

```
syms x1 x2 x3 x4 x5 x6 u
```

Warning: Class 'sym' is defined in a class folder and takes precedence over a function with the same name that is earlier on the MATLAB path. In a future release, class 'sym' will no longer be given precedence.

[Click here for the locations of the conflicting items.](#)
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```
syms M m1 m2 l1 l2 g
M = 1.5;
m1 = 0.5;
l1 = 0.5;
m2 = 0.75;
l2 = 0.75;
g = 9.81;
T_cart = 0.5*M*x4^2;
T_pendulum1 = 0.5*m1*((x4+l1*x5*cos(x2))^2 + (l1*x5*sin(x2))^2);
T_pendulum2 = 0.5*m2*((x4 + l1*x5*cos(x2) + l2*x6*cos(x3))^2 + (l1*x5*sin(x2) +
l2*x6*sin(x3))^2);
T_total = simplify(T_cart + T_pendulum1 + T_pendulum2);
V_Cart = 0;
V_pendulum1 = m1*g*l1*cos(x2);
V_pendulum2 = m2*g*(l1*cos(x2)+l2*cos(x3));
V_total = simplify(V_Cart + V_pendulum1 + V_pendulum2);
L = simplify(T_total - V_total);

dL_dx1 = diff(L, x1);
dL_dx2 = diff(L, x2);
dL_dx3 = diff(L, x3);
dL_dx4 = diff(L, x4);
dL_dx5 = diff(L, x5);
dL_dx6 = diff(L, x6);
q = [x1 ;x2; x3];
qd = [x4; x5; x6];
syms qdd1 qdd2 qdd3 real
qdd = [qdd1; qdd2; qdd3];
Jaco = jacobian([dL_dx4;dL_dx5;dL_dx6],[q;qd]);
d_dt_dLdqdot = Jaco*[qd; qdd];
dLdq = [dL_dx1;dL_dx2;dL_dx3];
Force = [u; 0; 0];
Lagrange_eq = simplify(d_dt_dLdqdot - dLdq -Force);
D = sym(zeros(3,3));
for i=1:3
    for j=1:3
        D(i,j) = simplify(diff(diff(T_total, qd(i)), qd(j)));
    end
end
D =
```

$$\begin{pmatrix} \frac{11}{4} & \frac{5 \cos(x_2)}{8} & \frac{9 \cos(x_3)}{16} \\ \frac{5 \cos(x_2)}{8} & \frac{5}{16} & \frac{9 \cos(x_2 - x_3)}{32} \\ \frac{9 \cos(x_3)}{16} & \frac{9 \cos(x_2 - x_3)}{32} & \frac{27}{64} \end{pmatrix}$$

```
G = simplify([ diff(V_total, x1);
    diff(V_total, x2);
    diff(V_total, x3) ])
```

$$G = \begin{pmatrix} 0 \\ -\frac{981 \sin(x_2)}{160} \\ -\frac{8829 \sin(x_3)}{1600} \end{pmatrix}$$

```
n = 3;
c = sym(zeros(n,n,n));
for i=1:n
    for j=1:n
        for k=1:n
            c(i,j,k) = 1/2*( diff(D(i,j), q(k)) + diff(D(i,k), q(j)) - diff(D(j,k),
q(i)) );
        end
    end
end

C = sym(zeros(n,n));
for i=1:n
    for j=1:n
        C(i,j) = simplify( reshape(c(i,j,:),[n,1]).' * qd );
    end
end

H = [1;0;0];
qdd = simplify(D\ (H*u - C*qd-G));
X = [q;qd];
f_sym = [qd; qdd]

f_sym =
```

$$\begin{aligned}
& \left. \begin{array}{c} x_4 \\ x_5 \\ x_6 \end{array} \right\} \\
& - \frac{280 u - 981 \sin(2x_2) + 100 x_5^2 \sin(x_2) + 45 x_6^2 \sin(x_3) - 120 u \cos(\epsilon)}{20 \sigma_2} \\
& \frac{1575 x_6^2 \sin(x_2 - x_3) - 30411 \sin(x_2) - 8829 \sin(x_2 - 2x_3) + 250 x_5^2 \sin(2x_2) + 1400 u \cos(x_2) + 450 x_5^2 \sin(x_3)}{50 \sigma_2} \\
& - \frac{300 \sin(x_2 - x_3) x_5^2 + 135 \sin(\sigma_3) x_6^2 - 2943 \sigma_1 + 2943 \sin(x_3) + 200 u \cos(2x_2)}{75 \cos(2x_2) + 135 \cos(\sigma_3) - 390}
\end{aligned}$$

where

$$\sigma_1 = \sin(2x_2 - x_3)$$

$$\sigma_2 = 5 \cos(2x_2) + 9 \cos(\sigma_3) - 26$$

$$\sigma_3 = 2x_2 - 2x_3$$

```
D_inv = inv(D)
```

$$\begin{pmatrix}
\frac{4 (3 \cos(x_2 - x_3)^2 - 5)}{\sigma_4} & \sigma_2 & \sigma_3 \\
\sigma_2 & \frac{16 (3 \cos(x_3)^2 - 11)}{\sigma_4} & \sigma_1 \\
\sigma_3 & \sigma_1 & \frac{320 (5 \cos(x_2)^2 - 11)}{27 \sigma_4}
\end{pmatrix}$$

where

$$\sigma_1 = \frac{32 (11 \cos(x_2 - x_3) - 5 \cos(x_2) \cos(x_3))}{3 \sigma_4}$$

$$\sigma_2 = \frac{8 (5 \cos(x_2) - 3 \cos(x_2 - x_3) \cos(x_3))}{\sigma_4}$$

$$\sigma_3 = \frac{80 (\cos(x_3) - \cos(x_2 - x_3) \cos(x_2))}{3 \sigma_4}$$

$$\sigma_4 = 33 \cos(x_2 - x_3)^2 - 30 \cos(x_2 - x_3) \cos(x_2) \cos(x_3) + 25 \cos(x_2)^2 + 15 \cos(x_3)^2 - 55$$

```
C
```

$$C = \begin{pmatrix} 0 & -\frac{5x_5 \sin(x_2)}{8} & -\frac{9x_6 \sin(x_3)}{16} \\ 0 & 0 & \frac{9x_6 \sin(x_2 - x_3)}{32} \\ 0 & -\frac{9x_5 \sin(x_2 - x_3)}{32} & 0 \end{pmatrix}$$

Funwork 3

Instructions

The objective of this assignment is to apply Linear Matrix Inequalities (LMI) to the design of linear controllers stabilizing a nonlinear system about a nonzero equilibrium state. Your controllers are to be tested on the nonlinear model.

Problem 1. (4 pts) Start with the non-linear model of the double inverted pendulum on a cart (DIPC) from FunWork 1. Show that there does not exist U_e that would make

$$x_e = [0.1 \quad 60^\circ \quad 45^\circ \quad 0 \quad 0 \quad 0]^\top$$

an equilibrium state.

Intuitively we can say the system won't be stable as only one control input is provided and there are three degrees of freedom which are initialized. I will show this by considering the equation for qdd which says that:

$$qdd = D(q)^{-1}(H.u - C.qd - G(q))$$

For equilibrium for some U_e and X_e we have:

$qdd = 0$ As at equilibrium, all derivates should be 0

$qd = 0$ (Given)

$$D(q)^{-1}(H.u_e - C.(0) - G(q)) = 0$$

$D(q)$ is invertible and also at the given states it is a non zero matrix. So to find the solution of the equation is to find solution for:

$$H.u_e - G = 0$$

```
syms u_e real
q_val_1 = [0.1; deg2rad(60); deg2rad(45)];
qd_val_1 = [0; 0; 0];
G_val = double(subs(G, [x1 x2 x3 x4 x5 x6], [q_val_1' qd_val_1']));
eq = H*u_e == G_val;
sol_u = solve(eq, u_e, 'Real', true)
```

`sol_u =`

Empty sym: 0-by-1

There is no solution for U that will take the state to equilibrium

Problem 2. (4 pts) Add an extra input in the non-linear DIPC model, namely, the torque at the first joint. Thus the system's inputs are

$$u = [u_1 \quad u_2]^\top,$$

where u_1 is the force applied to the cart and u_2 is the torque applied at the first joint. In summary, we now have a three-dimensional two-input system.

Show that there is no $u_e = [u_{1e} \quad u_{2e}]^\top$ that would make $x_e = [0.1 \quad 60^\circ \quad 45^\circ \quad 0 \quad 0 \quad 0]^\top$ an equilibrium state.

