

## Chapter -

### Transistor Biasing & Stabilisation -

The main function of a <sup>Transistor is</sup> amplifier (amp<sup>r</sup>).  
Amplifiers, basically it amplify the weak signal.  
→ actually it increases the magnitude of signal without any change in shape.

And the condition which allow the transistor to give desired  $Q_p$  is called Biasing.

In other words,

Transistor Biasing is the process of setting a transistor DC operating voltage or current condition to the correct level, so that any AC  $i_p$  signal can be amplified correctly by the transistor.

There are many factors which affects the operation of a transistor.  $Q$ -point is one of them.

$Q$  point is the operating point of a transistor ( $I_{CQ}$ ,  $V_{CEQ}$ ) at which it is biased. The concept of  $Q$ -point is used when the transistor act as an amplifier & hence operated in active region.

### Biasing of Transistor

Before applying any AC  $i_p$  biasing is applied for proper functioning.



for active region  $J_E$  is FB &  $J_C$  is FB.  
→ After applying DC voltage, DC current starts to flow in circuit. Which can be plot by  $\varphi_p$  char of transistor.

→ The Q point values can be calculated by drawing the intersection of  $\varphi_p$  char & Load line.\*

\* DC load line is the locus of  $I_C$  &  $V_{CE}$  at which BJT remain in active region. (i.e. it represents all the possible combination of  $I_C$  &  $V_{CE}$  for a given amp<sup>r</sup>.

→ Factor affects the operating point.

there are some factors which try to shift Q-point

i) Variation of parameters -

we know  $\alpha$  &  $\beta$  are decided at the time of manufacturing.

But what a component is replaced after damage, And Ideally it is not possible for two transistor with same  $\alpha$  or  $\beta$ . so they may change Q-point.

ii) Variation of Temp -



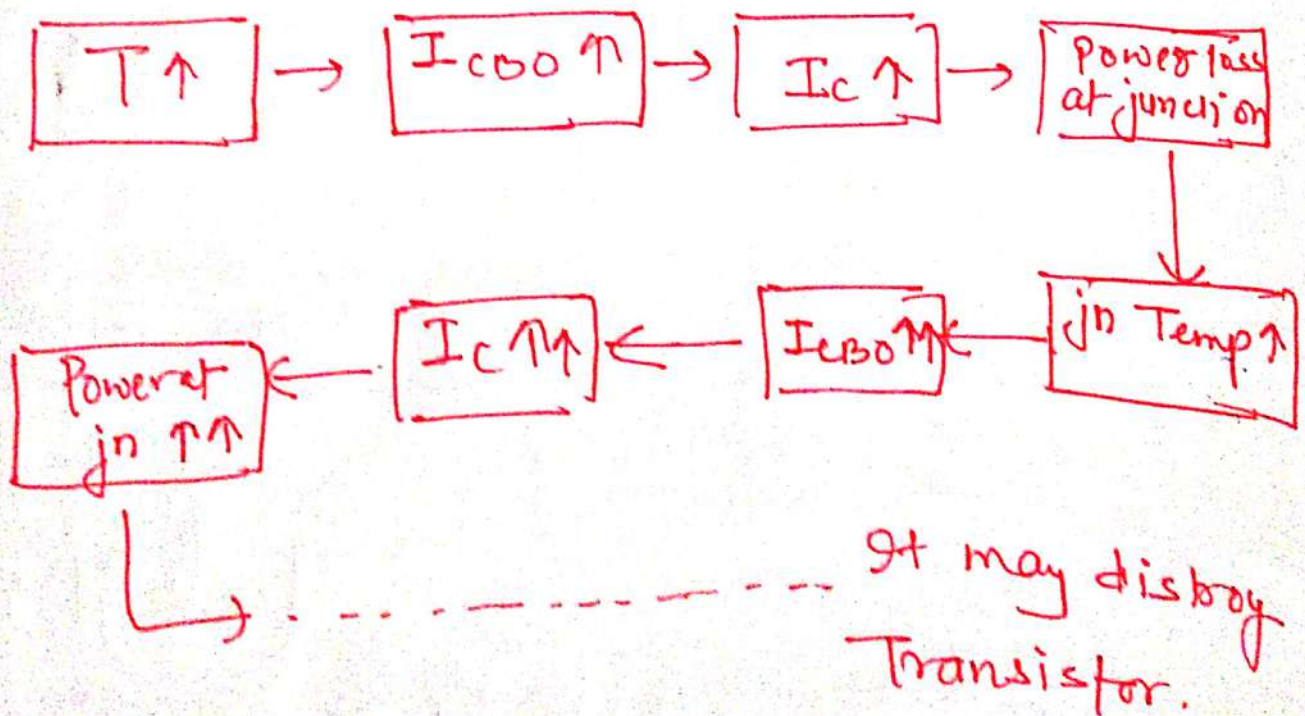
As we know  $I_C$  is dependent on  $I_{CBO}$

