



December 2015 Final Evaluation
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Diagnosis of Rolling Mill Cycloconverters Using Time-Frequency Signature Analysis

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Overview



01 Introduction

- Project goals and motivation
- Current Techniques

02 Theory Overview

- Cycloconverter Operation
- Time-Frequency Analysis
- Feature Identification
- Modeling

03 Operating Status Decision Boundary

- Error Analysis Technique
- Loaded Motor Error Statistical Analysis
- Unloaded Motor Statistical Analysis
- Error Decision Boundary Thresholds

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- Next Steps
- Closing Remarks

Introduction

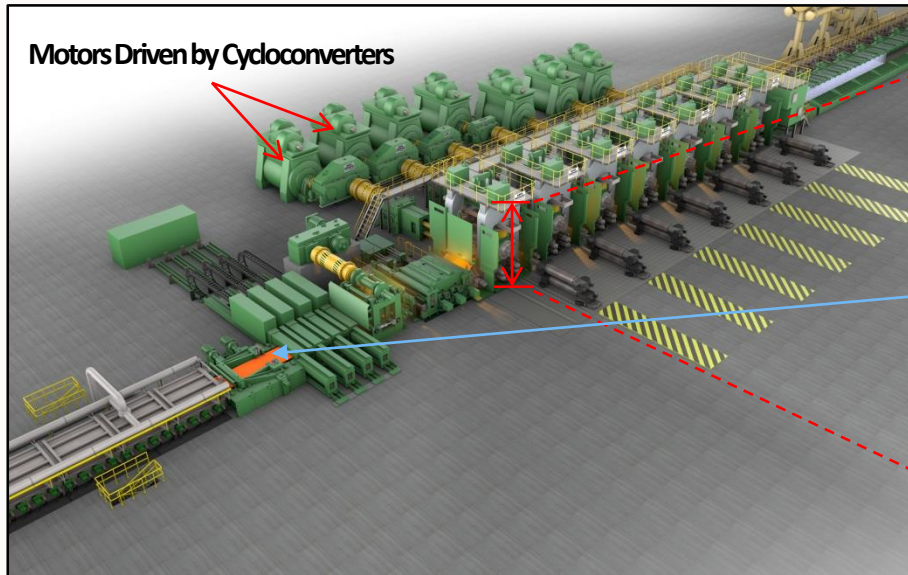
01 Project goals and motivation

02 Benchmarks



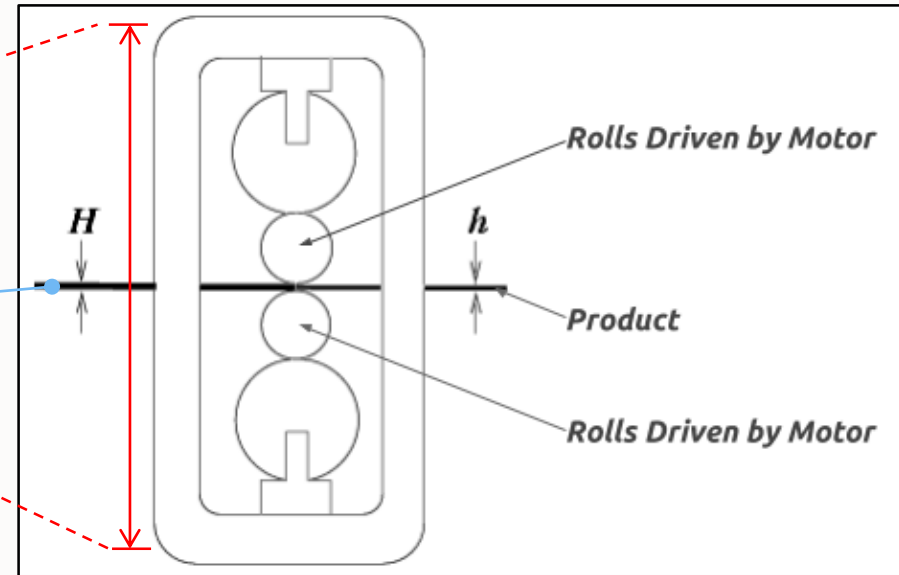
Introduction

Project Goals and Motivation



Motors Driven by Cycloconverters

Typical Rolling Mill Setup*



Roll Stack**

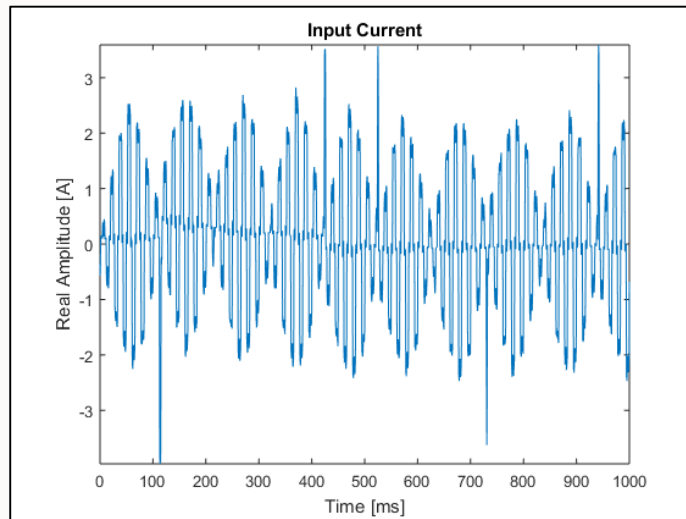
- Reduce gauge of steel in a controlled and reliable manner
 - Minimize damage to equipment and time down
- Confirm or call into question failure status of cycloconverter

* [Rendering by SMS Group] <<https://www.sms-group.com/pressedetail.php?id=1229>>

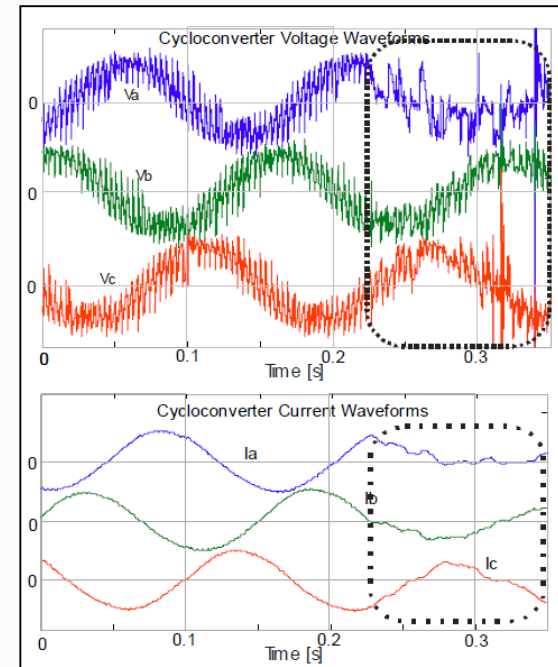
** [Open source Wikimedia file] <https://www.cds.caltech.edu/~murray/amwiki/index.php/Exercise:_Exploring_the_dynamics_of_rolling_mill>

Current Techniques

Benchmarking – Time Domain Analysis

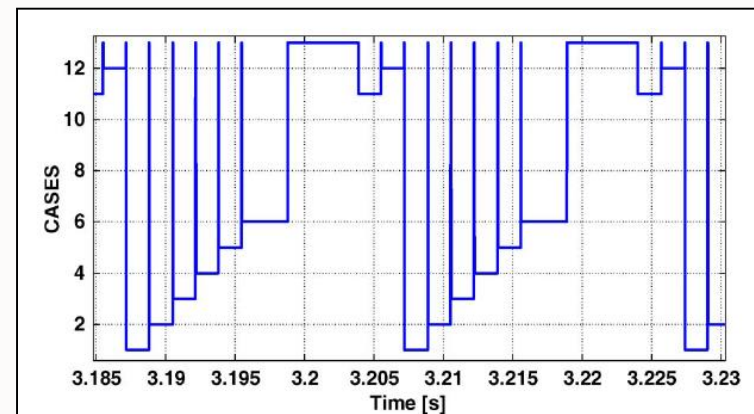
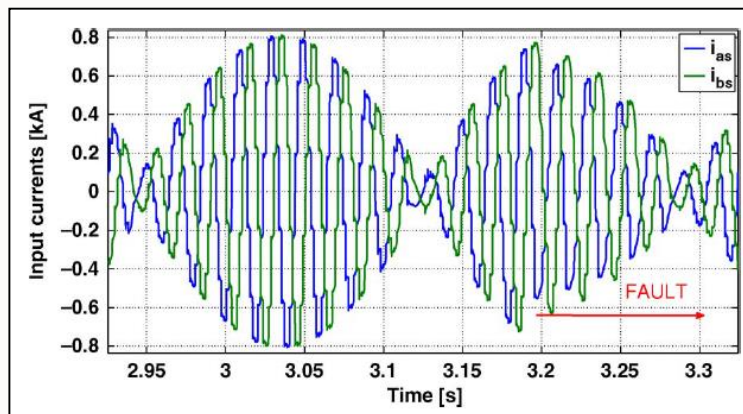


Damaged cycloconverter input current of concern



Loss of blocking capability in specific SCR [2]

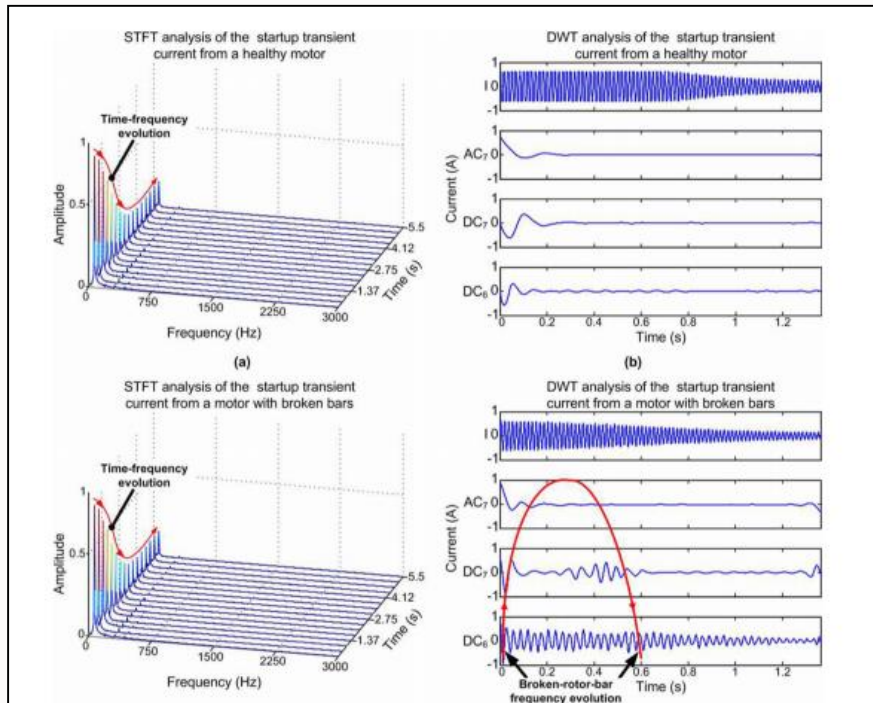
Attempt to identify faults in time domain [1]



