

# EECE423-01: 현대제어이론

## Modern Control Theory

### Chapter 4: Response of LTI Systems

Kim, Jung Hoon



◆ The main topics of this chapter are

1. Basic Concepts of Linear Systems

2. Equivalent State-Space Systems

3. Matrix Exponential

4. Solutions to LTI Systems

Appendix: Solutions to LTV Systems

# **1. Basic Concepts of Linear Systems**

## ◆ Causality

- Intuitive interpretation: If a system has the property that the output *before* some time  $t$  does not depend on the input *after* time  $t$ .

Such a system is called *causal*.

- Mathematical interpretation: An operator  $\mathbf{T}$  is said to be *causal* if

$$(\mathbf{T}f)_\tau = (\mathbf{T}f_\tau)_\tau, \quad \forall \tau \geq 0$$

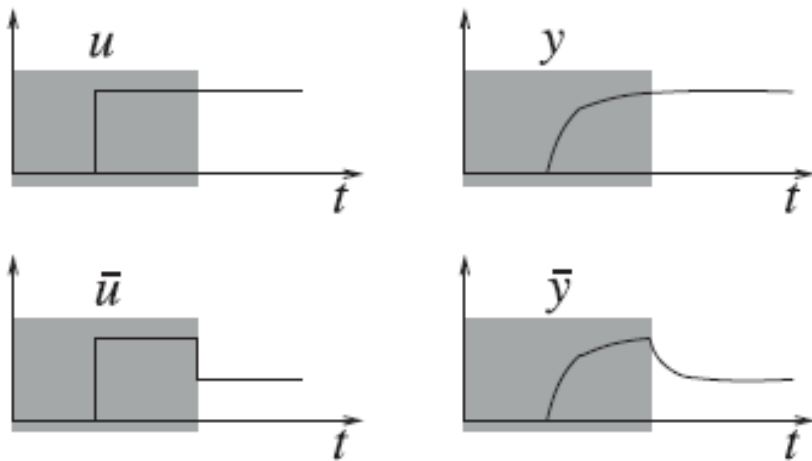
for an arbitrary  $f$ , where

$$f_\tau(t) = \begin{cases} f(t) & 0 \leq t \leq \tau \\ 0 & \tau < t \end{cases}$$

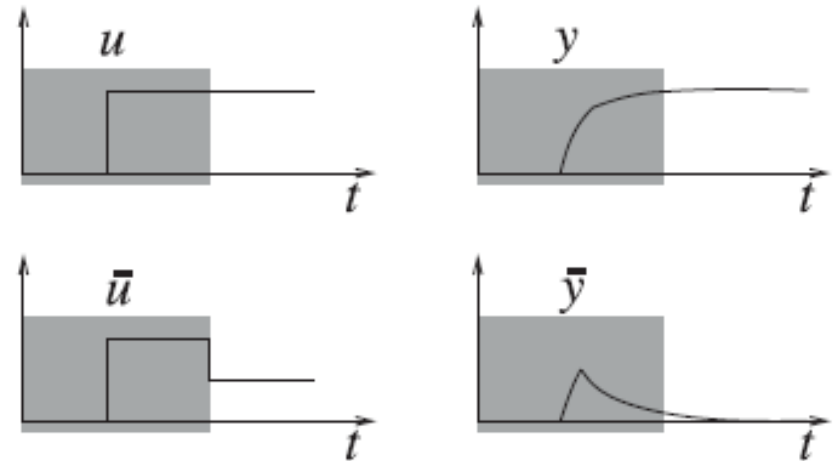
and it is called the truncation of  $f$  to the interval  $[0, \tau]$ .

- Remark: When we consider the *causality* of the operator describing the input/output behavior for LTI systems, the effect of the initial state (i.e.,  $x(0)$ ) is implicitly ignored. In general, there are many different outputs according to different initial conditions, even for the same inputs.

## ◆ Example



(a) Causal system



(b) Noncausal system

## ◆ Time invariance

- Intuitive interpretation: If a system has the property that time-shifting of its inputs results in time-shifting of the outputs, the system is called *time-invariant*.
- Mathematical interpretation: An operator  $\mathbf{T}$  is said to be *time-invariant* if