$$I_C = \beta I_E + (\beta + 1) I_{CBO}$$

&  $I_{CBO}$  is highly dependent to temp as it is developed by minority charge carrier.

So, temp can also affect Q-point.

Thermal runaway — If temp  $\uparrow$  rapidly it may convert to thermal runaway.





## Methods of Transistor Biasing -

There are four methods of transistor biasing.

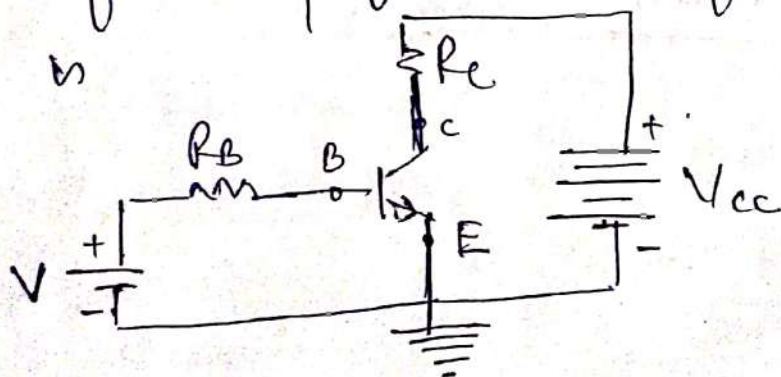
- i) Fixed Bias
- ii) Collector to Base Bias.
- iii) Emitter Bias.
- iv) Self Bias or voltage divider Bias.

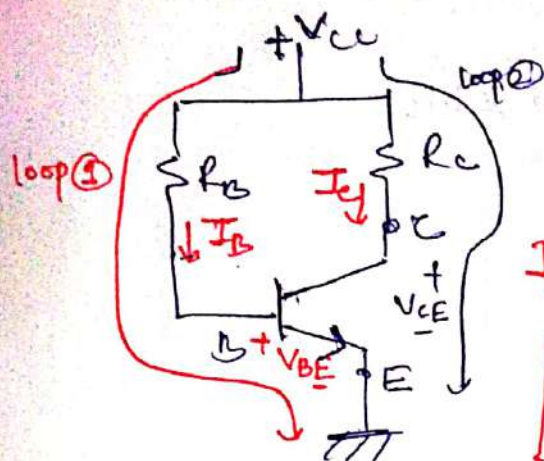
### i) Fixed Bias Circuit -

The Fixed Bias Circuit is the simplest transistor DC Biasing.

Even pnp tr is used in place of npn the configuration will be same by changing all the current direction & voltage polarities.

After simplification the final circuit obtain





By applying KVL in loop ①

$$+V_{CC} - R_B I_B - V_{BE} = 0$$

$$I_B R_B = -V_{BE} + V_{CC}$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

Circuit with only one Battery.

$V_{CC}$  &  $V_{BE}$  are constant values, so  $I_B$  depends upon  $R_B$ .

By applying KVL in loop ②

$$+V_{CC} - I_C R_C - V_{CE} = 0$$

$$V_{CE} = V_{CC} - R_C I_C$$

$$I_C = \beta I_B + I_{CBO}$$

$$I_C = \beta I_B \quad (\text{assume } I_{CBO} = 0)$$

$$(\text{Actually } I_{CBO} \approx 0)$$

$$I_C = \beta I_B$$

$$V_{CE} = V_C - V_E$$



Stability factor of fixed Bias.

$$S = \frac{\beta + 1}{1 - \beta \frac{dI_B}{dI_C}}$$

for fixed Bias

$$\frac{dI_B}{dI_C} = 0$$

$$\therefore, S = \frac{\beta + 1}{1 - \beta \cdot 0} = \beta + 1$$

Advantage

Simple in connection  
construction is simple

Disadvantage

Poor thermal stability.