- [1] V. Guerrero, J. Pontt, J. Dixon, and J. Rebolledo, "A novel noninvasive failure-detection system for high-power converters based on SCRs," *IEEE Trans. Ind. Electron.*, vol. 60, no. 2, pp. 450 - 458, Feb. 2013.
- [2] J. Pontt, J. Rodríguez, E. Cáceres, I. Illanes and J. Rebolledo, "Cycloconverter behavior for a grinding mill drive under firing pulses fault conditions," in *Industry Applications Conf., Hong Kong*, 2005, pp. 645-649

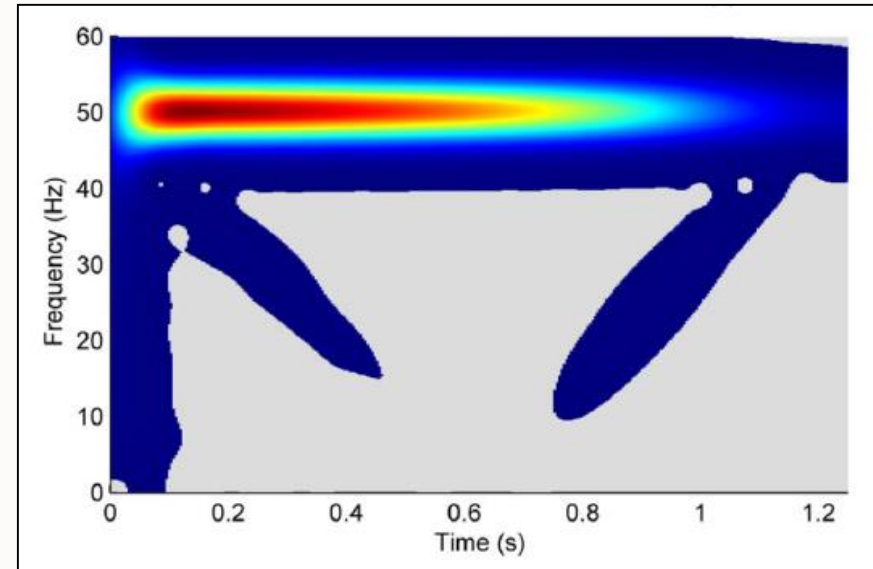
Current Techniques

Benchmarking – TF Domain Analysis

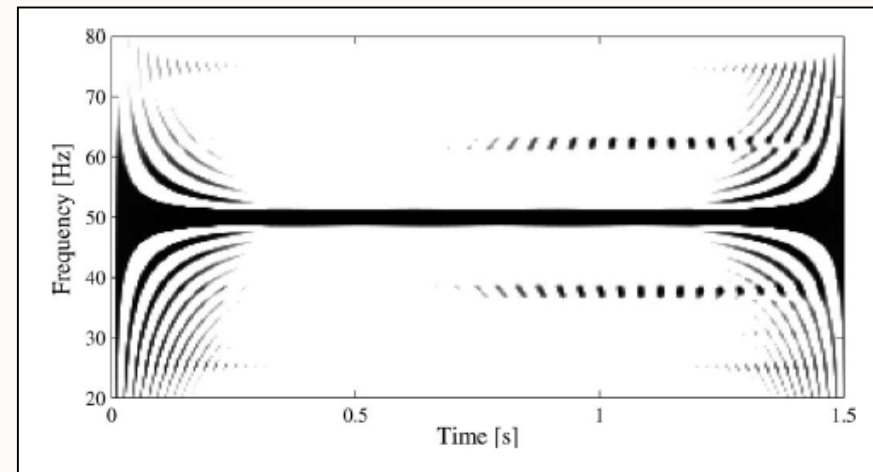


Attempt to characterize the motor in the time-frequency domain [3]

Gabor transform to quickly identify motor faults [4]



Acoustic analysis of motor [5]



[3] Eduardo Cabal-Yepez, Armando G. Garcia-Ramirez, Rened J. Romero-Troncoso, Arturo Garcia-Perez, and Roque A. Osornio-Rios, "Reconfigurable Monitoring System for Time-Frequency Analysis on Industrial Equipment Through STFT and DWT," *IEEE Trans. Ind. Informat.*, vol. 9, no. 2, pp. 760-771, May 2013.

[4] M. Riera-Guasp, M. Pineda-Sanchez, J. Perez-Cruz, R. Puche-Panadero, J. Roger-Folch, and J. A. Antonino-Daviu, "Diagnosis of induction motor faults via gabor analysis of the current in transient regime," *IEEE Trans. Instrum. Meas.*, vol. 61, no. 6, pp. 1583-1596, Jun. 2012.

[5] M. Blödt, M. Chabert, J. Regnier and J. Faucher, "Mechanical load fault detection in induction motors by stator current time-frequency analysis," *IEEE Trans. Ind. Appl.*, vol. 42, no. 6, pp. 1454-1463, Nov./Dec. 2006.

Theory Overview

- 01 Cycloconverter Operation
 - 02 Time-Frequency Analysis
 - 03 Feature Identification
 - 04 Modeling
-



Theory Overview

Cycloconverter Operation – General

$$\alpha = f(\theta_o) = \sin^{-1} r \sin \theta_o$$

$\alpha = \text{Firing Angle}$

$r = \text{DC Voltage Ratio}$

$$\theta_o = 2\pi f_o t$$

$f_o = \text{output frequency}$

Phase Modulation Term

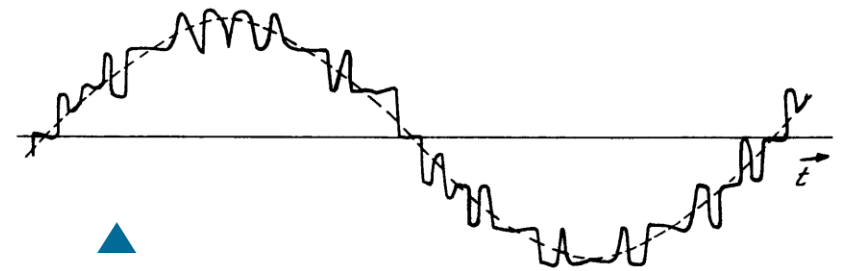
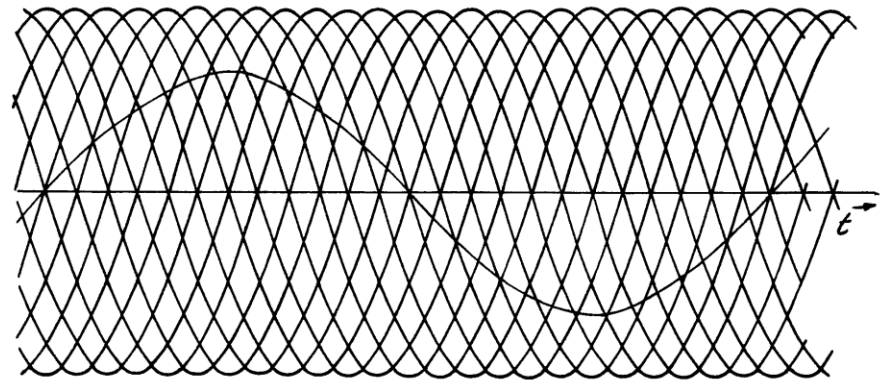
$$i_A = \hat{I}_o \sin(\theta_o + \phi_o) \cdot F_1\left(\theta_i - \frac{\pi}{2} + f(\theta_o)\right) \cdot F_P(\theta_o) \\ + \hat{I}_o \sin(\theta_o + \phi_o) \cdot F_1\left(\theta_i + \frac{\pi}{2} - f(\theta_o)\right) \cdot F_N(\theta_o)$$