```
syms u_1 u_2
u_new = [u_1; u_2];
H_new = [1 0;
          0 1;
          0 0];
qdd_new_1 = simplify(D\H_new*u_new - C*qd-G));
X_new_1 = [q;qd];
f_sym_new_1 = [qd; qdd_new_1]
f_sym_new_1 =
```

$$\begin{aligned}
& \frac{\partial}{\partial u_1} \left(\frac{280 u_1 - 981 \sin(2x_2) + 100 x_5^2 \sin(x_2) + 45 x_6^2 \sin(x_3) - 120 u_1 \cos(\sigma_4)}{20 \sigma_3} \right. \\
& \left. - \frac{1200 u_2 \cos(2x_3) - 8829 \sin(x_2 - 2x_3) - 30411 \sin(x_2) - 7600 u_2 + 1575 x_6^2 \sin(x_2 - x_3) + 250 x_5^2 \sin(2x_2)}{50 \sigma_3} \right. \\
& \left. - \frac{300 \sin(x_2 - x_3) x_5^2 + 135 \sin(\sigma_4) x_6^2 - 2943 \sigma_1 + 2943 \sin(x_3) + 200 u_1 \cos(2x_2 - x_3) + 40}{75 \cos(2x_2) + 135 \cos(\sigma_4) - 390} \right) \\
& \quad x_4 \\
& \quad x_5 \\
& \quad x_6
\end{aligned}$$

where

$$\sigma_1 = \sin(2x_2 - x_3)$$

$$\sigma_2 = \cos(x_2 - 2x_3)$$

$$\sigma_3 = 5 \cos(2x_2) + 9 \cos(\sigma_4) - 26$$

$$\sigma_4 = 2x_2 - 2x_3$$

```

syms u_e1 u_e2 real
q_val_1 = [0.1; deg2rad(60); deg2rad(45)];
qd_val_1 = [0; 0; 0];
G_val = double(subs(G, [x1 x2 x3 x4 x5 x6], [q_val_1' qd_val_1']));
eq = H_new*[u_e1 ; u_e2] == G_val;
sol_u = solve(eq, u_e1, u_e2, 'Real', true)

```

```

sol_u = struct with fields:
  u_e1: [0x1 sym]
  u_e2: [0x1 sym]

```

Problem 3. (4 pts) Add the third extra input in the non-linear DIPC model, namely, the torque at the second joint. Thus the system's input is

$$u = [u_1 \quad u_2 \quad u_3]^\top,$$

where u_1 is the force applied to the cart, u_2 is the torque applied at the first joint, and u_3 is the torque applied at the second joint. In summary, we now have a three-output three-input system.

Find $u_e = [u_{1e} \quad u_{2e} \quad u_{3e}]^\top$ that makes

$$x_e = [0.1 \quad 60^\circ \quad 45^\circ \quad 0 \quad 0 \quad 0]^\top$$

an equilibrium state.

```

syms u_3 u_e3 real

```

```

u_new_2 = [u_1; u_2; u_3];
H_new_2 = [1 0 0;
            0 1 0 ;
            0 0 1];
qdd_new_2 = simplify(D\H_new_2*u_new_2 - C*qd-G));
X_new_2 = [q;qd];
f_sym_new_2 = [qd; qdd_new_2]

```

$$\begin{aligned}
f_{sym_new_2} = & \left(\begin{array}{l} \\ \\ \\ \end{array} \right. \\
& - \frac{840 u_1 - 2943 \sin(2x_2) + 300 x_5^2 \sin(x_2) + 135 x_6^2 \sin(x_3) - 360 \sin(x_2 - x_3) - 26487 \sin(x_2 - 2x_3) - 91233 \sin(x_2) - 22800 u_2 + 4725 x_6^2 \sin(x_2 - x_3) + 750 x_5^2 \sin(x_2 - x_3) - 2700 \sin(x_2 - x_3) x_5^2 + 1215 \sin(\sigma_5) x_6^2 + 13600 u_3 - 26487 \sigma_1 + 26487 \sin(x_3)}{3600 u_2 \cos(2x_3) - 26487 \sin(x_2 - 2x_3) - 91233 \sin(x_2) - 22800 u_2 + 4725 x_6^2 \sin(x_2 - x_3) + 750 x_5^2 \sin(x_2 - x_3) - 2700 \sin(x_2 - x_3) x_5^2 + 1215 \sin(\sigma_5) x_6^2 + 13600 u_3 - 26487 \sigma_1 + 26487 \sin(x_3)} \\
& \left. \begin{array}{l} \\ \\ \\ \end{array} \right)
\end{aligned}$$

where

$$\sigma_1 = \sin(2x_2 - x_3)$$

$$\sigma_2 = \cos(2x_2 - x_3)$$

$$\sigma_3 = \cos(x_2 - 2x_3)$$

$$\sigma_4 = 5 \cos(2x_2) + 9 \cos(\sigma_5) - 26$$

$$\sigma_5 = 2x_2 - 2x_3$$

```

q_val_1 = [0.1; deg2rad(60); deg2rad(45)];
qd_val_1 = [0; 0; 0];
G_val = double(subs(G, [x1 x2 x3 x4 x5 x6], [q_val_1' qd_val_1']));
eq = H_new_2*[u_e1 ; u_e2 ; u_e3] == G_val;
sol_u = solve(eq, u_e1, u_e2, u_e3, 'Real', true);
u_e_new = double(struct2array(sol_u))

```

```

u_e_new = 1×3
    0    -5.3098    -3.9019

```

Problem 4. (4 pts) Perform Taylor's linearization about (x_e, u_e) .

```
A_sym_new = simplify(jacobian(f_sym_new_2, X));
B_sym_new = simplify(jacobian(f_sym_new_2, u_new_2));
vars = [x1; x2; x3; x4; x5; x6; u_1; u_2; u_3];
vals = [0.1; deg2rad(60); deg2rad(45); 0; 0; 0; u_e_new'];

A_lin_syms_new = double(subs(A_sym_new, vars, vals))
```

```
A_lin_syms_new = 6x6
    0         0         0    1.0000         0         0
    0         0         0         0    1.0000         0
    0         0         0         0         0    1.0000
    0   -0.5341   -1.1264         0         0         0
    0   22.5046  -17.8041         0         0         0
    0  -13.9883   21.7759         0         0         0
```

```
B_lin_syms_new = double(subs(B_sym_new, vars, vals))
```

```
B_lin_syms_new = 6x3
    0         0         0
    0         0         0
    0         0         0
    0.4252  -0.1742  -0.2887
   -0.1742   7.3409  -4.5629
   -0.2887  -4.5629   5.5808
```

Problem 5. (8 pts) Design a state-feedback controller, $u = -K_x x$, using LMIs and test it on the non-linear model.

Generate plots of the state variables versus time on the time interval $[0, 3]$ secs. When performing your simulations you have to use one of MATLAB's *ode* functions, for example, *ode23* or *ode45*. Compare their performance and see if you can notice any differences in your plots.

$$x_{\text{dot}} = Ax + Bu$$

$$x_{\text{dot}} = Ax + B(-K_x x)$$

$$x_{\text{dot}} = (A - BK_x)x$$

We need to create Lyapunov equation with this and then convert it into a format that can be solved using LMI

$$(A - BK)^T P + P(A - BK) < 0, P > 0$$

$$S = P^{-1}$$

$$Z = KS$$

$$SA^T + AS - Z^T B^T - BZ < 0, P > 0$$

We need to use the linearized matrices from the previous part

We need to solve the above equation as our LMI to get the state feedback controller design

```
n = 6 (size of A is (6,6))
```

```
m = 3 (size of B is (6,3))
```

```
cvx_begin sdp  
n = 6
```

```
n =  
6
```

```
m = 3
```

```
m =  
3
```

```
ep = 1e-6
```

```
ep =  
1.0000e-06  
  
variable S(n,n) symmetric  
variable Z(m,n)  
A_lin_syms_new*S + S*A_lin_syms_new' - Z'*B_lin_syms_new' - B_lin_syms_new*Z <= -ep*eye(n)  
S >= ep*eye(n)  
cvx_end
```

