j) + \|y(i, j)\|^2 - \gamma^2 \|w(i, j)\|^2\} \\
&\leq \hat{x}^T(i, j) \Xi_{k\tau} \hat{x}(i, j) < 0
\end{aligned} \tag{32}$$

Noting (27) with the zero boundary condition, we can infer that

$$\begin{aligned}
& \sum_{i=0}^{\hat{\kappa}_1} \sum_{j=0}^{\hat{\kappa}_2} \Delta V_1(i, j) \\
&= \sum_{i=0}^{\hat{\kappa}_1} V_1^v(i, \hat{\kappa}_2 + 1) + \sum_{j=0}^{\hat{\kappa}_2} V_1^h(\hat{\kappa}_1 + 1, j) \\
&\geq 0 \quad \forall \hat{\kappa}_1, \hat{\kappa}_2 = 1, 2, 3, \dots
\end{aligned} \tag{33}$$

Then, we can further deduce from (32) and (33) that

$$\begin{aligned}
& \sum_{i=0}^{\infty} \sum_{j=0}^{\infty} \mathbb{E}\{\|y(i, j)\|^2 - \gamma^2 \|w(i, j)\|^2\} \\
&\leq \sum_{i=0}^{\infty} \sum_{j=0}^{\infty} \mathbb{E}\{\Delta V_1(i, j) + \|y(i, j)\|^2 - \gamma^2 \|w(i, j)\|^2\} \\
&< 0
\end{aligned} \tag{34}$$

which suggests that (8) is satisfied. And this completes the proof of Theorem 1. \square

C. Analysis of Reachability

The reachability of the designed asynchronous 2D-SMC law for the concerned closed-loop 2D system (12) will be discussed in this subsection. By using a stochastic Lyapunov method, we provide a sufficient condition which will confirm that the designed asynchronous 2D-SMC law (10) can force the state trajectories of the concerned closed-loop 2D system (12) into a time-varying sliding region around the predefined 2D sliding surface (9).

Theorem 2. Consider the 2D-MJS (1) with asynchronous 2D-SMC law (10). If there exist matrices $K_\tau \in \mathbb{R}^{n_u \times n_x}$, $R_k > 0$, $F_k > 0$, and scalars $\epsilon_k > 0$, for any $k \in \mathcal{N}_1, \tau \in \mathcal{N}_2$, such that condition (15) and following inequality holds

$$2 \sum_{\tau=1}^{N_2} \bar{A}_{k\tau}^T (\mathcal{R}_k + G^T \mathcal{F}_k G) \bar{A}_{k\tau} - R_k < 0 \tag{35}$$

where \mathcal{R}_k is defined in Theorem 1, and $\mathcal{F}_k = \sum_{p=1}^{N_1} \lambda_{kp} F_p$. Then, the state trajectories of the concerned closed-loop 2D system (12) will be forced into a sliding region \mathcal{O} , around the predefined sliding surface (9), where \mathcal{O} is given as:

$$\mathcal{O} \equiv \left\{ \|s(i, j)\| \leq \rho^*(i, j) \right\} \tag{36}$$

and $\rho^*(i, j) = \max_{k \in \mathcal{N}_1} \sqrt{\hat{\rho}_k(i, j) / \lambda_{\min}(F_k)}$ with

$$\begin{aligned}
\hat{\rho}_k(i, j) = & 4(\|E_k^T \mathcal{R}_k E_k\| + \|E_k^T G^T \mathcal{R}_k G E_k\| \\
& + 2\varrho_2^2(\|B_k^T \mathcal{F}_k B_k\| + \|B_k^T G^T \mathcal{F}_k G B_k\|)) \|w(i, j)\|^2 \\
& + 8(\varrho_1 + \delta_k)^2 (\|B_k^T \mathcal{R}_k B_k\| + \|B_k^T G^T \mathcal{R}_k G B_k\|) \|x(i, j)\|^2.
\end{aligned}$$

$\lambda_{\min}(F_k)$ here denotes the minimum eigenvalue of F_k .