$\alpha = \text{Firing Angle}$

$F_1 = \text{Thyristor Switching Function}$

$F_{N \text{ or } P}(\theta_o) = \text{Negative and Postive Converter}$

Input Phases and Reference Waveform



Reference Waveform and Voltage Output

Relevant Voltage Waveforms

Theory Overview

Cycloconverter Operation – Input Current Harmonics

$$f_H = |[kq \pm 1]f_i \pm 6nf_o|$$

f_H = Harmonic Freq

f_i = Input Freq

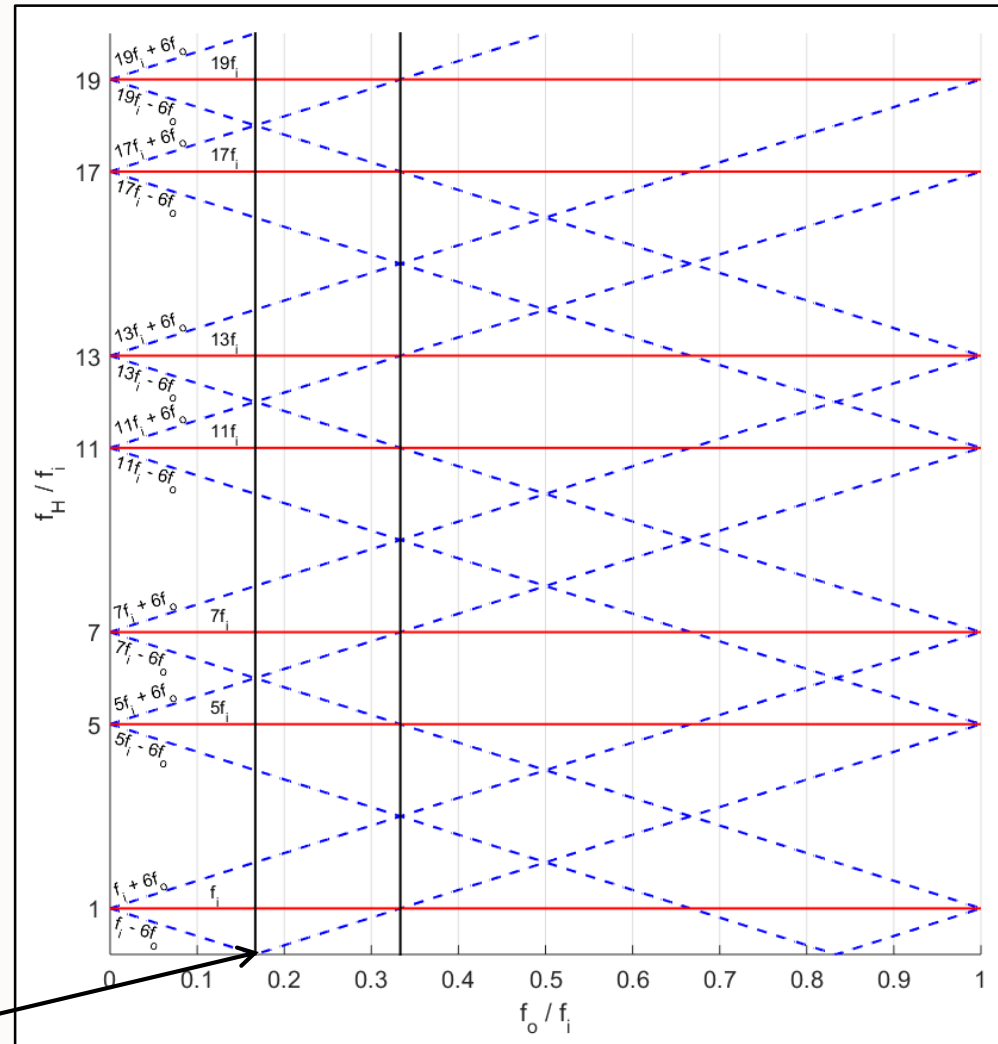
f_o = Output Freq

q = drive pulse number

k = any int from 1 to ∞

n = any int from 0 to ∞

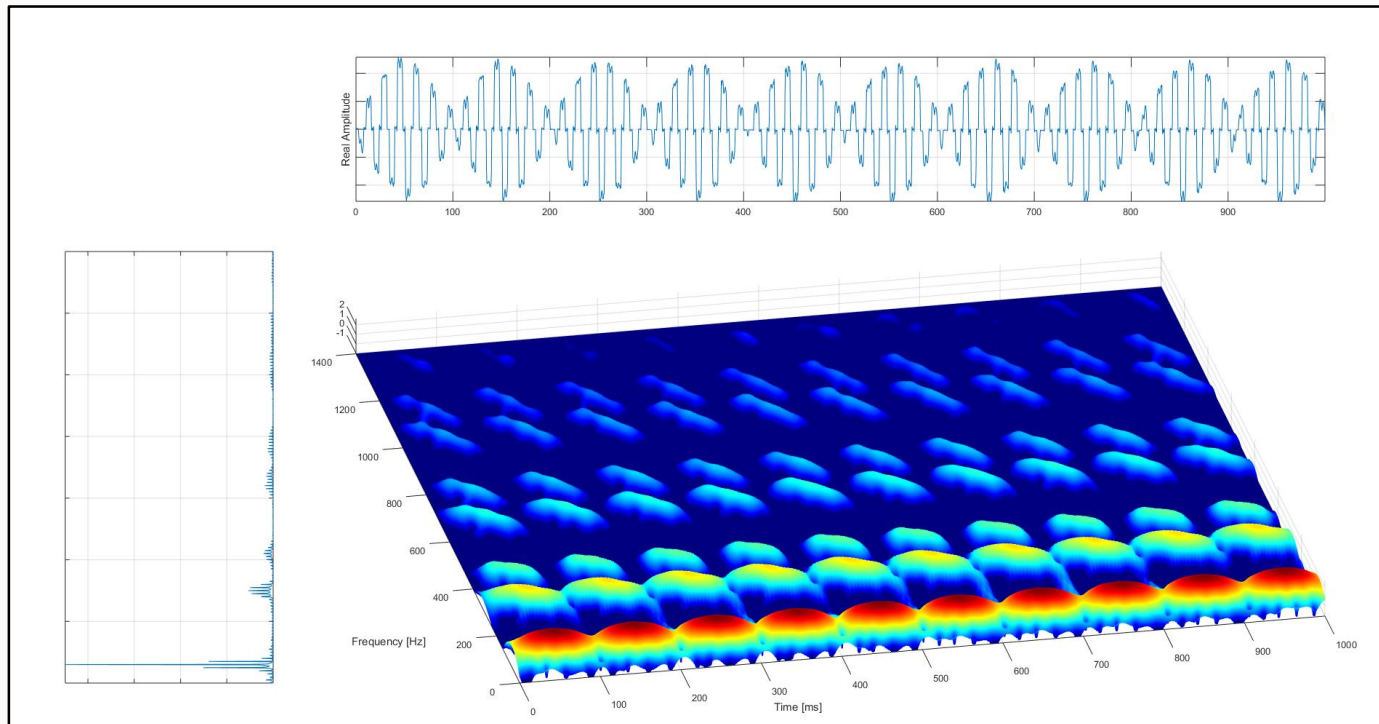
$$\frac{f_o}{f_i} = \frac{1}{6}$$



Predominant harmonic frequencies present in the input current for a 6-pulse cycloconverter

Theory Overview

Time-Frequency Analysis – General



*Spectrogram
Sample*

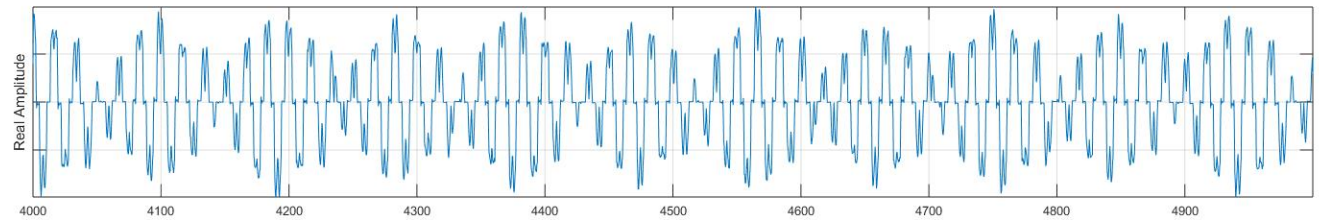
Features of Interest

- Frequency Centers of Chirps
- Harmonic Slopes in the Time-Frequency Domain

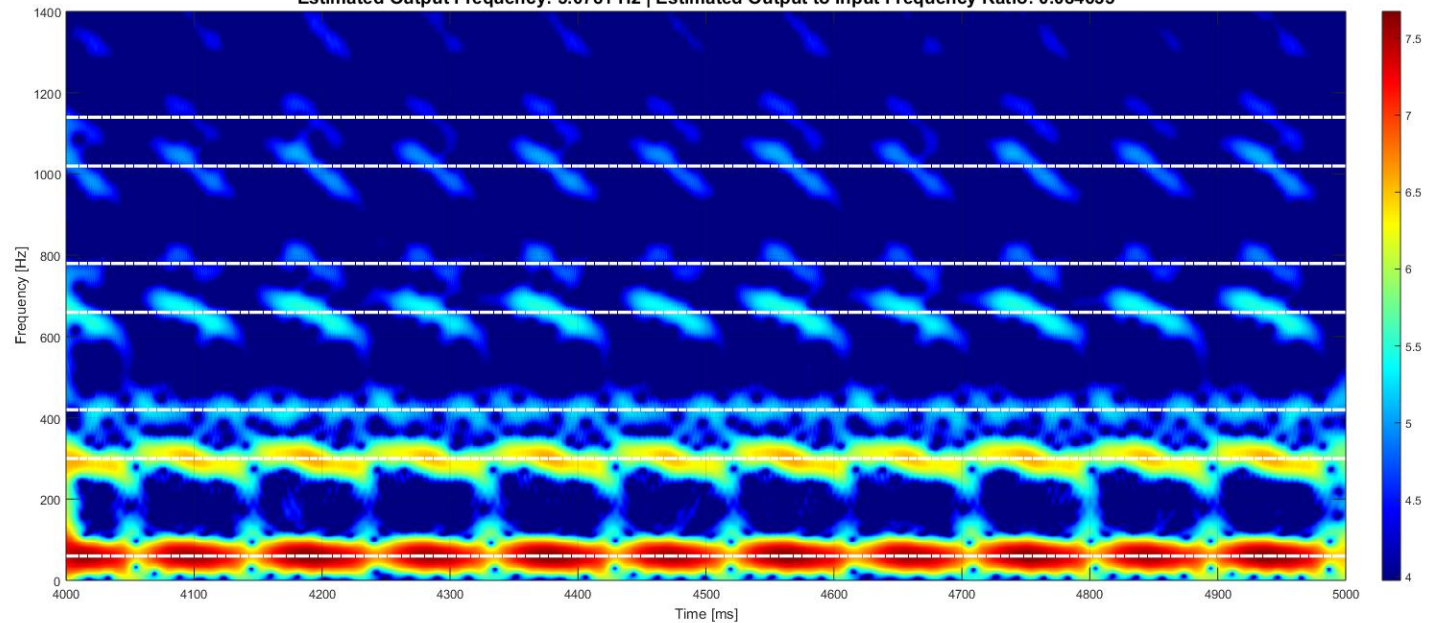
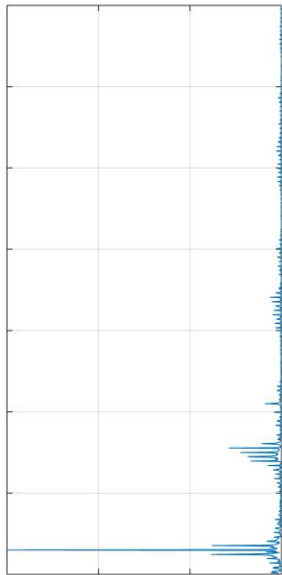
$$C(t, \omega) = \left| \frac{1}{\sqrt{2\pi}} \int e^{-j\omega\tau} s(\tau) h(\tau - t) d\tau \right|^2$$

Theory Overview

Feature Identification – Frequency Centers



Window: Hamming | Ln: 95 samp | Nf: 2858 | Threshold: 0.02 | Scale: Log
 Estimated Output Frequency: 5.0781 Hz | Estimated Output to Input Frequency Ratio: 0.084635

