

# ShanghaiTech

## SIST

### EE130P Final Report

Topic: ☒1 ☒2 ☐3 ☐4 ☒5

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2018.07

# Topic1 - Part I. Objective

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- Gain basic knowledge of patch antenna
- Design one patch antenna working at **3.55Ghz**

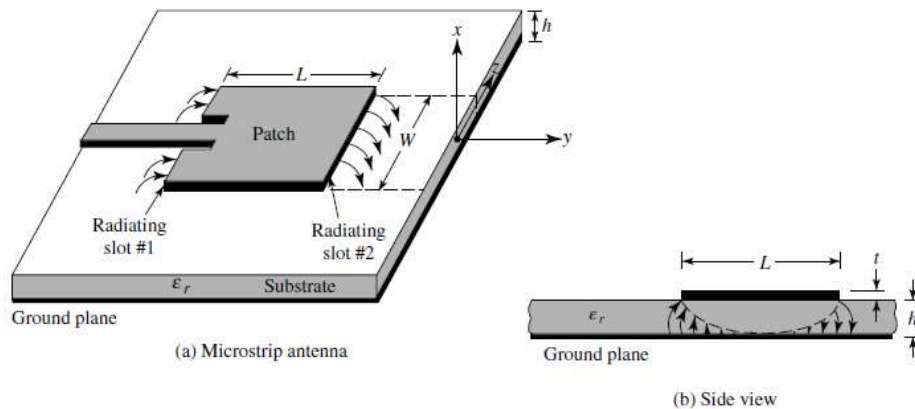
# Topic1 - Part II. Data

## - Parameters

- $f = 3.55GHz$
- $\epsilon_r = 4.6$
- $h = 1mm$
- $t = 35\mu m$

## - Formulas

- $W = \frac{v_0}{2f_r} \sqrt{\frac{2}{\epsilon_r + 1}}$
- $\epsilon_{eff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[ 1 + 12 \frac{h}{W} \right]^{-1/2}$
- $L = \frac{1}{2f_r \sqrt{\epsilon_{eff}} \sqrt{\mu_0 \epsilon_0}} - 2\Delta L$
- $\frac{\Delta L}{h} = 0.412 \frac{(\epsilon_{eff} + 0.3) \left( \frac{W}{h} + 0.264 \right)}{(\epsilon_{eff} - 0.258) \left( \frac{W}{h} + 0.8 \right)}$



# Topic1 - Part II. Data

## - Formulas

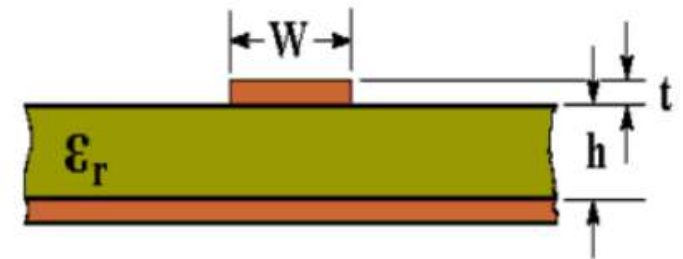
- $W = \frac{v_0}{2f_r} \sqrt{\frac{2}{\epsilon_r + 1}}$
- $\epsilon_{reff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[ 1 + 12 \frac{h}{W} \right]^{-1/2}$
- $L = \frac{1}{2f_r \sqrt{\epsilon_{reff}} \sqrt{\mu_0 \epsilon_0}} - 2\Delta L$
- $\frac{\Delta L}{h} = 0.412 \frac{(\epsilon_{reff} + 0.3) \left( \frac{W}{h} + 0.264 \right)}{(\epsilon_{reff} - 0.258) \left( \frac{W}{h} + 0.8 \right)}$
- $R_{in} = 90 \frac{(\epsilon_r)^2}{\epsilon_r - 1} \left( \frac{L}{W} \right)$
- $R_{in}(y = y_0) = R_{in}(y = 0) \cos^2\left(\frac{\pi}{L} y_0\right)$

## - Results:

- $W = 25.25mm$
- $\epsilon_{reff} = 4.282$
- $L = 19.5mm$
- $\Delta L = 0.459mm$
- $L_e = L + 2\Delta L = 20.418mm$
- $y_0 = 7.53mm$

# Topic1 - Part II. Data

With the help of **Microstrip line characteristic impedance calculator...**



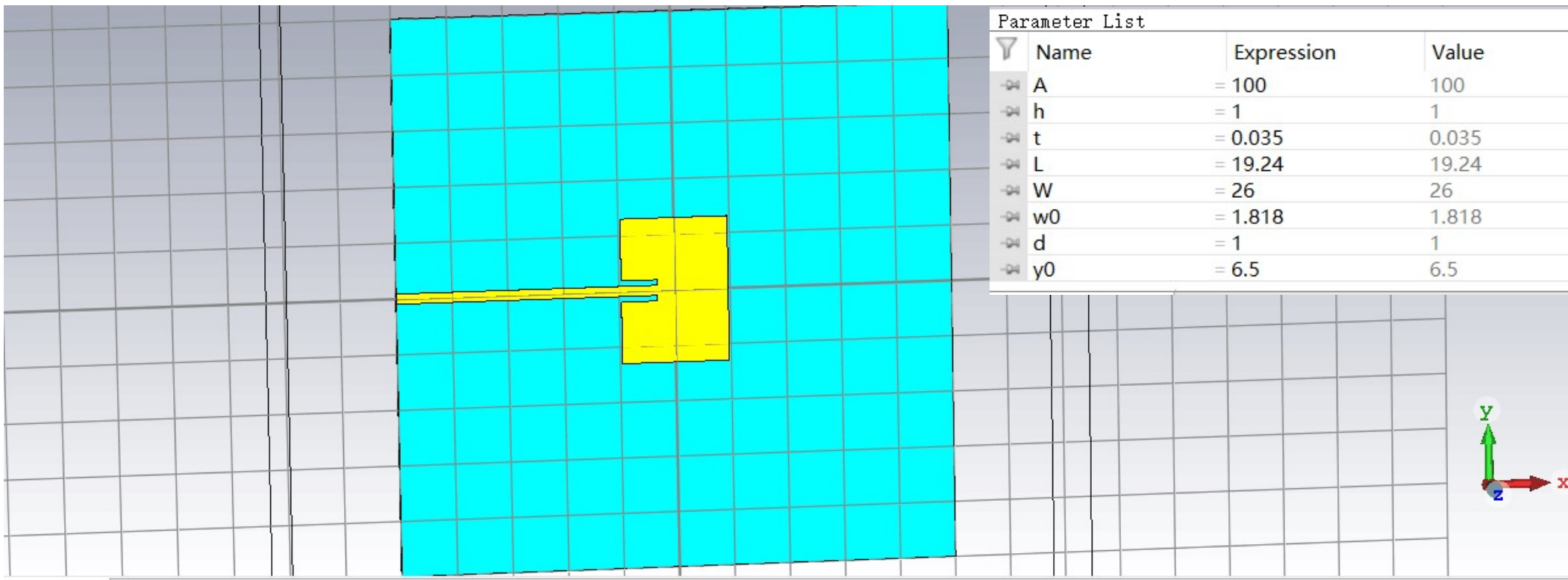
We get when the microstrip line's width is about **1.818mm**, the characteristic impedance can be **50 $\Omega$** , to meet the demand of this topic.

Find the value by changing  $W$  again and again until  $Z_0 = 50\Omega$ .

相对介电常数 $\epsilon_r$	4.6	
微带线线宽 $W$	1.818	毫米
微带线厚度 $t$	0.035	毫米
介质层厚度 $h$	1	毫米
等效介电常数 ( $\epsilon_{eff}$ ):	3.453	
特征阻抗 ( $Z_0$ ):	50	欧姆

Calculate

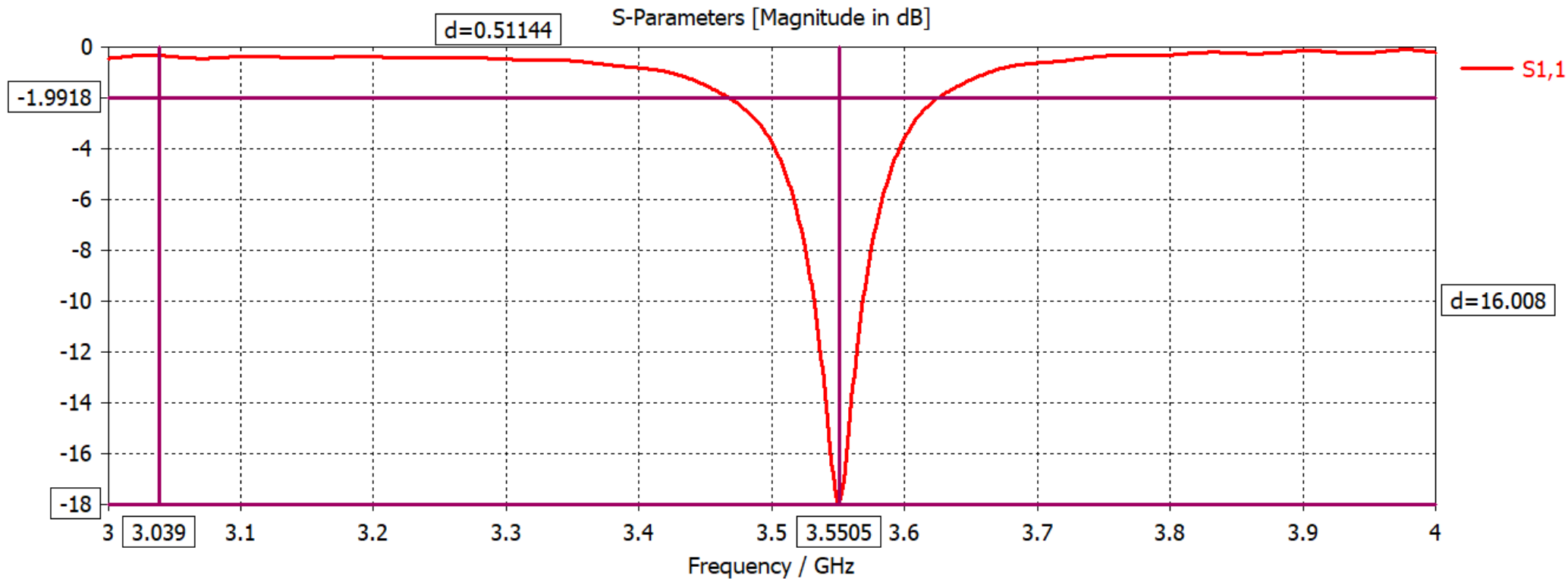
# Topic1 - Part II. Data



Simulated chart & Parameters

# Topic1 - Part II. Data

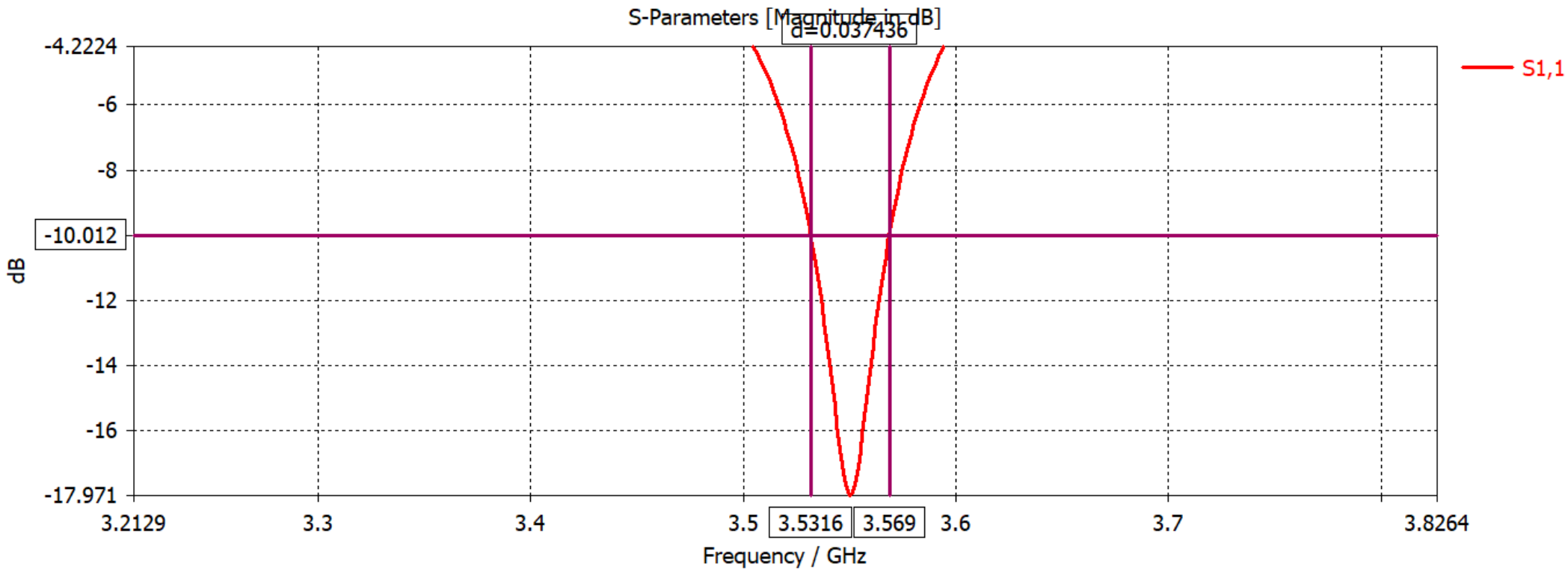
S-Parameters



By observing the position of the cursor, we can get that the working frequency is about 3.55GHz.