Proof. Above all, let's define $s(i, j) = \begin{bmatrix} s^h(i+1, j) \\ s^v(i, j+1) \end{bmatrix}$, it is easy to find that $s(i, j) = Gx(i, j)$. Then, we select the Lyapunov candidate as

$$V(i, j) = V_1(i, j) + V_2(i, j) \tag{37}$$

where $V_1(i, j)$ is defined in the proof of Theorem 1, and $V_2(i, j) = s^T(i, j) F_r(i, j) s(i, j)$. Similar with the proof pro-

cedure of Theorem 1, it is easy to find that

$$\begin{aligned}
& \mathbb{E}\{\Delta V_1(i, j)\} \\
&= \mathbb{E}\left\{x(i, j)^T R^*(i, j)x(i, j) - x^T(i, j)R_k x(i, j)\right\} \\
&= \sum_{\tau=1}^{N_2} \mu_{k\tau} \left\{ [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j) + E_k w(i, j)]^T \right. \\
&\quad \times \mathcal{R}_k [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j) + E_k w(i, j)] \left. \right\} \\
&\quad - x^T(i, j)R_k x(i, j) \\
&\leq 2x^T(i, j) \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T \mathcal{R}_k \bar{A}_{k\tau} x(i, j) \\
&\quad + 2[B_k \bar{\rho}_k(i, j) + E_k w(i, j)]^T \mathcal{R}_k \\
&\quad \times [B_k \bar{\rho}_k(i, j) + E_k w(i, j)] \\
&\quad - x^T(i, j)R_k x(i, j) \\
&\leq 2x^T(i, j) \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T \mathcal{R}_k \bar{A}_{k\tau} x(i, j) \\
&\quad + 4\bar{\rho}_k^T(i, j)B_k^T \mathcal{R}_k B_k \bar{\rho}_k(i, j) \\
&\quad + 4w^T(i, j)E_k^T \mathcal{R}_k E_k w(i, j) \\
&\quad - x^T(i, j)R_k x(i, j)
\end{aligned} \tag{38}$$

where $R^*(i, j)$ is defined in the proof of Theorem 1. Along with the sliding surface function (9), we can deduce that

$$\begin{aligned}
& \mathbb{E}\{\Delta V_2(i, j)\} \\
&= \mathbb{E}\left\{s(i, j)^T F^*(i, j)s(i, j) - s^T(i, j)F_k s(i, j)\right\} \\
&= \sum_{\tau=1}^{N_2} \mu_{k\tau} \left\{ [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j) + E_k w(i, j)]^T \right. \\
&\quad \times G^T \mathcal{F}_k G [\bar{A}_{k\tau} x(i, j) + B_k \bar{\rho}_k(i, j) + E_k w(i, j)] \left. \right\} \\
&\quad - s^T(i, j)F_k s(i, j) \\
&\leq 2x^T(i, j) \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T G^T \mathcal{F}_k G \bar{A}_{k\tau} x(i, j) \\
&\quad + 2[B_k \bar{\rho}_k(i, j) + E_k w(i, j)]^T G^T \mathcal{F}_k \\
&\quad \times G [B_k \bar{\rho}_k(i, j) + E_k w(i, j)] \\
&\quad - s^T(i, j)F_k s(i, j) \\
&\leq 2x^T(i, j) \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T G^T \mathcal{F}_k G \bar{A}_{k\tau} x(i, j) \\
&\quad + 4\bar{\rho}_k^T(i, j)B_k^T G^T \mathcal{F}_k G B_k \bar{\rho}_k(i, j) \\
&\quad + 4w^T(i, j)E_k^T G^T \mathcal{F}_k G E_k w(i, j) \\
&\quad - s^T(i, j)F_k s(i, j)
\end{aligned} \tag{39}$$

where $F^*(i, j) = \text{diag}\{F_{r(i+1, j)}^h, F_{r(i, j+1)}^v\}$. Combing condi-

tions (37)-(39), we can infer that

$$\begin{aligned}
& \mathbb{E}\{\Delta V(i, j)\} \\
&= \mathbb{E}\left\{\Delta_1(i, j) + \Delta V_2(i, j)\right\} \\
&\leq x^T(i, j) \left\{ 2 \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T (\mathcal{R}_k + G^T \mathcal{F}_k G) \bar{A}_{k\tau} \right\} x(i, j) \\
&\quad + \bar{\rho}_k(i, j) - x^T(i, j)R_k x(i, j) - \lambda_{\min}(F_k) \|s(i, j)\|^2
\end{aligned} \tag{40}$$

where

$$\begin{aligned}
& \bar{\rho}_k(i, j) \\
&= 4(\|B_k^T \mathcal{F}_k B_k\| + \|B_k^T G^T \mathcal{F}_k G B_k\|) \|\bar{\rho}_k(i, j)\|^2 \\
&\quad + 4(\|E_k^T \mathcal{R}_k E_k\| + \|E_k^T G^T \mathcal{R}_k G E_k\|) \|w(i, j)\|^2
\end{aligned} \tag{38}$$