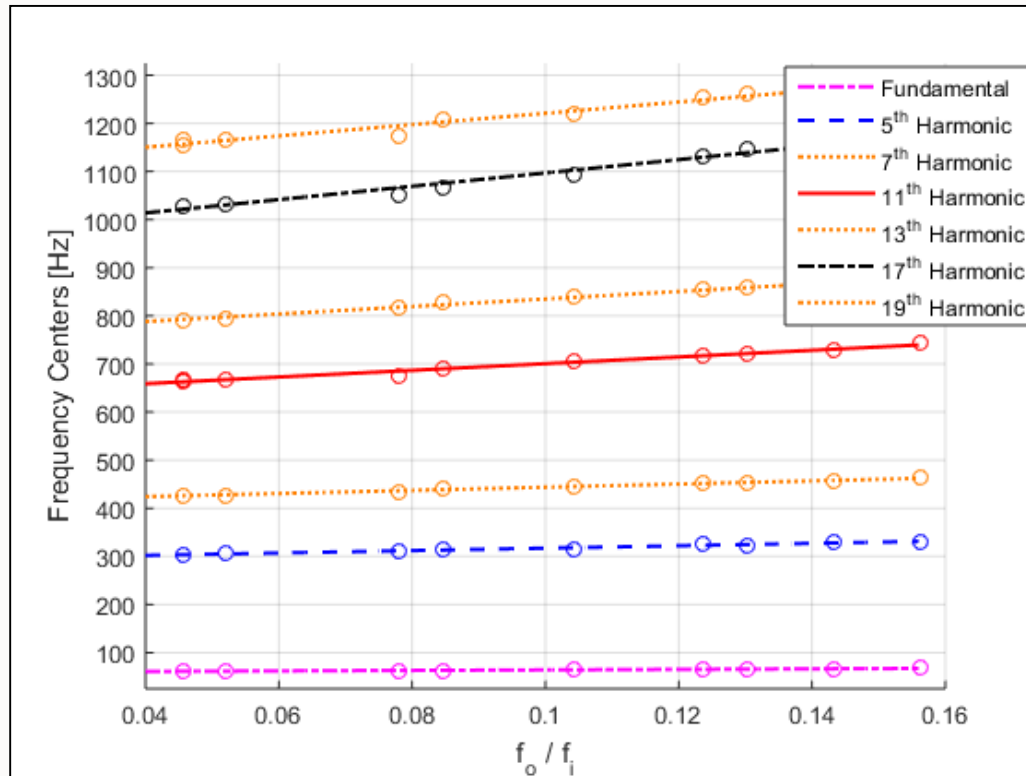


- White Lines = Frequency Centers of Chirps

$$\langle \omega \rangle = \int \omega |S(\omega)|^2 d\omega$$

Theory Overview

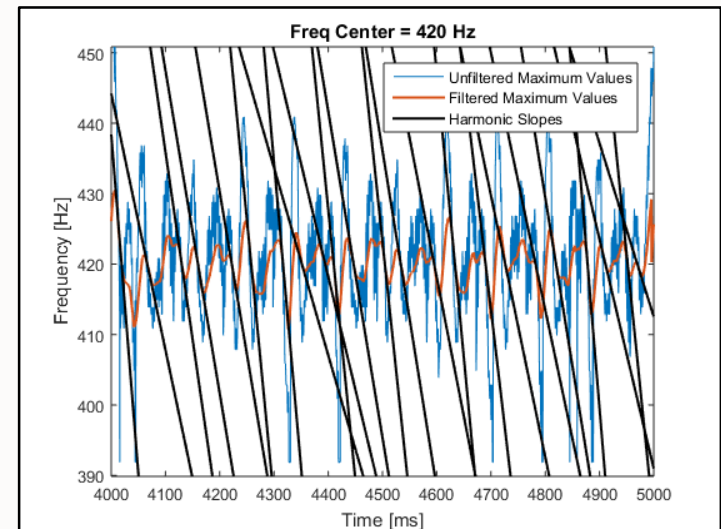
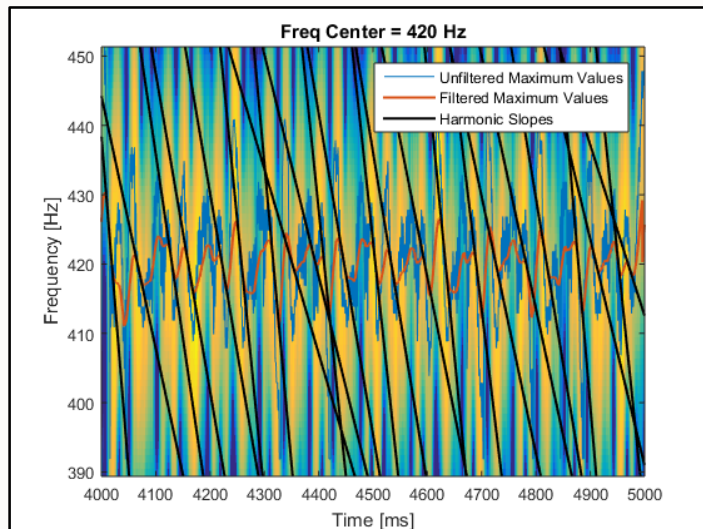
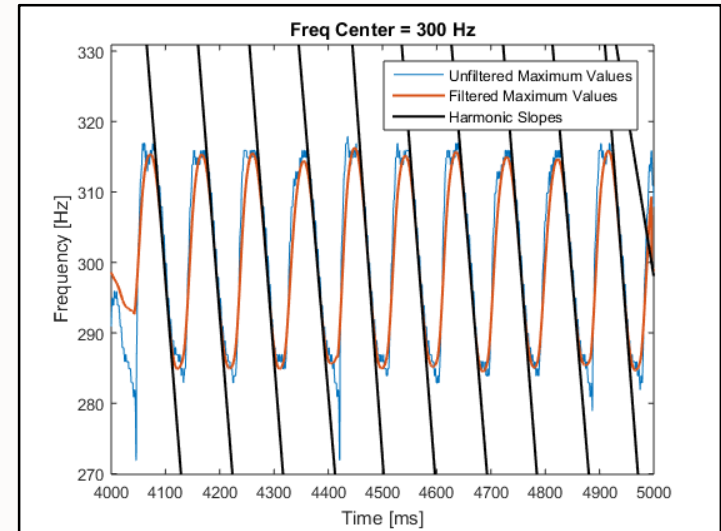
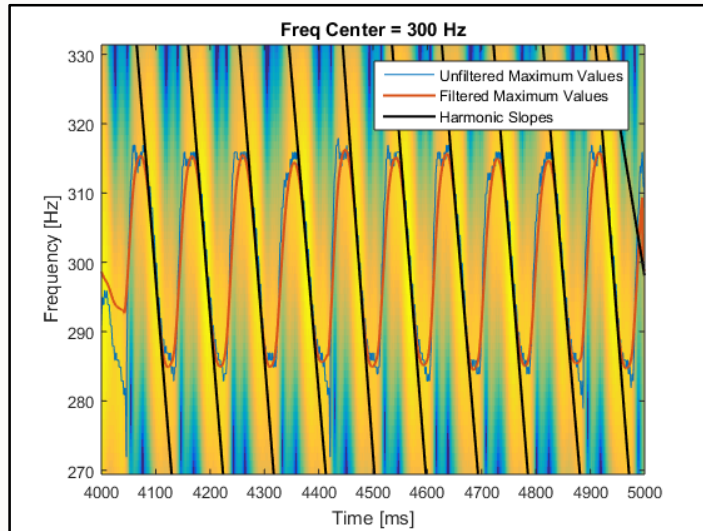
Feature Identification – Frequency Centers



- Unloaded motor frequency centers rise linearly
- Loaded motor frequency centers do not change

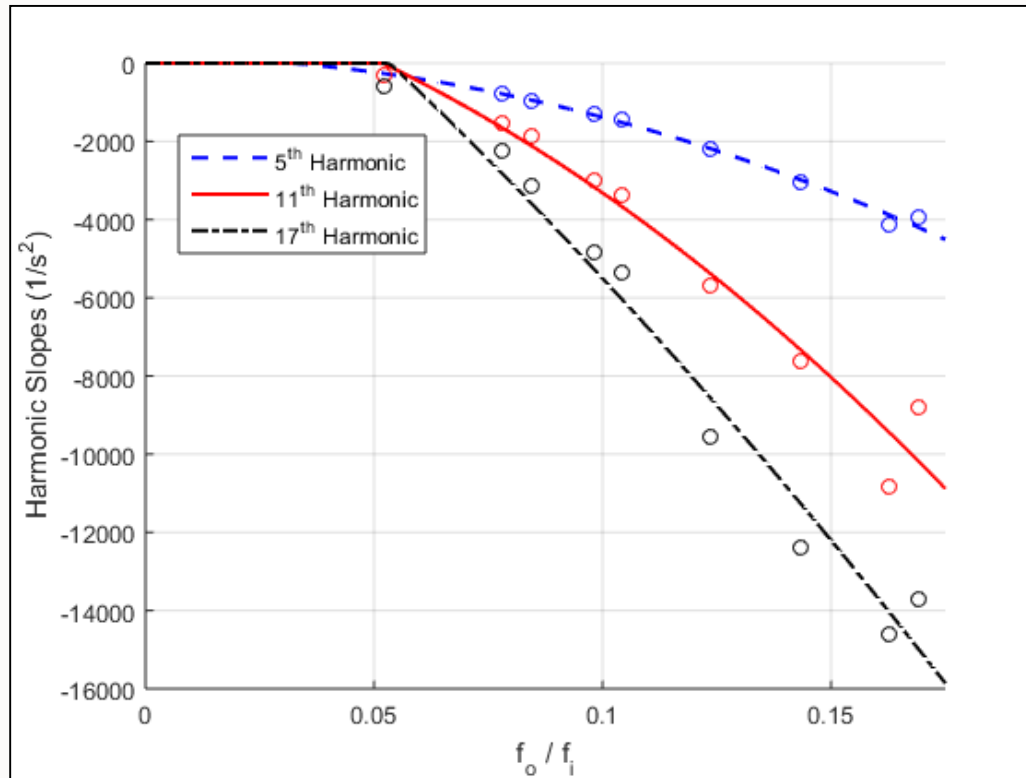
Theory Overview

Feature Identification – Harmonic Slopes



Theory Overview

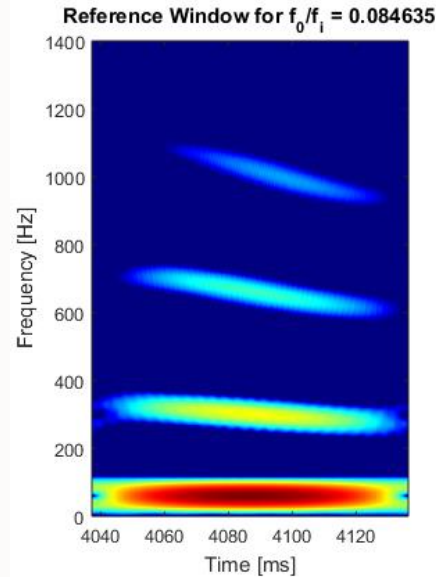
Feature Identification – Harmonic Slopes



- 2nd order polynomial fit to harmonic slope data for 5th, 11th, and 17th harmonics
 - Unknown behavior for higher ratios
 - Represented by $\beta \left(\gamma \left(\frac{f_o}{f_i} \right) \right)$ in modeling equation

Theory Overview

Modeling – Modeling Equation



Fund, 5th, 11th, and 17th

Amplitude
Modulation

$$\sin(2\pi f_o t) \sum_{n=0}^3 \left| \frac{1}{6n-1} \right| \sin \left(\left(|6n-1| \left(f_i + \left(\alpha_h \left(\frac{f_o}{f_i} \right) - f_i |6n-1| \right) \right) \right) 2\pi t \right)$$

Empirical Unloaded
Frequency Centers

f_i
= input freq.

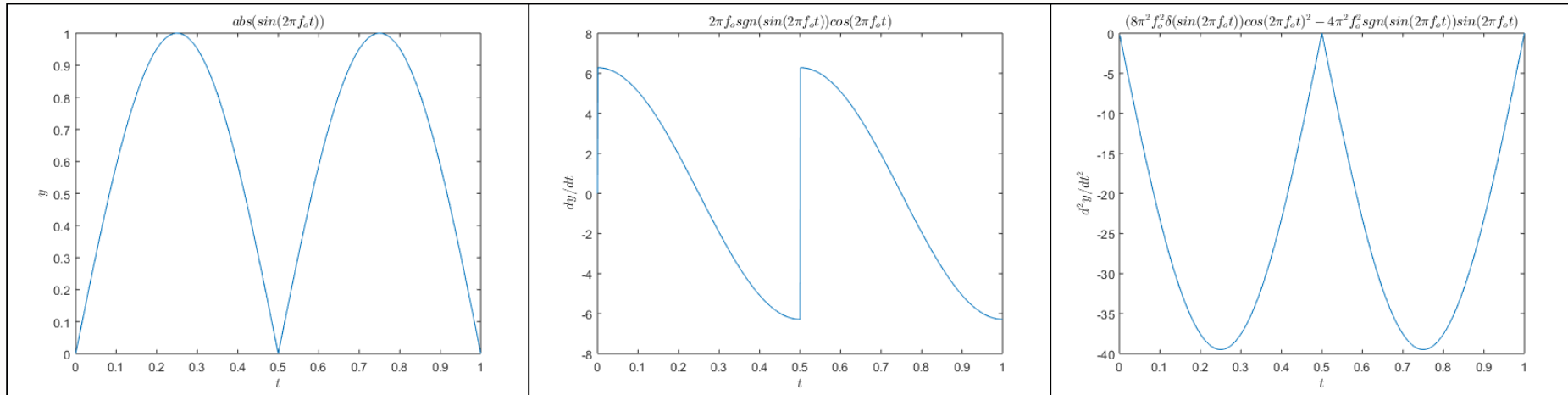
f_o
= output
freq.