$$\mathbf{T}S_\tau = S_\tau\mathbf{T}, \quad \forall \tau \in \mathbb{R}$$

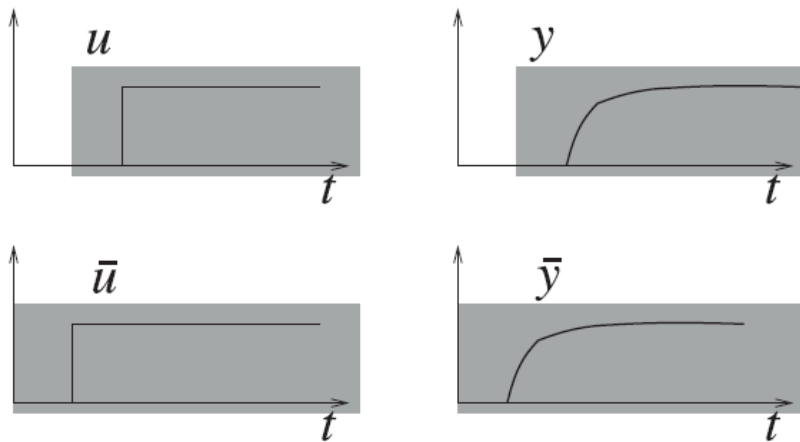
where  $S_\tau$  is a shift operator defined as

$$S_\tau(f(t)) := f(t - \tau)$$

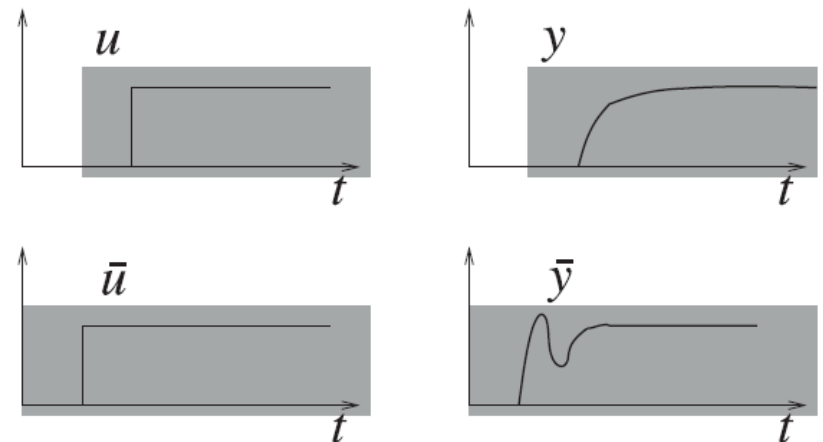
with a constant  $\tau$ .

- Remark: Similarly for the *causality*, the effect of the initial state is implicitly ignored when we consider the *time-invariance* of the operator describing the input/output behavior for LTI systems.

## ◆ Example



(a) Time-invariant system



(b) Not time-invariant system

## ◆ Linearity

- Intuitive interpretation: A system is regarded as a *linear* system when it can be viewed as a linear map from its inputs to corresponding outputs.
- Mathematical interpretation: Let  $y_1$  and  $y_2$  be the outputs of a state-space system corresponding to the inputs  $u_1$  and  $u_2$ , respectively. Then, the system is *linear* in the sense that for every  $\alpha, \beta \in \mathbb{R}$ ,  $\alpha y_1 + \beta y_2$  is the output corresponding to the input  $\alpha u_1 + \beta u_2$ .
- Remark:  $\alpha y_1 + \beta y_2$  is one of the outputs corresponding to the input  $\alpha u_1 + \beta u_2$ . In general, there may be many other outputs (obtained from different initial conditions) that will not be of this form.



## ◆ Characteristics of LTI systems

Let us consider the following state-space system:

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}$$

- This system is causal, linear, and time-invariant.
- This system is called a continuous-time linear time-invariant (LTI) system

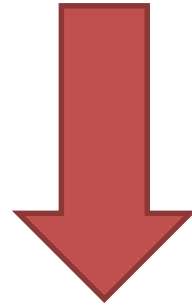
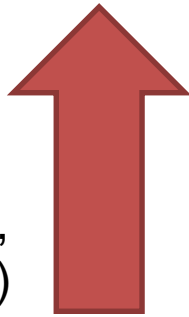
## **2. Equivalent State-Space Systems**

## ◆ Mathematical representations of control systems

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}$$

**Not uniformly determined**

(e.g., controllable canonical form,  
observable canonical form)



Uniformly determined

(e.g.,  $C(sI - A)^{-1}B + D$ )

$$G(s) = \frac{b_{n-1}s^{n-1} + \dots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0} + d$$

→ **There are various equivalent state-space equations for a given transfer function**

## ◆ Similarity transformation

Let us consider the following state-space system:

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}$$

For a given nonsingular matrix  $T$ , define a new state vector as

$$\tilde{x} := Tx$$

Here, the relation between  $x$  and  $\tilde{x}$  is one-to-one and onto.