It is obvious that $\bar{\rho}_k(i, j) < \hat{\rho}_k(i, j)$ for any $k \in \mathcal{N}_1$ after substituting $\|\bar{\rho}_k(i, j)\|^2$ with (14). Then, based on the condition (16), when the state trajectories are out of the region \mathcal{O} , we can infer that

$$-\lambda_{\min}(F_k) \|s(i, j)\|^2 + \bar{\rho}_k(i, j) < 0 \tag{41}$$

It yields from (35), (38), (40) and (41) that

$$\begin{aligned}
& \mathbb{E}\{\Delta V(i, j)\} \\
&\leq x^T(i, j) \left\{ 2 \sum_{\tau=1}^{N_2} \mu_{k\tau} \bar{A}_{k\tau}^T (\mathcal{R}_k + G^T \mathcal{F}_k G) \bar{A}_{k\tau} \right. \\
&\quad \left. - R_k \right\} x(i, j) < 0
\end{aligned} \tag{42}$$

which means that, when outside the region \mathcal{O} , the state trajectories of the concerned closed-loop 2D system (12) will strictly decrease in the sense of mean square. Now, the proof is completed. \square

D. Synthesis of Asynchronous 2D-SMC Law

It is obvious that, if the theorem 1 and the theorem 2 hold simultaneously, the asymptotic mean square stability with an H_∞ performance γ of the closed-loop 2D system (12) and the reachability of the predefined 2D sliding surface (9) can be guaranteed simultaneously. That is, the to-be-determined matrix K_τ in 2D-SMC law (10) should ensure that theorem 1, 2 are established at the same time. Now, in this subsection, we will continue our study with this idea.

Theorem 3. Consider the 2D-MJS (1) under the Assumption (1) and with the asynchronous 2D-SMC law (10). For a given scalar $\gamma > 0$, if there exist matrices $\tilde{K}_\tau \in \mathbb{R}^{n_u \times n_x}$, $L_\tau \in \mathbb{R}^{n_x \times n_x}$, $\tilde{R}_k = \text{diag}\{\tilde{R}_k^h, \tilde{R}_k^v\} > 0$, $\tilde{F}_k > 0$, $\tilde{Q}_{k\tau} > 0$, $\tilde{T}_{k\tau} > 0$ and scalars $\tilde{\epsilon}_k > 0$, for any $k \in \mathcal{N}_1, \tau \in \mathcal{N}_2$, such that the following inequalities hold:

$$\begin{bmatrix} -\tilde{\epsilon}_k I & \mathcal{B}_k \\ * & \mathcal{R}_k \end{bmatrix} < 0 \tag{43}$$

$$\begin{bmatrix} \mathcal{L}_{k\tau} & \mathcal{A}_{k\tau} & \mathcal{G}_{k\tau} \\ * & \mathcal{R}_k & 0 \\ * & * & \mathcal{F}_k \end{bmatrix} < 0 \tag{44}$$

$$\begin{bmatrix} \mathcal{H}_k & \mathcal{D}_k & \mathcal{P}_{k\tau} & \mathcal{Y}_{k\tau} \\ * & \mathcal{J}_k & 0 & 0 \\ * & * & \mathcal{Q}_{k\tau} & 0 \\ * & * & * & \mathcal{F}_{k\tau} \end{bmatrix} < 0 \quad (45)$$

where

$$\begin{aligned} \mathcal{B}_k &= [\sqrt{\lambda_{k1}}\tilde{e}_k B_k^T \quad \sqrt{\lambda_{k2}}\tilde{e}_k B_k^T \quad \cdots \quad \sqrt{\lambda_{kN_1}}\tilde{e}_k B_k^T] \\ \mathcal{R}_k &= \text{diag}\{-\tilde{R}_1, -\tilde{R}_2, \dots, -\tilde{R}_{N_1}\} \\ \mathcal{F}_k &= \text{diag}\{-\tilde{F}_1, -\tilde{F}_2, \dots, -\tilde{F}_{N_1}\} \\ \mathcal{J}_k &= \text{diag}\{-\tilde{e}_k, -I, -I, -\tilde{e}_k\} \\ \mathcal{Q}_{k\tau} &= \text{diag}\{-\tilde{Q}_{k1}, -\tilde{Q}_{k2}, \dots, -\tilde{Q}_{kN_2}\} \\ \mathcal{T}_{k\tau} &= \text{diag}\{-\tilde{T}_{k1}, -\tilde{T}_{k2}, \dots, -\tilde{T}_{kN_2}\} \\ \mathcal{L}_{k\tau} &= \text{diag}\{\tilde{Q}_{k\tau} - L_\tau^T - L_\tau, -\tilde{T}_{k\tau}\} \\ \mathcal{H}_k &= \begin{bmatrix} -\tilde{R}_k & \tilde{R}_k^T D_k^T \\ * & -\gamma^2 I \end{bmatrix} \\ \mathcal{A}_{k\tau} &= \begin{bmatrix} \sqrt{\lambda_{k1}}\tilde{A}_{k\tau}^T & \cdots & \sqrt{\lambda_{kN_1}}\tilde{A}_{k\tau}^T \\ \sqrt{\lambda_{k1}}\tilde{T}_{k\tau} B_k^T & \cdots & \sqrt{\lambda_{kN_1}}\tilde{T}_{k\tau} B_k^T \end{bmatrix} \\ \mathcal{G}_{k\tau} &= \begin{bmatrix} \sqrt{\lambda_{k1}}\tilde{A}_{k\tau}^T G^T & \cdots & \sqrt{\lambda_{kN_1}}\tilde{A}_{k\tau}^T G^T \\ 0 & \cdots & 0 \end{bmatrix} \\ \mathcal{D}_{k\tau} &= \begin{bmatrix} 2(\varrho_1 + \delta_k)\tilde{R}_k & \tilde{R}_k C_k^T & 0 & 0 \\ 0 & 0 & D_k^T & 2\varrho_2 \end{bmatrix} \\ \mathcal{P}_{k\tau} &= \begin{bmatrix} \sqrt{2\mu_{k1}}\tilde{R}_k & \cdots & \sqrt{2\mu_{kN_2}}\tilde{R}_k \\ 0 & \cdots & 0 \end{bmatrix} \\ \mathcal{Y}_{k\tau} &= \begin{bmatrix} 0 & \cdots & 0 \\ \sqrt{2\mu_{k1}}I & \cdots & \sqrt{2\mu_{kN_2}}I \end{bmatrix} \end{aligned}$$