# Topic1 - Part II. Data

Relative bandwidth (frequency range in which  $|S_{11}|$  is less than  $-10$  dB)

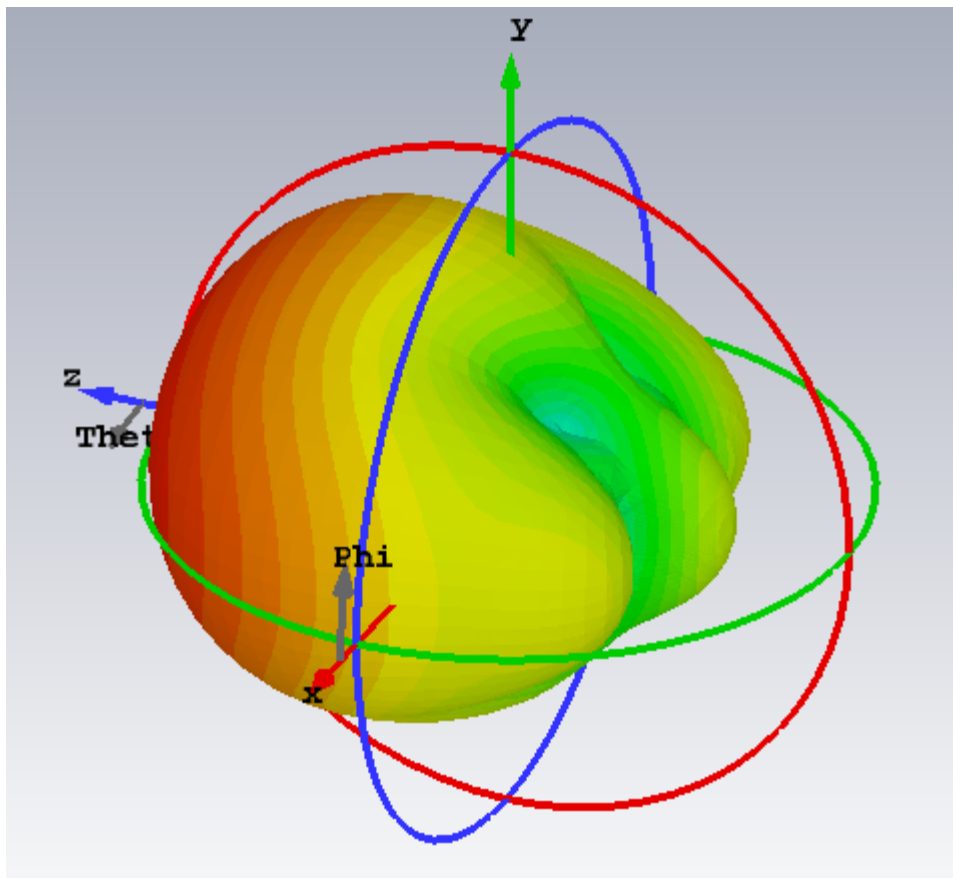


$$BW = \frac{f_{high} - f_{low}}{f_{design}} = \frac{0.037436}{3.55} * 100\% \approx 1.055\%$$



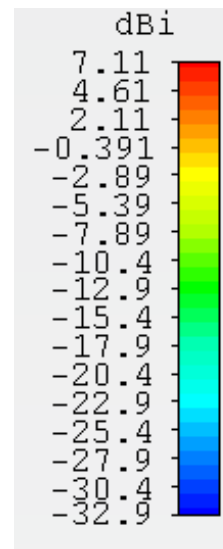
# Topic1 - Part II. Data

Radiation pattern(3D farfield)



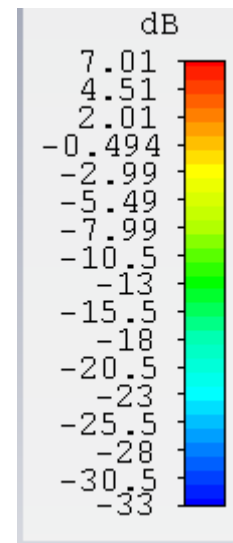
Radiation efficiency:-0.1030 dB  
Total efficiency:-0.1728 dB

Directivity



```
farfield (f=3.55) [1]
Type                Farfield
Approximation       enabled (kR >> 1)
Component           Abs
Output              Directivity
Frequency            3.55 GHz
Rad. effic.          -0.1030 dB
Tot. effic.          -0.1728 dB
Dir.                 7.109 dBi
```

Gain



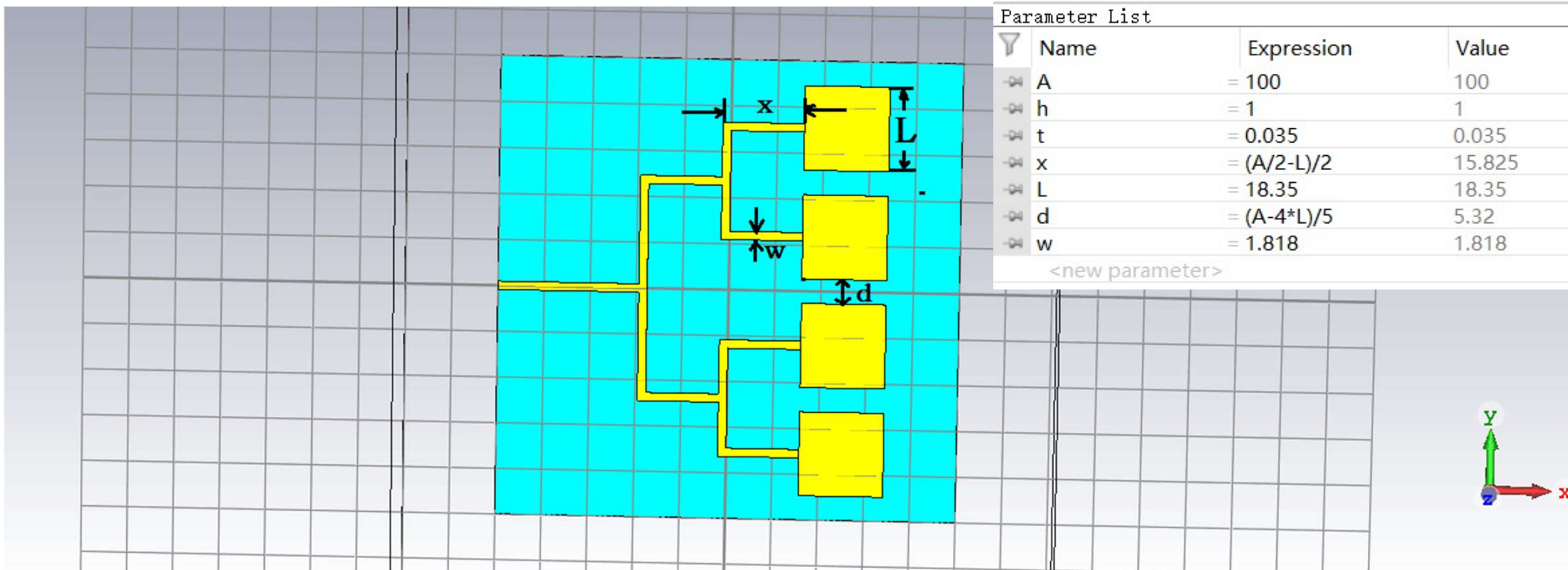
```
farfield (f=3.55) [1]
Type                Farfield
Approximation       enabled (kR >> 1)
Component           Abs
Output              Gain
Frequency            3.55 GHz
Rad. effic.          -0.1030 dB
Tot. effic.          -0.1728 dB
Gain                 7.006 dB
```

## Topic2 - Part I. Objective

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- Gain basic knowledge of patch antenna array
- Design two patch antenna arrays working at **3.55Ghz**
- Microstrip line feed method & probe feed method

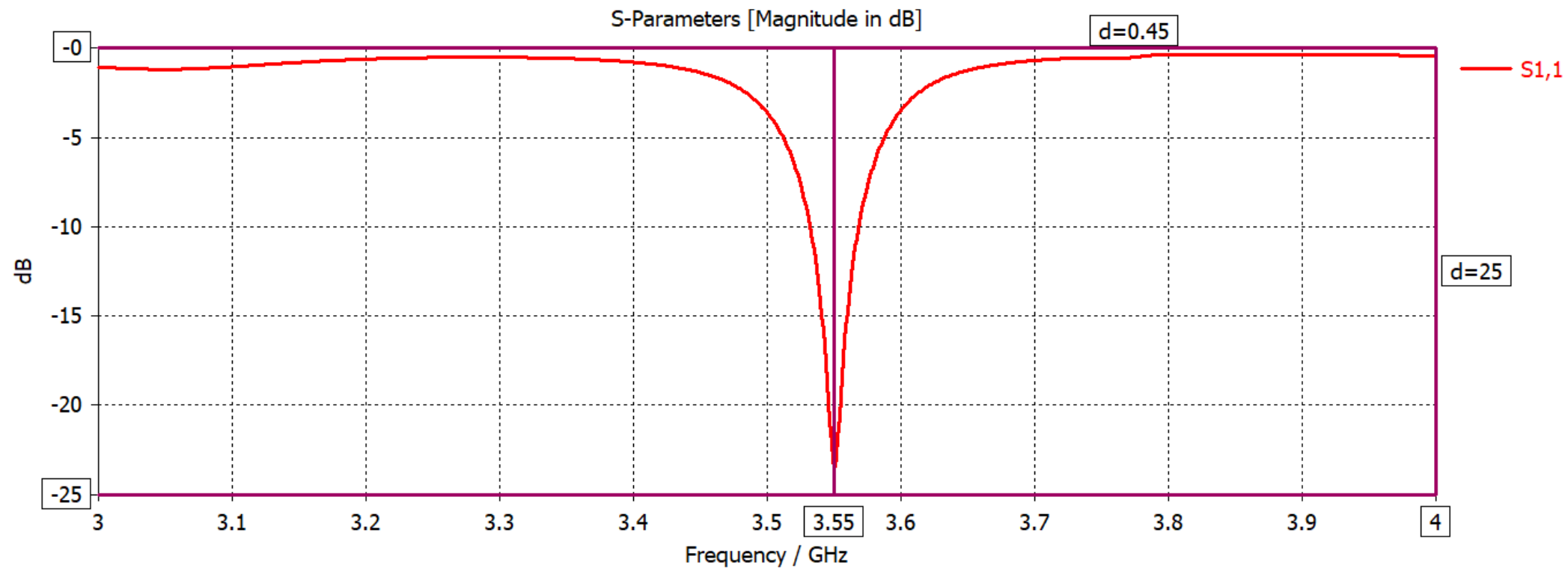
# Topic2 - Part II. Data(Microstrip Line Feed)



Simulated chart & Parameters

# Topic2 - Part II. Data(Microstrip Line Feed)

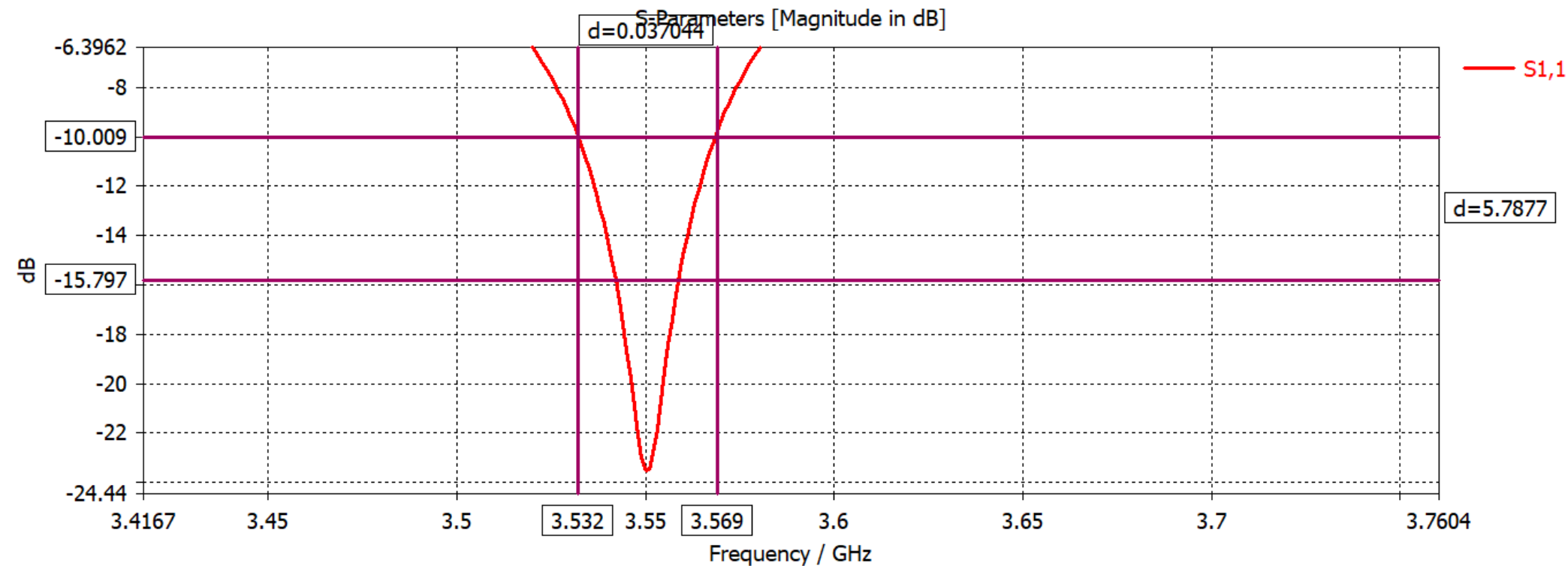
S-Parameters



By observing the position of the cursor, we can get that the working frequency is about 3.55GHz.