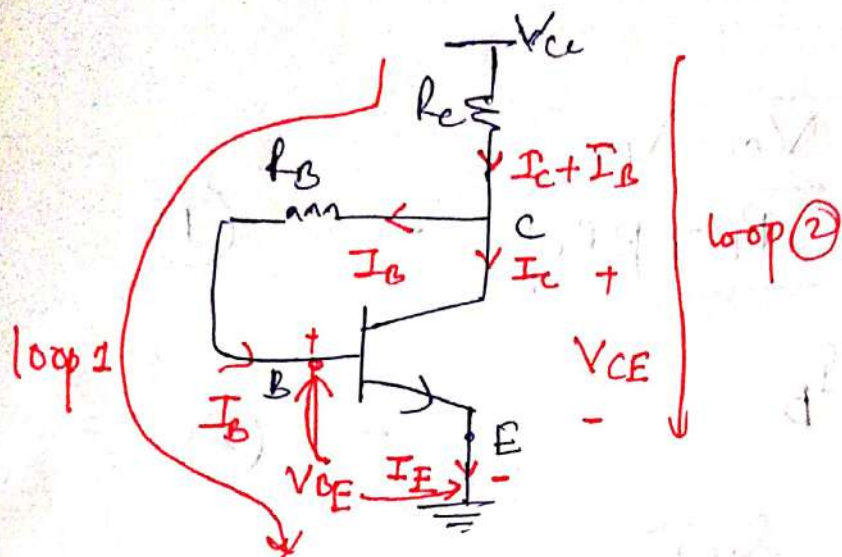
Collector to Base Bias Ckt -

In this Configuration, bias voltage to the base is given by collector instead of direct  $V_{CC}$  (as in fixed biasing ckt).

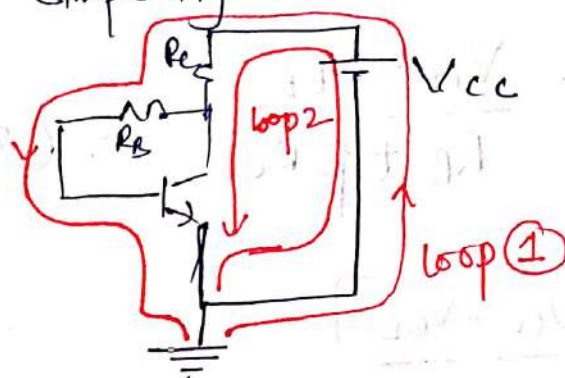
$R_B$  is used as feedback.

for DC analysis circuit shown is figure.





for simplicity we can redraw the circuit



the loops drawn in ckt 1 & 2 are same

$$+V_{cc} - R_c(I_c + I_b) - R_b I_b - V_{BE} = 0 \quad \text{--- (A)}$$

$$\begin{aligned} V_{cc} - V_{BE} &= R_c(I_c + I_b) + R_b I_b \\ &= I_b(R_c + R_b) + R_c I_c \\ &= I_b(R_c + R_b) + \beta I_b R_c \\ &= I_b(R_c + R_b + \beta R_c) \end{aligned}$$

$$\begin{aligned} V_{cc} - V_{BE} &= I_b(R_b + R_c(1 + \beta)) \\ I_b &= \frac{V_{cc} - V_{BE}}{R_b + R_c(1 + \beta)} \end{aligned}$$

As  $\beta$  is very large so,

$$\beta + 1 \approx \beta$$

so 
$$I_B = \frac{V_{CC} - V_{BE}}{R_B + \beta R_E} \quad \text{--- (1)}$$

$$I_C \approx \beta I_B \quad \text{--- (2)}$$

from (1) & (2)

$$I_C = \beta \frac{V_{CC} - V_{BE}}{R_B + \beta R_E} \quad \text{--- (3)}$$

$$I_C = \frac{V_{CC} - V_{BE}}{R_E + R_B/\beta}$$

(1) &  $V_{CC} \gg V_{BE}$

$$I_C \approx \frac{V_{CC}}{R_E + R_B/\beta} \quad \text{--- (4)}$$

from loop (2)

