Macro hw 1 (temporary)

1. Questions from Romer

(1) Romer 5.8.

mer C.U.max $\sum \left(\frac{1}{1+p}\right)^{\frac{1}{2}} \cdot L(A-DCd^2)$ The Atherest rate A=P.

A 7s Therest rate A=P.

 $CA = \beta C_{A} + t E_{A}, - | < \beta < 1$

CA! 1-20CA = 7AKAH! $9A = E_{k} \cdot (1+A)$ 9A+1

=> 1-20Cx=[=(1-20Cx+1)

- CA = Ax C+1

(b) Guess CA = X+BKA+8C+

KAH = KA+FX- X-BKA-YCA

= KA+PKA+CA-X-BKA-YCA

= CHP-B)KA+CI-Y)CA-X,

-. KAH = (1-1/3) KA + (1-1/) PA - X

C() FOC Th (a): C+= E+(++1)

Plug Th the guess. X+BK++ rex = Ex [X+BK+11 + rex1] = Ex [X+ 3 (14 - B) FA + (1- x) ex - x] | + x (det + Etti)] = X-BX+BCHP-B)K++(BCHY)+rg)C+ Method of undetermined coefficients (1) $A = X - BX \Rightarrow X = X(1-B)$. unless B = 0, A = 0. (2) B=B(H-B) => 1= HP-B. 1. B=P $(3) \gamma = \beta(r) + \gamma \beta \Rightarrow \gamma = \rho(r) + \gamma \beta$ $\gamma(1+p-\phi)=\rho$ => > = [-- \psi] (d) Tt= PK++EA only the praction goes to here Ct = PK+ + Ttp-p Cx KtH = Kt + 1-\$ Cx the rest are Thrested.
STACE there's no of it
goes to Etti 100%.

(2) Romer 5.9.

(a)
$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty}$$

mborne them.

$$V=20CA-20VA=E_{A}(V-20CAH-20VAH)$$
 $Ct+VA=E_{A}Ct+H$

(Since $E_{A}VAH=0$)

Cb) Guess
$$Ct = \alpha + \beta kt + \gamma V_{A}$$
.

 $kt_{1} = kt + Akt - Ct$

$$= (1+k)k_{A} - \alpha - \beta kt - \gamma V_{A}$$

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$$= (1+k)k_{A} - \alpha - \beta kt - \beta k$$

$$\begin{array}{cccc}
A = A - \beta A \Rightarrow X = 0 \\
B = \beta (HA - \beta) \Rightarrow \beta = A = \beta \\
(HY) = -\beta Y \Rightarrow | HY + \beta Y = 0. Y = \frac{-1}{|H|}$$

Cd) plugging in the solutions...

Ct = PKt - Itp NA

KtH = Kt+ Itp NA

Because positive NA

Austrasto for consume

Because pertue ut means distaste for consumer. But why to? consumption smoothing

(3) Romer 5.11.
(a) Lifetime maximized value
= maximized value of this period
= maximized value of this period + discounted maximized value from the next period.
Cb) $V(Kt,At) = MUX[In(A+bIn(I-J+) Ca,Jx] +e-P$ Bo+BkIn(Yx-Cx)+BAPAIn At FOC for Cx. S.t. Yx = Kx (AxLx) I-X$
to for the ker (Aula) lax
TOC TEACH.
$Ct = e^{-\rho}$, β_k . T_{t} - Ct .
$Ct/T_{t} = e^{\rho} \cdot \frac{1}{\beta \kappa} \cdot (T_{t} - C_{t}) / T_{t}$
= ep. J. Ch CA)
3r Cl 1x
$= \frac{C_{\Lambda}}{V_{\Lambda}} \left(1 + eP \cdot \frac{1}{\beta \kappa} \right) = eP \cdot \frac{1}{\beta \kappa} = \frac{eP}{V_{\Lambda}} : Constant$
Co Com to and but with to make the
So consumption - output ratio is constant, which is less than 1.
(C) $\frac{b}{1-lt} = \beta k \cdot \frac{(HA)K_{A}(A_{A}l_{A})^{-A}A_{A}}{(K_{A}(A_{A}l_{A})^{1-A}-C_{A}}$
$= \beta_{K}, \frac{(\Gamma \alpha) \cdot l_{\pi}, \Upsilon_{x}}{\Upsilon_{x} - C_{x}}$
$f_{\star}-c_{\star}$
= BK. (1-0) lx (- Ct/Tx
1 (- CX/TX

Hence It does not depend on At or 15t.