# Topic2 - Part II. Data(Microstrip Line Feed)

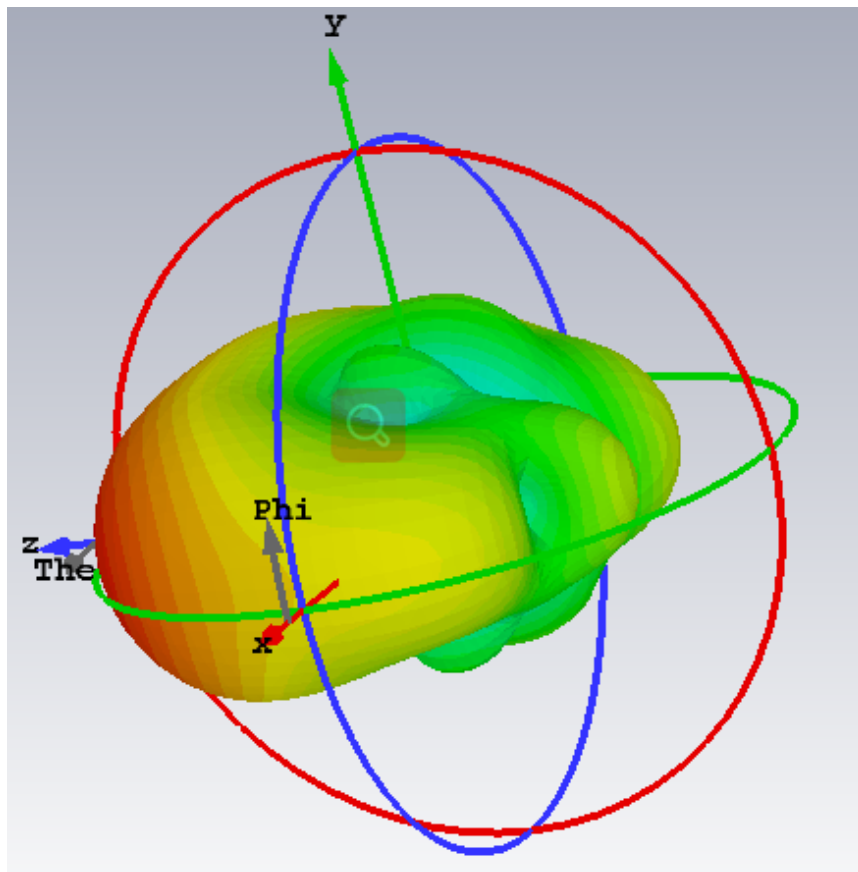
Relative bandwidth (frequency range in which  $|S_{11}|$  is less than  $-10$  dB)



$$BW = \frac{f_{high} - f_{low}}{f_{design}} = \frac{0.037044}{3.55} * 100\% \approx 1.043\%$$

# Topic2 - Part II. Data(Microstrip Line Feed)

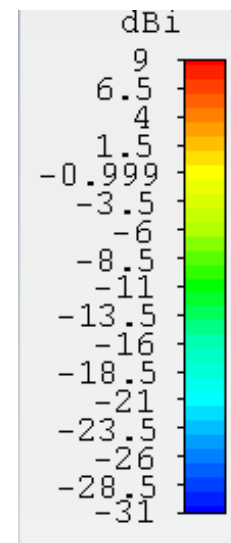
Radiation pattern(3D farfield)



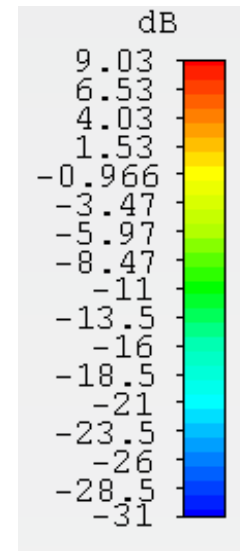
Radiation efficiency:-0.03227 dB

Total efficiency:-0.01295 dB

Directivity



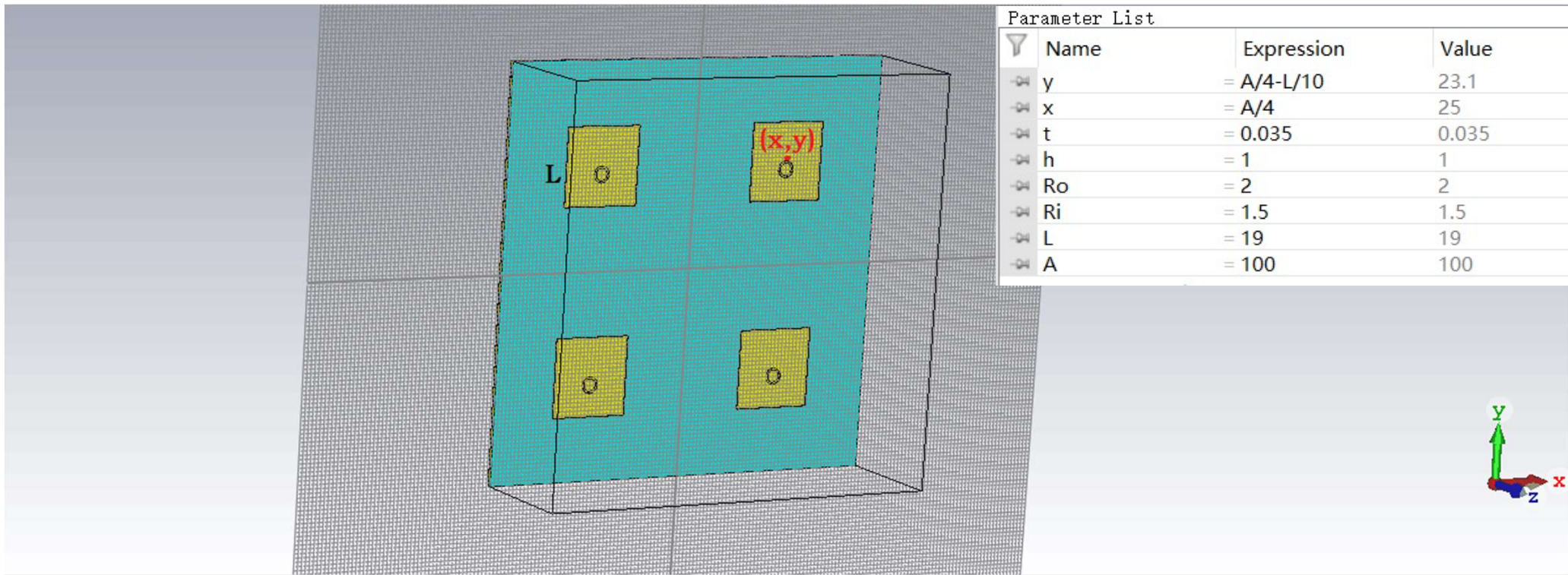
Gain



farfield (f=3.55) [1]	
Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Directivity
Frequency	3.55 GHz
Rad. eff.	0.03227 dB
Tot. eff.	0.01295 dB
Dir.	9.001 dBi

farfield (f=3.55) [1]	
Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Gain
Frequency	3.55 GHz
Rad. eff.	0.03227 dB
Tot. eff.	0.01295 dB
Gain	9.034 dB

## Topic2 - Part II. Data(Probe Feed)



Simulated chart & Parameters

# Topic2 - Part II. Data(Probe Feed)

farfield (f=3.55) [1[1,0]+2[1,20]+3[1,100]+4[1,180]]  
Abs

farfield (f=3.55) [1[1,0]+2[1,30]+3[1,45]+4[1,60]]  
Abs

farfield (f=3.55) [1[1,0]+2[1,37]+3[1,94]+4[1,139]]  
Abs

farfield (f=3.55) [1[1,0]+2[1,58]+3[1,148]+4[1,246]]  
Abs

farfield (f=3.55) [1[1,0]+2[1,80]+3[1,120]+4[1,160]]  
Abs

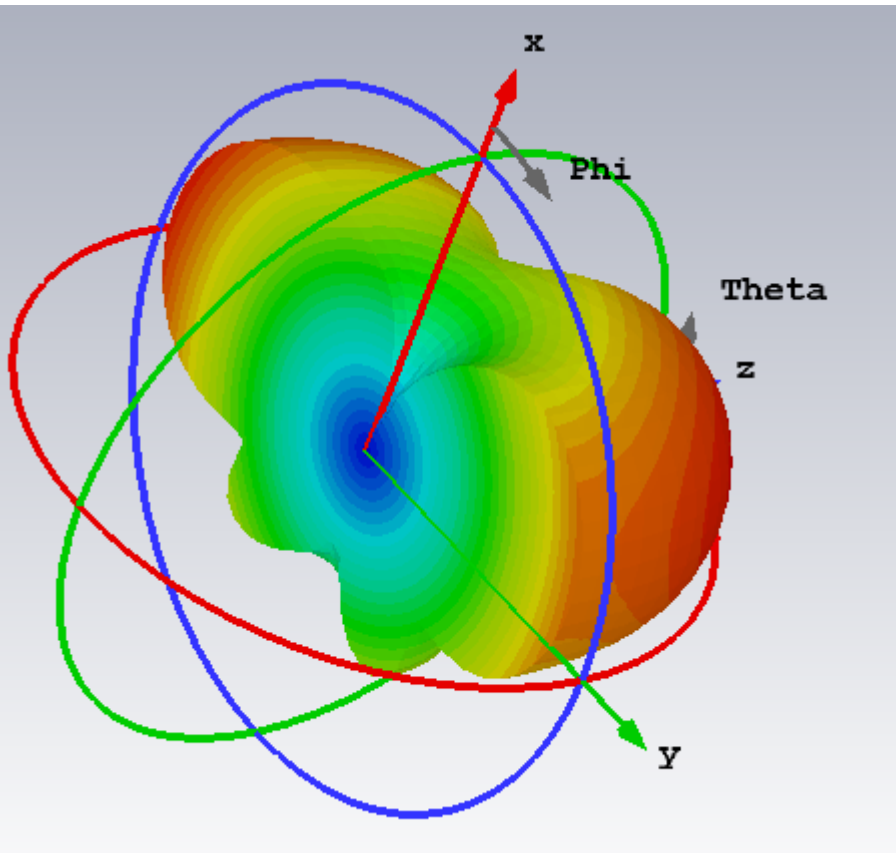
farfield (f=3.55) [1[1,0]+2[1,100]+3[1,111]+4[1,86]]  
Abs

	Amp	Phase1	Phase2	Phase3	Phase4
Ang1	1	0	20	100	180
Ang2	1	0	30	45	60
Ang3	1	0	37	94	139
Ang4	1	0	58	148	246
Ang5	1	0	80	120	160
Ang6	1	0	100	111	86

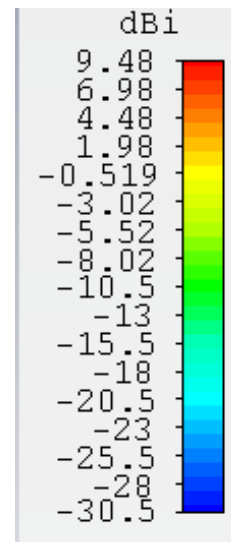


# Topic2 - Part II. Data(Probe Feed)

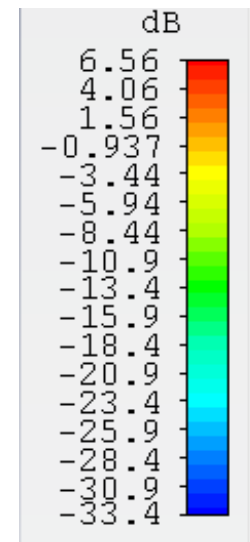
Ang1. Radiation pattern(3D farfield)



