

# CTRL 연구 참여 2주차

## Stability of the System

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# Pole & Zero

- Rational transfer function

$$H(s) = \frac{b_1 s^m + b_2 s^{m-1} + \dots + b_{m+1}}{s^n + a_1 s^{n-1} + \dots + a_n} = \frac{N(s)}{D(s)}$$

$$H(s) = K \frac{\prod_{i=1}^m (s - z_i)}{\prod_{i=1}^n (s - p_i)}$$

K: transfer function gain

- Pole:  $H(s)|_{s=p_i} = \infty$

-related to the system's stability

- Zero:  $H(s)|_{s=z_i} = 0$

# Pole & Zero

- Effect of pole locations
  - The **negative real part of the pole** determines the **decay rate** of the exponential envelope

complex poles:  $s = -\sigma \pm j\omega_d$

transfer function:  $H(s) = \frac{\omega_n^2}{(s + \sigma)^2 + \omega_d^2}$

$\zeta = \frac{\sigma}{\omega_n}$ : damping ratio  
 $\omega_n$ : undamped natural frequency  
 $\omega_d$ : damped natural frequency

impulse response :  $h(t) = \frac{\omega_n}{\sqrt{1 - \zeta^2}} e^{-\sigma t} (\sin \omega_d t) 1(t), (\sigma = \zeta \omega_n)$

- Stability of complex poles

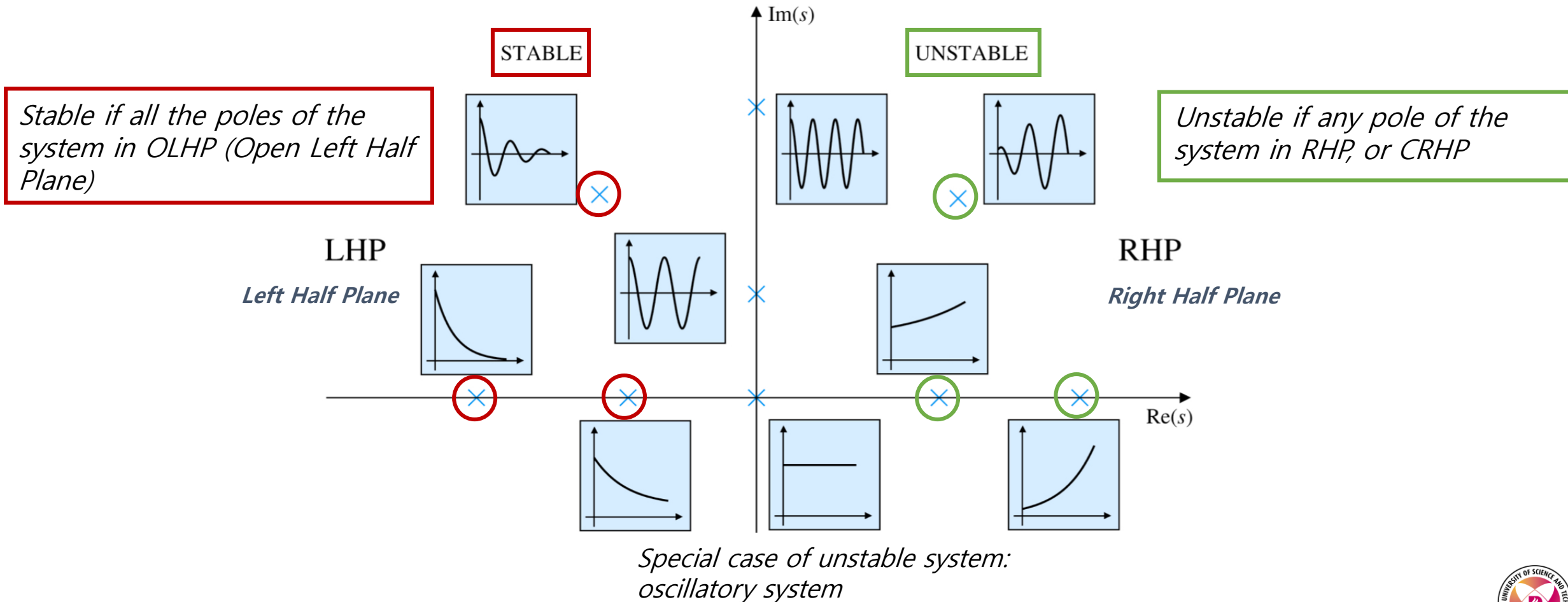
$\sigma < 0$  : unstable (real part is positive)

$\sigma = 0$  : neutrally stable

$\sigma > 0$  : stable (real part is negative)