(d) Re- wite the Bellman equation.

V(Kt,At) = max[In(A+bln(I-l+) Cx,lx +e-13 Bo+BkIn(K&(AxLx)-Cx)+BAPAIn At]

Results from (b)
$$\Delta$$
 (c) are

$$\frac{e^{\theta}}{h} = \frac{e^{\theta}}{1+\frac{e^{\theta}}{\beta k}} = \frac{e^{\theta}}{\beta k+e^{\theta}} \Rightarrow Ct = \left(\frac{e^{\theta}}{\beta k+e^{\theta}}\right)^{\frac{1}{1}}t$$
(b) $\frac{b}{h} = \frac{c}{\beta k} = \frac{c}{h} =$

$$\Rightarrow lA = \frac{(1-\alpha)}{(1+\alpha) + \frac{b}{pp}}$$

Now we can substitute them for the optimal

This is hideous

2. P/H and excess - smoothing 2-1.

$$\mathcal{L} = \max_{t=0}^{\infty} \sum_{t=0}^{\infty} \beta^{t} U((A) + \chi(A_{0} - \sum_{t=0}^{\infty} \beta^{t} ((A - \chi_{t})))$$

Now let's get the Impulse hespense.

Mo shock of all

(a)

$$f = M \cdot t + \phi T \cdot t - 1$$
 $f = M \cdot (t + 1) + \phi T \cdot t$
 $= M(t + 1) + \phi (Mt + \phi T \cdot t - 1)$
 $= M[t + 1 + \phi t] + \phi^2 T \cdot t - 1$

$$\Delta Tttl = \beta \Delta Tt$$

$$Tttl - Tt = \beta (Tt - Tt - 1)$$

$$Tt = M \cdot t + \phi Tt - 1 + \varepsilon t$$

$$Tt = M \cdot (t + 1) + \phi Tt$$

$$= M(t + 1) + \phi (Mt + \phi + 1 + \varepsilon t)$$

$$= M[t + \phi t] + \phi^{2} Tt - 1 + \phi \varepsilon t$$

$$\Rightarrow \frac{\partial Tt + s}{\partial \varepsilon t} = \phi^{S} \cdot \varepsilon t$$

TtH - Tt=
$$\beta$$
(Tt-Tt-1)

=) Tt+= $(I+\phi)$ Tt- β Tt-1

= $(I+\phi)$ ($(I+\phi)$) Tt- $I-\beta$ Tt-2

+ Et)

 $\Rightarrow \frac{\partial Ttts}{\partial Et} = CH\phi$) Et

shock 25 explosive,

Now revisit the FOC and the budget anstment.