Directivity



Gain

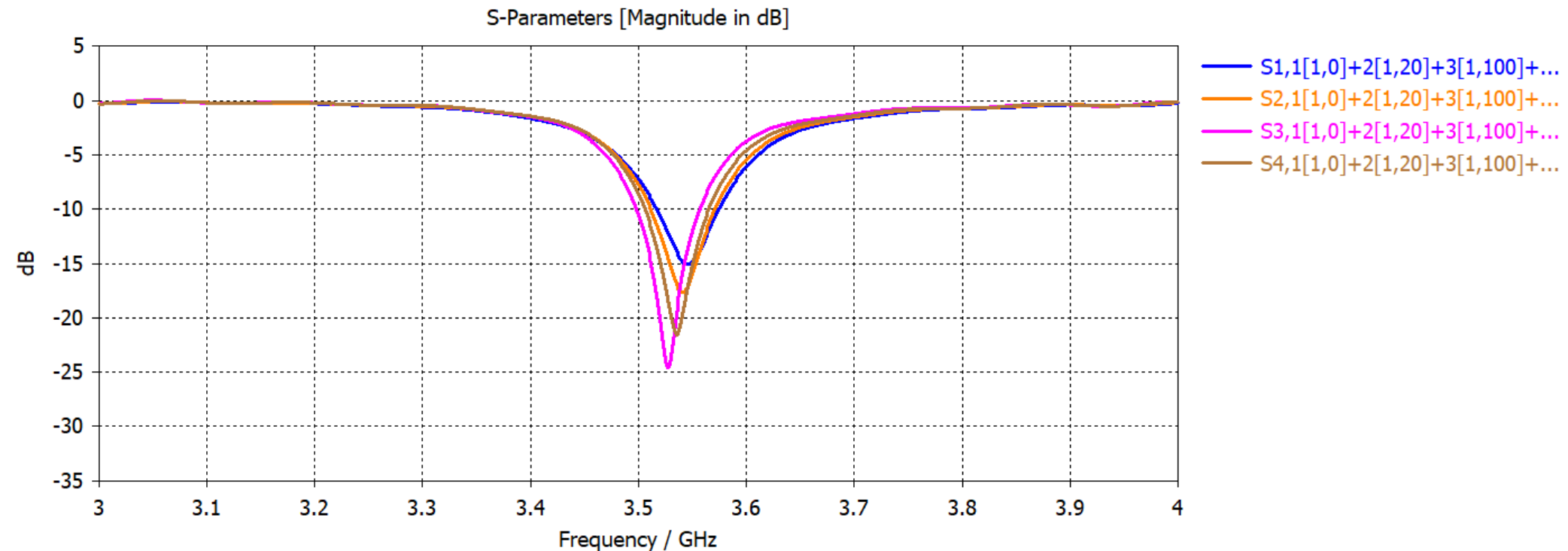


farfield (f=3.55) [1...]+3[1,1farfield (f=3.55) [1...]+3[1,100]+4[1,180]]			
Type	Farfield	Type	Farfield
Approximation	enabled (kR >> 1)	Approximation	enabled (kR >> 1)
Component	Abs	Component	Abs
Output	Directivity	Output	Gain
Frequency	3.55 GHz	Frequency	3.55 GHz
Rad. effic.	-2.918 dB	Rad. effic.	-2.918 dB
Tot. effic.	-3.084 dB	Tot. effic.	-3.084 dB
Dir.	9.481 dBi	Gain	6.563 dB

Radiation efficiency:-2.918 dB

Total efficiency:-3.084 dB

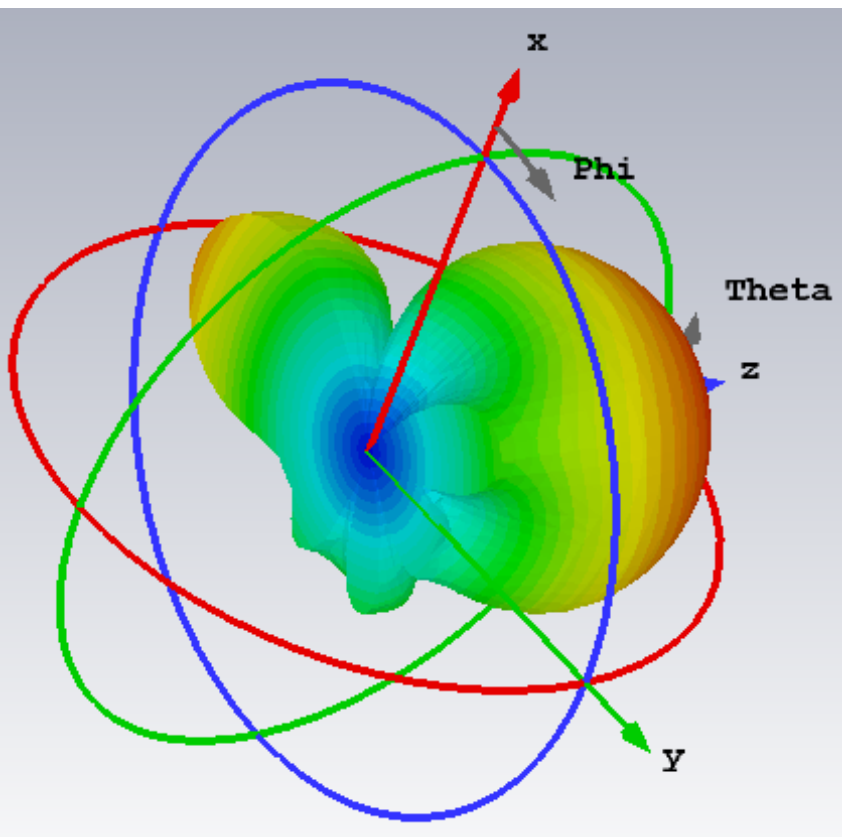
# Topic2 - Part II. Data(Probe Feed)



**Ang1.** S-parameters

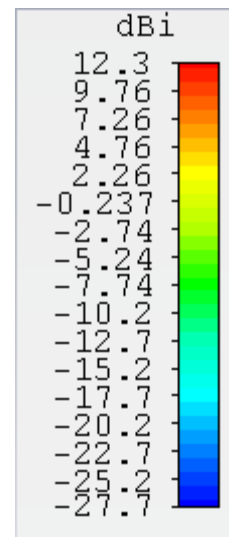
# Topic2 - Part II. Data(Probe Feed)

Ang2. Radiation pattern(3D farfield)

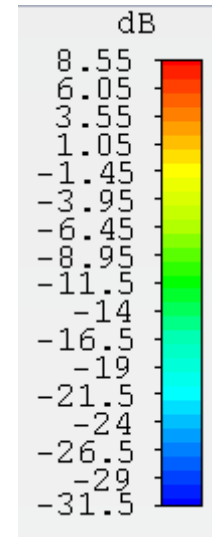


Radiation efficiency:-3.717 dB  
Total efficiency:-3.758 dB

Directivity

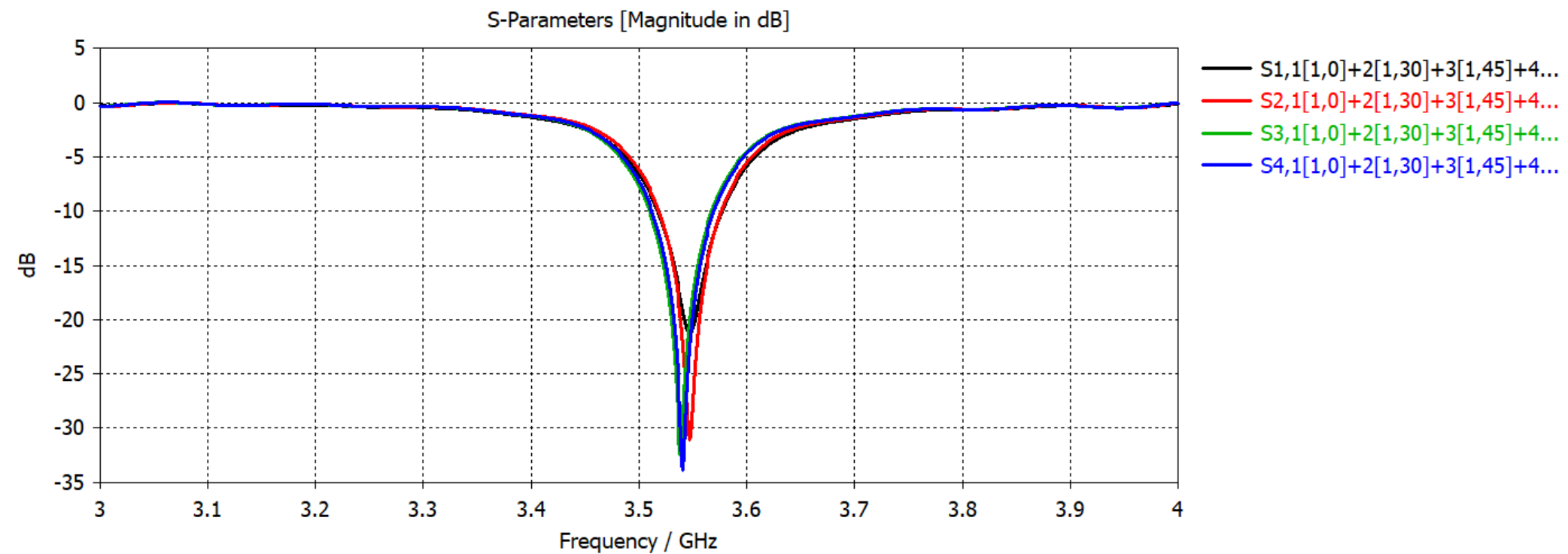


Gain



farfield (f=3.55) [1...30]+3[1,45]+4		farfield (f=3.55) [1...30]+3[1,45]+4[1,60]]	
Type	Farfield	Type	Farfield
Approximation	enabled (kR >> 1)	Approximation	enabled (kR >> 1)
Component	Abs	Component	Abs
Output	Directivity	Output	Gain
Frequency	3.55 GHz	Frequency	3.55 GHz
Rad. effic.	-3.717 dB	Rad. effic.	-3.717 dB
Tot. effic.	-3.758 dB	Tot. effic.	-3.758 dB
Dir.	12.26 dBi	Gain	8.547 dB

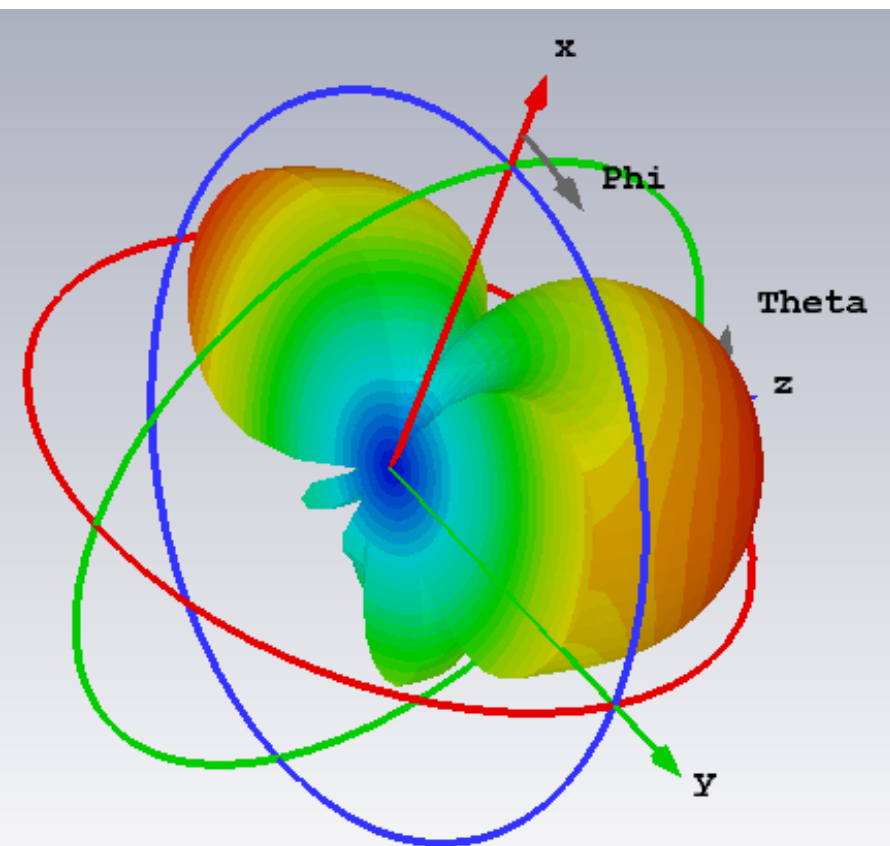
# Topic2 - Part II. Data(Probe Feed)



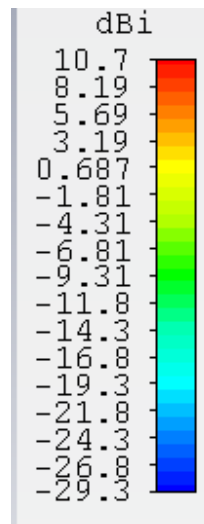
**Ang2.** S-parameters

# Topic2 - Part II. Data(Probe Feed)

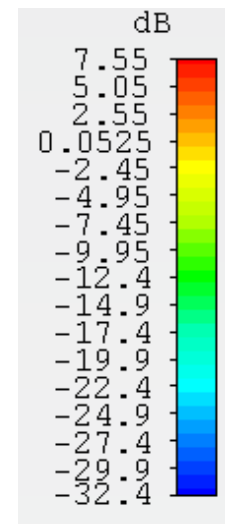
## Ang3. Radiation pattern(3D farfield)



### Directivity



### Gain



farfield (f=3.55) [1...7]+3[1, 94]·farfield (f=3.55) [1...7]+3[1, 94]+4[1, 139]]

