













# A Brief Review of Mono-dimensional Heat Transfer: Conduction and Convection

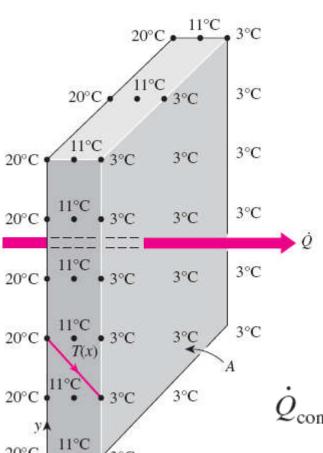
Ref: Y. A. Cengel, Heat Transfer, a practical approach

Energy and Environmental Technologies for Building Systems Piacenza Campus, 1st Semester 2018-2019



## Steady State heat conduction in Plane wall

- Heat transfer through the wall of a house can be modeled as *steady* and *one-dimensional*.
- The temperature of the wall in this case depends on one direction only (say the x-direction) and can be expressed as T(x).



$$\begin{pmatrix}
Rate \text{ of } \\
heat \text{ transfer } \\
\text{into the wall}
\end{pmatrix} - \begin{pmatrix}
Rate \text{ of } \\
heat \text{ transfer } \\
\text{out of the wall}
\end{pmatrix} = \begin{pmatrix}
Rate \text{ of change} \\
\text{of the energy} \\
\text{of the wall}
\end{pmatrix}$$

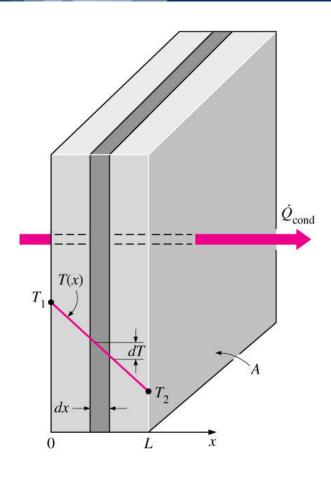
$$\dot{Q}_{\rm in} - \dot{Q}_{\rm out} = \frac{dE_{\rm wall}}{dt}$$
 for steady operation 
$$dE_{\rm wall}/dt = 0$$

✓ In steady operation, the rate of heat transfer through the wall is constant.

$$\dot{Q}_{\text{cond, wall}} = -kA \frac{dT}{dx}$$



#### Steady State heat conduction in Plane wall



✓ Under steady conditions, the temperature distribution in a plane wall is a straight line: dT/dx = const.

$$\dot{Q}_{\text{cond, wall}} = -kA \frac{dT}{dx}$$

$$\int_{x=0}^{L} \dot{Q}_{\text{cond, wall}} dx = -\int_{T=T_1}^{T_2} kA dT$$

$$\dot{Q}_{\text{cond, wall}} = kA \frac{T_1 - T_2}{L}$$
 (W)

The rate of heat conduction through a plane wall:

- ✓ is proportional to the average thermal conductivity, the wall area, and the temperature difference
- ✓ but is inversely proportional to the wall thickness.
- Once the rate of heat conduction is available, the temperature T(x) at any location x can be determined by replacing  $T_2$  by  $T_2$ , and  $T_2$  by  $T_3$ .



## **Thermal Resistance Concept**

$$\dot{Q}_{\text{cond, wall}} = kA \frac{T_1 - T_2}{L}$$

$$\dot{Q}_{\text{cond, wall}} = \frac{T_1 - T_2}{R_{\text{wall}}} \qquad (W)$$

$$R_{\text{wall}} = \frac{L}{kA}$$
 (°C/W)

- ✓ Conduction resistance of the wall: Thermal resistance of the wall against heat conduction.
- ✓ Thermal resistance of a medium depends on the geometry and the thermal properties of the medium.