Empirical Slopes

Frequency
Modulation

Theory Overview

Modeling - Frequency Modulation Term



Frequency Modulation Function

$$\phi(t) = \beta \left(\gamma_h \left(\frac{f_o}{f_i} \right) \right) |\sin(2\pi f_o t)|$$

Empirical Slopes

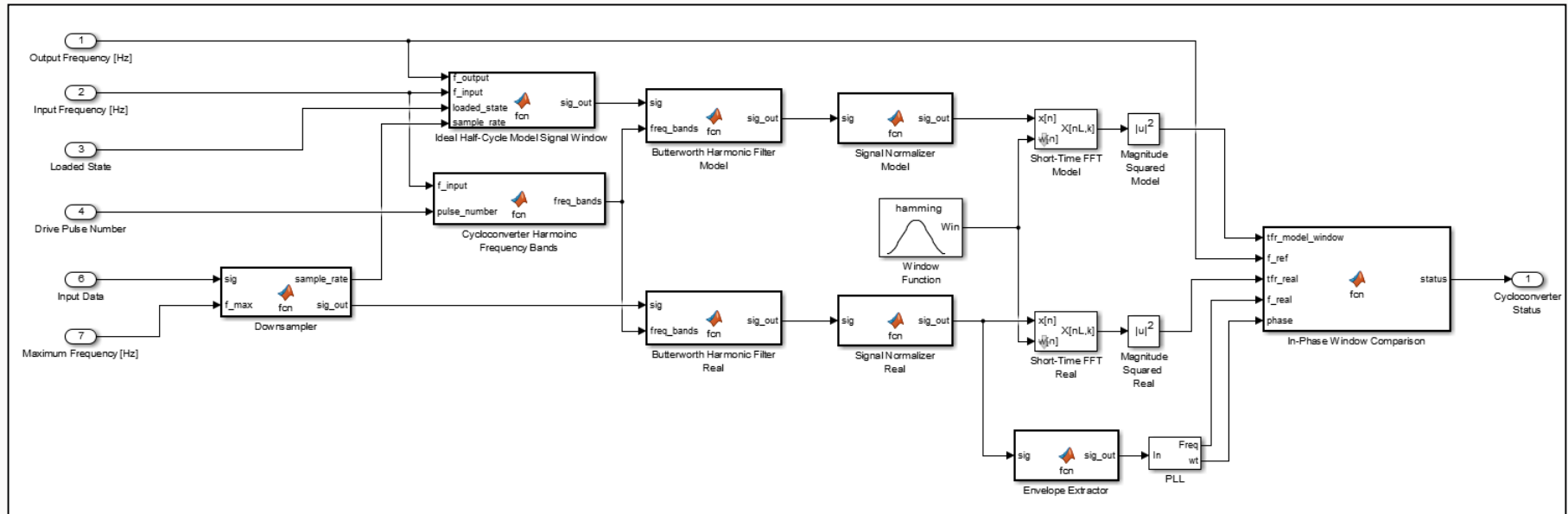
$$\beta \left(\gamma_h \left(\frac{f_o}{f_i} \right) \right) = \frac{\gamma_h \left(\frac{f_o}{f_i} \right)}{4 \pi^2 f_o \left(2 \delta \left(\sin \left(\frac{\pi}{2} \right) \right) \cos \left(\frac{\pi}{2} \right)^2 - \text{sgn} \left(\sin \left(\frac{\pi}{2} \right) \sin \left(\frac{\pi}{2} \right) \right) \right)}$$

f_i
= input freq.

f_o
= output
freq.

Theory Overview

Modeling – Model Block Diagram



- 1. Given inputs develop a model in the time domain and convert to time-frequency domain
- 2. Filter real input current data and time domain model
 - a. Normalize both signals
- 3. Convert to time-frequency domain with spectrogram
- 4. Compare reference window in phase to real data
 - a. Characterize cycloconverter as in normal or abnormal operation

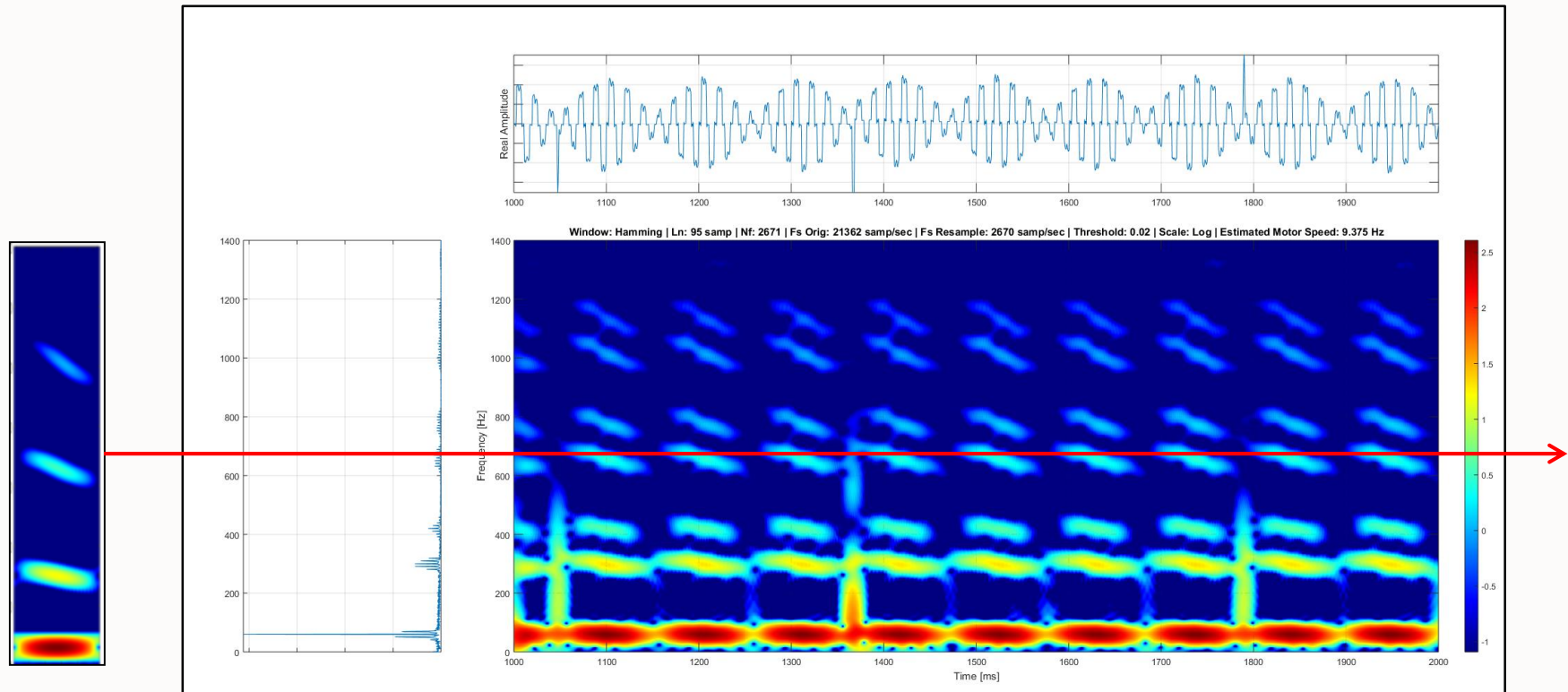
Operating Status Decision Boundary

- 01 Error Analysis Technique
- 02 Loaded Motor Error Statistical Analysis
- 03 Unloaded Motor Error Statistical Analysis
- 04 Error Decision Boundary Thresholds



Operating Status Decision Boundary

Error Analysis Technique

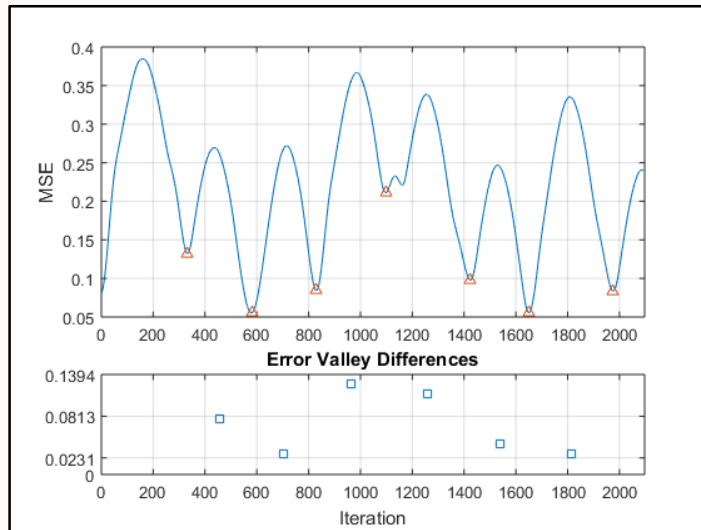


- Slide reference window through spectrogram
- Find error for each iteration, calculate MSE

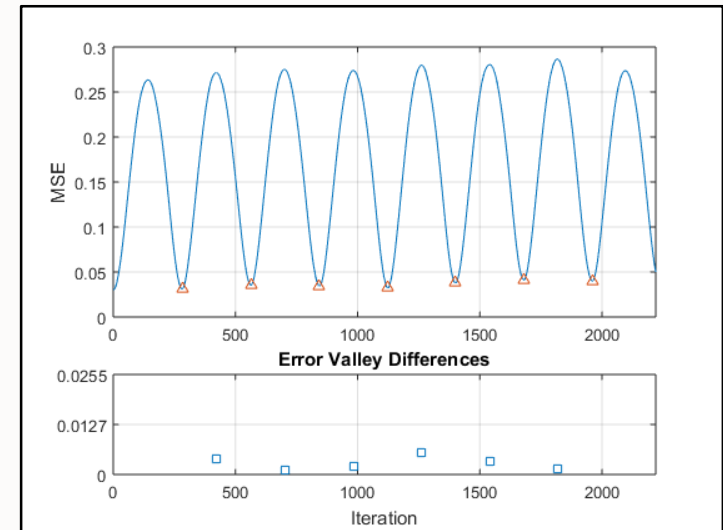
$$MSE = \frac{1}{N \cdot M} \sum_{n=1}^N \sum_{m=1}^M |C_{reference}[n, m] - C_{real}[n, m]|^2$$