and $\tilde{A}_{k\tau} = A_k L_\tau + B_k \tilde{K}_\tau$. Then, the concerned closed-loop 2D-MJS (12) is AMSS with an H_∞ disturbance attenuation performance γ , and the state trajectories of the concerned closed-loop 2D-MJS will be forced into a sliding region \mathcal{O} . Moreover, the to-be-determined matrix K_τ in 2D-SMC law (10) can be chosen as

$$K_\tau = \tilde{K}_\tau L_\tau^{-1} \quad (46)$$

if the LMIs (43)-(45) have feasible solutions.

Proof. As we discussed above, the objective is to testify that, the conditions (15)-(17) in Theorem 1 and (35) in Theorem 2 can be guaranteed simultaneously by (43)-(45). Before that, let's make some notations as $\tilde{K}_\tau = K_\tau L_\tau$, $\tilde{R}_k = R_k^{-1}$, $\tilde{F}_k = F_k^{-1}$, $\tilde{Q}_{k\tau} = Q_{k\tau}^{-1}$, $\tilde{T}_{k\tau} = T_{k\tau}^{-1}$ and $\tilde{e} = e_k^{-1}$. First of all, let's prove that (43) is equivalent to (15). Pre- and post-multiplying the inequalities given in (43) by $\text{diag}\{e_k I, I, I, \dots, I\}$, respectively, and applying Schur complement after that, then, we can see (15) is satisfied. Next, we will verify that (44)-(45) are sufficient to ensure (16)-(17) and (35) hold simultaneously. Using $\text{diag}\{R_k, I, I, \dots, I\}$ to pre- and post-multiply the inequality given in (45), and applying Schur complement after that, then we will have (16) satisfied. It follows from (44) that $\tilde{Q}_{k\tau} - L_\tau^T - L_\tau < 0$, that is $L_\tau^T + L_\tau$ is positive definite, which can further deduces that the matrix L_τ is invertible. Noting that $Q_{k\tau} > 0$, then we can infer the following formulation holds

$$(\tilde{Q}_{k\tau} - L_\tau)^T \tilde{Q}_{k\tau}^{-1} (\tilde{Q}_{k\tau} - L_\tau) \geq 0 \quad (47)$$

which means

$$-L_\tau^T \tilde{Q}_{k\tau} L_\tau \leq \tilde{Q}_{k\tau} - L_\tau^T - L_\tau \quad (48)$$

Recalling the condition given in (45), then we can infer that

$$\begin{bmatrix} \tilde{\mathcal{L}}_{k\tau} & \mathcal{A}_{k\tau} & \mathcal{G}_{k\tau} \\ * & \mathcal{R}_k & 0 \\ * & * & \mathcal{F}_k \end{bmatrix} < 0 \quad (49)$$

where $\tilde{\mathcal{L}}_{k\tau} = \text{diag}\{-L_\tau^T \tilde{Q}_{k\tau} L_\tau, -\tilde{T}_{k\tau}\}$.