# Pole & Zero

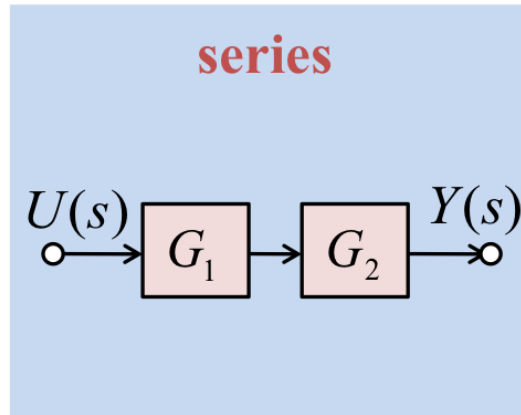
- Summary of pole location
  - Pole locations determine the way of it behaves for impulse response of the system



# Transfer function corresponding to the block diagram

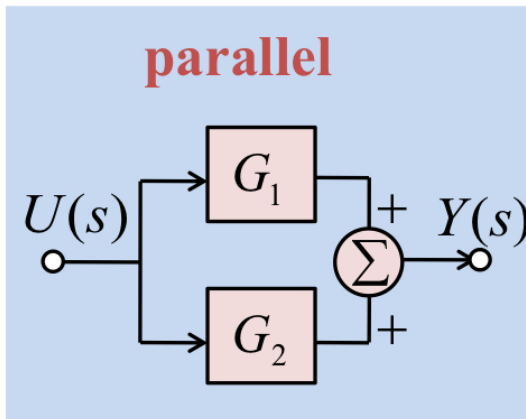
- Block diagram
  - It can be used to illustrate the relationship between the components of given system

- Series



$$\frac{Y(s)}{U(s)} = G_2(s)G_1(s)$$

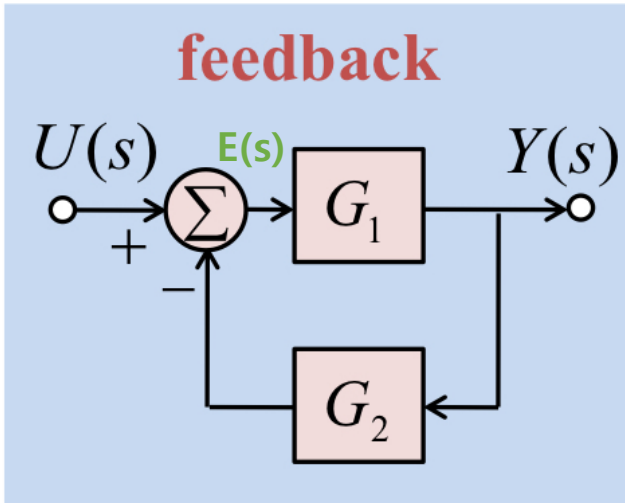
- Parallel



$$\frac{Y(s)}{U(s)} = G_1(s) + G_2(s)$$

# Transfer function corresponding to the block diagram

- Feedback



$$\frac{Y(s)}{U(s)} = \frac{G_1(s)}{1 + G_1(s)G_2(s)}$$

$$Y(s) = G_1(s)E(s)$$
$$E(s) = U(s) - G_2(s)Y(s)$$

$$\rightarrow Y(s) = G_1(s)U(s) - G_2(s)G_1(s)Y(s)$$
$$\rightarrow (1 + G_1(s)G_2(s))Y(s) = G_1(s)U(s)$$

# Transfer function corresponding to the block diagram

- Relation between state-space equation and transfer function

$$\begin{aligned}\frac{dx}{dt} &= Ax + Bu \\ y &= Cx + Du\end{aligned}$$



$$G(s) = \frac{b_{n-1}s^{n-1} + \dots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0} + d$$

- Poles of  $G(s)$  = Eigenvalues of  $A$

$$G(s) = C(sI - A)^{-1} + D$$

$$\text{eigenvalues of } A: |\lambda I - A| = 0$$



# Root locus

- Motivation
  - Poles of the feedback systems are closely related to the responses of the feedback systems

- Concepts

- closed-loop transfer function:

$$\frac{Y(s)}{R(s)} = T(s) = \frac{D(s)G(s)}{1 + D(s)G(s)H(s)}$$

- Characteristic equation:

$$1 + D(s)G(s)H(s) = 0 \rightarrow a(s) + Kb(s) = 0 \quad (K := \text{parameter of interest})$$
$$\rightarrow 1 + KL(s) = 0 \quad (L(s) = \frac{b(s)}{a(s)})$$

- Root locus: plot the locus of all possible roots of  $1 + KL(s)$  as  $K$  varies from 0 to  $\infty$   
 $\rightarrow$  find the pole's location!