$$I = \frac{\mathbf{V}_1 - \mathbf{V}_2}{R_e} \qquad R_e = L/\sigma_e A$$

$$\mathbf{V}_1 \bullet \qquad \qquad \mathbf{V}_2$$

$$R_e$$

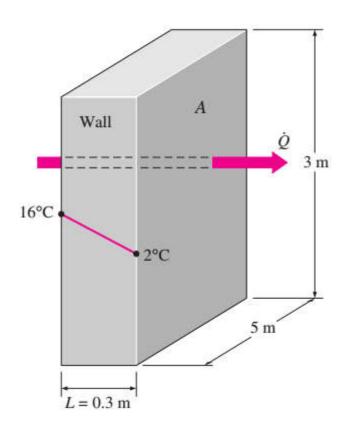
(b) Electric current flow

Analogy between thermal and electrical resistance concepts:

rate of heat transfer → electric current thermal resistance → electrical resistance temperature difference → voltage difference



## **Example A: Steady State heat conduction**



Find the rate of heat loss through the wall

✓ K=0.9 W/m C



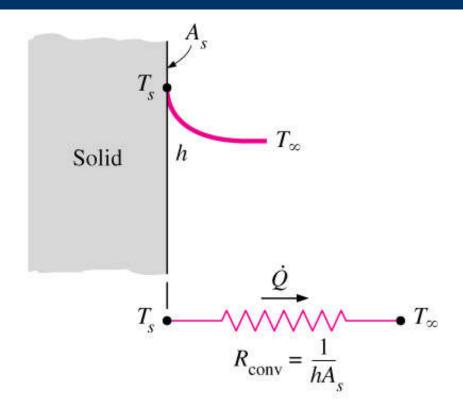
### **Convection: Newton's law of cooling**

$$\dot{Q}_{\rm conv} = hA_s(T_s - T_{\infty})$$

$$\dot{Q}_{\rm conv} = \frac{T_s - T_{\infty}}{R_{\rm conv}} \tag{W}$$

$$R_{\text{conv}} = \frac{1}{hA_s}$$
 (°C/W)

Convection resistance of the surface: Thermal resistance of the surface against heat convection.



- ✓ When the convection heat transfer coefficient is very large  $(h \to \infty)$ , the convection resistance becomes zero and  $T_s \approx T$ .
- ✓ That is, the surface offers *no resistance to convection*, and thus it does not slow down the heat transfer process.
- ✓ This situation is approached in practice at surfaces where boiling and condensation occur.



### **Thermal Resistance Network**

$$\begin{array}{c} \left( \begin{array}{c} \text{Rate of } \\ \text{heat convection} \\ \text{into the wall} \end{array} \right) = \left( \begin{array}{c} \text{Rate of } \\ \text{heat convection} \\ \text{from the wall} \end{array} \right) = \left( \begin{array}{c} \text{Rate of } \\ \text{heat convection} \\ \text{from the wall} \end{array} \right) \\ \\ \dot{Q} = \frac{T_{\infty 1} - T_1}{1/h_1 A} = \frac{T_1 - T_2}{L/kA} = \frac{T_2 - T_{\infty 2}}{1/h_2 A} \\ \\ = \frac{T_{\infty 1} - T_1}{R_{\text{conv}, 1}} = \frac{T_1 - T_2}{R_{\text{wall}}} = \frac{T_2 - T_{\infty 2}}{R_{\text{conv}, 2}} \\ \\ \dot{Q} = \frac{T_{\infty 1} - T_{\infty 2}}{R_{\text{conv}, 1} + R_{\text{wall}} + R_{\text{conv}, 2}} \\ \\ & = \frac{T_{\infty 1} - T_{\infty 2}}{R_{\text{conv}, 1} + R_{\text{wall}} + R_{\text{conv}, 2}} \\ \\ & = \frac{V_1 - V_2}{R_{e, 1} + R_{e, 2} + R_{e, 3}} \\ \\ & = \frac{V_1 - V_2}{R_{e, 1} + R_{e, 2} + R_{e, 3}} \\ \end{array} \quad V_1 \stackrel{\dot{L}}{\longrightarrow} \begin{array}{c} R_{e, 1} \\ R_{e, 1} \\ R_{e, 1} \\ R_{e, 2} \\ \end{array} \quad \begin{array}{c} R_{e, 3} \\ R_{e, 3} \\ \\ \end{array} \quad \begin{array}{c} R_$$

