

# An Oscillating Reaction Network With an Exact Closed-Form Time-Domain Solution: Solution Derivation

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## 1 Preliminaries

This write-up provides details on the derivation of the time domain solution for the reaction network depicted in Fig. 1. Recall that the reaction network is constructed to be a system of linear ODEs. As such, the time domain solution is an initial value problem (IVP).

The reaction network has 8 parameters. There are 6 kinetic constants,  $k_i$ ,  $i \in \{1, 2, 3, 4, 5, 6\}$ . And there are two initial concentrations,  $x_n(0)$ ,  $n \in \{1, 2\}$ , where  $x_n(0)$  is the initial concentration for  $S_n$ .

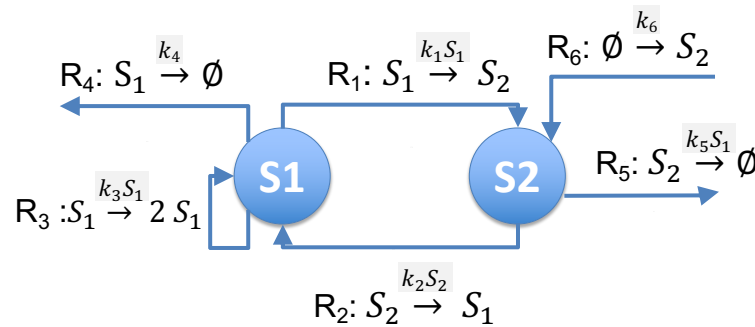
Because the reaction network can be described as a system of linear system (by construction), we know that oscillations are sinusoids. Let  $x_n(t)$  be the concentration of species  $S_n$  at time  $t$ . Then, an oscillating solution has the form

$$x_n(t) = \alpha_n \sin(\theta_n t + \phi_n) + \omega_n,$$

where  $\alpha_n$  is the amplitude of the sinusoid for  $S_n$ ,  $\theta_n$  is its frequency,  $\phi_n$  is its phase, and  $\omega_n$  is the DC offset (the mean value of the sinusoid over time). It turns out that both species have the same frequency, as we show shortly. So,  $\theta_n = \theta$ , and there are just 7 parameters. We refer to  $\alpha_n, \theta, \phi_n, \omega_n$  as the **oscillation characteristics (OC)** of the reaction network.

We use the following notation:

- $\mathbf{A}$  - Jacobian matrix
- $\alpha_n$  - amplitude of oscillation for species  $n$
- $\mathbf{c} = \begin{pmatrix} c_1 \\ c_2 \end{pmatrix}$  - constants associated with the homogeneous solution
- $\Delta$  -  $\det \mathbf{A}$
- $\mathbf{F}(t)$  - fundamental matrix
- $i$  - indexes constants
- $k_i, k_d$  - positive constant
- $K$  - number of constants
- $\lambda$  - eigenvalue
- $n$  - indexes species
- $N$  - number of species
- $\omega_n$  - offset of species  $n$
- $\phi_n$  - phase in radians
- $t$  - time
- $\tau$  -  $\text{tr}(\mathbf{A})$
- $\theta$  - frequency in radians
- $\mathbf{u}$  - forced input (kinetic constants for zeroth order rates)  $\mathbf{x}$  ( $N \times 1$ ) is the state vector



**Figure 1** Reaction network that creates oscillations in the chemical species  $S_1, S_2$ . The reaction network is designed so that its time domain solution is a system of linear differential equations. The text describes constraints on the kinetic constants ( $k_i$ ) and initial conditions of the chemical species to create an oscillator such that species concentrations are non-negative, a requirement for biological feasibility.

- $\dot{\mathbf{x}}(t)$  - derivative w.r.t. time of  $\mathbf{x}$
- $x_n(t)$  - time varying concentration of species  $n$

Since we have constructed the reaction network so that the dynamics can be described as a system of linear ODEs, it can be described using the vector differential equation:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{u}$$

where the Jacobian matrix is  $\mathbf{A} = \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix}$

## 2 Jacobian and Eigenvalues

Here, we calculate the eigenvalues for the reaction network described in the text. If there is an oscillating solution for this system, then the eigenvalues of  $\mathbf{A}$  must be pure imaginary. Since this is a two state system, this means that if  $\theta i$  is an eigenvalue, then  $-\theta i$  must also be an eigenvalue. This means that  $\theta_1 = \theta = \theta_2$ , which justifies our previous claim.