```
Calling SDPT3 4.0: 60 variables, 21 equality constraints
```

```
-----  
num. of constraints = 21  
dim. of sdp var = 12, num. of sdp blk = 2  
dim. of free var = 18 *** convert ublk to lblk  
*****  
SDPT3: Infeasible path-following algorithms  
*****  
version predcorr gam expon scale_data  
HKM 1 0.000 1 0  
it pstep dstep pinfeas dinfeas gap prim-obj dual-obj cputime  
-----  
0|0.000|0.000|5.2e+02|9.2e+02|2.0e+05| 0.000000e+00| 0.000000e+00| 0:0:00| chol 1 1  
1|1.000|0.884|6.0e-04|1.1e+02|5.6e+03| 0.000000e+00| 1.058790e-04| 0:0:00| chol 1 1  
2|1.000|0.988|2.0e-04|1.3e+00|2.4e+01| 0.000000e+00| 1.260239e-06| 0:0:01| chol 1 1  
3|1.000|0.989|5.0e-06|1.5e-02|1.8e-01| 0.000000e+00| 1.442981e-08| 0:0:01| chol 1 1  
4|1.000|0.990|1.2e-06|2.5e-04|3.6e-03| 0.000000e+00| 2.250779e-10| 0:0:01| chol 1 1  
5|1.000|1.000|5.4e-08|2.0e-04|5.7e-04| 0.000000e+00| 7.070191e-12| 0:0:01| chol 1 1  
6|1.000|0.978|1.3e-09|3.2e-05|8.2e-05| 0.000000e+00| 1.066474e-12| 0:0:01| chol 1 1  
7|1.000|0.989|9.7e-11|4.6e-06|1.0e-05| 0.000000e+00| 1.182627e-14| 0:0:01| chol 1 1  
8|1.000|0.962|3.1e-13|5.7e-07|1.3e-06| 0.000000e+00| 8.990980e-15| 0:0:01| chol 1 1  
9|1.000|0.828|3.0e-13|7.1e-08|1.6e-07| 0.000000e+00| 2.503882e-15| 0:0:01| chol 1 1  
10|1.000|0.863|2.0e-12|8.9e-09|2.1e-08| 0.000000e+00| 5.397701e-16| 0:0:01| chol 1 1  
11|1.000|0.890|4.9e-13|1.2e-09|2.8e-09| 0.000000e+00| 8.372175e-17| 0:0:01|  
stop: max(relative gap, infeasibilities) < 1.49e-08  
-----
```

```
number of iterations = 11  
primal objective value = 0.00000000e+00  
dual objective value = 8.37217523e-17  
gap := trace(XZ) = 2.76e-09  
relative gap = 2.76e-09
```

```

actual relative gap      = -8.37e-17
rel. primal infeas (scaled problem) = 4.94e-13
rel. dual      "      "      "      = 1.16e-09
rel. primal infeas (unscaled problem) = 0.00e+00
rel. dual      "      "      "      = 0.00e+00
norm(X), norm(y), norm(Z) = 7.1e+01, 2.3e-11, 7.8e-10
norm(A), norm(b), norm(C) = 9.4e+01, 1.0e+00, 1.0e+00
Total CPU time (secs)   = 0.77
CPU time per iteration = 0.07
termination code        = 0
DIMACS: 4.9e-13  0.0e+00  1.2e-09  0.0e+00  -8.4e-17  2.8e-09
-----
```

```

Status: Solved
Optimal value (cvx_optval): +0
```

K_cvx = Z/S

```

K_cvx = 3×6
0.5059    0.7096    1.4190    1.9847    0.5756    0.7611
0.0858    5.2626    2.4848    0.4269    1.1523    1.1960
0.1171    1.5430    8.7194    0.5831    1.2254    1.8557
```

Controller gain matrix K has been computed using the CVX solver. I will proceed to plot the simulation graphs.

A_cvx = A_lin_syms_new-B_lin_syms_new*K_cvx

```

A_cvx = 6×6
0         0         0     1.0000         0         0
0         0         0         0     1.0000         0
0         0         0         0         0     1.0000
-0.1664   0.5265   1.2203   -0.6012   0.3097   0.4205
-0.0074  -8.9635   3.9880   -0.1271  -2.7669  -0.1801
-0.1158   1.6182  -15.1377  -0.7336  -1.4150  -4.6790
```

```
%Checking the poles of the new system
poles = eig(A_cvx);
disp('Poles of the new system:');
```

Poles of the new system:

disp(poles);

```

-0.3433 + 0.2471i
-0.3433 - 0.2471i
-1.5654 + 3.4358i
-1.5654 - 3.4358i
-2.1149 + 2.1402i
-2.1149 - 2.1402i
```

Poles are all in open left hand plane. It is a stable design

```
% Define the state variables for the function handles
X_vars = [x1; x2; x3; x4; x5; x6];

% Create the required .m files in your current folder
matlabFunction(D, 'File', 'D_func', 'Vars', {X_vars.'}, 'Optimize', false);
```

```

matlabFunction(C, 'File', 'C_func', 'Vars', {X_vars.'}, 'Optimize', false);
matlabFunction(G, 'File', 'G_func', 'Vars', {X_vars.'}, 'Optimize', false);

tspannew = [0 10];
x0 = [0.1; deg2rad(60); deg2rad(45); 0; 0; 0]; % Initial conditions

odefun = @(t,x) nonlinear_closed_loop(t, x, K_cvx, u_e_new', x0);

opts = odeset('RelTol', 1e-6, 'AbsTol', 1e-9);
[t45, x45] = ode45(odefun, tspannew, x0, opts);
[t23, x23] = ode23(odefun, tspannew, x0, opts);

% --- Plotting Results ---
% --- Plotting Results ---
figure('Position', [100, 100, 1200, 800]);

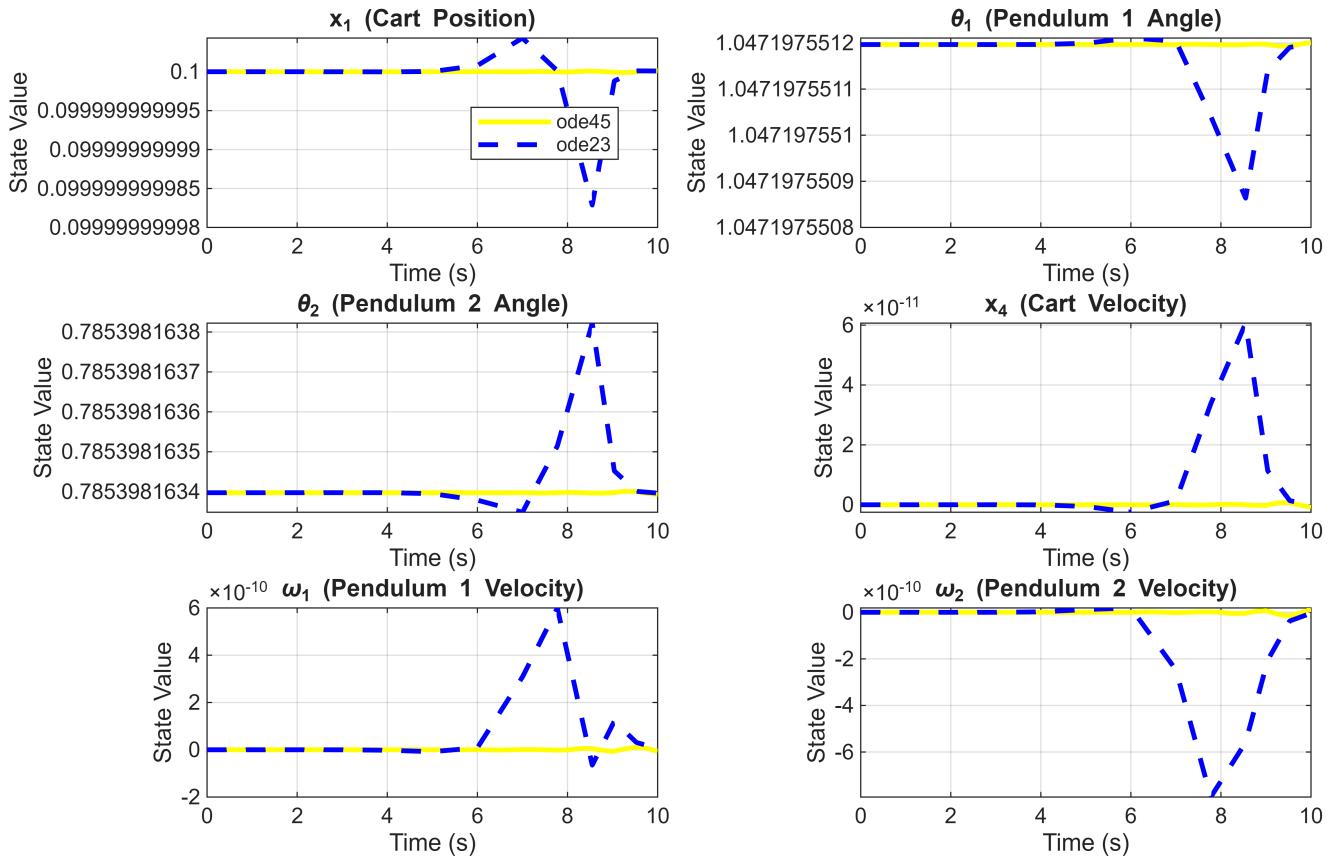
sgtitle('State Variables vs. Time (ode45 vs. ode23)', 'FontSize', 16, 'FontWeight',
'bold');