The thermal resistance network for heat transfer through a plane wall subjected to convection on both sides, and the electrical analogy.

$$R_{\text{total}} = R_{\text{conv, 1}} + R_{\text{wall}} + R_{\text{conv, 2}} = \frac{1}{h_1 A} + \frac{L}{kA} + \frac{1}{h_2 A}$$
 (°C/W)



#### **Temperature Drop**

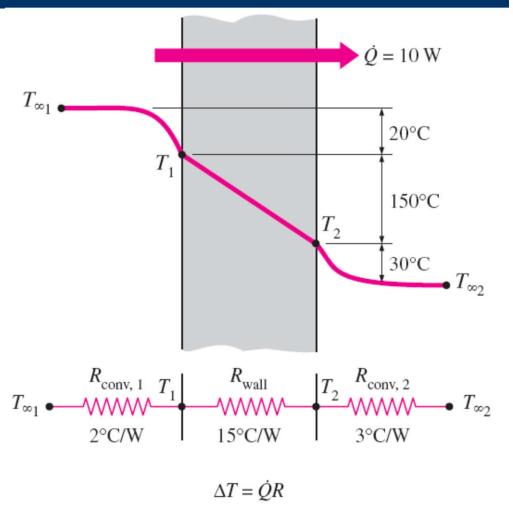
$$\Delta T = \dot{O}R$$
 (°C)  
 $\dot{Q} = UA \Delta T$  (W)

$$UA = \frac{1}{R_{\text{total}}}$$
 (°C/K)

*U:* overall heat transfer coefficient

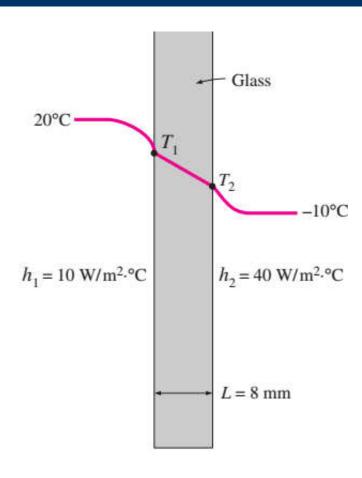
Once Q is evaluated, the surface temperature  $T_1$  can be determined from

$$\dot{Q} = \frac{T_{\infty 1} - T_1}{R_{\text{conv}, 1}} = \frac{T_{\infty 1} - T_1}{1/h_1 A}$$





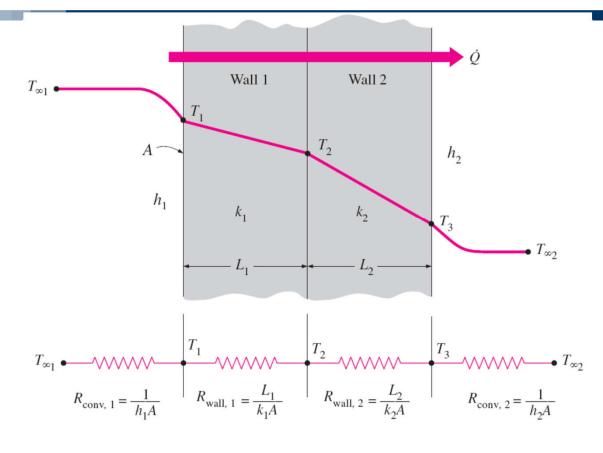
#### **Example B: Heat loss through a single pane window**