For  $\tilde{x}$ , we can obtain the following:

$$\begin{cases} \frac{d\tilde{x}}{dt} &= T \frac{dx}{dt} = TAx + TBu = TAT^{-1}\tilde{x} + TBu \\ y &= Cx + Du = CT^{-1}\tilde{x} + Du \end{cases}$$

This can be written as

$$\begin{cases} \frac{d\tilde{x}}{dt} &= \tilde{A}\tilde{x} + \tilde{B}u \\ y &= \tilde{C}\tilde{x} + \tilde{D}u \end{cases}$$

where

$$\tilde{A} := TAT^{-1}, \quad \tilde{B} := TB, \quad \tilde{C} := CT^{-1}, \quad \tilde{D} := D$$

This procedure is called a *similarity transformation* or  
an *equivalent transformation*.

## ◆ Algebraically equivalent

Two continuous-time LTI systems

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases} \quad \text{or} \quad \begin{cases} \frac{d\tilde{x}}{dt} &= \tilde{A}\tilde{x} + \tilde{B}u \\ y &= \tilde{C}\tilde{x} + \tilde{D}u \end{cases}$$

respectively, are called *algebraically equivalent* if there exists a nonsingular matrix  $T$  such that the followings hold:

$$\tilde{A} := TAT^{-1}, \quad \tilde{B} := TB, \quad \tilde{C} := CT^{-1}, \quad \tilde{D} := D$$

The corresponding map  $\tilde{x} = Tx$  is called  
a *similarity transformation* or an *equivalent transformation*.

## ◆ Properties of algebraically equivalent

Suppose that two state-space LTI systems are algebraically equivalent.

- (1) With every input  $u$ , both systems associate the same set of outputs  $y$ . However, the output is generally not the same for the same initial conditions, except the case when the initial conditions are zero.
- (2) The systems are zero-state equivalent, i.e., both systems have the same transfer function. However, zero-state equivalence does not imply algebraic equivalence.

$$\begin{aligned}\tilde{C}(sI - \tilde{A})^{-1}\tilde{B} + \tilde{D} &= CT^{-1}(sI - TAT^{-1})^{-1}TB + D \\ &= C(T^{-1}(sI - TAT^{-1})T)^{-1}B + D \\ &= C(sT^{-1}IT - T^{-1}TAT^{-1}T)^{-1}B + D \\ &= C(sI - A)^{-1}B + D\end{aligned}$$

## ◆ Example

$$A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C = [1 \quad 2], \quad D = 1$$

$$\text{Let } T = \begin{bmatrix} 2 & 1 \\ -1 & -1 \end{bmatrix} \text{ together with } T^{-1} = \begin{bmatrix} 1 & 1 \\ -1 & -2 \end{bmatrix}$$

$$\text{Then, } \tilde{A} = TAT^{-1} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}, \quad \tilde{B} = TB = \begin{bmatrix} 2 \\ -1 \end{bmatrix}$$

$$\tilde{C} = CT^{-1} = [-1 \quad -2], \quad \tilde{D} = D = 1$$

$$\rightarrow C(sI - A)^{-1}B + D = \tilde{C}(sI - \tilde{A})^{-1}\tilde{B} + \tilde{D} = \frac{s^2 + 4s + 1}{s^2 + 3s + 2}$$



### **3. Matrix Exponential**

## ◆ Characteristics of solutions to LTI state-space systems

Consider the solutions  $x(t)$  and  $y(t)$  for the following state-space system:

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}$$

- (1) If we can explicitly compute  $x(t)$ ,  $y(t)$  is readily obtained through  $y = Cx + Du$ .
- (2)  $x(t)$  is uniformly determined according to  $x(0)$  together with  $u(t)$  ( $t \geq 0$ ).
- (3)  $x(0)$  is called an *initial vector* or an *initial value*.

## ◆ Homogenous LTI systems

As a preliminary step to obtain  $x(t)$  (as well as  $y(t)$ ),

$$\text{we assume } u(t) \equiv 0 \text{ in } \begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}.$$

Then, we consider the following homogenous LTI system:

$$\frac{dx}{dt} = Ax \quad \text{with} \quad x(0) = x_0 \in \mathbb{R}^n$$

## ◆ Solutions to homogenous LTI systems

$$\frac{dx}{dt} = Ax \quad \text{with} \quad x(0) = x_0 \in \mathbb{R}^n$$

In the case of a scalar system (i.e.,  $n = 1$  and  $A = a$ ),

$$x(t) = e^{at}x_0$$

Similarly, in the case of a multi-variable system (i.e.,  $n \geq 2$ ),

$$x(t) = e^{At}x_0$$

→ How can we define  $e^{At}$ ?