Operating Status Decision Boundary

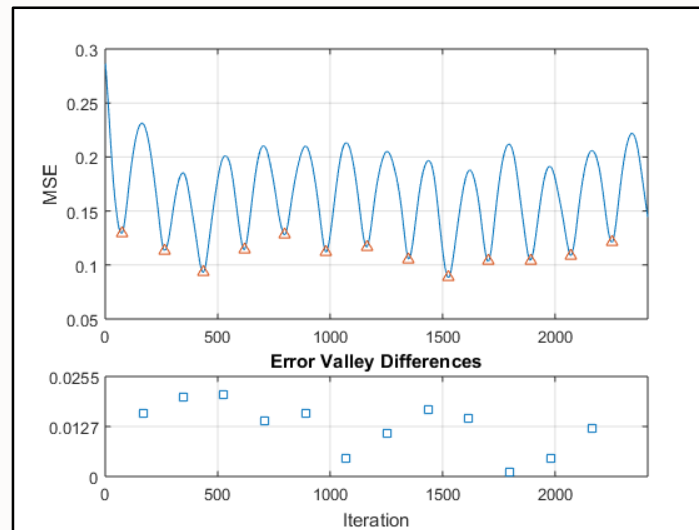
Error Analysis Technique



Damaged Loaded



Undamaged Loaded

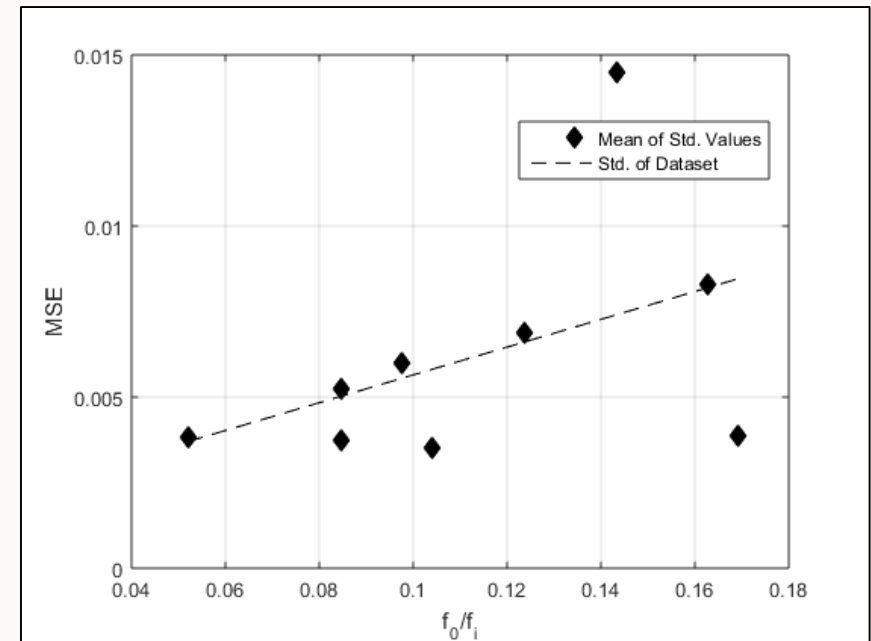
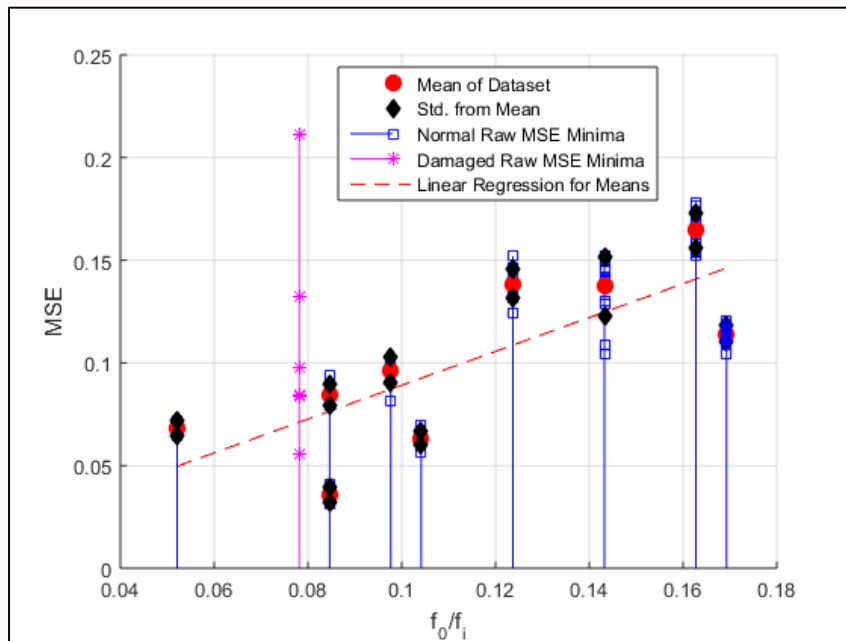


Undamaged Unloaded

Operating Status Decision Boundary

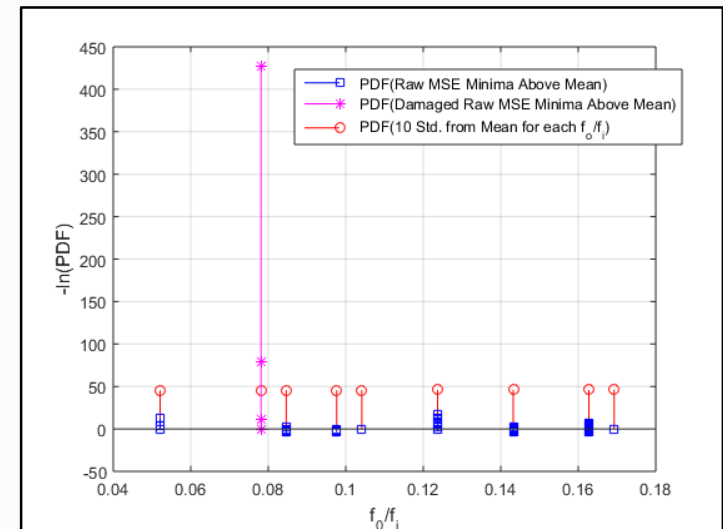
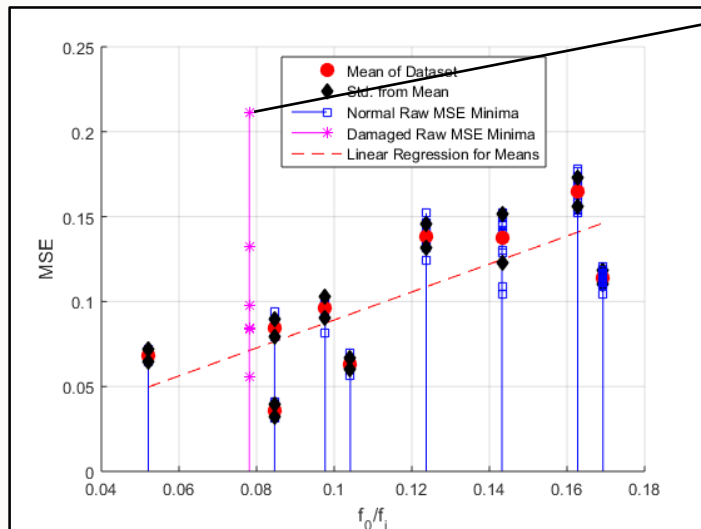
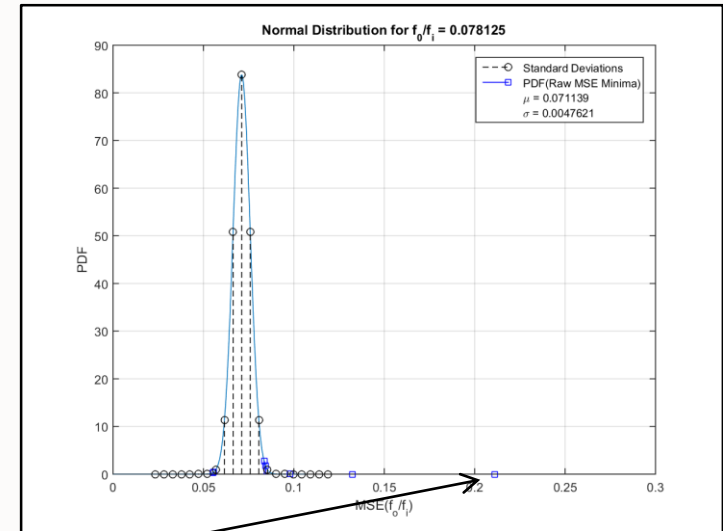
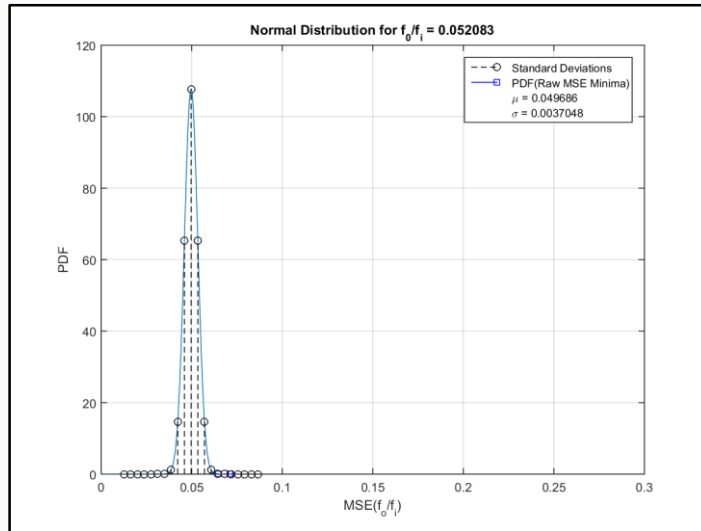
Loaded Motor Error Statistical Analysis – MSE

Fund. Freq (Hz)	60																					
Output Frequency (Hz)	Notes	f_o/f_i	Mean	Std.	Loaded Motor Local Minima MSE																	
3.1250	F6	0.0521	0.0681	0.0033	0.065	0.071	0.065	0.072														
4.6875	Damaged F1	0.0781	0.1029	0.0505	0.132	0.055	0.084	0.211	0.098	0.056	0.084											
5.0781		F6	0.0846	0.0836	0.0048	0.085	0.079	0.08	0.083	0.088	0.079	0.082	0.094									
5.0781	F1	0.0846	0.0360	0.0035	0.031	0.035	0.034	0.032	0.038	0.041	0.04											
5.8594	F1	0.0977	0.0966	0.0057	0.098	0.081	0.1	0.1	0.092	0.098	0.098	0.101	0.096	0.101								
6.2500	F6	0.1042	0.0634	0.0033	0.066	0.066	0.065	0.062	0.069	0.065	0.061	0.063	0.061	0.056								
7.4219	F6	0.1237	0.1385	0.0066	0.124	0.132	0.138	0.138	0.134	0.139	0.137	0.137	0.146	0.152	0.145	0.141	0.137					
8.5938	F6	0.1432	0.1373	0.0140	0.137	0.138	0.15	0.146	0.149	0.142	0.152	0.145	0.152	0.139	0.137	0.13	0.129	0.109	0.104			
9.7656	F2	0.1628	0.1651	0.0081	0.16	0.161	0.17	0.154	0.156	0.172	0.163	0.168	0.172	0.173	0.152	0.154	0.177	0.178	0.169	0.159	0.16	0.174
10.1563	F2	0.1693	0.1141	0.0037	0.119	0.113	0.104	0.111	0.113	0.118	0.121	0.117	0.115	0.113	0.116	0.112	0.11	0.113	0.115	0.117	0.115	0.112