❖Consider a 0.8 m high and 1.5 m wide glass window, shown above with a thermal conductivity of k =0.78 W/m·°C. Determine the steady rate of heat transfer through this glass window and the temperature of its inner surface



## **Multi-layer Plane walls**



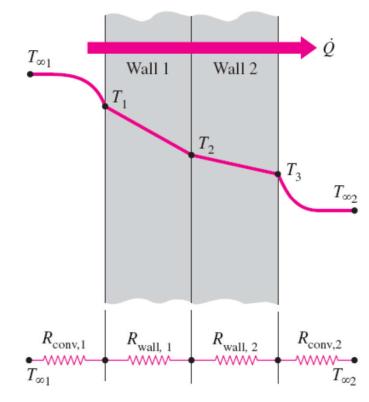
$$\dot{Q} = \frac{T_{\infty 1} - T_{\infty 2}}{R_{\text{total}}}$$

$$\begin{split} R_{\text{total}} &= R_{\text{conv, 1}} + R_{\text{wall, 1}} + R_{\text{wall, 2}} + R_{\text{conv, 2}} \\ &= \frac{1}{h_1 A} + \frac{L_1}{k_1 A} + \frac{L_2}{k_2 A} + \frac{1}{h_2 A} \end{split}$$



$$\dot{Q} = \frac{T_i - T_j}{R_{\text{total}, i-j}}$$

$$\dot{Q} = \frac{T_{\infty 1} - T_2}{R_{\text{conv}, 1} + R_{\text{wall}, 1}} = \frac{T_{\infty 1} - T_2}{\frac{1}{h_1 A} + \frac{L_1}{k_1 A}}$$



The evaluation of the surface and interface temperatures when  $T_{\infty 1}$  and  $T_{\infty 2}$  are given and  $\dot{Q}$  is calculated.

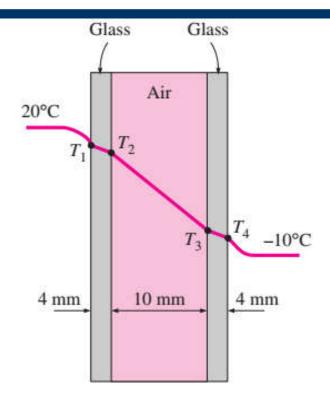
To find 
$$T_1$$
:  $\dot{Q} = \frac{T_{\infty_1} - T_1}{R_{\text{conv},1}}$ 

To find 
$$T_2$$
:  $\dot{Q} = \frac{T_{\infty_1} - T_2}{R_{\text{conv},1} + R_{\text{wall},1}}$ 

To find 
$$T_3$$
:  $\dot{Q} = \frac{T_3 - T_{\infty 2}}{R_{\text{conv},2}}$ 



#### **Example C: Heat loss through a double pane window**



Consider a 0.8-m-high and 1.5-m-wide double-pane window consisting of two 4-mm-thick layers of glass (k= 0.78 W/m. $^{\circ}$ C) separated by a 10-mm-wide stagnant air space (k= 0.026 W/m. $^{\circ}$ C). Determine the steady rate of heat transfer through this double-pane window and the temperature of its inner surface.

✓ Take the convection heat transfer coefficients on the inner and outer surfaces of the window to be  $hI = 10 \text{ W/m}2 \cdot ^{\circ}\text{C}$  and  $h2 = 40 \text{ W/m}2 \cdot ^{\circ}\text{C}$ , which includes the effects of radiation.