Next we develop the conditions for the Jacobian  $\mathbf{A}$  to have a pure imaginary eigenvalues. The determinant of  $\mathbf{A}$  is  $\det(\mathbf{A}) = a_{11}a_{22} - a_{12}a_{21} = \Delta$ . The trace of  $\mathbf{A}$  is  $\text{tr}(\mathbf{A}) = a_{11} + a_{22} = \tau$ . So, the eigenvalues  $\lambda$  are in  $\frac{1}{2}(-\tau \pm \sqrt{\tau^2 - 4\Delta})$ . We get pure imaginary eigenvalues if the following constraints hold:

- $\tau = 0$
- $\Delta > 0$ .

Now, we analyze  $\mathbf{A}$  for the reaction network.

$$\mathbf{A} = \begin{pmatrix} k_3 - k_1 & k_2 \\ k_1 - k_5 & -k_2 \end{pmatrix}$$

and

$$\mathbf{u} = \begin{pmatrix} -k_4 \\ k_6 \end{pmatrix}$$

So the trace and determinant are:

$$\begin{aligned} \tau &= k_3 - k_1 - k_2 \\ \Delta &= (k_3 - k_1)(-k_2) - k_2(k_1 - k_5) \\ &= k_2(k_5 - k_3) \end{aligned}$$

To obtain purely imaginary solutions, we require that  $\tau = 0$  and  $\Delta > 0$ . The former implies that  $k_3 = k_1 + k_2$ . The latter implies that that  $k_5 > k_3$ . We define  $k_d = k_5 - k_3 > 0$ . Applying the foregoing to the  $\mathbf{A}$  matrix, we first note that

$$\begin{aligned} k_1 - k_5 &= k_1 - k_3 - k_d \\ &= k_3 - k_2 - k_3 - k_d \\ &= -k_2 - k_d \end{aligned}$$

Applying the constraints, we see that

$$\mathbf{A} = \begin{pmatrix} k_2 & k_2 \\ -k_2 - k_d & -k_2 \end{pmatrix}$$

Observe that  $\Delta = k_2 k_d$ . As a result  $\theta = \pm\sqrt{\Delta} = \pm\sqrt{k_2 k_d}$ . Hereafter, we drop the  $\pm$ .

### 3 Eigenvectors and Fundamental Matrix

We find the eigenvectors of  $\mathbf{A}$  as an intermediate step to finding the time domain solution.

First, observe that that since  $k_d > 0$ ,  $\mathbf{A}$  is nonsingular, and so we can calculate eigenvectors directly.

$$\mathbf{w}_1 = \begin{pmatrix} -\frac{k_2}{k_2 + k_d} + \frac{i\theta}{k_2 + k_d} \\ 1 \end{pmatrix}$$

for the eigenvalue  $\lambda_1 = -\sqrt{k_d k_2}$ .

$$\mathbf{w}_2 = \begin{pmatrix} -\frac{k_2}{k_2+k_d} - \frac{i\theta}{k_2+k_d} \\ 1 \end{pmatrix}$$

for the eigenvalue  $\lambda_1 = \sqrt{k_d k_2}$ .

The solution to the initial value problem is a sum of eigenvectors multiplied by their eigenvalues. The **fundamental matrix**  $\mathbf{F}$  of a system of linear ODEs has a column for each eigenvector multiplied by its eigenvalue,  $\mathbf{w}_n e^{\lambda_n}$ .