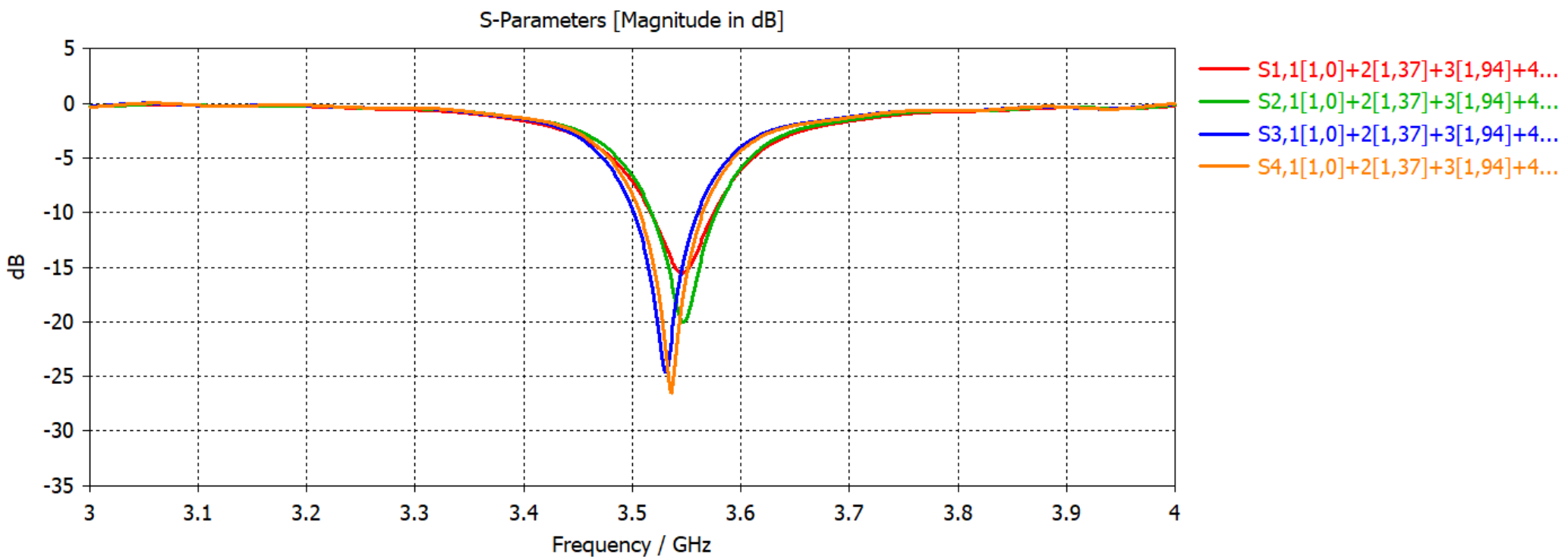
Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Directivity
Frequency	3.55 GHz
Rad. effic.	-3.134 dB
Tot. effic.	-3.259 dB
Dir.	10.69 dBi

Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Gain
Frequency	3.55 GHz
Rad. effic.	-3.134 dB
Tot. effic.	-3.259 dB
Gain	7.553 dB

Radiation efficiency:-3.134 dB

Total efficiency:-3.259 dB

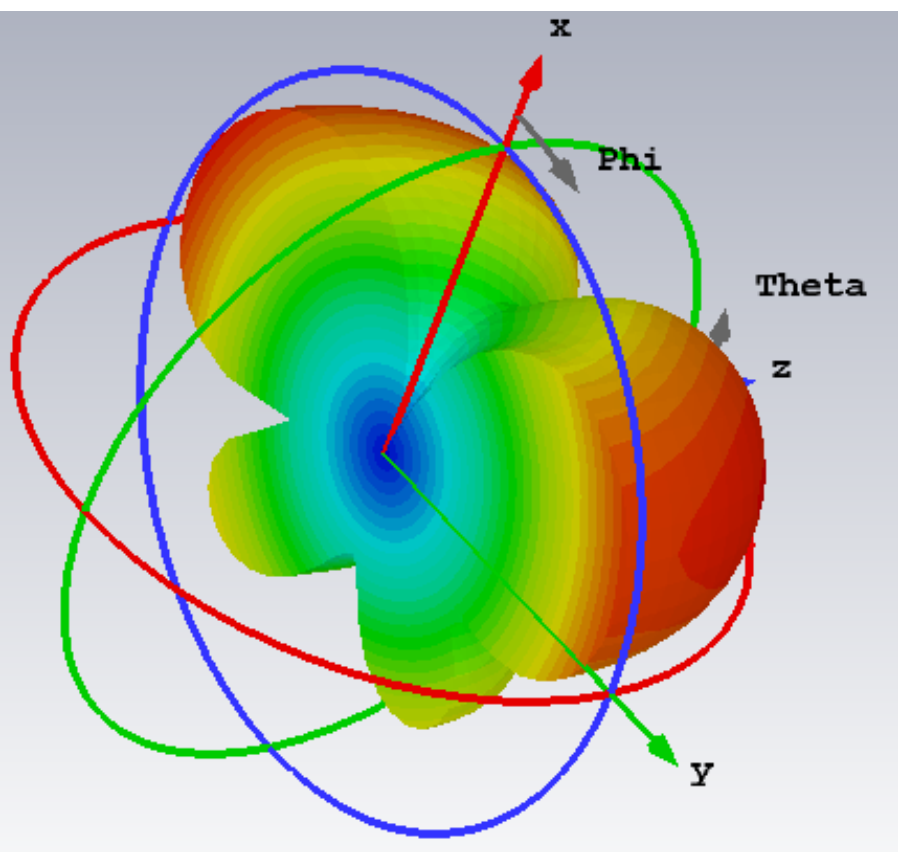
# Topic2 - Part II. Data(Probe Feed)



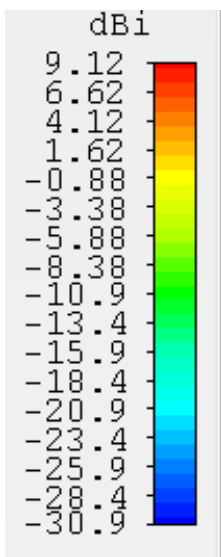
**Ang3.** S-parameters

# Topic2 - Part II. Data(Probe Feed)

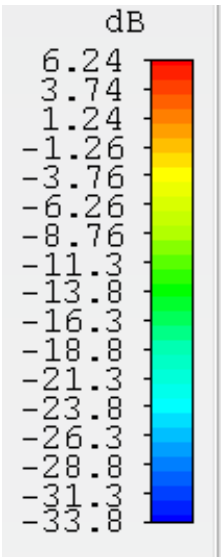
Ang4. Radiation pattern(3D farfield)



Directivity



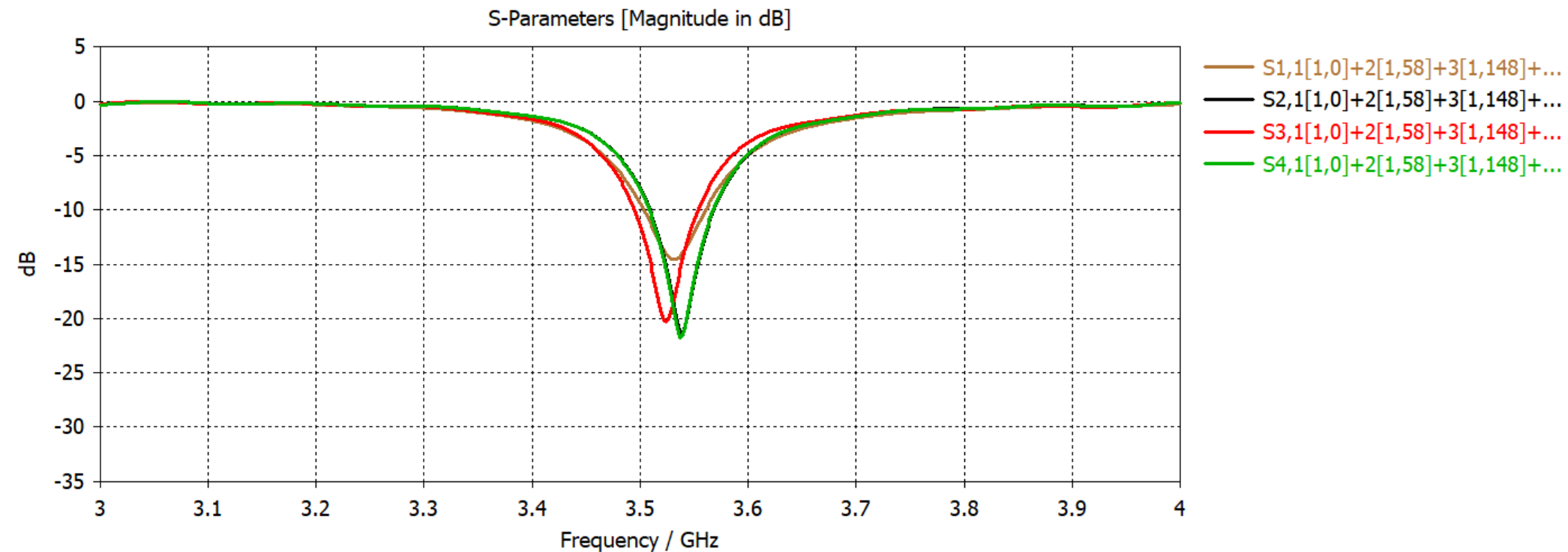
Gain



Radiation efficiency:-2.882 dB  
Total efficiency:-3.090 dB

farfield (f=3.55) [1...]+3[1,148]				farfield (f=3.55) [1...]+3[1,148]+4[1,246]]			
Type	Farfield	Type	Farfield	Type	Farfield	Type	Farfield
Approximation	enabled (kR >> 1)	Approximation	enabled (kR >> 1)	Approximation	enabled (kR >> 1)	Approximation	enabled (kR >> 1)
Component	Abs	Component	Abs	Component	Abs	Component	Abs
Output	Directivity	Output	Gain	Output	Gain	Output	Gain
Frequency	3.55 GHz	Frequency	3.55 GHz	Frequency	3.55 GHz	Frequency	3.55 GHz
Rad. effic.	-2.882 dB	Rad. effic.	-2.882 dB	Rad. effic.	-2.882 dB	Rad. effic.	-2.882 dB
Tot. effic.	-3.090 dB	Tot. effic.	-3.090 dB	Tot. effic.	-3.090 dB	Tot. effic.	-3.090 dB
Dir.	9.120 dBi	Gain	6.238 dB				

# Topic2 - Part II. Data(Probe Feed)

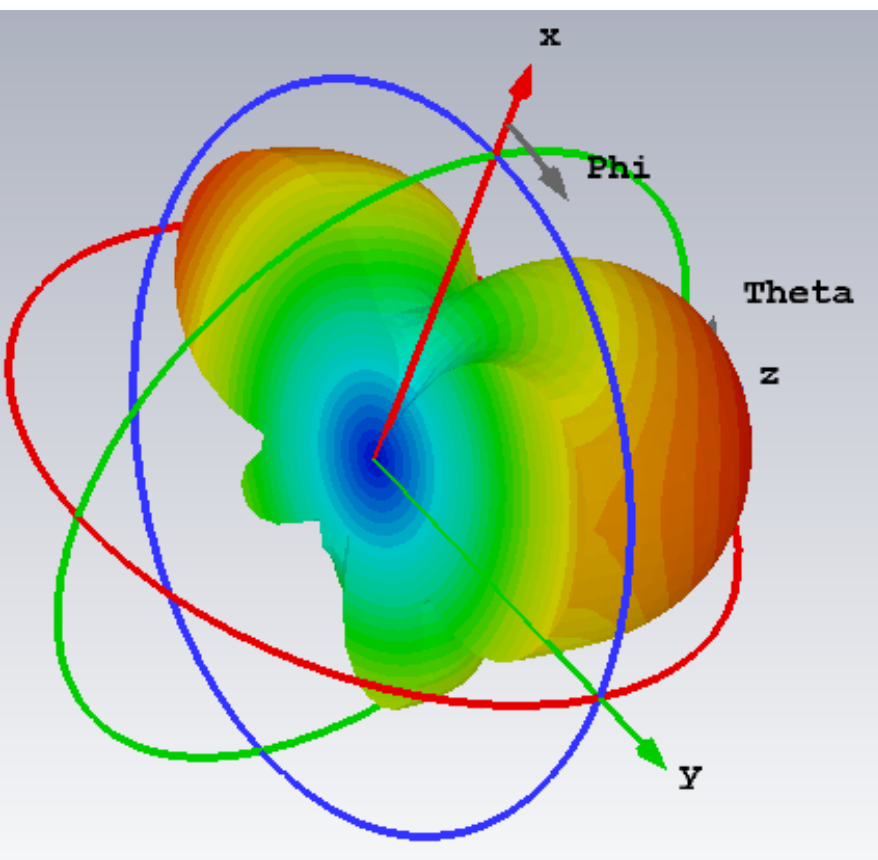


**Ang4.** S-parameters



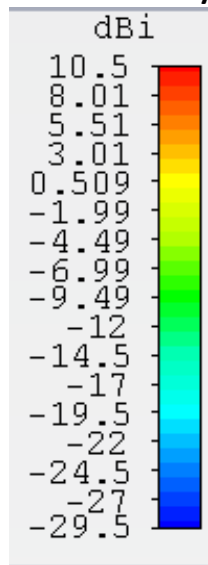
# Topic2 - Part II. Data(Probe Feed)

Ang5. Radiation pattern(3D farfield)