## ◆ Definition of matrix exponential

$$\frac{dx}{dt} = Ax \quad \text{with} \quad x(0) = x_0 \in \mathbb{R}^n$$

$$\rightarrow x(t) = e^{At}x_0$$

Here,  $e^{At}$  is called a *state transition matrix*.

Motivated by Taylor series of the scalar exponential,

$$e^{At} = \sum_{i=0}^{\infty} \frac{(At)^i}{i!} = I + At + \frac{1}{2!}A^2t^2 + \frac{1}{3!}A^3t^3 + \dots + \frac{1}{n!}A^nt^n + \dots$$

## ◆ Properties of matrix exponential

(1) The  $i$ th column of  $e^{At}$  is the unique solution to

$$\frac{dx}{dt} = Ax, \quad x(0) = e_i, \quad t \geq 0,$$

where  $e_i$  is the  $i$ th standard basis of  $\mathbb{R}^n$ .

(2) For every  $t, \tau \in \mathbb{R}$ ,

$$e^{At}e^{A\tau} = e^{A(t+\tau)}.$$

(3) For every  $t \in \mathbb{R}$ ,  $e^{At}$  is nonsingular and

$$(e^{At})^{-1} = e^{-At}.$$

(4) Regarding to derivative, the followig holds:

$$\frac{de^{At}}{dt} = A + A^2t + \frac{1}{2!}A^3t^2 + \dots = Ae^{At} = e^{At}A.$$

(5) Regarding to integral, the following holds:

$$\int e^{At}dt = C + It + \frac{1}{2!}At^2 + \frac{1}{3!}A^2t^3 + \dots.$$

Indeed, when  $|A| \neq 0$ ,

$$\int e^{At}dt = A^{-1}e^{At} + C' = e^{At}A^{-1} + C' \quad (C' := C - A^{-1}).$$

(6) When  $AB = BA$ , the following holds:

$$e^{(A+B)t} = e^{At}e^{Bt}.$$

In general,  $e^{(A+B)t} \neq e^{At}e^{Bt}$  when  $AB \neq BA$ .

## ◆ Advanced Property of matrix exponential

(7) For every  $n \times n$  matrix  $A$ , there exists  $n$  scalar functions

$\alpha_0(t), \alpha_1(t), \dots, \alpha_{n-1}(t)$  for which

$$e^{At} = \sum_{i=0}^{n-1} \alpha_i(t) A^i, \quad \forall t \in \mathbb{R}.$$

*Proof:* Recall the Cayley-Hamilton theorem that

$$A^n + a_1 A^{n-1} + a_2 A^{n-2} + \dots + a_{n-1} A + a_n I = 0,$$

where the  $a_i$  ( $i = 1, \dots, n$ ) are the coefficients of the characteristic

equation of  $A$ , i.e.,  $|sI - A| = 0$ . Therefore,

$$A^n = -a_1 A^{n-1} - a_2 A^{n-2} - \dots - a_{n-1} A - a_n I.$$



This implies that

$$\begin{aligned}
A^{n+1} &= -a_1 A^n - a_2 A^{n-1} - \dots - a_{n-1} A - a_n A \\
&= a_1(a_1 A^{n-1} + a_2 A^{n-2} + \dots + a_{n-1} A + a_n I) - a_2 A^{n-1} - \dots - a_n A \\
&= (a_1^2 - a_2) A^{n-1} + (a_1 a_2 - a_3) A^{n-2} + \dots + (a_1 a_{n-1} - a_n) A + a_1 a_n I.
\end{aligned}$$

It turns out that  $A^{n+1}$  can be written as a linear combination of  $A^{n-1}, \dots, A, I$ .

Applying the same procedure for increasing powers of  $A$ , every  $A^k$  ( $k \geq 0$ ) can be written as

$$A^k = \bar{a}_{n-1}(k) A^{n-1} + \dots + \bar{a}_1(k) A + \bar{a}_0(k) I \quad \forall k \geq 0.$$

with appropriate coefficients  $\bar{a}_i(k)$ .

By substituting this into the definition of  $e^{At}$ , we obtain

$$e^{At} = \sum_{k=0}^{\infty} \frac{t^k}{k!} A^k = \sum_{k=0}^{\infty} \frac{t^k}{k!} \sum_{i=0}^{n-1} \bar{a}_i(k) A^i.$$

Exchanging the order of summation means

$$e^{At} = \sum_{i=0}^{n-1} \left( \sum_{k=0}^{\infty} \frac{t^k \bar{a}_i(k)}{k!} \right) A^i.$$

Defining  $\alpha_i(t) := \sum_{k=0}^{\infty} \frac{t^k \bar{a}_i(k)}{k!}$  completes the proof.