state_names = {'x_1 (Cart Position)', '\theta_1 (Pendulum 1 Angle)', '\theta_2
(Pendulum 2 Angle)', ...
               'x_4 (Cart Velocity)', '\omega_1 (Pendulum 1 Velocity)', '\omega_2
(Pendulum 2 Velocity)'};

for i = 1:6
    subplot(3, 2, i);
    % Changed plot colors to yellow ('y-') and blue ('b--')
    plot(t45, x45(:,i), 'y-', 'LineWidth', 2);
    hold on;
    plot(t23, x23(:,i), 'b--', 'LineWidth', 2);
    grid on;
    title(state_names{i});
    xlabel('Time (s)');
    ylabel('State Value');
    if i == 1
        legend('ode45', 'ode23', 'Location', 'best');
    end
end

```

State Variables vs. Time (ode45 vs. ode23)



```

function dx = nonlinear_closed_loop(t, x, K, u_e, x_e)

% Decompose state vector
q    = x(1:3);
qd   = x(4:6);

% Evaluate dynamics matrices at the current state.
% These call the .m files we generated with matlabFunction.
D_mat = D_func(x.');
```

% Pass state as a row vector

```

C_mat = C_func(x.');
```

```

G_vec = G_func(x.');
```

% Calculate the state-feedback control input

```

u = u_e - K * (x - x_e); % u is 3x1
```

% Input matrix H is the identity matrix

```

H_mat = eye(3);
```

qdd = D_mat \ (H_mat * u - C_mat * qd - G_vec); % Ensure G is a column vector

% Return the state derivative vector

```

dx = [qd; qdd];
```

```
end
```

Problem 6. (4 pts) Use LMIs to design an output-feedback controller, $u = -K_o y$. Generate plots of state variables versus time on the time interval $[0, 3]$ secs. This can be one figure with subplots.

$$\dot{x} = Ax + Bu$$

$$y = Cx$$

$$u = -K_o y$$

$$u = -K_o Cx$$

$$\dot{x} = Ax + B(-K_o Cx)$$

$$\dot{x} = (A - BK_o C)x$$

$$(A - BK_o C)^T P + P(A - BK_o C) < 0, P > 0$$

$$A^T P + PA - C^T K^T M B^T - BM K C < 0$$

$$A^T P + PA - C^T N^T B^T - BN C < 0, BM = PB, P > 0$$

$$K = M^{-1}N$$

```
p = size(C,1);
C_new = [1 0 0 0 0 0;
          0 1 0 0 0 0;
          0 0 1 0 0 0];
cvx_begin sdp quiet
variable P(n,n) symmetric
variable N(m,p)
variable M(m,m)
P*A_lin_syms_new+A_lin_syms_new'*P-C_new'*N'*B_lin_syms_new'-
B_lin_syms_new*N*C_new<-ep*eye(n)
```

Warning: The use of strict inequalities in CVX is strongly discouraged,
because solvers treat them as non-strict inequalities. Please
consider using " \leq " instead.

```
B_lin_syms_new*M == P*B_lin_syms_new
P >= ep*eye(n);
cvx_end
K_o = M\N
```

```
K_o = 3x3
    1.1331    0.3146    0.4202
   -0.0227    3.9816    0.8455
   -0.0213    0.7901    5.2143
```

```
A_o = A_lin_syms_new - B_lin_syms_new*K_o*C_new;
eig(A_o)
```

```
ans = 6x1 complex
 0.0000 + 0.6546i
```

```

0.0000 - 0.6546i
0.0000 + 1.8611i
0.0000 - 1.8611i
-0.0000 + 1.7345i
-0.0000 - 1.7345i

```

$n \leq m + p - 1$ (where $n = 6$, $m = 3$, $p = 3$) is not satisfied in this case and we can see that the system is not stable in this case.

```

odefun2 = @(t,x) nonlinear_closed_loop2(t, x, K_o, u_e_new', x0,C_new);

opts = odeset('RelTol', 1e-6, 'AbsTol', 1e-9);
[t45_o, x45_o] = ode45(odefun2, tspannew, x0, opts);
[t23_o, x23_o] = ode23(odefun2, tspannew, x0, opts);
figure('Position', [100, 100, 1200, 800]);

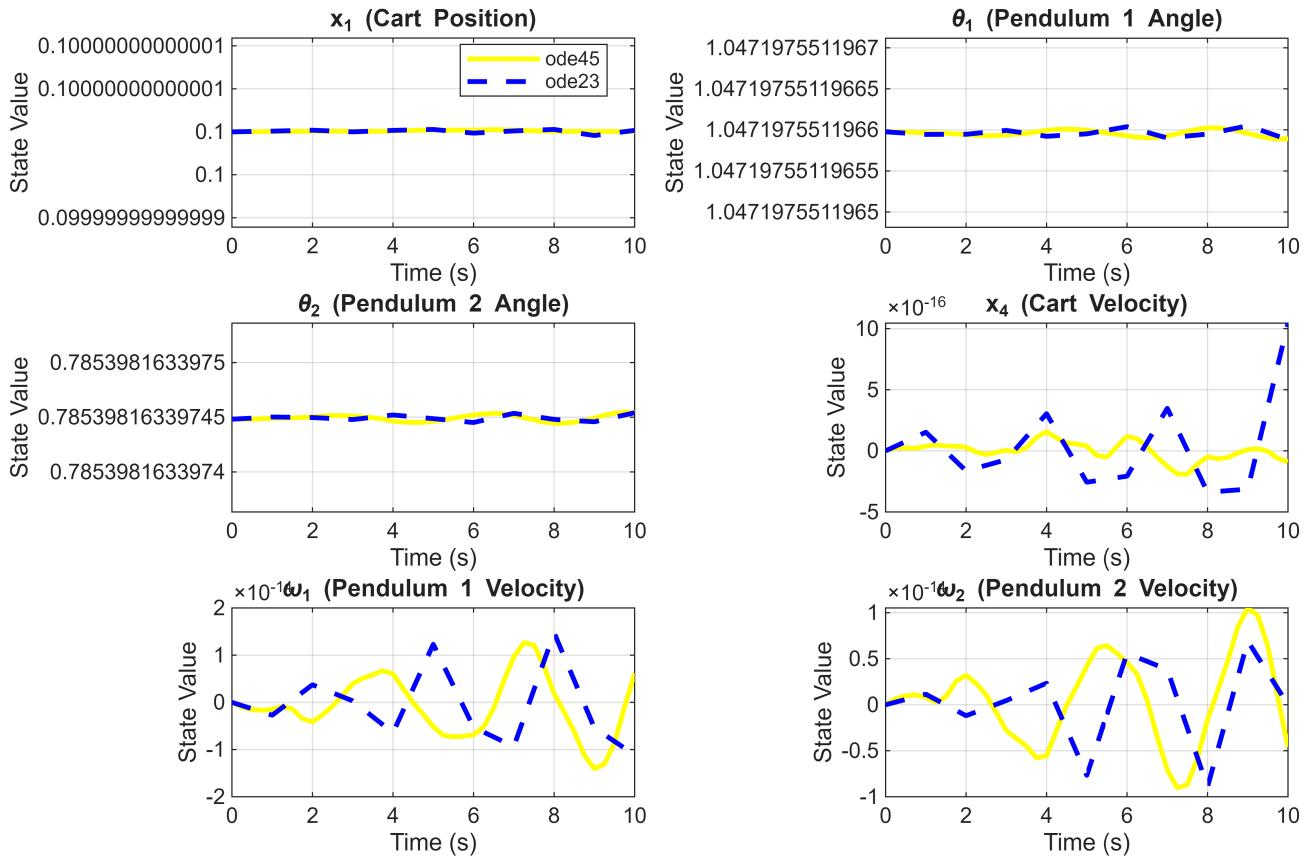
sgtitle('State Variables vs. Time (ode45 vs. ode23)', 'FontSize', 16, 'FontWeight',
'bold');