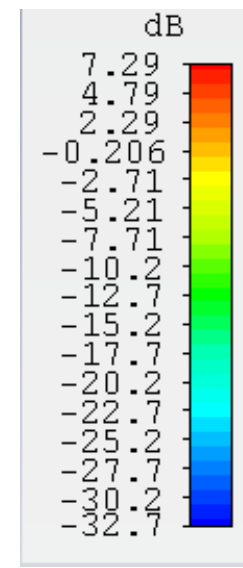


Radiation efficiency:-3.215 dB  
Total efficiency:-3.350 dB

Directivity



Gain

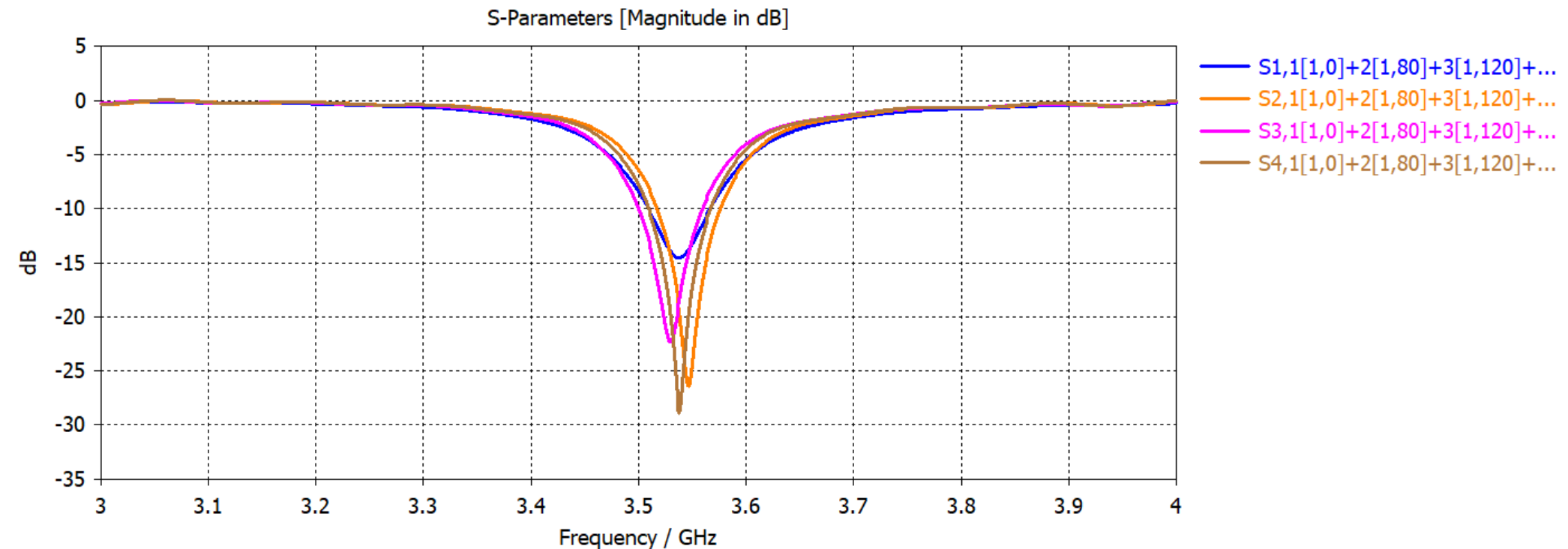


farfield (f=3.55) [1...]+3[1,120]+ farfield (f=3.55) [1...]+3[1,120]+4[1,160]]

Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Directivity
Frequency	3.55 GHz
Rad. effic.	-3.215 dB
Tot. effic.	-3.350 dB
Dir.	10.51 dBi

Type	Farfield
Approximation	enabled (kR >> 1)
Component	Abs
Output	Gain
Frequency	3.55 GHz
Rad. effic.	-3.215 dB
Tot. effic.	-3.350 dB
Gain	7.294 dB

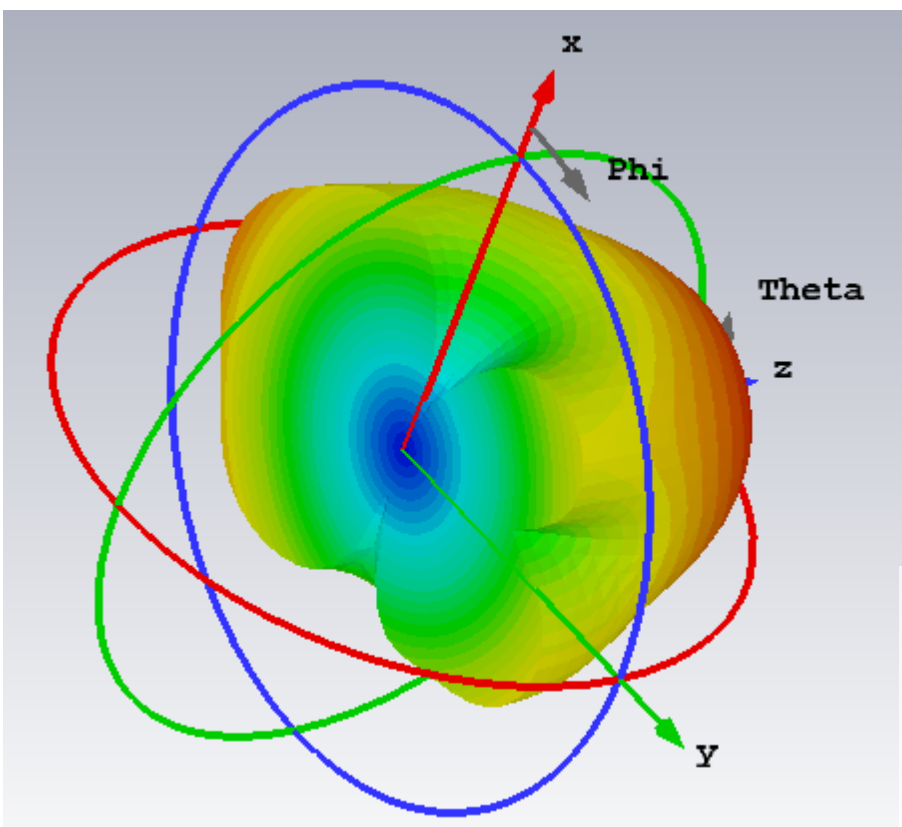
# Topic2 - Part II. Data(Probe Feed)



**Ang5.** S-parameters

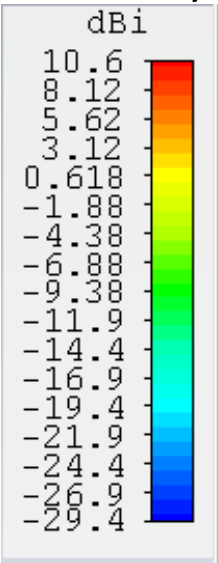
# Topic2 - Part II. Data(Probe Feed)

Ang6. Radiation pattern(3D farfield)

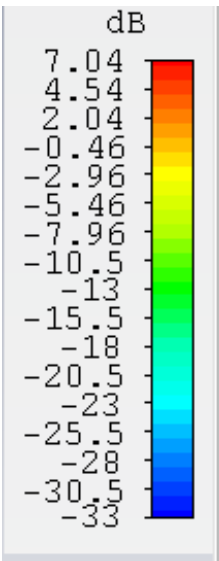


Radiation efficiency:-3.578 dB  
Total efficiency:-3.675 dB

Directivity

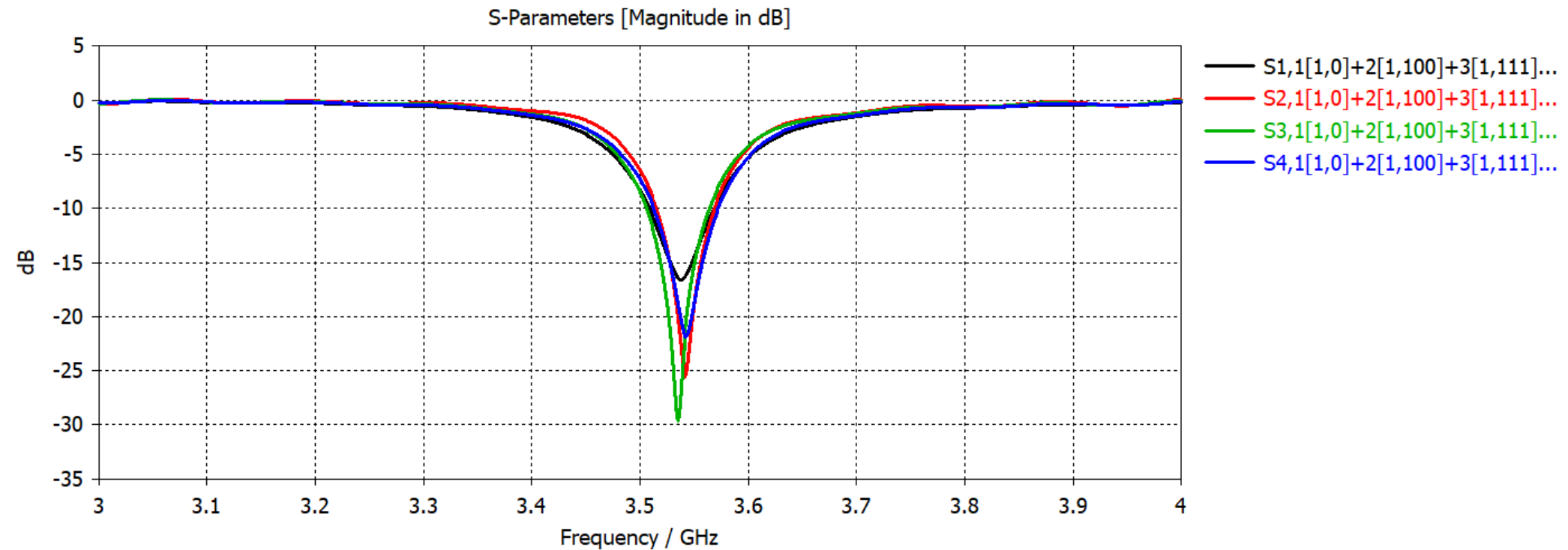


Gain



farfield (f=3.55) [1...0]+3[1,111]				farfield (f=3.55) [1...0]+3[1,111]+4[1,86]]			
Type	Farfield			Type	Farfield		
Approximation	enabled (kR >> 1)			Approximation	enabled (kR >> 1)		
Component	Abs			Component	Abs		
Output	Directivity			Output	Gain		
Frequency	3.55 GHz			Frequency	3.55 GHz		
Rad. effic.	-3.578 dB			Rad. effic.	-3.578 dB		
Tot. effic.	-3.675 dB			Tot. effic.	-3.675 dB		
Dir.	10.62 dBi			Gain	7.040 dB		

# Topic2 - Part II. Data(Probe Feed)



**Ang6.** S-parameters

# **Topic5 - Part I. Objective**

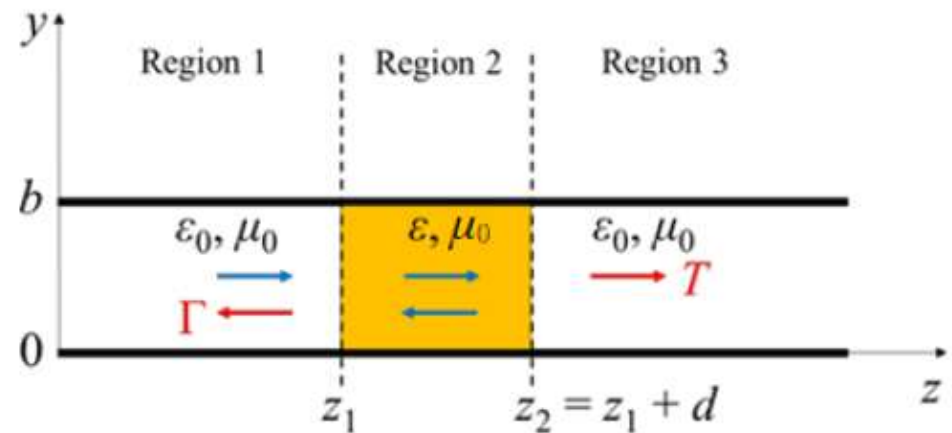
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- Use rectangular waveguide to measure dielectric property
- Gain knowledge of using VNA

# Topic5 - Part II. Data

- Parameters

- $f = 3.95 \sim 5.85 \text{GHz}$
- WR – 187
- $L * W = 47 * 22 \text{mm}$
- $H = 19.6 \text{mm} / 15.6 \text{mm}$



# Topic5 - Part II. Data

Let the incident wave  $E=1$  and  $z_1$  is the origin point.  
We have

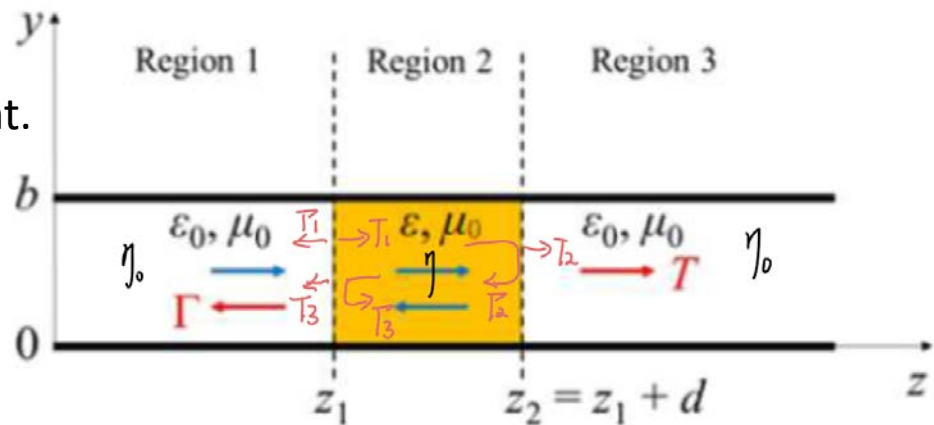
$$\Gamma = \frac{\eta_1 - \eta_2}{\eta_1 + \eta_2} e^{j\gamma z} \quad T = \frac{2\eta_2}{\eta_1 + \eta_2}$$