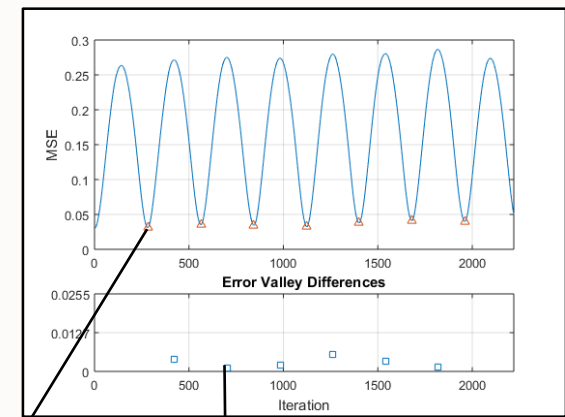
Operating Status Decision Boundary

Loaded Motor Error Statistical Analysis – MSE



Operating Status Decision Boundary

Loaded Motor Error Statistical Analysis – MSE Differences

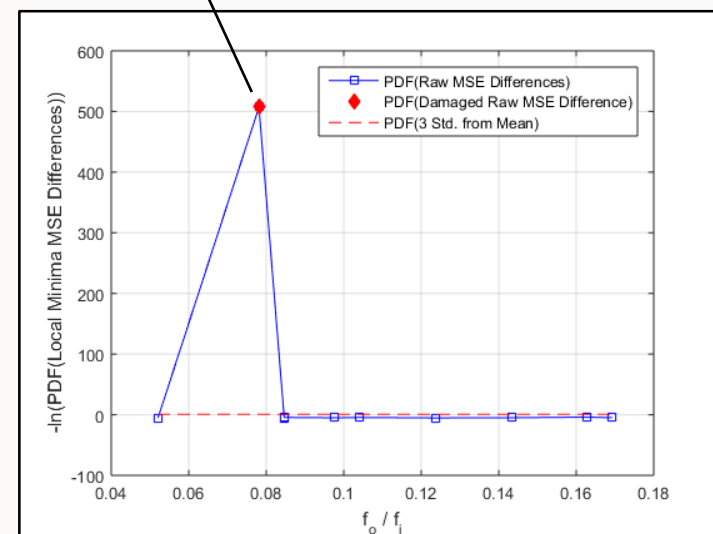
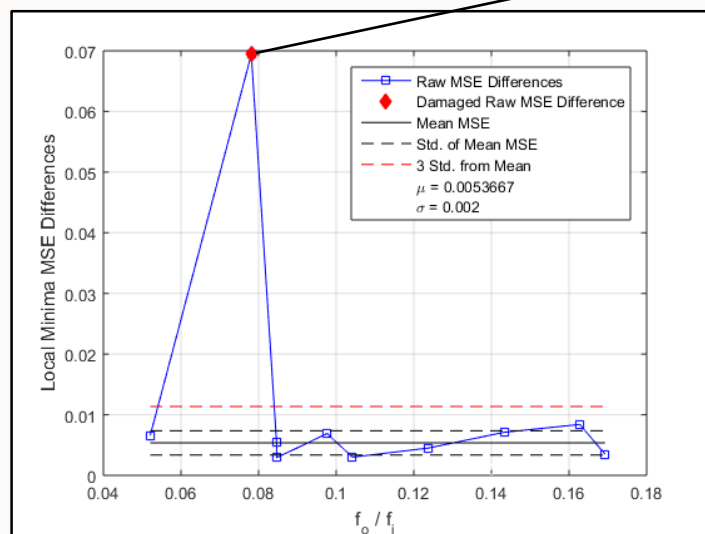
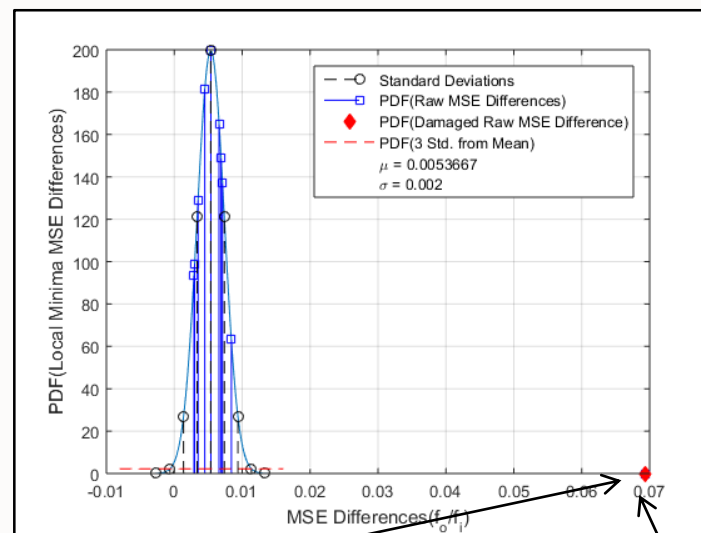


Fund. Freq (Hz)	60																				
Output Frequency (Hz)	Notes	f_o/f_i	Mean	Std.	Loaded Motor Local Minima MSE																
3.1250	F6	0.0521	0.0681	0.0033	0.065	0.071	0.065	0.072													
4.6875	Damaged F1	0.0781	0.1029	0.0505	0.132	0.055	0.084	0.211	0.098	0.056	0.084										
5.0781	F6	0.0846	0.0836	0.0048	0.085	0.079	0.08	0.083	0.088	0.079	0.082	0.094									
5.0781	F1	0.0846	0.0360	0.0035	0.031	0.035	0.034	0.032	0.038	0.041	0.04										
5.8594	F1	0.0977	0.0966	0.0057	0.098	0.081	0.1	0.1	0.092	0.098	0.098	0.101	0.096	0.101							
6.2500	F6	0.1042	0.0634	0.0033	0.066	0.066	0.065	0.062	0.069	0.065	0.061	0.063	0.061	0.056							
7.4219	F6	0.1237	0.1385	0.0066	0.124	0.132	0.138	0.138	0.134	0.139	0.137	0.137	0.146	0.152	0.145	0.141	0.137				
8.5938	F6	0.1432	0.1373	0.0140	0.137	0.138	0.15	0.146	0.149	0.142	0.152	0.145	0.152	0.139	0.137	0.13	0.129	0.109	0.104		
9.7656	F2	0.1628	0.1651	0.0081	0.16	0.161	0.17	0.154	0.156	0.172	0.163	0.168	0.172	0.173	0.152	0.154	0.177	0.178	0.169	0.159	0.16
10.1563	F2	0.1693	0.1141	0.0037	0.119	0.113	0.104	0.111	0.113	0.118	0.121	0.117	0.115	0.113	0.116	0.112	0.11	0.113	0.115	0.117	0.115

Fund. Freq (Hz)	60																				
Output Frequency (Hz)	Notes	f_o/f_i	Mean	Std.	Loaded Motor Local Minima MSE Differences																
3.1250	F6	0.0521	0.0066	0.0002	0.006	0.006	0.007														
4.6875	Damaged F1	0.0781	0.0694	0.0394	0.077	0.029	0.127	0.113	0.042	0.028											
5.0781	F6	0.0846	0.0054	0.0038	0.006	8E-04	0.003	0.005	0.009	0.002	0.013										
5.0781	F1	0.0846	0.0029	0.0016	0.004	0.001	0.002	0.006	0.003	0.002											
5.8594	F1	0.0977	0.0069	0.0063	0.017	0.019	3E-04	0.008	0.006	9E-05	0.003	0.005	0.005								
6.2500	F6	0.1042	0.0030	0.0022	3E-04	0.001	0.003	0.007	0.005	0.003	0.001	0.001	0.005								
7.4219	F6	0.1237	0.0045	0.0026	0.007	0.006	3E-04	0.004	0.005	0.002	3E-04	0.009	0.006	0.007	0.005	0.003					
8.5938	F6	0.1432	0.0071	0.0051	4E-04	0.012	0.005	0.004	0.007	0.01	0.007	0.007	0.012	0.003	0.007	1E-03	0.02	0.004			
9.7656	F2	0.1628	0.0084	0.0069	1E-03	0.009	0.015	0.002	0.016	0.009	0.005	0.004	0.001	0.021	0.002	0.022	0.001	0.009	0.01	9E-04	0.013
10.1563	F2	0.1693	0.0035	0.0021	0.005	0.009	0.007	0.001	0.006	0.003	0.004	0.003	0.001	0.003	0.004	0.002	0.004	0.001	0.002	0.002	0.003

Operating Status Decision Boundary

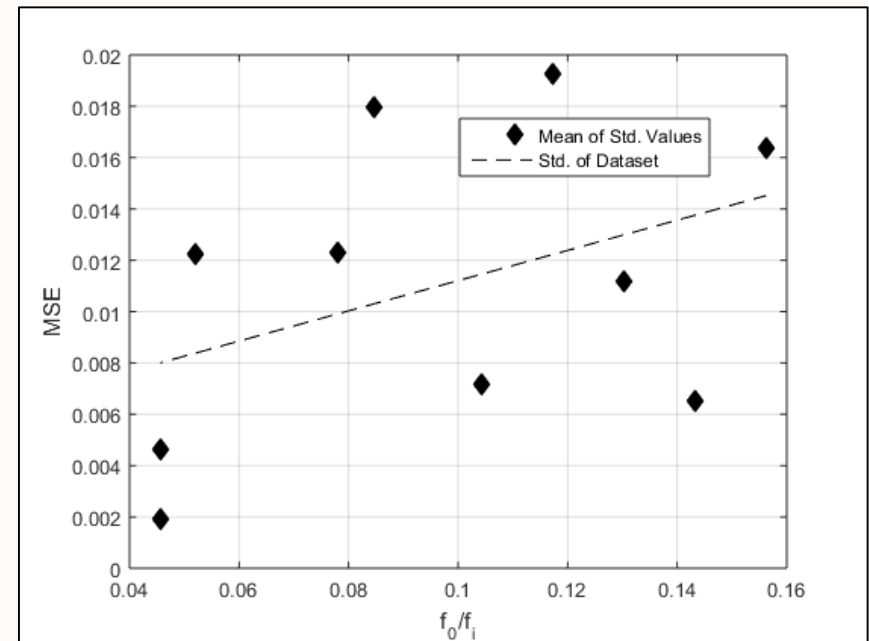
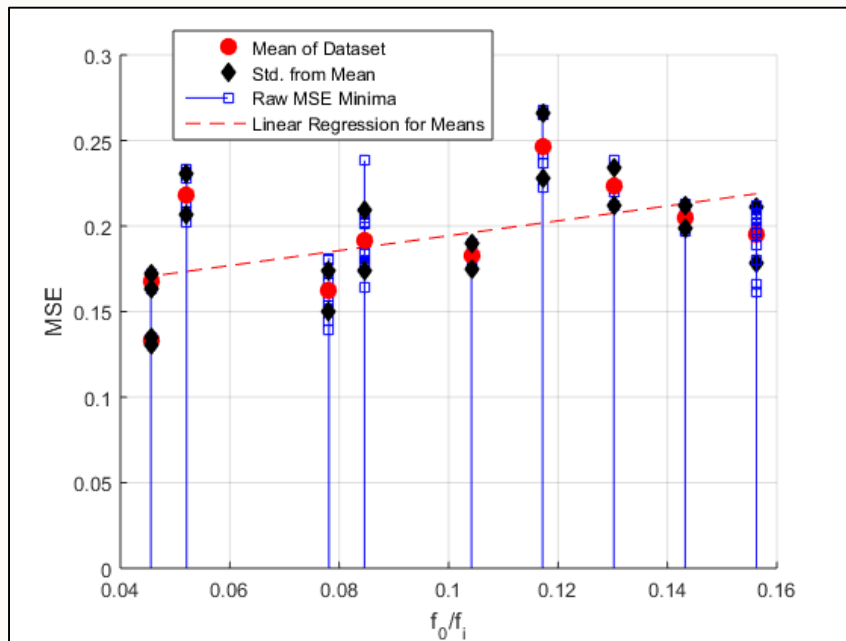
Loaded Motor Error Statistical Analysis – MSE Differences