Noting that the slack matrix L_τ is invertible, we denote $h_{k\tau} = \text{diag}\{L_\tau^{-1}, T_{k\tau}, I, I, \dots, I\}$. Using $h_{k\tau}$ to pre- and post-multiply the inequality given in (49), and applying Schur complement after that, then the following inequality will be obtained

$$\hat{A}_{k\tau}^T \mathcal{R}_k \hat{A}_{k\tau} + \hat{A}_{k\tau}^T \mathcal{F}_k \hat{A}_{k\tau} - \text{diag}\{Q_{k\tau}, T_{k\tau}\} < 0 \quad (50)$$

where $\hat{A}_{k\tau} = [\tilde{A}_{k\tau} \quad 0]$. It is clear that (17) can be guaranteed by (50).

Combing (16) and (50), we will have

$$\mathcal{A} + 2 \sum_{\tau=0}^{N_2} \mu_{k\tau} \left\{ \hat{A}_{k\tau}^T \mathcal{R}_k \hat{A}_{k\tau} + \hat{A}_{k\tau}^T \mathcal{F}_k \hat{A}_{k\tau} \right\} < 0 \quad (51)$$

which further implies (35) holds based on the property of positive definite matrix. It is clear that, the gain matrix K_τ can not be obtained directly from LMIs in Theorem 3 while \tilde{K}_τ is obtained. Thanks to the fact that matrix L_τ is invertible, K_τ can be calculated indirectly with $K_\tau = \tilde{K}_\tau L_\tau^{-1}$. Now, the proof is finished. \square

It is clear that, the conditions in Theorem 3 are presented in the form of LMI, which can be easily solved with Matlab LMI toolbox. Next, we will propose an algorithm to obtain the asynchronous 2D-SMC law with the minimum disturbance attenuation performance γ^* . The 2D-SMC law design algorithm is summarized as follows:

- Step 1: Select the parameters β_k properly and compute matrix G , such that, for any $k \in \mathcal{N}_1$, the matrix GB_k is nonsingular.
- Step 2: Figure out the scalars ϱ_1 and ϱ_2 in (11).
- Step 3: Get the matrices \tilde{K}_τ and L_τ by solving the following optimization problem

$$\min \tilde{\sigma} \text{ subject to (43)-(45) with } \tilde{\sigma} = \gamma^2. \quad (52)$$
- Step 4: Finally, if Step 3 has feasible solutions, then, the sliding mode controller matrix K_τ can be obtained with $K_\tau = \tilde{K}_\tau L_\tau^{-1}$.

IV. NUMERICAL EXAMPLE

In this section, we are going to provide an simulation example to verify the effectiveness of the proposed asynchronous 2D-SMC design method. As is well-known that several dynamical processes, for instance, gas absorption, water stream heating and air drying can be represented by the Darboux equation [25]. It is generally presented in the form of partial differential equations, and can be easily transformed into a 2D system in Roesser model with a similar approach applied in [28]. In this example, the concerned 2D-MJS and the

asynchronous 2D-SMC both consist of two operation modes, that is, $\mathcal{N}_1 = \{1, 2\}$, $\mathcal{N}_2 = \{1, 2\}$, and the relevant system parameters are given as follows:

Mode 1:

$$A_1 = \begin{bmatrix} -1.0 & 0.4 \\ 0.2 & -1.0 \end{bmatrix}, B_1 = \begin{bmatrix} 0.2 & 0.1 \\ -0.2 & -0.3 \end{bmatrix}, D_1 = \begin{bmatrix} -0.1 \\ 0 \end{bmatrix}$$

$$C_1 = \begin{bmatrix} 0.1 & -0.1 \\ -0.2 & 0.1 \end{bmatrix}, E_1 = \begin{bmatrix} -0.1 \\ 0.1 \end{bmatrix}$$

Mode 2:

$$A_2 = \begin{bmatrix} -0.8 & 0.6 \\ 0.2 & -1.2 \end{bmatrix}, B_2 = \begin{bmatrix} 0.2 & -0.2 \\ -0.1 & -0.2 \end{bmatrix}, D_2 = \begin{bmatrix} -0.1 \\ 0.2 \end{bmatrix}$$

$$C_2 = \begin{bmatrix} -0.2 & -0.1 \\ 0.1 & 0.2 \end{bmatrix}, E_2 = E_1$$

The nonlinear function $f(x(i, j), r(i, j))$ is set as

$$f((x(i, j), r(i, j))) = \begin{cases} 0.2 \sin \|x(i, j)\|, & r(i, j) = 1 \\ 0.3 \sin \|x(i, j)\|, & r(i, j) = 2 \end{cases}$$

Thus, the parameter δ_k can be selected as first mode with $\delta_1 = 0.2$ and second mode with $\delta_2 = 0.3$.