Then,

$$\Gamma_1 = \frac{\eta - \eta_0}{\eta + \eta_0} = \frac{\frac{1}{\sqrt{\epsilon}} - 1}{\frac{1}{\sqrt{\epsilon}} + 1} = \frac{1 - \sqrt{\epsilon}}{1 + \sqrt{\epsilon}}$$

$$\Gamma_2 = \frac{\eta_0 - \eta}{\eta + \eta_0} e^{j\gamma d} = -\Gamma_1 e^{j\gamma d} = \Gamma_4 = \Gamma_6 = \dots$$

$$\Gamma_3 = \frac{\eta_0 - \eta}{\eta + \eta_0} = -\Gamma_1 = \Gamma_5 = \Gamma_7 = \dots$$



$$T_1 = \frac{2\eta}{\eta + \eta_0} = \frac{\frac{2}{\sqrt{\epsilon}}}{\frac{1}{\sqrt{\epsilon}} + 1} = \frac{2}{1 + \sqrt{\epsilon}}$$

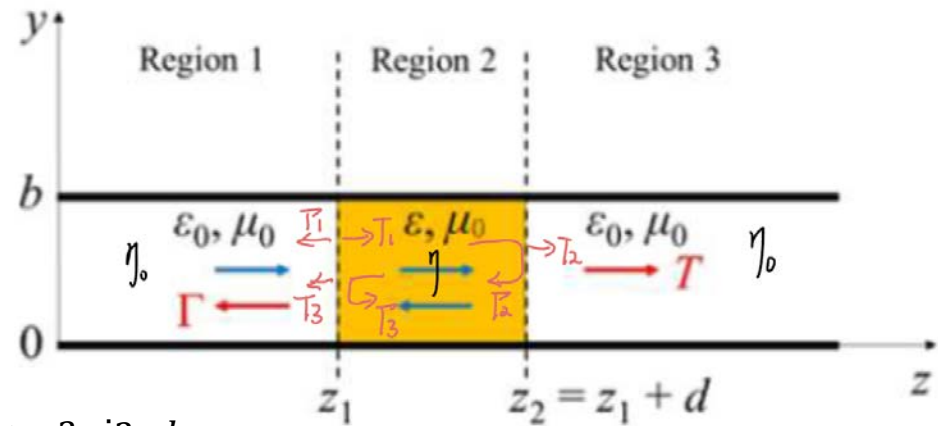
$$\Gamma_2 = \frac{2\eta_0}{\eta + \eta_0} e^{j\gamma d} = (2 - T_1) e^{j\gamma d} = T_4 = T_6 = \dots$$

$$T_3 = \frac{2\eta_0}{\eta + \eta_0} = (2 - T_1) = T_5 = T_7 = \dots$$

# Topic5 - Part II. Data

At  $z=z_1$ , we can get

$$\begin{aligned}
 S_{11} = \Gamma &= \Gamma_1 + T_1 \Gamma_2 T_3 + T_1 \Gamma_2 \Gamma_3 \Gamma_4 T_5 \\
 &\quad + T_1 \Gamma_2 \Gamma_3 \Gamma_4 \Gamma_5 \Gamma_6 T_7 + \dots \dots \\
 &= \Gamma_1 - T_1(2 - T_1)\Gamma_1 e^{j\gamma d} - T_1(2 - T_1)\Gamma_1^3 e^{j2\gamma d} \\
 &\quad - T_1(2 - T_1)\Gamma_1^5 e^{j3\gamma d} + \dots \dots \\
 &= \Gamma_1 - T_1(2 - T_1)(\Gamma_1 e^{j\gamma d} + \Gamma_1^3 e^{j2\gamma d} + \Gamma_1^5 e^{j3\gamma d} \\
 &\quad + \Gamma_1^7 e^{j4\gamma d} \dots \dots) \\
 &= \Gamma_1 - \frac{T_1(2 - T_1)\Gamma_1 e^{j\gamma d}}{1 - \Gamma_1^2 e^{j\gamma d}}
 \end{aligned}$$



In the same way, we can get the expression of  $S_{22}$ ,  $S_{12}$ ,  $S_{21}$ .

Then substituting the measured value into the expression, we can get the  $\epsilon$



## Topic5 - Part II. Data

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$$S_{11} = R_1^2 \left[ \frac{\Gamma - (1 - T^2)}{1 - \Gamma^2 T^2} \right]$$

$$S_{22} = R_2^2 \left[ \frac{\Gamma - (1 - T^2)}{1 - \Gamma^2 T^2} \right]$$

$$S_{21} = R_1 R_2^2 \left[ \frac{T - (1 - \Gamma^2)}{1 - \Gamma^2 T^2} \right]$$

$$R_i = e^{-\gamma_0 L_i}$$

$$T = e^{-\gamma D}$$

$$\Gamma = \frac{\gamma_0/\mu_0 - \gamma/\mu}{\gamma_0/\mu_0 + \gamma/\mu}$$

## Topic5 - Part II. Data

$$S_1 = S_{11} + S_{21}$$

$$S_2 = S_{21} - S_{11}$$

$$X = \frac{1 - S_1 S_2}{S_1 - S_2}$$

$$\Gamma = X \pm \sqrt{X^2 - 1} \quad (|\Gamma| \leq 1)$$

$$T = \frac{(S_{11} + S_{21}) - \Gamma}{1 - (S_{11} + S_{21})\Gamma}$$

$$\mu_r^2 = \left( \frac{1 + \Gamma}{1 - \Gamma} \right)^2 \left( \frac{1}{\lambda_0^2} \mu_r \varepsilon_r - \frac{1}{\lambda c^2} \right) / \left( \frac{1}{\lambda_0^2} - \frac{1}{\lambda c^2} \right)$$

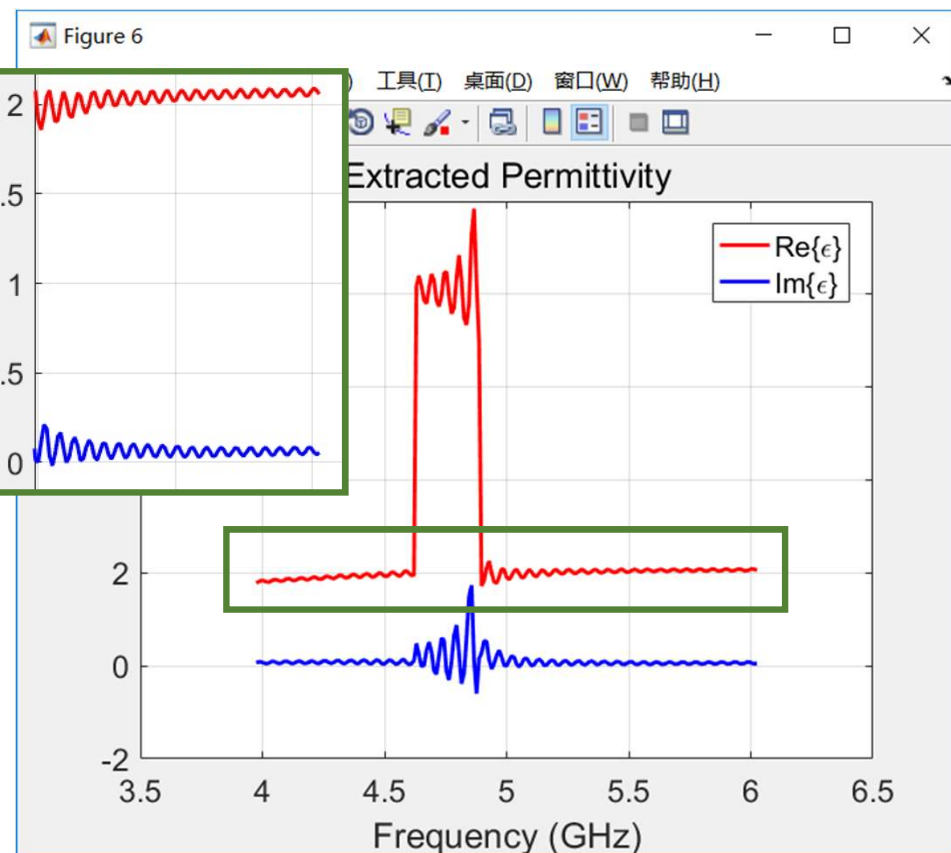
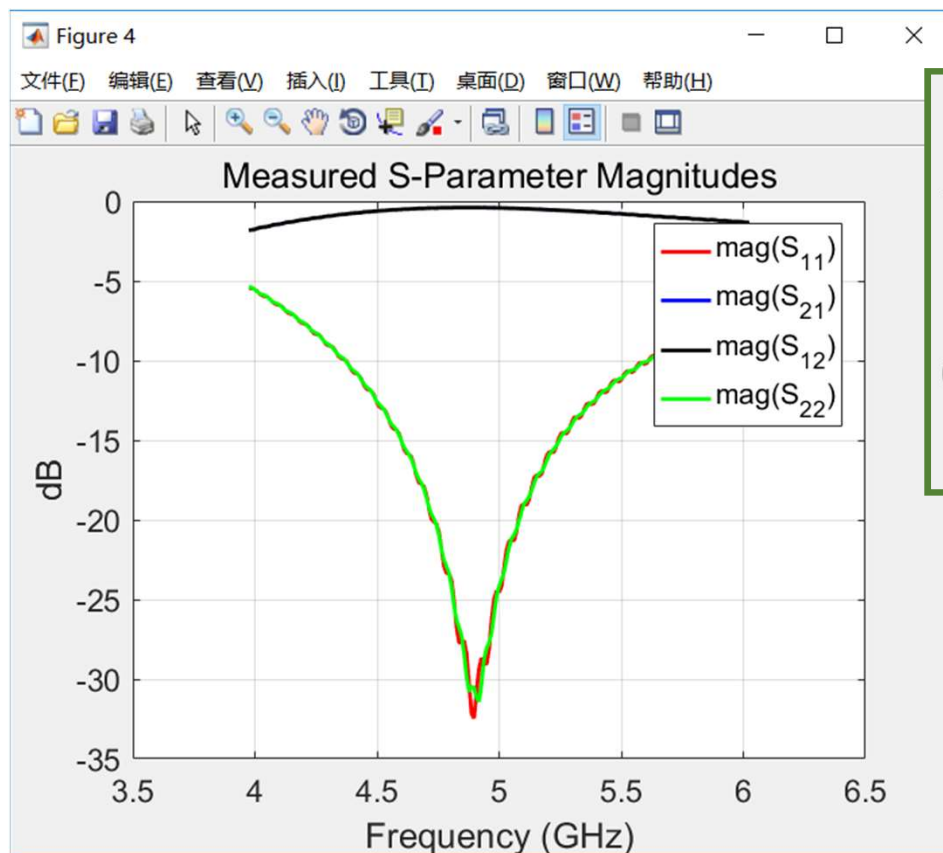
$$\frac{1}{\Lambda^2} = \frac{1}{\lambda_0^2} \mu_r \varepsilon_r - \frac{1}{\lambda c^2} = - \left\{ \frac{1}{2\pi D} \ln \left( \frac{1}{T} \right) \right\}^2$$

$$\mu_r = \left( \frac{1 + \Gamma}{1 - \Gamma} \right) \frac{1}{\Lambda} \frac{1}{\sqrt{\frac{1}{\lambda_0^2} - \frac{1}{\lambda c^2}}}$$

$$\varepsilon_r = \left( \frac{1}{\Lambda^2} + \frac{1}{\lambda c^2} \right) \lambda_0^2 / \mu_r$$