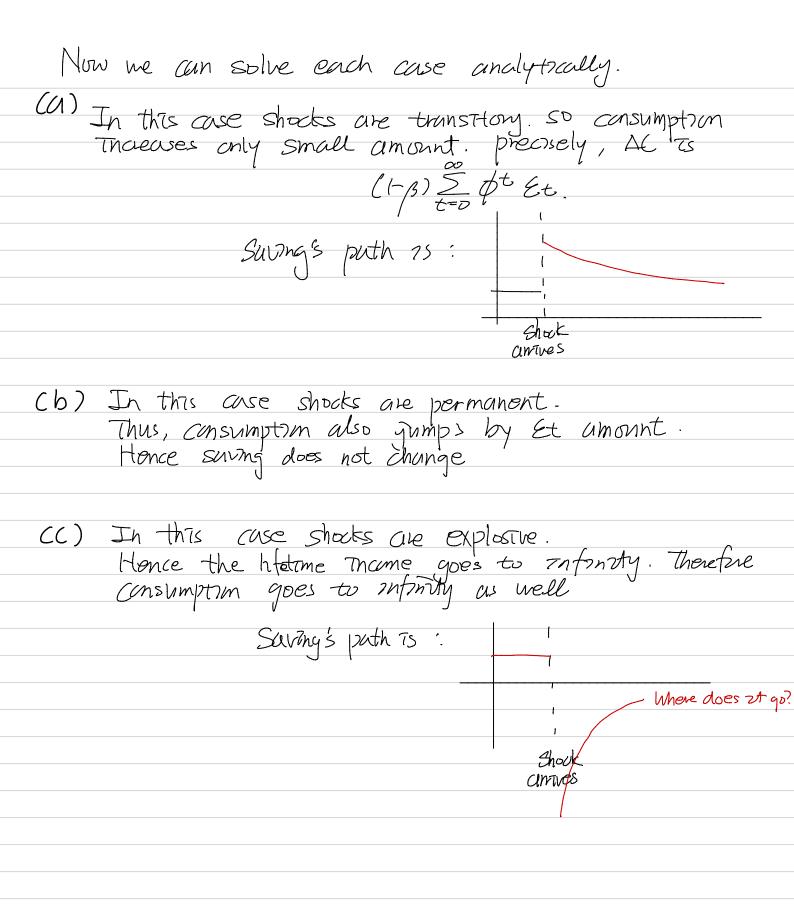
FOC: U((4)=) = C=(2= ··· = C* Budget constraint: Ao=Et & B+CC+-Tx)

=> Ex 2 pt Cx = A0 + Ex 2 pt Tx

Quadratic utility implies that consumption follows

= Aot Eo Sota

Thus, consumption is a fruction of lettime traceme $C = (1-\beta) \cdot Ao + (1-\beta) Eo = \beta + \gamma + \gamma$



2-2.

Result from ear imples that as long as shocks are transitiony, consumption is always smoother than trame.

tax cut should be meffective - but not 2 Bomoning constraint
2 Substitute level of consumption

2-3.

Tes. If Thame follows a nindern nath, (b) Triphes that consumption is no longer smoother than Thame.

3.
$$\int_{-\infty}^{\infty} R_{A}^{S} (L-T) F(K_{A}, L_{A}) - W_{A} L_{A} - J_{A} (H \alpha(E_{A}^{T} - S))$$
 $+ g_{A} ((1-S) k_{A} + J_{A} 1 - k_{A} 4)^{3}$

Ohoose K_{A}, L_{A}, J_{A}
 $\frac{2L}{2l_{A}}$: $W_{A} = (L-Z) C_{C} C_{C} (K_{A})^{\alpha}$

$$\frac{\partial L}{\partial IA}$$
: $g_{\star} = [+ \alpha(\frac{I_{\star}}{K_{\star}} - \delta) + \alpha \cdot \frac{I_{\star}}{K_{\star}}]$

Log Mnearzation.

(1)
$$W_{x} = \alpha K_{t} - \alpha L_{x}$$

(3)
$$g_t = \frac{2u\delta}{1+u\delta} (J_t - K_t)$$

gt, It it are observable, assume that we have an

we can mn a regression

and interpret
$$\beta$$
 as $\frac{2a\delta}{+a\delta} \Rightarrow \beta + \beta a\delta = 2a\delta$

$$\Rightarrow \beta = \lambda(2\delta - \beta\delta) \Rightarrow \lambda = \frac{3}{2\delta - \beta\delta}$$

emor term moludes unexplained parts of gar Value of firm might not be explained solely by must most and capital stock they have. It gat is aggregate variable. Wat und be its interpretation

(2) Log-tinearized Enler eghatim:
Log- (inearized biler eghatim.

