Introduction to Computer Control Systems, 5 credits, 1RT485

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Allowed aid:

- A basic calculator
- Beta mathematical handbook

Solutions have to be explained in detail and possible to reconstruct.

<u>NB</u>: Only one problem per sheet. Write your name and personal number if you do not have an anonymous code.

Best of luck!

Useful results

Laplace transform table

Table 1: Basic Laplace transforms

f(t)	F(s)	f(t)	F(s)
unit impulse $\delta(t)$	1	$\sinh(bt)$	$\frac{b}{s^2 - b^2}$
unit step $1(t)$	1 8	$\cosh(bt)$	$\frac{s}{s^2-b^2}$
t	$\frac{\tilde{1}}{s^2}$	$\frac{1}{2b}t\sin(bt)$	$\frac{s}{(s^2+b^2)^2}$
t^n	$\frac{\frac{1}{s^2}}{\frac{n!}{s^{n+1}}}$	$t\cos(bt)$	$\frac{s^2-b^2}{(s^2+b^2)^2}$
e^{-at}	$\frac{1}{s+a}$	$\frac{\cos(bt) - \cos(at)}{a^2 - b^2}$; $(a^2 \neq b^2)$	$\frac{s}{(s^2+a^2)(s^2+b^2)}$
$\frac{1}{2}(1-e^{-at})$	$\frac{1}{s(s+a)}$	$\frac{\sin(at)+at\cos(at)}{2a}$	$\frac{(s+a)(s+b)}{(s^2+a^2)^2}$
$\frac{1}{(n-1)!}t^{n-1}e^{-at}; (n=1,2,3)$	$\frac{1}{(s+a)^n}$	Zu Zu	(8 74)
$\sin(bt)$	$\frac{b}{s^2+b^2}$		
$\cos(bt)$	$\frac{\frac{s}{s^2+b^2}}{}$		
$e^{-at}\sin(bt)$	$\frac{b}{(s+a)^2+b^2}$		
$e^{-at}\cos(bt)$	$\frac{s+a}{(s+a)^2+b^2}$		

Table 2: Properties of Laplace Transforms

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$$\mathcal{L}[af(t)] = aF(s)$$

$$\mathcal{L}[f_1(t) + f_2(t)] = F_1(s) + F_2(s)$$

$$\mathcal{L}\left[\frac{d}{dt}f(t)\right] = sF(s) - f(0)$$

$$\mathcal{L}\left[\frac{d^2}{dt^2}f(t)\right] = s^2F(s) - sf(0) - f'(0)$$

$$\mathcal{L}\left[\int f(t) dt\right] = \frac{F(s)}{s} + \frac{1}{s}\left[\int f(t) dt\right]_{t=0}$$

$$\mathcal{L}\left[f(t-a)\right] = e^{-as}F(s)$$

$$\mathcal{L}\left[e^{-at}f(t)\right] = F(s+a)$$

Matrix exponential

$$e^{At} \triangleq \mathcal{L}^{-1} \left\{ (sI - A)^{-1} \right\}$$

Open-loop and sensitivity functions

$$G_o(s) = G(s)F_y(s), \qquad S(s) = \frac{1}{1 + G_o(s)}, \qquad T(s) = 1 - S(s)$$

State-space forms and transfer function relations

• State-space form and transfer function

$$\dot{x} = Ax + Bu$$

 $y = Cx + Du$ \Rightarrow $G(s) = C(sI - A)^{-1}B + D$

· Associated matrices

$$S = \begin{bmatrix} B & AB & \cdots & A^{n-1}B \end{bmatrix} \qquad \mathcal{O} = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

• LTI system with transfer function

$$G(s) = \frac{b_0 s^n + b_1 s^{n-1} + \dots + b_n}{s^n + a_1 s^{n-1} + \dots + a_n}$$

i) Observable canonical form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \vdots \\ \dot{x}_n \end{bmatrix} = \begin{bmatrix} -a_1 & 1 & 0 & \cdots & 0 \\ -a_2 & 0 & 1 & \cdots & 0 \\ -a_3 & 0 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ -a_n & 0 & 0 & \cdots & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} b_1 - a_1 b_0 \\ b_2 - a_2 b_0 \\ b_3 - a_3 b_0 \\ \vdots \\ b_n - a_n b_0 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & \cdots & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} + b_0 u$$

ii) Controllable canonical form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \vdots \\ \dot{x}_n \end{bmatrix} = \begin{bmatrix} -a_1 & -a_2 & -a_3 & \cdots & -a_n \\ 1 & 0 & 0 & \cdots & 0 \\ 0 & 1 & 0 & \cdots & 0 \\ \vdots & 0 & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ x_n \end{bmatrix} u$$

$$y = \begin{bmatrix} b_1 - a_1b_0 & b_2 - a_2b_0 & \cdots & b_n - a_nb_0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} + b_0 u$$

• Solution to state-space equation

$$\dot{x}(t) = Ax(t) + Bu(t), \quad x(0) = x_0$$

can be written as

$$x(t) = e^{At}x_0 + \int_0^t e^{A au}Bu(t- au)d au$$

iii) Consider a system with transfer function

$$G(s) = \frac{s+1}{(s+2)(s+5)}.$$

Suppose the same system is described in state-space that is a minimal realization. Then the eigenvalues of A equal -2 and -5.