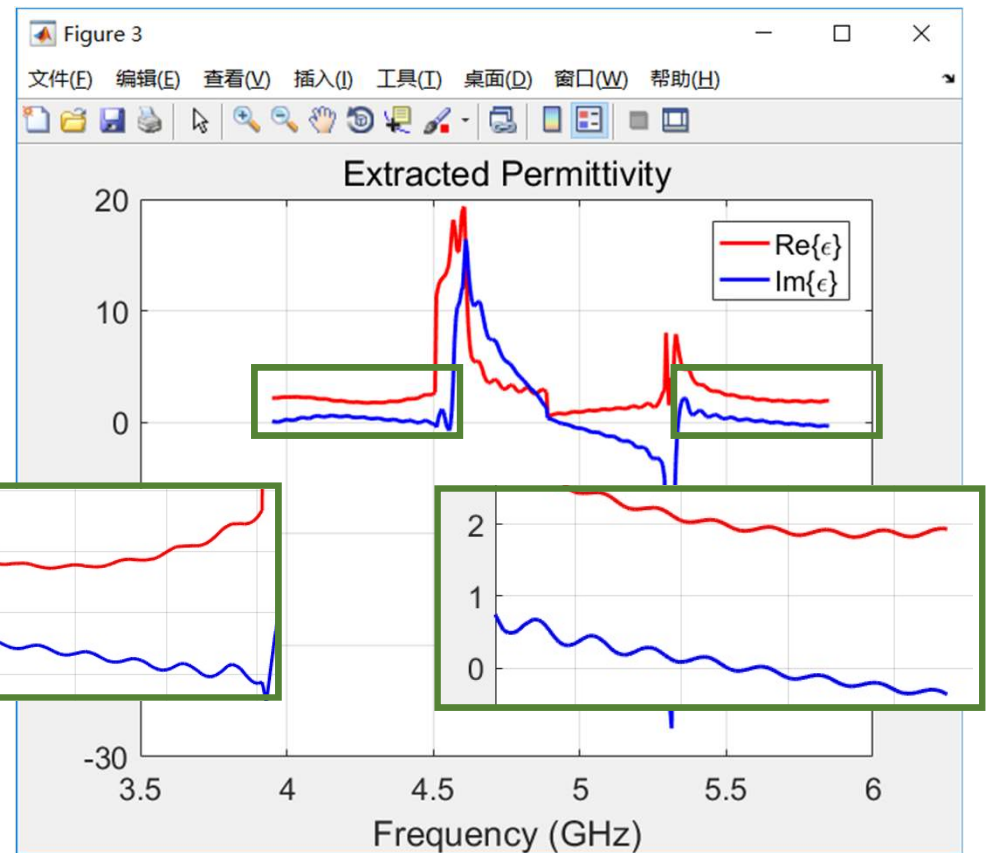
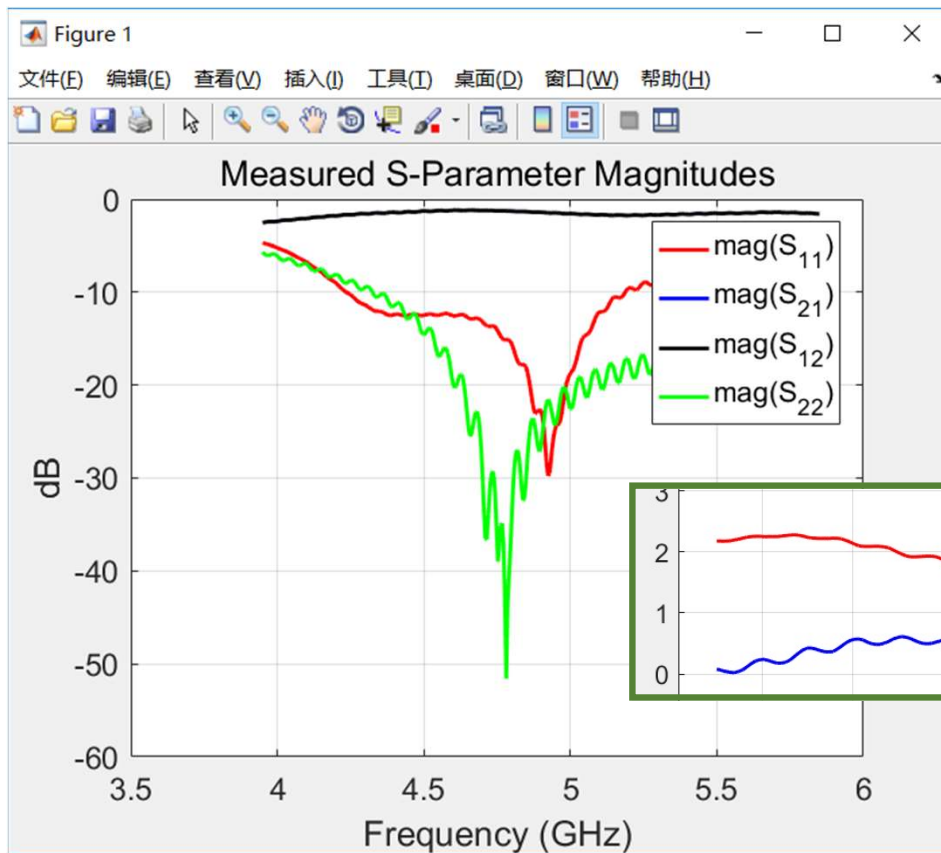
# Topic5 - Part II. Data

**Data A(All, H=19.6mm)** (We've tried many times, here we will show the best two of them.)



# Topic5 - Part II. Data

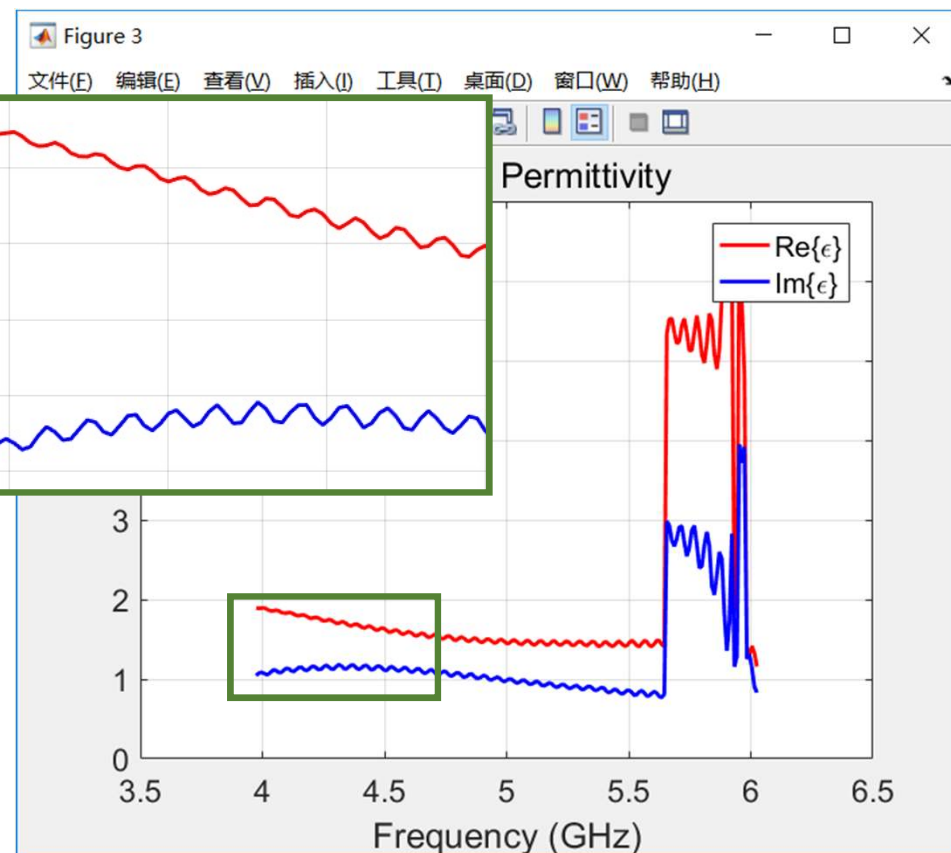
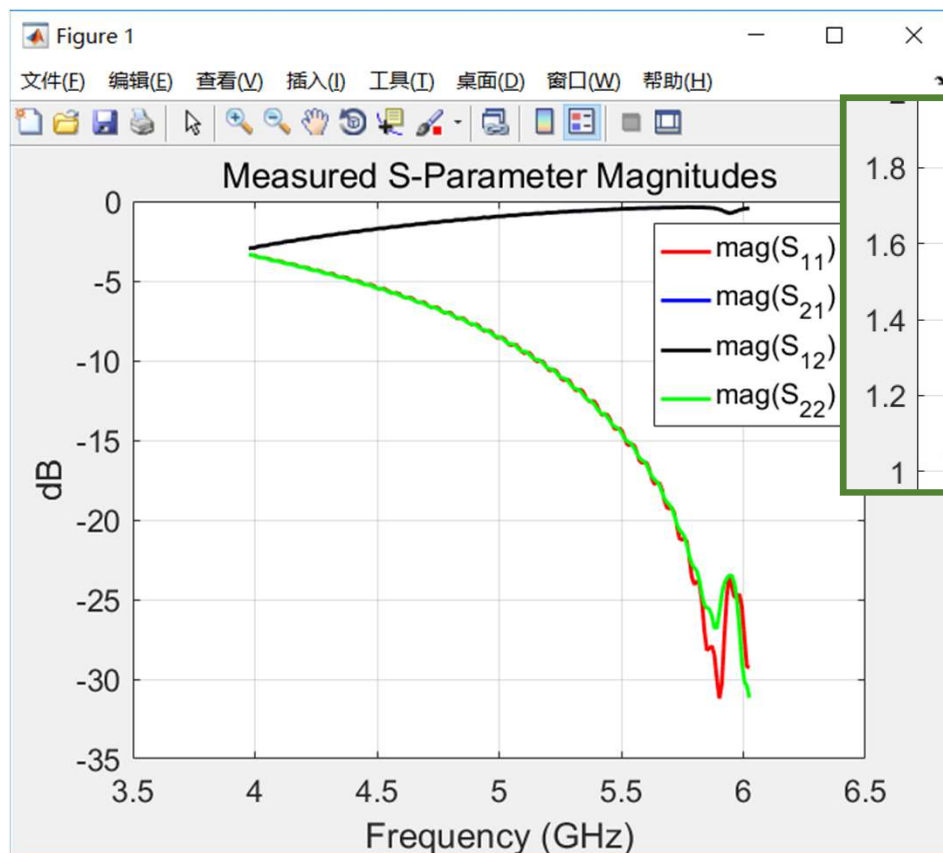
**Data B(All, H=19.6mm)** (We've tried many times, here we will show the best two of them.)



# Topic5 - Part II. Data

**Data A(Half, H=15.6mm)**

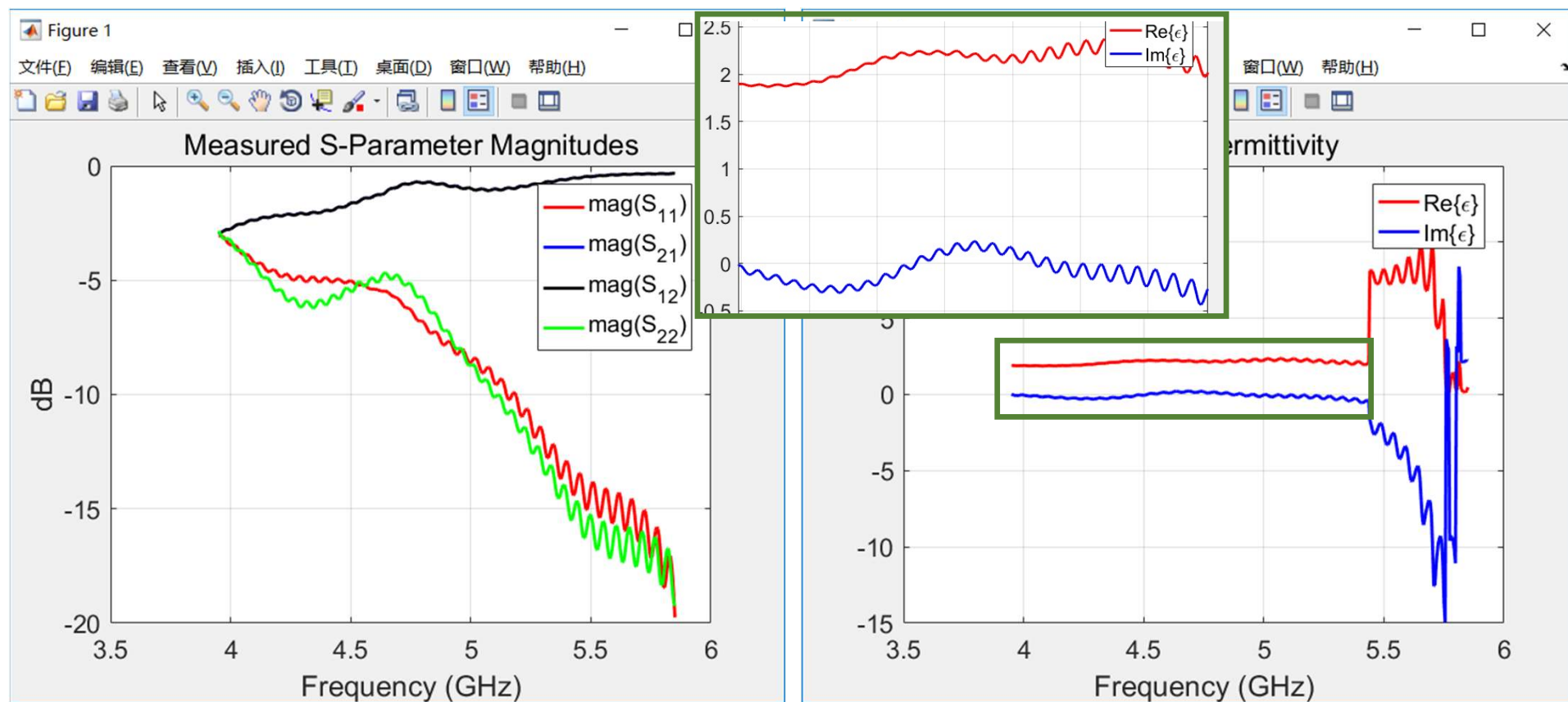
(We've tried many times, here we will show the best two of them.)



# Topic5 - Part II. Data

Data B(Half, H=15.6mm)

(We've tried many times, here we will show the best two of them.)



## Topic5 - Part II. Data

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According to above, the extracted permittivity is about 1.9~2.5.

The relevant codes, images and data can be viewed at

*<https://github.com/Mine4ever/Electromagnetics-Project.git>*