## **Generalized Thermal Resistence Networks**

$$\dot{Q} = \dot{Q}_1 + \dot{Q}_2 = \frac{T_1 - T_2}{R_1} + \frac{T_1 - T_2}{R_2} = (T_1 - T_2) \left(\frac{1}{R_1} + \frac{1}{R_2}\right)$$

$$\dot{Q} = \frac{T_1 - T_2}{R_{\text{total}}}$$

$$Q = \frac{1}{R_{\text{total}}}$$

$$\frac{1}{R_{\text{total}}} = \frac{1}{R_1} + \frac{1}{R_2} \longrightarrow R_{\text{total}} = \frac{R_1 R_2}{R_1 + R_2}$$

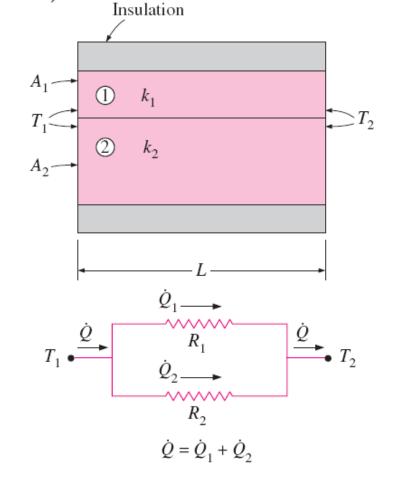
$$Q = \frac{1}{R_{\text{total}}}$$

$$Q = \frac{1}{R_{\text{total}}}$$

$$Q = \frac{1}{R_{\text{total}}}$$

$$Q = \frac{1}{R_1 + R_2}$$

Thermal resistance network for two parallel layers.





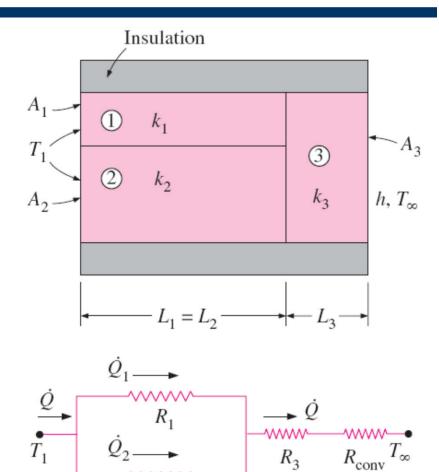
## **Generalized Thermal Resistence Networks**

$$\dot{Q} = \frac{T_1 - T_{\infty}}{R_{\text{total}}} \qquad R_1 = \frac{L_1}{k_1 A_1} \qquad R_2 = \frac{L_2}{k_2 A_2}$$

$$R_3 = \frac{L_3}{k_3 A_3} \qquad R_{\text{conv}} = \frac{1}{h A_3}$$

$$R_{\text{total}} = R_{12} + R_3 + R_{\text{conv}} = \frac{R_1 R_2}{R_1 + R_2} + R_3 + R_{\text{conv}}$$

- Two possible assumptions in solving complex multidimensional heat transfer problems by treating them as one-dimensional using the thermal resistance network are:
- ✓ any plane wall normal to the *x*-axis is *isothermal* (i.e., to assume the temperature to vary in the *x*-direction only)
- ✓ any plane parallel to the *x*-axis is *adiabatic* (i.e., to assume heat transfer to occur in the *x*-direction only)



Thermal resistance network for combined series-parallel arrangement.



#### **Example D: Heat loss through a composite wall**

- ✓ A 3 m high and 5 m wide wall consists of long 16 cm 22 cm cross section horizontal bricks ( $k = 0.72 \text{ W/m} \cdot ^{\circ}\text{C}$ ) separated by 3 cm thick plaster layers ( $k = 0.22 \text{ W/m} \cdot ^{\circ}\text{C}$ ).
- ✓ There are also 2 cm thick plaster layers on each side of the brick and a 3-cm-thick rigid foam (k 0.026 W/m · °C) on the inner side of the wall
- The indoor and the outdoor temperatures are 20°C and 10°C, and the convection heat transfer coefficients on the inner and the outer sides are *h*1=10 W/m2 · °C and *h*2 =25 W/m2 · °C, respectively. Assuming one-dimensional heat transfer and disregarding radiation, determine the rate of heat transfer through the wall.