(3 p)

Problem 2 (6/30)

a) Consider a mechanical system with input u(t) and output y(t) that can be written as

 $Y(s) = G(s)U(s) = \frac{1}{s+a}U(s).$

We apply feedback controller to output to follow a reference signal r(t). Specifically a P-controller F(s) = K is used with K set to 8.

We now are interested to know for which pole locations of G(s) is the closed-loop system stable: For which a will $G_c(s)$ be stable?

(3 p)

b) Consider the following configuration of the system above

$$Y(s) = G(s)U(s) = \frac{1}{s+2}U(s),$$

which we control using a feedback controller $F(s) = 1 + \frac{K_i}{s}$. Let the reference signal r(t) be a step. That is,

$$r(t) = \begin{cases} r_0, & t \ge 0 \\ 0 & \text{otherwise} \end{cases}$$

Set $K_i = 10$ and calculate the stationary error of the controller: e(t) = r(t) - y(t) as $t \to \infty$.

(3 p)

Problem 3 (6/30)

a) Consider a controlling a thermal process with an output modeled as

$$Y(s) = G(s)U(s),$$

where the process model can be written as

$$G(s) = \frac{s+3}{s^2 + 6s + 11}.$$

Assuming the states can be obtained, design a stable closed-loop system from r to y with poles located at -2 and -5.

(4 p)

b) To prepare for the design of a state observer,

$$\dot{\hat{x}} = A\hat{x} + Bu + K(y - C\hat{x}),$$

write the system above on observable canonical form.

(2 p)

Problem 4 (6/30)

(a) When working with a control problem, Mr. Stu Dent generated the four Bode diagrams in Figure 1.

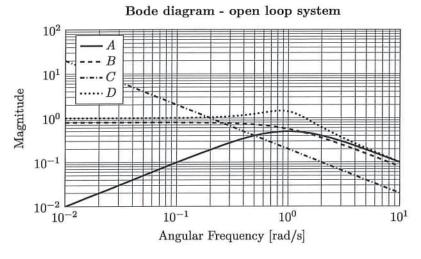


Figure 1: Bode diagrams of the open loop systems.

He then proceeded to generate step responses for both the open loop systems in Figure 2 and the closed loop systems in Figure 3. The closed loop systems used standard feedback with F(s)=1. By accident, Stu mix up all the systems and used different labels in the legends. Help Stu match the Bode diagrams with the step responses.

(I) Pair the Bode diagrams A-D with the open loop step responses 1-4 in Figure 2.

(2 p)

Step response - open loop system

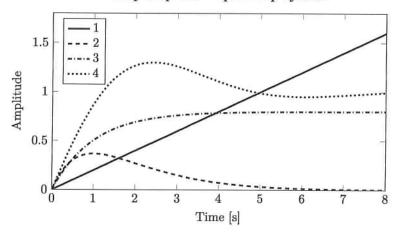


Figure 2: Step responses for the open loop systems.

(II) Pair the Bode diagrams A-D with the closed loop step responses I-IV in Figure 3.

(2 p)

Step response - closed loop system

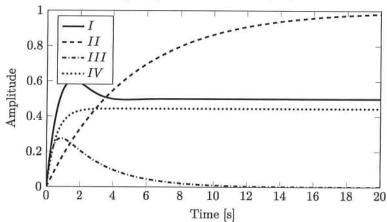


Figure 3: Step responses for the closed loop systems using standard feedback with F(s) = 1.

(b) The Bode diagram for an industrial process is shown in Figure 4.

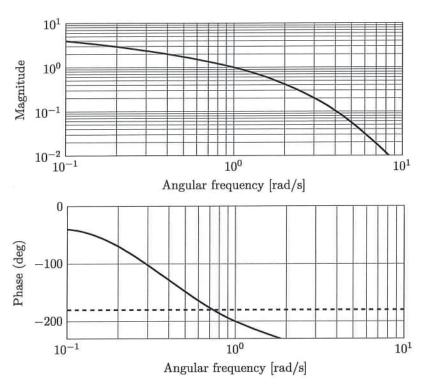


Figure 4: Bode diagram for an industrial process.

(I) What is the crossover frequency ω_c and the phase margin φ_m for the process?

(1 p)

(II) If a pure time delay of T=0.8 s is added to the output of the process, that is we measure $\tilde{y}(t)=y(t-T)$ instead of y(t), will the resulting closed loop system be stable when using standard feedback with F(s)=1?

(1 p)

Problem 5 (6/30)

A certain physical model with the state vector

$$x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

has the following state-space representation

$$\begin{split} \dot{x} &= \begin{bmatrix} 0 & -a \\ a & 0 \end{bmatrix} x + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u \\ y &= \begin{bmatrix} 1 & 1 \end{bmatrix} x \end{split}$$

a) Discretise the state-space system (using zero order hold) with sampling time T.

(2 p)

b) For what values of T is the discretised system observable?

(2 p)

c) Pick $T = \frac{\pi}{2a}$ and construct an observer

$$K = \begin{bmatrix} k_1 \\ k_2 \end{bmatrix}$$

such that the discrete time observer poles are located in ± 0.5 .

(2 p)