Rather than writing  $\mathbf{F}(t)$  immediately, we first observe that it can be transformed into a real valued matrix. We can use the decomposition of eigenvectors into real and imaginary parts along with Euler formulas to express  $\mathbf{F}(t)$  in terms of *sin* and *cos*. We do some further simplifications by taking linear combinations of the columns of the fundamental matrix, transformations that change the basis for the solution space but not the solution space itself.

$$\mathbf{F}(t) = \begin{pmatrix} -\frac{k_2 \cos(t\theta)}{k_2+k_d} + \frac{\theta \sin(t\theta)}{k_2+k_d} & -\frac{k_2 \sin(t\theta)}{k_2+k_d} - \frac{\theta \cos(t\theta)}{k_2+k_d} \\ \cos(t\theta) & \sin(t\theta) \end{pmatrix}$$

## 4 Solving the Initial Value Problem

We proceed in the usual way to solve an IVP:

- 1 Find the solution to the homogeneous system  $\dot{\mathbf{x}}^H(t) = \mathbf{A}\mathbf{x}^H(t)$ .
- 2 Find a particular solution such that  $\dot{x}^P(t) = \mathbf{A}\mathbf{x}^P(t) + \mathbf{u}$
- 3  $\mathbf{x}(t) = \begin{pmatrix} c_1 x_1^H(t) \\ c_2 x_2^H(t) \end{pmatrix} + \mathbf{x}^P(t)$ , where  $\mathbf{c}$  is determined by the initial conditions.

$\mathbf{x}^H(t) = \mathbf{F}(t)\mathbf{c}$ , where  $\mathbf{c}$  is a vector of unknown constants that are determined based on initial conditions, initial conditions are the initial concentrations of  $S_1$ ,  $S_2$ .

We assume that  $\mathbf{x}^P(t) = \mathbf{F}(t)\mathbf{v}$ . This means that

$$\begin{aligned} \dot{\mathbf{x}}^P(t) &= \dot{\mathbf{F}}(t)\mathbf{v} + \mathbf{F}(t)\dot{\mathbf{v}} \\ \dot{\mathbf{F}}(t)\mathbf{v} + \mathbf{F}(t)\dot{\mathbf{v}} &= \mathbf{A}\mathbf{F}(t)\mathbf{v} + \mathbf{u} \\ \mathbf{A}\mathbf{F}(t)\mathbf{v} + \mathbf{F}(t)\dot{\mathbf{v}} &= \mathbf{A}\mathbf{F}(t)\mathbf{v} + \mathbf{u} \\ \mathbf{F}(t)\dot{\mathbf{v}} &= \mathbf{u} \\ \mathbf{v} &= \int (\mathbf{F}^{-1}(t)\mathbf{u}) dt \end{aligned}$$

Calculating this integral (with help from the python package `sympy`), we have

$$\begin{aligned} \mathbf{x}^P(t) &= \mathbf{F}(t)\mathbf{v} \\ &= \begin{pmatrix} \frac{-k_2^2 k_4 \cos(t\theta) - k_2^2 k_4 + k_2^2 k_6 \cos(t\theta) + k_2^2 k_6 - k_2 k_4 k_d \cos(t\theta) - k_2 k_4 k_d + k_2 k_4 \theta \sin(t\theta) - k_2 k_6 \theta \sin(t\theta) + k_4 k_d \theta \sin(t\theta) + k_6 \theta^2}{\theta^2 (k_2 + k_d)} \\ \frac{k_2 k_4 \cos(t\theta) + k_2 k_4 - k_2 k_6 \cos(t\theta) - k_2 k_6 + k_4 k_d \cos(t\theta) + k_4 k_d}{\theta^2} \end{pmatrix} \end{aligned}$$

$$\begin{aligned}
\mathbf{x}(t) &= \mathbf{x}^H(t) + \mathbf{x}^P(t) \\
&= \begin{pmatrix} -\frac{k_2 \cos(t\theta)}{k_2+k_d} + \frac{\theta \sin(t\theta)}{k_2+k_d} & -\frac{k_2 \sin(t\theta)}{k_2+k_d} - \frac{\theta \cos(t\theta)}{k_2+k_d} \end{pmatrix} \begin{pmatrix} c_1 \\ c_2 \end{pmatrix} \\
&\quad + \begin{pmatrix} \frac{-k_2^2 k_4 \cos(t\theta) - k_2^2 k_4 + k_2^2 k_6 \cos(t\theta) + k_2^2 k_6 - k_2 k_4 k_d \cos(t\theta) - k_2 k_4 k_d + k_2 k_4 \theta \sin(t\theta) - k_2 k_6 \theta \sin(t\theta) + k_4 k_d \theta \sin(t\theta) + k_6 \theta^2}{\theta^2(k_2+k_d)} \\ \frac{k_2 k_4 \cos(t\theta) + k_2 k_4 - k_2 k_6 \cos(t\theta) - k_2 k_6 + k_4 k_d \cos(t\theta) + k_4 k_d}{\theta^2} \end{pmatrix}
\end{aligned}$$