Operating Status Decision Boundary

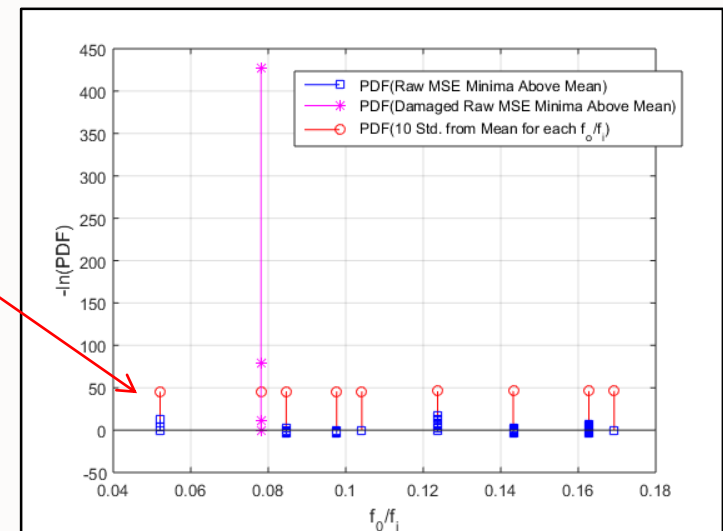
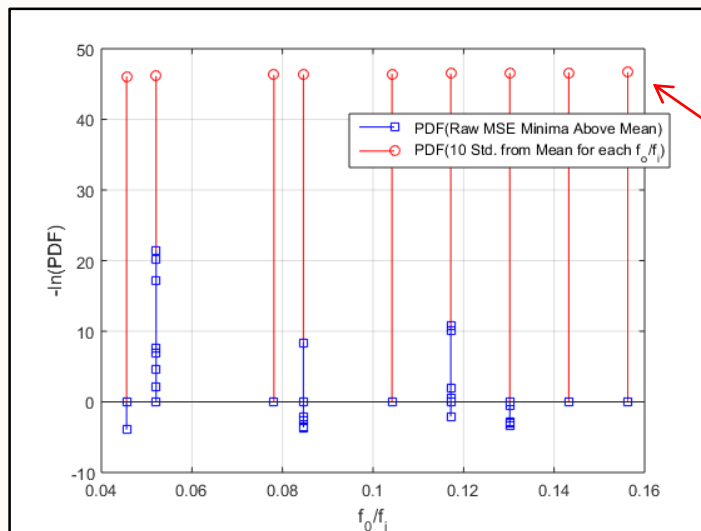
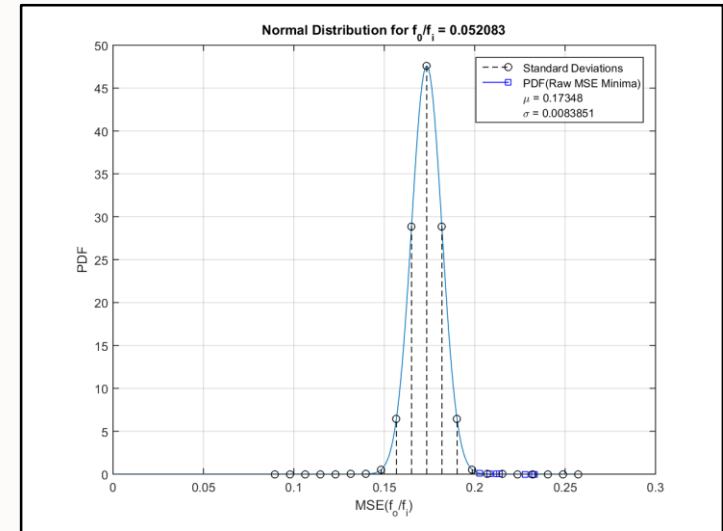
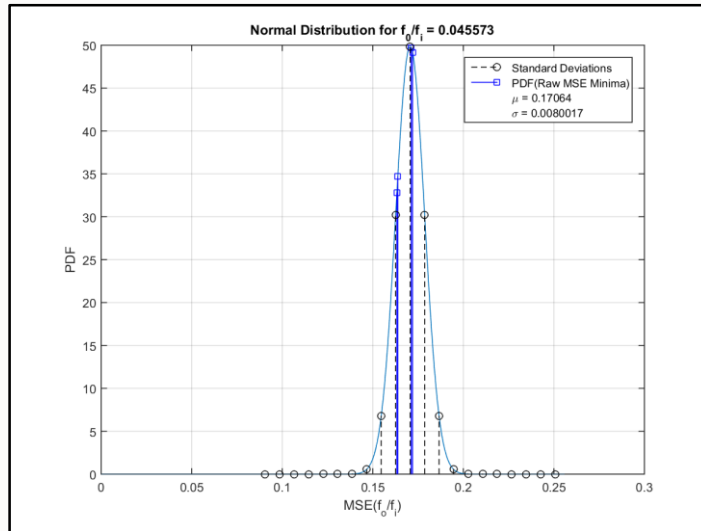
Unloaded Motor Error Statistical Analysis – MSE

Fund. Freq (Hz)	60																				
Output Frequency (Hz)	Notes	f_o/f_i	Mean	Std.	Unloaded Motor Local Minima MSE																
2.7344	F1	0.0456	0.1676	0.0040	0.171	0.164	0.172	0.163													
2.7344	F2	0.0456	0.1328	0.0015	0.132	0.135	0.131														
3.1250	F6	0.0521	0.1824	0.0059	0.175	0.19	0.182														
4.6875	F1	0.0781	0.2185	0.0113	0.232	0.228	0.214	0.233	0.212	0.203	0.208										
5.0781	F6	0.0846	0.2468	0.0172	0.242	0.222	0.237	0.265	0.267												
6.2500	F6	0.1042	0.2233	0.0097	0.223	0.22	0.239	0.212													
7.0313	F6	0.1172	0.2051	0.0058	0.203	0.202	0.21	0.197	0.213												
7.8125	F2	0.1302	0.1620	0.0118	0.18	0.167	0.145	0.167	0.181	0.163	0.167	0.154	0.139	0.157	0.156	0.158	0.172				
8.5938	F6	0.1432	0.1904	0.0172	0.178	0.164	0.192	0.179	0.202	0.184	0.238	0.19	0.202	0.205	0.203	0.184	0.185	0.176	0.176		
9.375	F6	0.1563	0.1947	0.0157	0.196	0.18	0.161	0.166	0.212	0.207	0.206	0.204	0.208	0.189	0.205	0.198	0.201				



Operating Status Decision Boundary

Unloaded Motor Error Statistical Analysis – MSE

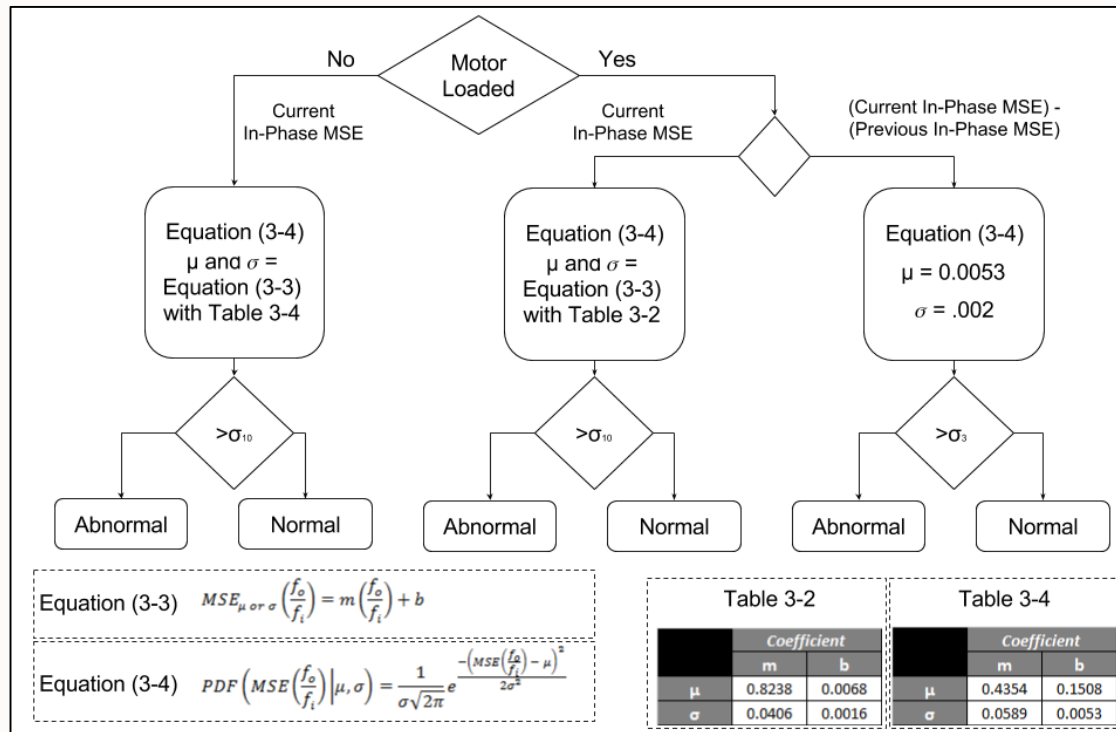


Loaded Data for Comparison

Operating Status Decision Boundary

Error Decision Boundary Thresholds

Error Type	State	PDF μ	PDF σ	Standard Deviation Threshold
In-Phase MSE	Loaded	Equation (3-3) with Table 3-2	Equation (3-3) with Table 3-2	10
	Unloaded	Equation (3-3) with Table 3-4	Equation (3-3) with Table 3-4	10
In-Phase MSE Differences	Loaded	0.0053	0.002	3
	Unloaded	N/A	N/A	N/A



Conclusion and Continued Research

01 Next Steps

02 Closing Statements



Conclusion and Continued Research

Next Steps

- Summary of work
 - Identified characteristics used to diagnosis cycloconverter status
 - Developed model that uses these characteristics to find an error value
 - Defined decision boundaries based on said error
 - Strong foundation on which further research can evolve
- Improvements
 - Consider other frequency modulation terms
 - Improved harmonic slope estimator
 - Improved output frequency estimator
- Next Steps
 - Modify current algorithms for real time system