state_names = {'x_1 (Cart Position)', '\theta_1 (Pendulum 1 Angle)', '\theta_2
(Pendulum 2 Angle)', ...
               'x_4 (Cart Velocity)', '\omega_1 (Pendulum 1 Velocity)', '\omega_2
(Pendulum 2 Velocity)'};

for i = 1:6
    subplot(3, 2, i);
    plot(t45_o, x45_o(:,i), 'y-', 'LineWidth', 2);
    hold on;
    plot(t23_o, x23_o(:,i), 'b--', 'LineWidth', 2);
    grid on;
    title(state_names{i});
    xlabel('Time (s)');
    ylabel('State Value');
    if i == 1
        legend('ode45', 'ode23', 'Location', 'best');
    end
end

```

State Variables vs. Time (ode45 vs. ode23)



```

function dx = nonlinear_closed_loop2(t, x, K, u_e, x_e,C_k)

q    = x(1:3);
qd   = x(4:6);

D_mat = D_func(x. ');
C_mat = C_func(x. ');
G_vec = G_func(x. ');

u = u_e-K*C_k*(x-x_e);

H_mat = eye(3);

qdd = D_mat \ (H_mat * u - C_mat * qd - G_vec);

dx = [qd; qdd];
end

```

Problem 7. (4 pts) Simulate the combined state-feedback controller-observer compensator and compare its performance against the output feedback controller.

Generate plots of state variables versus time, where \tilde{x}_i is an estimate of x_i . Note that you can always set your observer's initial conditions to zero, if you wish, since you have complete access to your design.

For combined state feedback controller-observer compensator we have:

We already checked the eigenvalues of A-BK which were in open left hand plane, for the observer we have:

$$(A - LC)^T P + P(A - LC) < 0$$

$$P = P^T, P > 0$$

$$A^T P + PA - C^T L^T P - PLC < 0$$

$$A^T P + PA - C^T Y^T - YC + 2\alpha P \leq 0, P > 0$$

$$L = P^{-1}Y$$

```
cvx_begin sdp
variable P(n,n) symmetric
variable Y(n,p)
P*A_lin_syms_new + A_lin_syms_new'*P - C_new'*Y'-Y*C_new + P <= 0
P >= eps*eye(n)
cvx_end
```

Calling SDPT3 4.0: 56 variables, 17 equality constraints

```
-----
num. of constraints = 17
dim. of sdp var = 12, num. of sdp blk = 2
dim. of free var = 14 *** convert ublk to lblk
*****
***** SDPT3: Infeasible path-following algorithms *****
***** version predcorr gam expon scale_data *****
      HKM    1    0.000    1    0
it pstep dstep pinfeas dinfeas   gap      prim-obj      dual-obj      cputime
-----
0|0.000|0.000|4.0e+02|1.8e+02|2.5e+04| 0.000000e+00| 0.000000e+00| 0:0:00| chol 1 1
1|0.961|0.844|1.6e+01|2.8e+01|1.2e+03| 0.000000e+00| 1.688997e-14| 0:0:00| chol 1 1
2|1.000|0.896|1.5e-05|3.0e+00|7.3e+01| 0.000000e+00| 6.705122e-15| 0:0:00| chol 1 1
3|1.000|0.988|6.6e-06|3.5e-02|7.3e-01| 0.000000e+00| 8.077666e-17| 0:0:00| chol 1 1
4|1.000|0.990|9.2e-07|4.6e-04|9.4e-03| 0.000000e+00| 1.099275e-18| 0:0:00| chol 1 1
5|1.000|0.998|4.5e-08|1.1e-05|2.2e-04| 0.000000e+00| 2.790843e-20| 0:0:00| chol 1 1
6|1.000|1.000|2.0e-09|1.3e-05|4.3e-05| 0.000000e+00| 2.544383e-21| 0:0:00| chol 1 1
7|1.000|0.989|1.0e-10|2.5e-06|5.6e-06| 0.000000e+00| 2.773511e-23| 0:0:00| chol 1 1
8|1.000|0.969|4.9e-13|3.3e-07|7.3e-07| 0.000000e+00| 3.683199e-24| 0:0:00| chol 1 1
9|1.000|0.774|1.0e-13|4.2e-08|9.6e-08| 0.000000e+00| 1.067711e-24| 0:0:00| chol 1 1
10|1.000|0.846|4.4e-13|5.6e-09|1.3e-08| 0.000000e+00| 2.695667e-25| 0:0:00|
stop: max(relative gap, infeasibilities) < 1.49e-08
-----
number of iterations = 10
primal objective value =  0.00000000e+00
dual objective value =  2.69566748e-25
gap := trace(XZ) = 1.32e-08
```

```

relative gap          = 1.32e-08
actual relative gap   = -2.70e-25
rel. primal infeas (scaled problem) = 4.35e-13
rel. dual      "      "      "      = 5.60e-09
rel. primal infeas (unscaled problem) = 0.00e+00
rel. dual      "      "      "      = 0.00e+00
norm(X), norm(y), norm(Z) = 6.4e+01, 1.2e-10, 4.0e-09
norm(A), norm(b), norm(C) = 8.8e+01, 1.0e+00, 1.0e+00
Total CPU time (secs)   = 0.20
CPU time per iteration = 0.02
termination code        = 0
DIMACS: 4.4e-13  0.0e+00  5.6e-09  0.0e+00  -2.7e-25  1.3e-08
-----
```

```

Status: Solved
Optimal value (cvx_optval): +0
```

$L = P \setminus Y$

```

L = 6x3
2.0286  -0.0808  -0.0754
-0.1215   4.7416  -1.6842
-0.2884  -1.3439   4.4698
2.8472  -0.4678  -1.9145
0.2812  52.9516  -40.3881
-1.9718 -36.9974   47.1164
```

```

A_l = A_lin_syms_new - L*C_new;
eigenvalues = eig(A_l)
```

```

eigenvalues = 6x1 complex
-3.0645 + 6.4422i
-3.0645 - 6.4422i
-1.0264 + 1.2420i
-1.0264 - 1.2420i
-1.5291 + 1.6701i
-1.5291 - 1.6701i
```

Eigenvalues of the observer are in the open left hand plane.

We have

$$\delta x_{\text{dot}} = (A - LC)\delta x + B\delta u$$

$$\delta y = C\delta x + D\delta u,$$

For combined observer controller compensator :

$$z_{\text{dot}} = Az + B\delta u + L(\delta y - \delta y_{\text{est}})$$

$$\delta y_{\text{est}} = Cz + D\delta u$$

$$\delta u = -Kz + v (\text{will set } v \text{ to 0})$$

where z is estimator of x or x_{est}

$$(\delta y - \delta y_{\text{est}}) = C(\delta x - z)$$

$$z_{\text{dot}} = (A - BK - LC)z + LC\delta x$$

Here K is out K_{cvx} which we calculated for Problem 5, we calculated L above.

Let's combine them for Combined Observer-Controller Compensator

```

function dx_aug_dt = nonlinear_combined_loop(t, x_aug, K, L, A, B, C, x_e, u_e)
    x_real = x_aug(1:6);
    z = x_aug(7:12);
    u_dev = -K*z;
    u = u_e - K*z;
    q_real = x_real(1:3);
    qd_real = x_real(4:6);
    D_mat = D_func(x_real.');
    C_mat = C_func(x_real.');
    G_vec = G_func(x_real.');
    H_mat = eye(3);
    qdd_real = D_mat \ (H_mat*u - C_mat*qd_real - G_vec);
    dx_real_dt = [qd_real; qdd_real];
    y_dev_real = C*(x_real-x_e);
    y_dev_est = C*z;
    dz_dt = A*z + B*u_dev + L * (y_dev_real - y_dev_est);
    dx_aug_dt = [dx_real_dt; dz_dt];
end

tspannew = [0 10];

x_e = [0.1; deg2rad(60); deg2rad(45); 0; 0; 0];
u_e = [0; -5.3098; -3.9019];

x0_real = [0.2; deg2rad(65); deg2rad(40); 0; 0; 0];

z0 = zeros(6,1);

x_aug_0 = [x0_real; z0];