$$V_{CC} = V_{CE} + (I_C + I_B) R_E$$

as  $I_C \gg I_B$

so 
$$V_{CE} = V_{CC} - I_C R_E \quad \text{--- (5)}$$



Stability factor

$$S = \frac{1 + \beta}{1 - \beta \frac{dI_B}{dI_C}}$$

from eq<sup>n</sup> (A)

$$V_{CC} = V_{BE} + (I_B + I_C)R_C + I_B R_B$$

$$V_{CC} - V_{BE} - I_C R_C = I_B (R_C + R_B)$$

$$I_B = \frac{V_{CC} - V_{BE} - I_C R_C}{R_C + R_B}$$

differentiating w.r.t  $I_C$

$$\frac{dI_B}{dI_C} = \frac{0 - 0 - R_C}{R_C + R_B}$$

$$= \frac{-R_C}{R_C + R_B}$$

$$S = \frac{1 + \beta}{1 - \beta \left( \frac{-R_C}{R_C + R_B} \right)}$$

$$S = \frac{1 + \beta}{1 + \beta \left( \frac{R_C}{R_C + R_B} \right)}$$



Advantage —

Simple Biasing, only  $R_E$  is required.

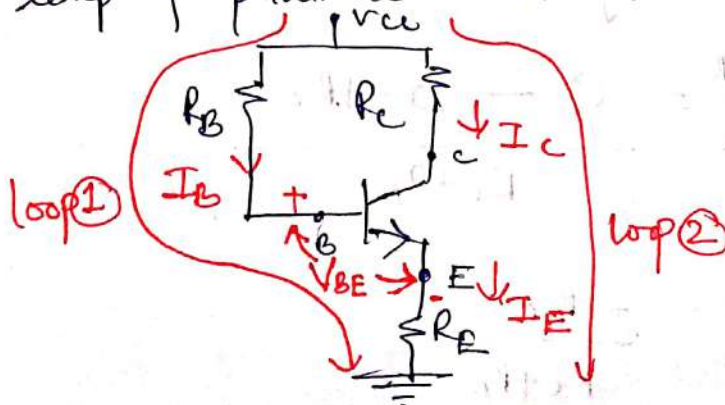
Disadvantage

$\beta$  is very high.

### Emitter Bias

It is also known as base bias with emitter feedback.

It contains  $R_E$  to improve stability. The more stable a configuration, the less its response will change due to undesirable change in temp. & parameter variation.



KVL in loop ①

$$V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0 \quad \text{--- ①}$$

$$I_E = (\beta + 1) I_B \quad \text{--- ②}$$

from ① & ②

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1) R_E} \quad \text{--- ③}$$



$$I_C = \beta I_B$$

$$I_C = \frac{V_{CC} - V_{BE}}{R_E + R_B/\beta}$$

as  $V_{CC} \gg V_{BE}$

$$I_C = \frac{V_{CC}}{R_E + R_B/\beta}$$

from loop (2)

$$V_{CE} + I_E R_E - V_{CC} + I_C R_C = 0$$

Since  $I_E \approx I_C$

$$V_{CE} + I_C R_E - V_{CC} + I_C R_C = 0$$

$$V_{CE} = V_{CC} - I_C (R_E + R_C)$$

$$V_E = I_E R_E = I_C R_E$$

$$V_C = V_{CC} - I_C R_C$$

Stability factor.

from eqn (1)

$$V_{BE} + I_E R_E - V_{CC} + I_B R_B = 0 \quad \text{--- (A)}$$

$$I_E = I_B + I_C \quad \text{--- (B)}$$

from eqn (A) & (B)

$$V_{BE} + (I_B + I_C) R_E - V_{CC} + I_B R_B = 0$$



$$I_B = \frac{V_{CC} - V_{BE} - I_C R_E}{R_E + R_B}$$

diff. w.r.t  $I_C$

$$\frac{dI_B}{dI_C} = \frac{0 - 0 - R_E}{R_E + R_B}$$

$$S = \frac{1 + \beta}{1 - \beta \left( -R_E / (R_E + R_B) \right)}$$

$$S = \frac{1 + \beta}{1 + \beta \left( \frac{R_E}{R_E + R_B} \right)}$$

Advantage  
Has better stabilization.



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