## ◆ Methods for computing matrix exponential

Question: How can we compute  $e^{At}$ ?

(1) Direct computation of  $e^{At} = I + At + \frac{1}{2!}A^2t^2 + \cdots + \frac{1}{n!}A^nt^n + \cdots$

→ In general, only an approximate computation is possible.

(2) Laplace transform of

$$\frac{d}{dt}e^{At} = Ae^{At}, \quad e^{A \cdot 0} = I, \quad t \geq 0.$$

→ Let  $f(t) := e^{At}$ , and use  $\mathcal{L}\{\dot{f}(t)\} = sF(s) - f(0)$ .

In other words, we have

$$sF(s) - I = AF(s)$$

where  $F(s) := \mathcal{L}\{e^{At}\}$ . Hence,

$$F(s) = (sI - A)^{-1} \Leftrightarrow e^{At} = \mathcal{L}^{-1}\{(sI - A)^{-1}\}$$

Thus,

$$e^{At} = \mathcal{L}^{-1}\{(sI - A)^{-1}\}$$

(3) When  $A$  is a diagonalizable matrix,

$$T^{-1}AT = \Lambda := \begin{bmatrix} \lambda_1 & & \\ & \ddots & \\ & & \lambda_n \end{bmatrix}$$

where  $\lambda_1, \dots, \lambda_n$  is the eigenvalues of  $A$ .

Here, if we note that

$$A = T\Lambda T^{-1} = T \begin{bmatrix} \lambda_1 & & \\ & \ddots & \\ & & \lambda_n \end{bmatrix} T^{-1}$$

together with

$$e^{At} = I + At + \frac{1}{2!}A^2t^2 + \dots + \frac{1}{n!}A^nt^n + \dots$$

then we obtain

$$\begin{aligned} e^{At} &= TIT^{-1} + T(\Lambda t)T^{-1} + T\left(\frac{1}{2!}\Lambda^2 t^2\right)T^{-1} + \dots \\ &= Te^{\Lambda t}T^{-1} \\ &= T \begin{bmatrix} e^{\lambda_1 t} & & \\ & \ddots & \\ & & e^{\lambda_n t} \end{bmatrix} T^{-1} \end{aligned}$$

In other words,

$$e^{At} = T \begin{bmatrix} e^{\lambda_1 t} & & \\ & \ddots & \\ & & e^{\lambda_n t} \end{bmatrix} T^{-1}$$

(4) When  $A$  is a non-diagonalizable matrix,

$$J = P^{-1}AP = \begin{bmatrix} J_{p_1}(\lambda_1) & & & \\ & J_{p_2}(\lambda_2) & & \\ & & \ddots & \\ & & & J_{p_N}(\lambda_N) \end{bmatrix}$$

where  $J_{p_i}(\lambda_i)$  is a Jordan block defined as

$$J_{p_i}(\lambda_i) = \begin{bmatrix} \lambda_i & 1 & 0 & \cdots & 0 \\ 0 & \lambda_i & 1 & \ddots & 0 \\ 0 & 0 & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & 1 \\ 0 & \cdots & 0 & 0 & \lambda_i \end{bmatrix} \quad (p_i \times p_i)$$

and each  $\lambda_i$  is an eigenvalue of  $A$ .

Similarly for the case of a diagonalizable matrix,

$$A = PJP^{-1} = P \begin{bmatrix} J_{p_1}(\lambda_1) & & \\ & \ddots & \\ & & J_{p_N}(\lambda_N) \end{bmatrix} P^{-1}$$

and thus

$$e^{At} = Pe^{Jt}P^{-1} = P \begin{bmatrix} e^{J_{p_1}(\lambda_1)t} & & \\ & \ddots & \\ & & e^{J_{p_N}(\lambda_N)t} \end{bmatrix} P^{-1}$$



where  $e^{J_{p_i}(\lambda_i)t}$  is given by

$$e^{J_{p_i}(\lambda_i)t} = \begin{bmatrix} e^{\lambda_i t} & te^{\lambda_i t} & \dots & \frac{t^{p_i-1}}{(p_i-1)!} e^{\lambda_i t} \\ & e^{\lambda_i t} & \ddots & \vdots \\ & & \ddots & te^{\lambda_i t} \\ & & & e^{\lambda_i t} \end{bmatrix}$$