4. Practice log-traeatzatzon

(:- NX = 0 2n Steady state)

$$\gamma = \chi \vec{P}$$
 7n s,s, $\gamma = \chi \vec{P}$

Now let's get X

3. In steady state
$$k = (1-\delta)k + I - \beta(\frac{T}{k} - \delta)^{2}I$$

If we assume that I= SK Th steady state, then 169-17 nearzation for this 75

If we assume that $I \neq 0$ K, then $y(\bar{k} - \delta)^2 I \neq 0$

$$Kt = \frac{(H\sigma)K}{K} \cdot Kt + \frac{I}{K} It - \frac{I}{K} \psi (\frac{I}{K} - \sigma)^2 (\psi (\frac{It}{Kt + 1} - \sigma)^2 It)$$

Mere

$$\psi(\frac{It}{kt-1}-\delta)^2It = 2(\frac{It}{kt-1}-\delta) + It$$

$$-\frac{1}{2} \cdot \left(\frac{1}{k} - \frac{1}{k} \cdot \frac{1}{k} - \frac{1}{k} \cdot \left(\frac{1}{k} - \frac{1}{k} \cdot \left(\frac{1}{k} - \frac{1}{k} \cdot \frac{1}{k} - \frac{1}{k} \cdot \frac{1}{k} - \frac{1}{k} \cdot \left(\frac{1}{k} - \frac{1}{k} \cdot \frac{1}{k} \frac{1}{k} \cdot \frac{1}{k} \cdot \frac{1}{k} \cdot \frac{1}{k} \cdot \frac{1}{k} - \frac{1}{k} \cdot \frac{1}{k}$$

In Steady state,
$$\phi(\frac{J\xi}{Jt-1})^2Jt=0$$
.
Hence the answer is same as #3

5. Take log.

At = Pallog Pt - logPt-1) + Py (logy+ - logy+ -1) + PAt-1

The Steady state, A = PA = A = 0

At is already a small number, with Steady state

Value zero. So it is alway to just state in = in

Then next steps are straight femand.

Pallog Pt - logPt-1) - Pallog P- logP)

= Pallog Pt-logPt-1 - Pallog Pt-logP)

- At = Pallog Pt + Py Yt + PAt-1

6. A. F(L) =
$$\frac{U_L(C, I-L)}{U_C(C, I-L)}$$

In steady state, $\overline{A} \cdot F(\overline{C}) = \frac{U_L(\overline{C}, I-\overline{L})}{U_C(\overline{C}, I-\overline{L})}$
Take log.
 $logA + log F(L) = log U_L(C,I-L) - log U_C(C,I-L)$
 $Taylor approximatron$
 $logA \approx log \overline{A} + \frac{1}{A} (A-\overline{A})$

$$logA \approx logA + \frac{1}{A}(A-\overline{A})$$

$$logF(L) = logF(\overline{L}) + \frac{F'(\overline{L})}{F(\overline{L})}(L-\overline{L})$$

$$logULCC(1-L)$$

$$= \log \text{McCC}, I-L) + \frac{\text{McL}}{\text{Mc}} (C-C) - \frac{\text{Mac}}{\text{Mc}} CL-L)$$

$$\Rightarrow A + \frac{L \cdot F(CL)}{F(CL)} = U_{LC} \cdot C \cdot C \left(\frac{1}{UL} - \frac{1}{UC} \right) - U_{LC} \cdot L \cdot C \left(\frac{1}{UL} - \frac{1}{UC} \right)$$

7. First take log

log Tx = axlog Kx + (1-ax) log Lx.

Then do 1st order Taylor approximation

around Steady state.

 $\frac{f_{A}-f_{-}}{f}=(\log K-\log L)(XX-X)+\frac{X}{K}(KX-K)+\frac{(DA)}{L}(LX-L)$ $\therefore f_{A}=XK+C(DA)LX+A(\log L)X+$