The mode jumps of the considered 2D-MJS and 2D-SMC are governed by the transition probability matrix Λ and Ψ , respectively, which are set as follows:

$$\Lambda = \begin{bmatrix} 0.8 & 0.2 \\ 0.3 & 0.7 \end{bmatrix}, \Psi = \begin{bmatrix} 0.6 & 0.4 \\ 0.4 & 0.6 \end{bmatrix}$$

A possible time sequences with two different directions of

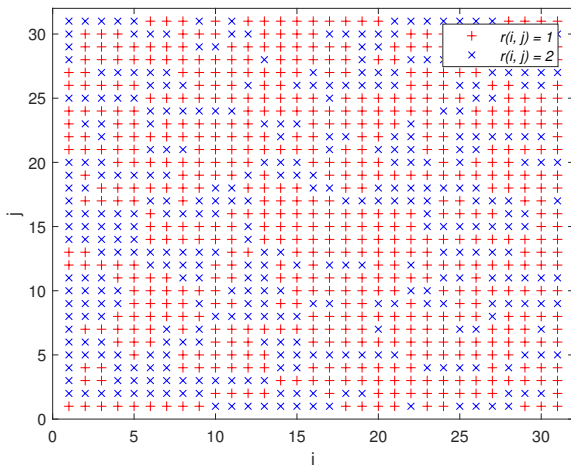


Fig. 1. Modes of the considered 2D system

the system modes and the asynchronous controller modes are depicted in Fig.1-2. By comparison, it is clear that the designed controller run asynchronously with the original 2D system. Based on the corresponding assumptions, the boundary con-

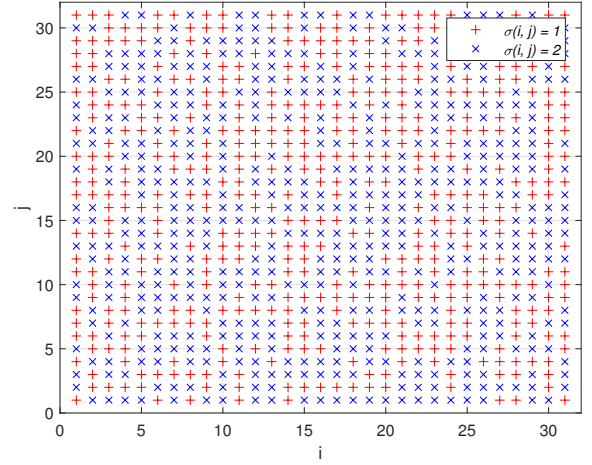


Fig. 2. Modes of the 2D-SMC

dition X_0 and exogenous disturbance $w(i, j)$ are assumed to be

$$x^h(0, j) = \begin{cases} 0.1, & 0 \leq j \leq 10 \\ 0, & \text{elsewhere} \end{cases}$$

$$x^v(i, 0) = \begin{cases} 0.1, & 0 \leq i \leq 10 \\ 0, & \text{elsewhere} \end{cases}$$

$$w(i, j) = \begin{cases} 0.2, & 0 \leq i, j \leq 10 \\ 0, & \text{elsewhere} \end{cases}$$

The horizontal and vertical state responses of the open-

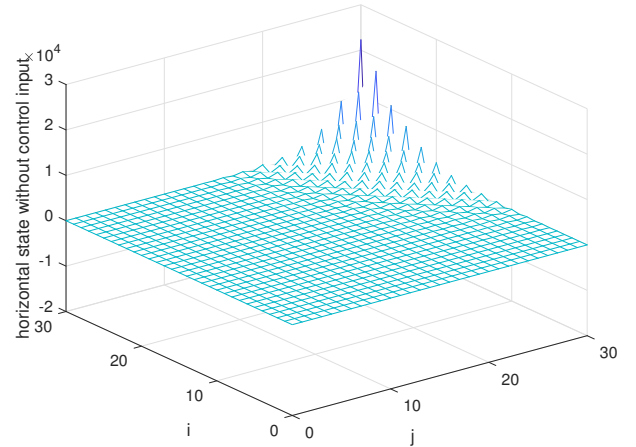


Fig. 3. Horizontal state $x^h(i, j)$ with $u(i, j) = 0$

loop system (1) under $u(i, j) = 0$ are depicted in Fig.3 and Fig.4, respectively. The obtained result implies the considered 2D system is unstable under zero control input. Next, let's follow the procedures of asynchronous 2D-SMC law design algorithm, and obtain the sliding model controller gain. Letting $\beta_1 = 0.6$ and $\beta_2 = 0.4$, then the matrix G can be calculated as follows:

$$G = \begin{bmatrix} 0.2 & -0.16 \\ -0.02 & -0.26 \end{bmatrix}$$

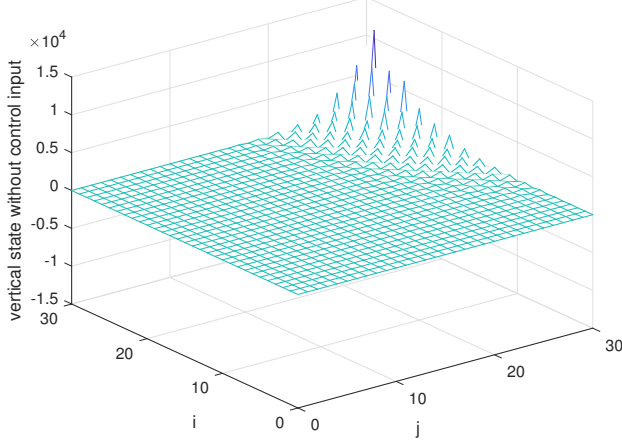


Fig. 4. Vertical state $x^v(i, j)$ with $u(i, j) = 0$

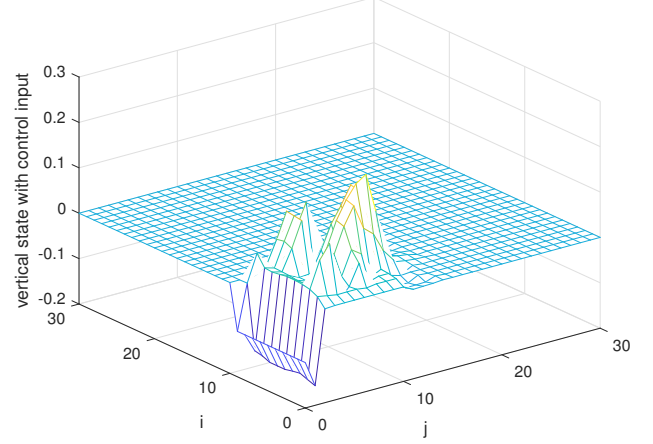


Fig. 6. Vertical state $x^v(i, j)$ with asynchronous 2D-SMC

It's easy to verify that the non-singularity of the matrix GB_k is satisfied for any $k \in \mathcal{N}_1$. The parameters ϱ_1 and ϱ_2 can be calculated as $\varrho_1 = 0.3$ and $\varrho_2 = 0.6872$, respectively. By solving optimization problem (52), we can obtain the following sliding mode controller gains

Mode1

$$K_1 = \begin{bmatrix} 4.4147 & -4.3512 \\ -0.6827 & -2.1886 \end{bmatrix}$$

Mode2

$$K_2 = \begin{bmatrix} 4.3706 & -3.8453 \\ -0.6826 & -2.3252 \end{bmatrix}$$

with the minimum H_∞ disturbance attenuation performance $\gamma^* = 0.3164$.

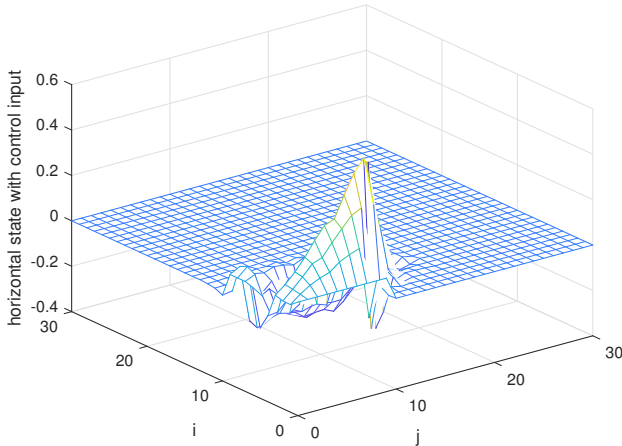


Fig. 5. Horizontal state $x^h(i, j)$ with asynchronous 2D-SMC

The horizontal and vertical state response of the closed-loop system (12) with asynchronous 2D-SMC law are depicted in Fig.5-6. It is clear that both horizontal and vertical system state converge to zero within finite steps. The sliding surface $s(i, j)$ and the asynchronous 2D-SMC law can be obtained based on the conditions given in (9) and (10), respectively. Then, the

horizontal 2D-SMC input, vertical 2D-SMC input, horizontal sliding surface and vertical sliding surface are depicted in Fig.7-10. Clearly, the observed simulation results imply that the proposed asynchronous 2D-SMC law is effective for the considered 2D-MJS.