To put it another way,

$$e^{At} = P \begin{bmatrix} e^{J_{p_1}(\lambda_1)t} & & \\ & \ddots & \\ & & e^{J_{p_N}(\lambda_N)t} \end{bmatrix} P^{-1}$$

with

$$e^{J_{p_i}(\lambda_i)t} = \begin{bmatrix} e^{\lambda_i t} & te^{\lambda_i t} & \dots & \frac{t^{p_i-1}}{(p_i-1)!} e^{\lambda_i t} \\ & e^{\lambda_i t} & \ddots & \vdots \\ & & \ddots & te^{\lambda_i t} \\ & & & e^{\lambda_i t} \end{bmatrix}$$

## ◆ Example

For  $A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$ , let us compute  $e^{At}$ .

$$\begin{aligned} \text{(a) } (sI - A)^{-1} &= \begin{bmatrix} s & -1 \\ 2 & s+3 \end{bmatrix}^{-1} = \begin{bmatrix} \frac{s+3}{(s+1)(s+2)} & \frac{1}{(s+1)(s+2)} \\ \frac{-2}{(s+1)(s+2)} & \frac{s}{(s+1)(s+2)} \end{bmatrix} \\ &= \begin{bmatrix} \frac{2}{s+1} - \frac{1}{s+2} & \frac{1}{s+1} - \frac{1}{s+2} \\ \frac{-2}{s+1} + \frac{2}{s+2} & \frac{-1}{s+1} + \frac{2}{s+2} \end{bmatrix} \end{aligned}$$

Thus,

$$e^{At} = \mathcal{L}^{-1}\{(sI - A)^{-1}\} = \begin{bmatrix} 2e^{-t} - e^{-2t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix}$$

(b)  $A$  has eigenvalues  $\lambda_1 = -1$ ,  $\lambda_2 = -2$  together with

corresponding eigenvectors  $v_1 = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ ,  $v_2 = \begin{bmatrix} 1 \\ -2 \end{bmatrix}$ .

Then, by  $T = \begin{bmatrix} 1 & 1 \\ -1 & -2 \end{bmatrix}$  and  $T^{-1} = \begin{bmatrix} 2 & 1 \\ -1 & -1 \end{bmatrix}$ ,

$$\begin{aligned} e^{At} &= T \begin{bmatrix} e^{-t} & \\ & e^{-2t} \end{bmatrix} T^{-1} = \begin{bmatrix} 1 & 1 \\ -1 & -2 \end{bmatrix} \begin{bmatrix} e^{-t} & \\ & e^{-2t} \end{bmatrix} \begin{bmatrix} 2 & 1 \\ -1 & -1 \end{bmatrix} \\ &= \begin{bmatrix} 2e^{-t} - e^{-2t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix} \end{aligned}$$

## ◆ Case study for state transition matrix

- $\Phi(t) := e^{At}$
- $\Phi_{ij}(t)$ :  $(i, j)$ th element of  $\Phi(t)$
- $\lambda_k$  ( $k = 1, \dots, n$ ):  $k$ th eigenvalue of  $A$

$$(1) \operatorname{Re}(\lambda_k) < 0 \quad (\forall k = 1, \dots, n)$$

$$\Rightarrow \Phi_{ij}(t) \rightarrow 0 \quad (t \rightarrow \infty), \quad \forall i = 1, \dots, n; \quad \forall j = 1, \dots, n$$

$$(2) \text{ There exists a } \lambda_k \text{ such that } \operatorname{Re}(\lambda_k) > 0$$

$$\Rightarrow \text{ There exists a } \Phi_{ij}(t) \text{ such that } \Phi_{ij}(t) \rightarrow \infty \quad (t \rightarrow \infty)$$

(3)  $\operatorname{Re}(\lambda_k) \leq 0$  ( $\forall k = 1, \dots, n$ )

(i) All the Jordan blocks corresponding to  $\operatorname{Re}(\lambda_k) = 0$  have size of 1

$\Rightarrow \Phi_{ij}(t)$  is bounded for  $t \geq 0$ ,  $\forall i = 1, \dots, n; \forall j = 1, \dots, n$

(ii) There exists a Jordan block corresponding to  $\operatorname{Re}(\lambda_k) = 0$   
with size larger than 1

$\Rightarrow$  There exists a  $\Phi_{ij}(t)$  such that  $\Phi_{ij}(t) \rightarrow \infty$  ( $t \rightarrow \infty$ )

→ This will be also considered in ‘Chapter 5. Stability.’