% --- Run the Simulation ---
opts = odeset('RelTol', 1e-6, 'AbsTol', 1e-9);
odefun_obs = @(t,x_aug) nonlinear_combined_loop(t, x_aug, K_cvx, L, ...
    A_lin_syms_new, B_lin_syms_new, C_new, x_e, u_e);

[t_obs, x_obs_aug] = ode45(odefun_obs, tspannew, x_aug_0, opts);

x_real = x_obs_aug(:, 1:6);
z = x_obs_aug(:, 7:12);
x_est = z + x_e'; % Add x_e to each row

% --- Plotting Results for Problem 7 ---
figure('Position', [100, 100, 1200, 800]);
sgtitle('Problem 7: Combined State-Feedback Controller-Observer', 'FontSize', 16,
'FontWeight', 'bold');

state_names = {'x_1 (Cart Position)', '\theta_1 (Pendulum 1 Angle)', '\theta_2
(Pendulum 2 Angle)', ...
    'x_4 (Cart Velocity)', '\omega_1 (Pendulum 1 Velocity)', '\omega_2
(Pendulum 2 Velocity)'};

```

```

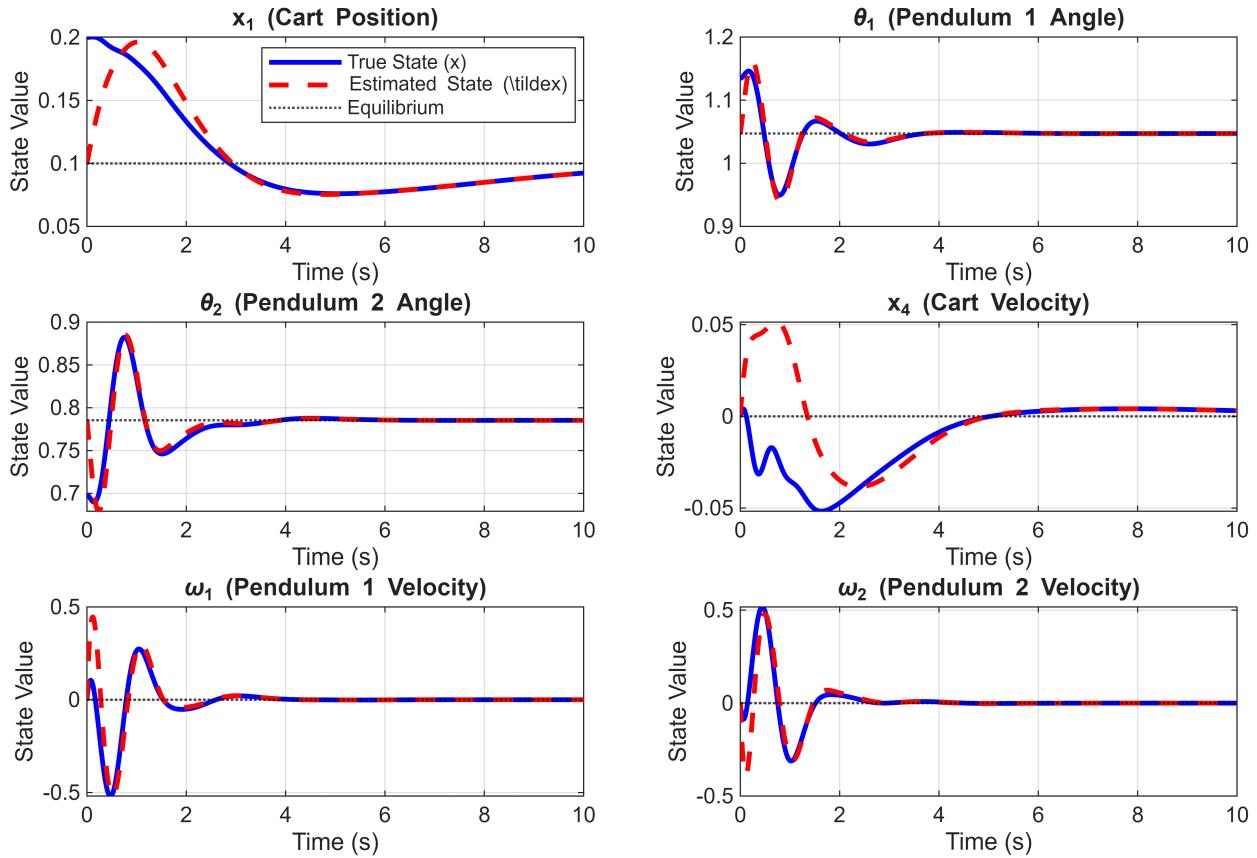
for i = 1:6
    subplot(3, 2, i);
    plot(t_obs, x_real(:,i), 'b-', 'LineWidth', 2);
    hold on;
    plot(t_obs, x_est(:,i), 'r--', 'LineWidth', 2);

    % Plot the equilibrium line
    yline(x_e(i), 'k:', 'LineWidth', 1);

    grid on;
    title(state_names{i});
    xlabel('Time (s)');
    ylabel('State Value');
    if i == 1
        legend('True State (x)', 'Estimated State (\tilde{x})', 'Equilibrium',
        'Location', 'best');
    end
end

```

Problem 7: Combined State-Feedback Controller-Observer



Now, checking the output-feedback vs combined state feedback controller-observer

```

figure('Position',[100 100 1200 800]);
sgtitle('Problem 7: Output-Feedback vs Combined Observer-Controller (Estimated
States)', ...
    'FontSize',14,'FontWeight','bold');

state_names = {'x_1 (Cart Position)', '\theta_1 (Pendulum 1 Angle)', '\theta_2
(Pendulum 2 Angle)', ...
    'x_4 (Cart Velocity)', '\omega_1 (Pendulum 1 Velocity)', '\omega_2
(Pendulum 2 Velocity)'};
[t45_oo, x45_oo] = ode45(odefun2, tspannew, x0_real, opts);

for i = 1:6
    subplot(3,2,i);

    % True state from output-feedback controller
    plot(t45_oo, x45_oo(:,i), 'g-', 'LineWidth', 1.8); hold on;

    % Estimated state from combined observer-controller
    plot(t_obs, x_est(:,i), 'y--', 'LineWidth', 1.8);