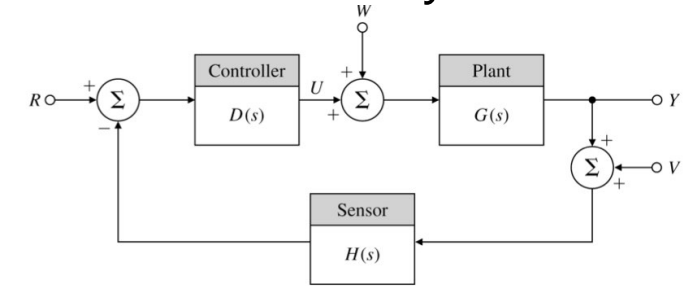


Figure 5.1 Basic closed loop block diagram

# Root locus

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- A graphical representation of closed loop poles as a system parameter varied
- Select a particular value of  $K$  that will meet the specifications for static and dynamic response

# Nyquist plot

- Nyquist stability
  - Relationship between the stability of closed loop system and the frequency response of the plant

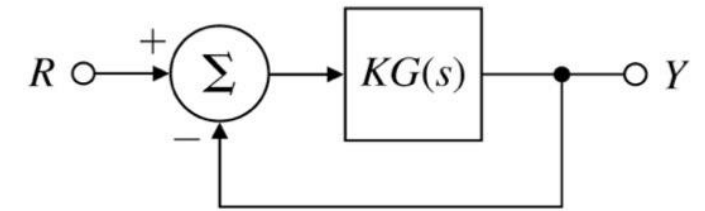
- For all points  $s$  on the root locus

$$1 + KG(s) = 0 \rightarrow |KG(s)| = 1 \text{ and } \angle G(s) = 180^\circ$$

- neutral stability condition (at the point of neutral stability)

$$|KG(j\omega_0)| = 1 \text{ and } \angle G(j\omega_0) = 180^\circ$$

→ relates the open-loop frequency response to the number of RHP poles of the closed-loop system



# Nyquist plot

- There are some systems where  $|KG(j\omega)|$  crosses magnitude=1 more than once  
→ use Nyquist stability criterion
- a contour map of  $KG(s)$  will encircle -1 **N=Z-P** times (by the argument principle)  
*where Z: the number of RHP zeros of  $1+KG(s)$*   
*P: the number of RHP poles of  $KG(s)$*

$$1 + KG(s) = 1 + K \frac{b(s)}{a(s)} = \frac{a(s) + Kb(s)}{a(s)}$$

- [ Poles of  $G(s)$  = poles of  $1+KG(s)$  = poles of  $KG(s)$
- [ Closed loop poles = zeros of  $1+KG(s)$
- [ Poles of  $G(s)$  in RHP = poles of  $(1+KG(s))$  in RHP = poles of  $(1+KG(s))$  in RHP
- [ Closed loop poles in RHP = zeros of  $(1+KG(s))$  in RHP

# Nyquist plot

- Nyquist stability criterion  $\frac{Y(s)}{R(s)} = T(s) = \frac{KG(s)}{1 + KG(s)}$ , we have  $Z = N + P$  → want to know!

***Z: the number of RHP poles of closed-loop system***

***N: the number of clockwise encirclement of KG(s) about -1***

***P: the number of RHP poles of open-loop system***

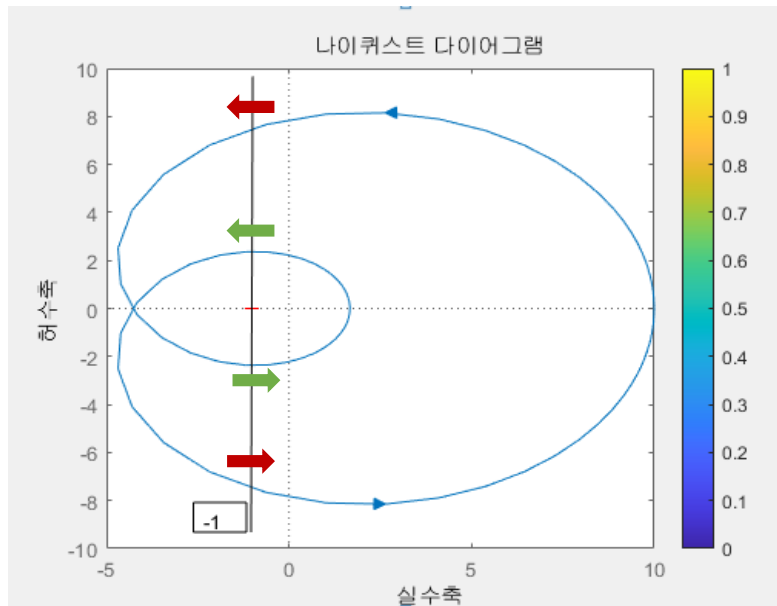
→ stability of the closed-loop system can be determined in terms of  
the **number of RHP poles of the open-loop system (KG(s))**  
and **the Nyquist plot**  
(the number of clockwise encirclement of KG(s) about -1)

# Nyquist plot

- example

$$KG(s) : L(s) = \frac{10(s+1)(s+2)}{(s-3)(s-4)} (K=1)$$

```
>> H = tf([10 30 20],[1 -7 12]);  
nyquist(H)
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$$Z = N - P \quad N = -2 \quad \text{and} \quad P = 2 \quad \text{so} \quad Z = 0$$

→ stable system

- We can also determine system's gain K using gain margin

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# Q&A