## ◆ Another interpretation for state transition matrix

(a) There exists a complex eigenvalue of  $A$

$\Rightarrow e^{At}$  is vibrational as  $t$  becomes larger

(b) All the eigenvalues of  $A$  are real

$\Rightarrow e^{At}$  is not vibrational as  $t$  becomes larger

(c) 0 is an eigenvalue of  $A$

$\Rightarrow e^{At}$  plays as an integrator

## **4. Solutions to LTI Systems**



## ◆ Solutions to general case

Consider the general case  $u(t) \not\equiv 0$  for the following system:

$$\frac{dx}{dt} = Ax + Bu$$

Assume that

$$x(t) = e^{At}(x(0) + z(t)), \quad z(0) = 0$$

Then,  $x(t)$  satisfies  $x(0) = x_0$ .

By substituting  $x(t)$  into  $\frac{dx}{dt} = Ax + Bu$ , we obtain

$$Ae^{At}(x(0) + z(t)) + e^{At}\dot{z}(t) = Ae^{At}(x(0) + z(t)) + Bu$$

This implies that

$$\dot{z}(t) = e^{-At}Bu(t)$$

This together with  $z(0) = 0$  leads to

$$z(t) = \int_0^t e^{-A\tau}Bu(\tau)d\tau$$

Thus, we can obtain the following solution:

$$x(t) = e^{At} \left( x(0) + \int_0^t e^{-A\tau}Bu(\tau)d\tau \right)$$

We return to the following case with the output equation:

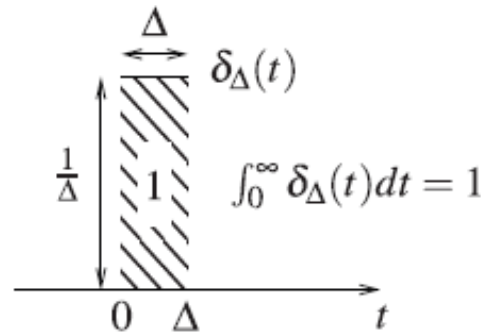
$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du \end{cases}$$

Then, we have the following solution:

$$y(t) = Ce^{At}x(0) + \int_0^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

## ◆ Impulse signal

$$\delta(t) := \lim_{\Delta \rightarrow 0} \delta_{\Delta}(t)$$



## ◆ Impulse response

$$\begin{cases} \frac{dx}{dt} &= Ax + Bu \\ y &= Cx \end{cases}$$

Compute  $y(t)$  when  $u(t) = \delta(t)e_i$  with  $x(0) = 0$ .

By substituting  $u(t) = \delta(t)e_i$ ,  $x(0) = 0$  together with  $D = 0$  into

$$y(t) = Ce^{At}x(0) + \int_0^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

we obtain

$$\begin{aligned} y(t) &= C \int_0^t e^{A(t-\tau)} B \delta(\tau) e_i d\tau = Ce^{At} \lim_{\Delta \rightarrow 0} \int_0^{\Delta} e^{-A\tau} B \frac{1}{\Delta} e_i d\tau \\ &= Ce^{At} B e_i \end{aligned}$$

Thus, we have

$$y(t) = Ce^{At} B e_i$$

## **Appendix: Solutions to LTV Systems**

## ◆ Causality

- Intuitive interpretation: If a system has the property that the output *before* some time  $t$  does not depend on the input *after* time  $t$ .  
Such a system is called *causal*.
- Mathematical interpretation: The state-space system is *causal* in the sense that if  $y$  is one of the outputs that corresponds to the input  $u$ , then for every other input  $\bar{u}$  for which

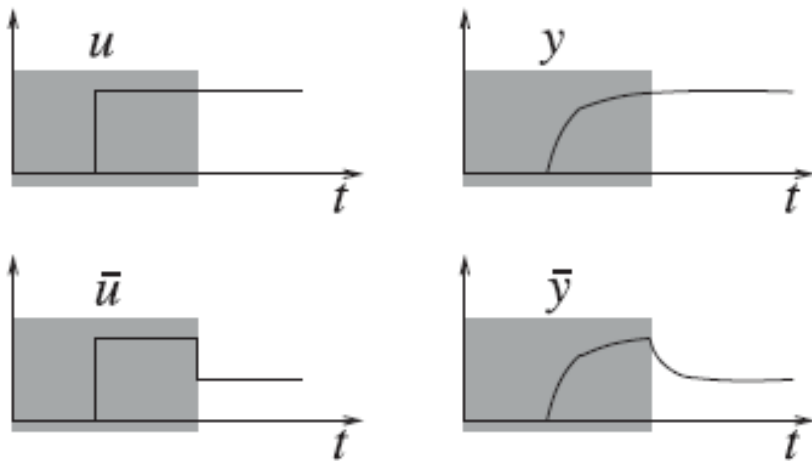
$$\bar{u}(t) = u(t), \quad 0 \leq \forall t < T$$

for some  $T > 0$ , the system exhibits (at least) one output  $\bar{y}$  that satisfies