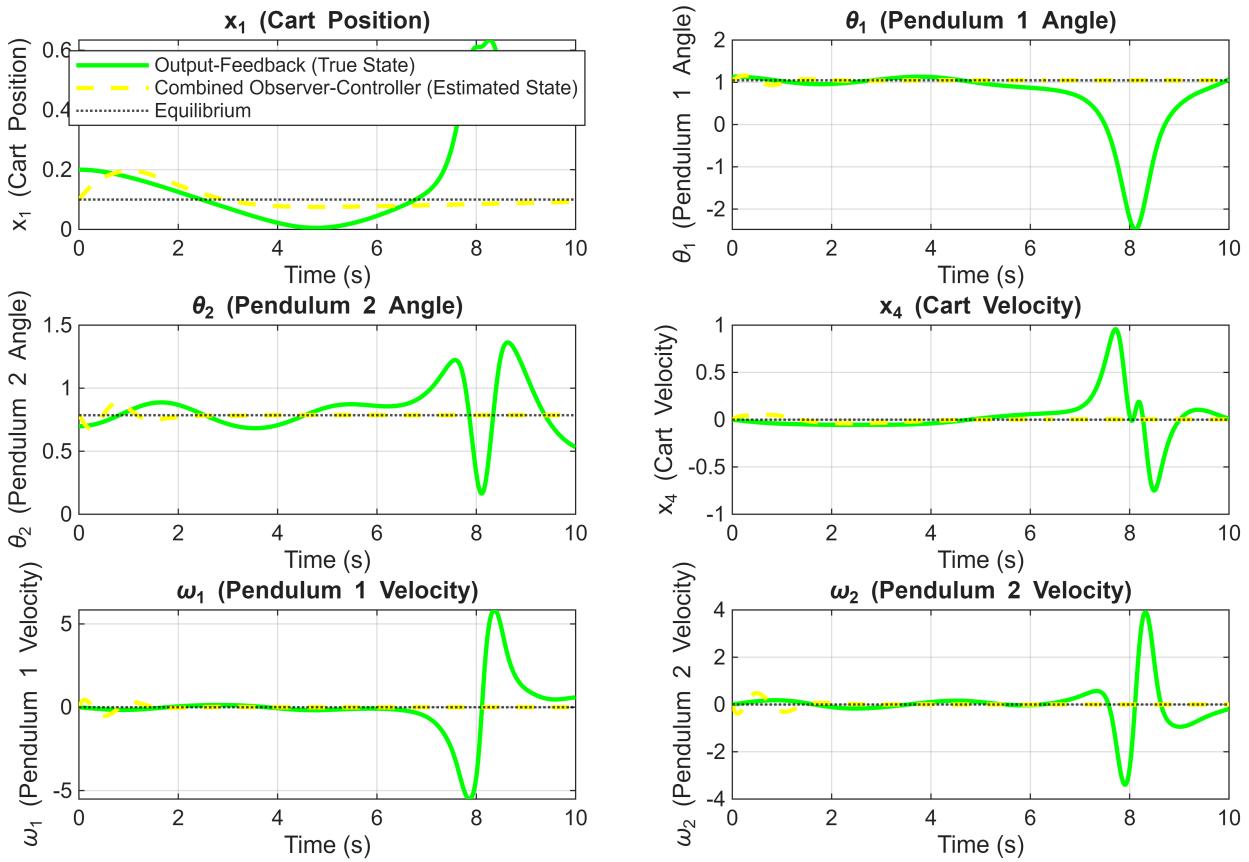
    % Equilibrium reference line
    yline(x_e(i), 'k:', 'LineWidth', 1);

    grid on;
    xlabel('Time (s)');
    ylabel(state_names{i});
    title(state_names{i});

    if i == 1
        legend('Output-Feedback (True State)', ...
            'Combined Observer-Controller (Estimated State)', ...
            'Equilibrium', 'Location', 'best');
    end
end

```

Problem 7: Output-Feedback vs Combined Observer-Controller (Es)



We can clearly see that the output feedback has failed to stabilize. This was anyways bound to happen because the poles were placed at the imaginary axis. But we can see that in long run combined observer controller does better.

For problem 8:

We need our observer poles atleast 3-4 times behind the controller poles in the open left hand plane, let's try to redesign by choosing some value of α that will give us sufficient value for it.

```
alpha = 4
```

```
alpha =
4

cvx_begin sdp
variable P_new(n,n) symmetric
variable Y_new(n,p)
P_new*A_lin_syms_new + A_lin_syms_new'*P_new - C_new'*Y_new - Y_new*C_new +
2*alpha*P_new <= 0
P_new >= eps*eye(n)
cvx_end
```

```
Calling SDPT3 4.0: 56 variables, 17 equality constraints
```

```
-----  
num. of constraints = 17  
dim. of sdp var = 12, num. of sdp blk = 2  
dim. of free var = 14 *** convert ublk to lblk  
*****  
SDPT3: Infeasible path-following algorithms  
*****  
version predcorr gam expon scale_data  
HKM 1 0.000 1 0  
it pstep dstep pinfeas dinfeas gap prim-obj dual-obj cputime  
-----  
0|0.000|0.000|4.5e+02|1.8e+02|2.5e+04| 0.000000e+00 0.000000e+00| 0:0:00| chol 1 1  
1|0.931|0.941|3.1e+01|1.1e+01|5.2e+02| 0.000000e+00 2.876690e-14| 0:0:00| chol 1 1  
2|1.000|0.794|5.0e-05|2.2e+00|5.4e+01| 0.000000e+00 2.517729e-14| 0:0:00| chol 1 1  
3|1.000|0.988|9.5e-06|2.8e-02|5.8e-01| 0.000000e+00 3.177904e-16| 0:0:00| chol 1 1  
4|1.000|0.992|1.6e-06|3.3e-04|6.7e-03| 0.000000e+00 3.615910e-18| 0:0:00| chol 1 1  
5|1.000|1.000|5.5e-07|1.0e-05|2.0e-04| 0.000000e+00 9.691114e-20| 0:0:00| chol 1 1  
6|1.000|1.000|1.2e-08|1.1e-05|3.6e-05| 0.000000e+00 9.387425e-21| 0:0:00| chol 1 1  
7|1.000|0.987|6.5e-10|2.0e-06|4.2e-06| 0.000000e+00 2.047189e-22| 0:0:00| chol 1 1  
8|1.000|0.973|8.2e-12|2.4e-07|4.7e-07| 0.000000e+00 2.087649e-23| 0:0:00| chol 1 1  
9|1.000|0.974|5.3e-13|2.7e-08|5.3e-08| 0.000000e+00 2.385924e-24| 0:0:00| chol 1 1  
10|1.000|0.854|9.1e-14|3.0e-09|6.1e-09| 0.000000e+00 5.052433e-25| 0:0:00|  
stop: max(relative gap, infeasibilities) < 1.49e-08  
-----  
number of iterations = 10  
primal objective value = 0.00000000e+00  
dual objective value = 5.05243336e-25  
gap := trace(XZ) = 6.12e-09  
relative gap = 6.12e-09  
actual relative gap = -5.05e-25  
rel. primal infeas (scaled problem) = 9.13e-14  
rel. dual " " " = 3.00e-09  
rel. primal infeas (unscaled problem) = 0.00e+00  
rel. dual " " " = 0.00e+00  
norm(X), norm(y), norm(Z) = 5.3e+01, 1.9e-10, 2.5e-09  
norm(A), norm(b), norm(C) = 9.2e+01, 1.0e+00, 1.0e+00  
Total CPU time (secs) = 0.22  
CPU time per iteration = 0.02  
termination code = 0  
DIMACS: 9.1e-14 0.0e+00 3.0e-09 0.0e+00 -5.1e-25 6.1e-09  
-----
```

```
Status: Solved
```

```
Optimal value (cvx_optval): +0
```

```
L_new = P_new\Y_new
```

```
L_new = 6x3  
11.6989 -0.1113 -0.1233  
-0.8345 17.1915 1.3549  
-1.5255 0.4878 18.0611  
60.0531 -0.8879 -2.4854  
2.9333 104.5949 -25.1762  
-3.2046 -21.8558 104.2521
```

```
eig(A_lin_syms_new-L_new*C_new)
```

```
ans = 6x1 complex
```

```
-12.6832 + 0.0000i  
-5.8284 + 5.0757i  
-5.8284 - 5.0757i  
-5.9172 + 0.0000i  
-8.3472 + 4.4935i  
-8.3472 - 4.4935i
```