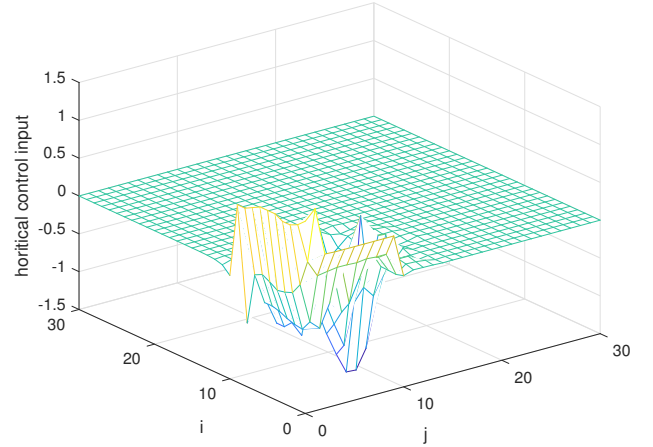


Fig. 7. Horizontal asynchronous 2D-SMC input $u^h(i, j)$

V. CONCLUSIONS

This work has investigated the problem of asynchronous SMC for 2D-MJSs in Roesser model. In consideration that the system modes are not always accessible to the controller, an asynchronous 2D-SMC law design method is explored with hidden Markov model. By utilizing Lyapunov function, the asymptotic mean square stability for the concerned 2D-MJS and the reachability of the sliding mode dynamics are analyzed, respectively. A sufficient condition is derived that can guarantee the concerned closed-loop 2D system is AMSS with an H_∞ disturbance attenuation performance, and the reachability of the 2D sliding mode dynamics is ensured simultaneously. Finally, the asynchronous SMC law design

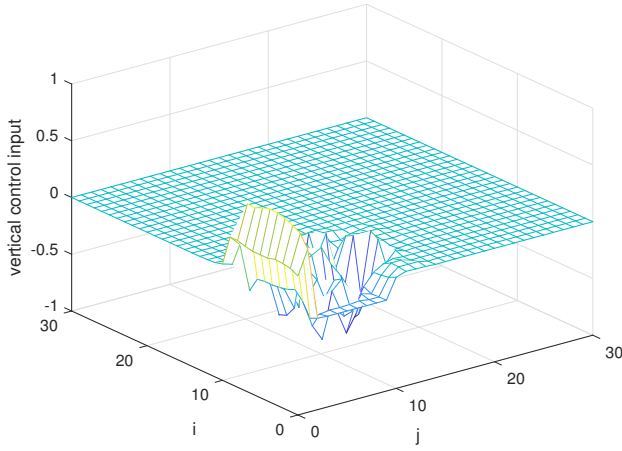


Fig. 8. Vertical asynchronous 2D-SMC input $u^v(i, j)$

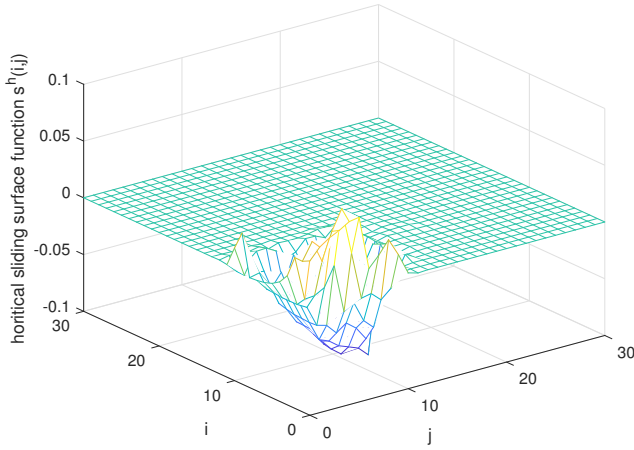


Fig. 9. Horizontal sliding surface $s^h(i, j)$

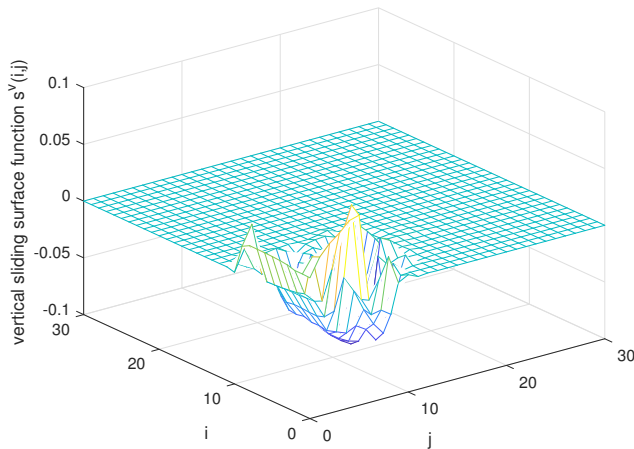


Fig. 10. Vertical sliding surface $s^v(i, j)$

procedures are summarized as an algorithm whose effectiveness is verified by a numerical example.

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