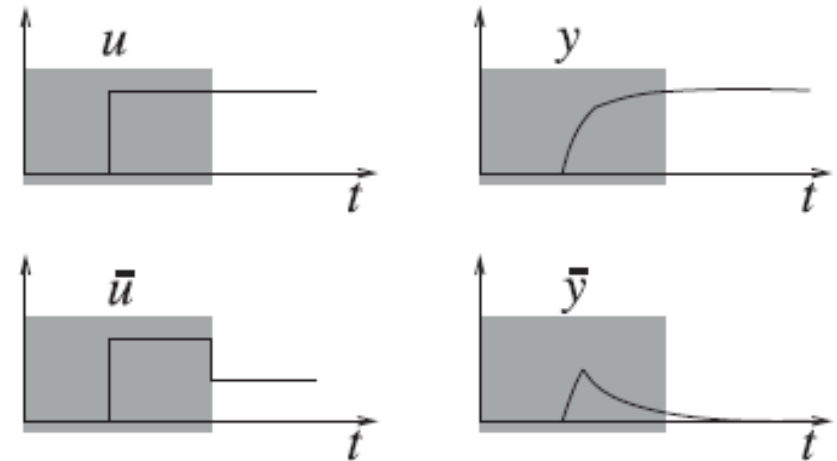
$$\bar{y}(t) = y(t), \quad 0 \leq \forall t < T$$

- Remark: The *causality* property does not mean “for every input  $\bar{u}$  that matches  $u$  on  $[0, T)$ , every output  $\bar{y}$  matches  $y$  on  $[0, T)$ .” In general, only one output  $\bar{y}$  (obtained with the same initial condition) will match  $y$ .

## ◆ Example



(a) Causal system



(b) Noncausal system



## ◆ Homogenous LTV systems

As a preliminary step to obtain  $x(t)$  (as well as  $y(t)$ ),

$$\text{we assume } u(t) \equiv 0 \text{ in } \begin{cases} \frac{dx(t)}{dt} &= A(t)x(t) + B(t)u(t) \\ y(t) &= C(t)x(t) + D(t)u(t) \end{cases}.$$

Then, we consider the following homogenous LTI system:

$$\frac{dx(t)}{dt} = A(t)x(t) \quad \text{with} \quad x(0) = x_0 \in \mathbb{R}^n$$

## ◆ Peano-Baker series

$$\frac{dx(t)}{dt} = A(t)x(t) \quad \text{with} \quad x(0) = x_0 \in \mathbb{R}^n$$

The unique solution is given by

$$x(t) = \Phi(t, 0)x_0, \quad x_0 \in \mathbb{R}^n, \quad t \geq 0$$

where

$$\begin{aligned} \Phi(t, 0) := I &+ \int_0^t A(s_1)ds_1 + \int_0^t A(s_1) \int_0^{s_1} A(s_2)ds_2ds_1 \\ &+ \int_0^t A(s_1) \int_0^{s_1} A(s_2) \int_0^{s_2} A(s_3)ds_3ds_2ds_1 + \cdots. \end{aligned}$$

The  $n \times n$  matrix  $\Phi(t, 0)$  is called the state transition matrix.

## ◆ Properties of state transition matrix

1.  $\Phi(t, 0)$  is the unique solution to

$$\frac{d}{dt}\Phi(t, 0) = A(t)\Phi(t, 0), \quad \Phi(0, 0) = I, \quad t \geq 0$$

2.  $\Phi(0, 0) = I$

3. For every  $t_1, t_2 \geq 0$ ,

$$\Phi(t_2, t_1)\Phi(t_1, 0) = \Phi(t_2, 0)$$

4.  $\Phi(t, 0) = \Phi(0, t)^{-1}$

The proofs are readily followed by the definition of  $\Phi(t, 0)$

## ◆ Solutions to general LTV systems

We return to the following case with the output equation:

$$\begin{cases} \frac{dx(t)}{dt} &= A(t)x(t) + B(t)u(t) \\ y(t) &= C(t)x(t) + D(t)u(t) \end{cases}$$

Then, we have the following solutions:

$$\begin{aligned} x(t) &= \Phi(t, 0)x(0) + \int_0^t \Phi(t, \tau)B(\tau)u(\tau)d\tau \\ y(t) &= C(t)\Phi(t, 0)x(0) + \int_0^t C(t)\Phi(t, \tau)B(\tau)u(\tau)d\tau + Du(t) \end{aligned}$$