We find  $c_1, c_2$  by solving

$$\begin{aligned}
\mathbf{x}(0) &= \begin{pmatrix} x_1(0) \\ x_2(0) \end{pmatrix} \\
&= \begin{pmatrix} -\frac{k_2 \cos(t\theta)}{k_2+k_d} + \frac{\theta \sin(t\theta)}{k_2+k_d} & -\frac{k_2 \sin(t\theta)}{k_2+k_d} - \frac{\theta \cos(t\theta)}{k_2+k_d} \end{pmatrix} \begin{pmatrix} c_1 \\ c_2 \end{pmatrix} \\
&\quad + \begin{pmatrix} \frac{-k_2^2 k_4 \cos(t\theta) - k_2^2 k_4 + k_2^2 k_6 \cos(t\theta) + k_2^2 k_6 - k_2 k_4 k_d \cos(t\theta) - k_2 k_4 k_d + k_2 k_4 \theta \sin(t\theta) - k_2 k_6 \theta \sin(t\theta) + k_4 k_d \theta \sin(t\theta) + k_6 \theta^2}{\theta^2(k_2+k_d)} \\ \frac{k_2 k_4 \cos(t\theta) + k_2 k_4 - k_2 k_6 \cos(t\theta) - k_2 k_6 + k_4 k_d \cos(t\theta) + k_4 k_d}{\theta^2} \end{pmatrix}
\end{aligned}$$

The result is

$$\begin{aligned}
x_1(t) &= \frac{1}{\theta} \left( -\frac{k_2 \sin(t\theta)}{k_2+k_d} - \frac{\theta \cos(t\theta)}{k_2+k_d} \right) (-k_2 x_1(0) - k_2 x_2(0) + k_6 - k_d x_1(0)) \\
&\quad + \frac{1}{\theta^2} \left( -\frac{k_2 \cos(t\theta)}{k_2+k_d} + \frac{\theta \sin(t\theta)}{k_2+k_d} \right) (-2k_2 k_4 + 2k_2 k_6 - 2k_4 k_d + \theta^2 x_2(0)) \\
&\quad + \frac{1}{\theta^2(k_2+k_d)} (-k_2^2 k_4 \cos(t\theta) - k_2^2 k_4 + k_2^2 k_6 \cos(t\theta) + k_2^2 k_6 + k_6 \theta^2 - k_2 k_4 k_d) \\
&\quad + \frac{1}{\theta^2(k_2+k_d)} (-k_2 k_4 k_d \cos(t\theta) + k_2 k_4 \theta \sin(t\theta) - k_2 k_6 \theta \sin(t\theta) + k_4 k_d \theta \sin(t\theta))
\end{aligned} \tag{1}$$

$$\begin{aligned}
x_2(t) &= \frac{1}{\theta} (-k_2 x_1(0) - k_2 x_2(0) + k_6 - k_d x_1(0)) \sin(t\theta) \\
&\quad + \frac{1}{\theta^2} (-2k_2 k_4 + 2k_2 k_6 - 2k_4 k_d + \theta^2 x_2(0)) \cos(t\theta) \\
&\quad + \frac{1}{\theta^2} (k_2 k_4 \cos(t\theta) + k_2 k_4 - k_2 k_6 \cos(t\theta) - k_2 k_6 + k_4 k_d \cos(t\theta) + k_4 k_d)
\end{aligned} \tag{2}$$

## 5 Formulas for Oscillation Characteristics

Our final task is to restructure  $\mathbf{x}(t)$  to isolate the oscillation characteristics  $\theta, \alpha_n, \phi_n, \omega_n$ . From this The first step is to factor Eq. (1) and Eq. (2) so that

$$x_n(t) = a_n \cos(\theta t) + b_n \sin(\theta t) + \omega_n \tag{3}$$

That is, the sum of terms that are not multiplied by  $\cos, \sin$  will constitute the DC offset. From Eq. (3), we calculate  $\alpha_n, \phi_n$  using the trigonometric equality  $a_n \cos(\theta t) + b_n \sin(\theta t) = \sqrt{a_n^2 + b_n^2} \sin(\theta t + \tan^{-1} \frac{a_n}{b_n})$ . Thus,  $\alpha_n = \sqrt{a_n^2 + b_n^2}$ , and  $\phi_n = \tan^{-1} \frac{a_n}{b_n}$ .

The results are:

- $\theta = \sqrt{k_2 k_d}$
- $\alpha_1 = \frac{\sqrt{\nu_1}}{\theta^2(k_2 + k_d)}$

$$\begin{aligned} \nu_1 = & \theta^2 (k_2^2 x_1(0) + k_2^2 x_2(0) - k_2 k_4 + k_2 k_d x_1(0) - k_4 k_d + \theta^2 x_2(0))^2 \\ & + (k_2^2 k_4 - k_2^2 k_6 + k_2 k_4 k_d + k_2 \theta^2 x_1(0) - k_6 \theta^2 + k_d \theta^2 x_1(0))^2 \end{aligned}$$

- $\alpha_2 = \frac{\sqrt{\theta^2(k_2 x_1(0) + k_2 x_2(0) - k_6 + k_d x_1(0))^2 + (k_2 k_4 - k_2 k_6 + k_4 k_d - \theta^2 x_2(0))^2}}{\theta^2}$
- $\phi_1 = \tan^{-1} \left( \frac{k_2^2 k_4 - k_2^2 k_6 + k_2 k_4 k_d + k_2 \theta^2 x_1(0) - k_6 \theta^2 + k_d \theta^2 x_1(0)}{\theta(k_2^2 x_1(0) + k_2^2 x_2(0) - k_2 k_4 + k_2 k_d x_1(0) - k_4 k_d + \theta^2 x_2(0))} \right) + \pi_1$
- $\phi_2 = \tan^{-1} \left( \frac{k_2 k_4 - k_2 k_6 + k_4 k_d - \theta^2 x_2(0)}{\theta(k_2 x_1(0) + k_2 x_2(0) - k_6 + k_d x_1(0))} \right) + \pi_2$
- $\omega_1 = \frac{-k_2^2 k_4 + k_2^2 k_6 - k_2 k_4 k_d + k_6 \theta^2}{k_2 \theta^2 + k_d \theta^2}$
- $\omega_2 = \frac{k_2 k_4 - k_2 k_6 + k_4 k_d}{\theta^2}$

$\pi_1, \pi_2$  arise from technical conditions related to taking the inverse of the tangent function. Tangent is only defined over a range of  $\pi$  since it is calculated from the ration of  $a_n$  to  $b_n$ . Hence we cannot distinguish between to positive values of these number, and two negative values of these numbers.

$$\begin{aligned} cond_1 = & \frac{k_2^2 x_1(0)}{k_2 \theta + k_d \theta} + \frac{k_2^2 x_2(0)}{k_2 \theta + k_d \theta} + \frac{k_2 k_4 \theta}{k_2 \theta^2 + k_d \theta^2} - \frac{2k_2 k_4}{k_2 \theta + k_d \theta} - \frac{k_2 k_6 \theta}{k_2 \theta^2 + k_d \theta^2} \\ & + \frac{k_2 k_6}{k_2 \theta + k_d \theta} + \frac{k_2 k_d x_1(0)}{k_2 \theta + k_d \theta} + \frac{k_4 k_d \theta}{k_2 \theta^2 + k_d \theta^2} - \frac{2k_4 k_d}{k_2 \theta + k_d \theta} + \frac{\theta x_2(0)}{k_2 + k_d} \end{aligned}$$

$$\begin{aligned} \pi_1 = & \pi \text{ if } cond_1 < 0 \\ = & 0 \text{ otherwise} \end{aligned}$$

$$cond_2 = \frac{k_2 x_1(0)}{\theta} + \frac{k_2 x_2(0)}{\theta} - \frac{k_6}{\theta} + \frac{k_d x_1(0)}{\theta}$$

$$\begin{aligned} \pi_2 = & \pi \text{ if } cond_2 > 0 \\ = & 0 \text{ otherwise} \end{aligned}$$