```
eig(A_lin_syms_new - B_lin_syms_new*K_cvx)
```

```
ans = 6x1 complex  
-0.3433 + 0.2471i  
-0.3433 - 0.2471i  
-1.5654 + 3.4358i  
-1.5654 - 3.4358i  
-2.1149 + 2.1402i  
-2.1149 - 2.1402i
```

f_sym =

$$\left\{ \begin{array}{l} x_4 \\ x_5 \\ x_6 \\ - \frac{280 u - 981 \sin(2x_2) + 100 x_3^2 \sin(x_2) + 45 x_6^2 \sin(x_3) - 120 u \cos(x_3) + 45 x_6^2 \sigma_1}{20 \sigma_2} \\ \frac{1575 x_6^2 \sin(x_2 - x_3) - 30411 \sin(x_2) - 8829 \sin(x_2 - 2x_3) + 250 x_3^2 \sin(2x_2) + 1400 u \cos(x_2) + 450 x_3^2 \sin(x_3) - 600 u \cos(x_2 - 2x_3) + 225 x_6^2 \sin(x_2 + x_3)}{50 \sigma_2} \\ - \frac{300 \sin(x_2 - x_3) x_3^2 + 135 \sin(x_3) x_6^2 - 2943 \sigma_1 + 2943 \sin(x_3) + 200 u \cos(2x_2 - x_3) - 200 u \cos(x_3)}{75 \cos(2x_2) + 135 \cos(x_3) - 390} \end{array} \right\}$$

f_sym_new_1 =

$$\left\{ \begin{array}{l} x_4 \\ x_5 \\ x_6 \\ -\frac{280 u_1 - 981 \sin(2x_2) + 100 x_5^2 \sin(x_2) + 45 x_6^2 \sin(x_3) - 120 u_1 \cos(\sigma_4) - 560 u_2 \cos(x_2) + 45 x_6^2 \sigma_1 + 240 u_2 \sigma_2}{20 \sigma_3} \\ \frac{1200 u_2 \cos(2x_3) - 8829 \sin(x_2 - 2x_3) - 30411 \sin(x_2) - 7600 u_2 + 1575 x_6^2 \sin(x_2 - x_3) + 250 x_5^2 \sin(2x_2) + 1400 u_1 \cos(x_2) + 450 x_5^2 \sin(\sigma_4) - 600 u_1 \sigma_2 + 225 x_6^2 \sin(x_2 + x_3)}{50 \sigma_3} \\ -\frac{300 \sin(x_2 - x_3) x_5^2 + 135 \sin(\sigma_4) x_6^2 - 2943 \sigma_1 + 2943 \sin(x_3) + 200 u_1 \cos(2x_2 - x_3) + 400 u_2 \cos(x_2 + x_3) - 200 u_1 \cos(x_3) - 1360 u_2 \cos(x_2 - x_3)}{75 \cos(2x_2) + 135 \cos(\sigma_4) - 390} \end{array} \right\}$$

where

$$\sigma_1 = \sin(2x_2 - x_3)$$

$$\sigma_2 = \cos(x_2 - 2x_3)$$

$$\sigma_3 = 5 \cos(2x_2) + 9 \cos(\sigma_4) - 26$$

$$\sigma_4 = 2x_2 - 2x_3$$

```
f_sym_new_2 =
```

$$\left\{ \begin{array}{l} x_4 \\ x_5 \\ x_6 \\ - \frac{840 u_1 - 2943 \sin(2x_2) + 300 x_5^2 \sin(x_2) + 135 x_6^2 \sin(x_3) - 360 u_1 \cos(\sigma_3) + 800 u_3 \sigma_2 - 1680 u_2 \cos(x_2) - 800 u_3 \cos(x_3) + 135 x_6^2 \sigma_1 + 720 u_2 \sigma_3}{60 \sigma_4} \\ - \frac{3600 u_2 \cos(2x_3) - 26487 \sin(x_2 - 2x_3) - 91233 \sin(x_2) - 22800 u_2 + 4725 x_6^2 \sin(x_2 - x_3) + 750 x_5^2 \sin(2x_2) - 4000 u_3 \cos(x_2 + x_3) + 4200 u_1 \cos(x_2) + 1350 x_5^2 \sin(\sigma_3) - 1800 u_1 \sigma_3 + 13600 u_3 \cos(x_2 - x_3) + 675 x_6^2 \sin(x_2 + x_3)}{150 \sigma_4} \\ - \frac{2700 \sin(x_2 - x_3) x_5^2 + 1215 \sin(\sigma_3) x_6^2 + 13600 u_3 - 26487 \sigma_1 + 26487 \sin(x_3) - 4000 u_3 \cos(2x_2) + 1800 u_1 \sigma_2 + 3600 u_2 \cos(x_2 + x_3) - 1800 u_1 \cos(x_3) - 12240 u_2 \cos(x_2 - x_3)}{135 \sigma_4} \end{array} \right\}$$

```

1 %% DIPC: Nonlinear sim + observer-controller + 3D animation (updated for 30s + video)
2 clear; clc; close all;
3
4 % -----
5 % System parameters
6 % -----
7 M = 1.5; m1 = 0.5; l1 = 0.5; m2 = 0.75; l2 = 0.75; g = 9.81;
8
9 % Equilibrium (from earlier)
10 x_e = [0.1; deg2rad(60); deg2rad(45); 0; 0; 0];
11 u_e = [0; -5.3098; -3.9019];
12
13 % Linearized matrices
14 A = [ 0, 0, 0, 1.0000, 0, 0;
15      0, 0, 0, 0, 1.0000, 0;
16      0, 0, 0, 0, 0, 1.0000;
17      0, -0.5341, -1.1264, 0, 0, 0;
18      0, 22.5046, -17.8041, 0, 0, 0;
19      0, -13.9883, 21.7759, 0, 0, 0 ];
20 B = [ 0, 0, 0; 0, 0, 0; 0, 0, 0;
21      0.4252, -0.1742, -0.2887;
22      -0.1742, 7.3409, -4.5629;
23      -0.2887, -4.5629, 5.5808 ];
24 C = [1 0 0 0 0 0;
25      0 1 0 0 0 0;
26      0 0 1 0 0 0];
27
28 % Controller K
29 K = [ 0.5059, 0.7096, 1.4190, 1.9847, 0.5756, 0.7611;
30      0.0858, 5.2626, 2.4848, 0.4269, 1.1523, 1.1960;
31      0.1171, 1.5430, 8.7194, 0.5831, 1.2254, 1.8557 ];
32
33 alpha = 4;
34 n = size(A,1); p = size(C,1); ep = 1e-6;
35 L = [];
36 try
37     cvx_begin sdp quiet
38         variable P(n,n) symmetric
39         variable Y(n,p)
40         A'*P + P*A + 2*alpha*P - C'*Y' - Y*C <= -ep*eye(n)
41         P >= ep*eye(n)
42     cvx_end
43     if exist('cvx_status','var') && strcmpi(cvx_status,'Solved')
44         L = P\Y;
45     end
46 catch
47 end
48 if isempty(L)
49     warning('CVX/L not available – using backup observer gain.');
50     L = eye(n,p)*5;
51 end
52
53
54 tspan = [0 15];
55 x0_real = [3; 0; 0; 0; 0; 0];
56 z0 = zeros(6,1);
57 x_aug0 = [x0_real; z0];
58 params = struct('M',M,'m1',m1,'m2',m2,'l1',l1,'l2',l2,'g',g);
59 opts = odeset('RelTol',1e-6,'AbsTol',1e-9);
60

```

```

61 [t_out, x_aug_out] = ode45(@(t,xa) aug_dynamics(t,xa,K,L,A,B,C,x_e,u_e,params), tspan, x_aug0,
62 opts);
63 frameRate = 30;
64 t_uniform = linspace(t_out(1), t_out(end), ceil(frameRate*(t_out(end)-t_out(1)))); 
65 x_real = interp1(t_out, x_aug_out(:,1:6), t_uniform, 'linear', 'extrap');
66 t = t_uniform;
67
68 xc = x_real(:,1);
69 theta1 = x_real(:,2);
70 theta2 = x_real(:,3);
71 z_offset1 = 0.03; z_offset2 = -0.03;
72 p1x = xc + l1*sin(theta1); p1y = l1*cos(theta1);
73 p2x = p1x + l2*sin(theta2); p2y = p1y + l2*cos(theta2);
74
75 fig = figure('Name','DIPC 3D Animation','Color','w','Units','normalized','Position',[0.2 0.2 0.6
0.6]);
76 ax = axes('Parent',fig);
77 axis(ax,[-10 10 -0.2 2 -1 1]);
78 view(0,120); grid on; hold on;
79 xlabel('X'); ylabel('Y'); zlabel('Z');
80 title('Double Inverted Pendulum on Cart (3D)');
81 axis equal;
82 set(gcf,'Renderer','opengl');
83
84 [Xg,Zg] = meshgrid(-10:0.2:10, -1:0.2:1);
85 Yg = -0.05 * ones(size(Xg));
86 surf(Xg,Yg,Zg,'FaceColor',[0.95 0.95 0.95], 'EdgeColor','none', 'FaceAlpha',0.9);
87
88 CART_W = 0.5; CART_H = 0.2; CART_D = 0.3;
89 [XcCube, YcCube, ZcCube] = ndgrid([-CART_W/2, CART_W/2],[0, CART_H],[-CART_D/2, CART_D/2]);
90 cart_base_verts = [XcCube(:), YcCube(:), ZcCube(:)];
91 cart_faces = [1 2 4 3; 1 2 6 5; 2 4 8 6; 4 3 7 8; 3 7 5 1; 7 8 6 5];
92 init_x = xc(1);
93 cart_patch = patch('Vertices', cart_base_verts + [init_x 0 0], 'Faces', cart_faces, ...
94 'FaceColor',[0.8 0.2 0.2], 'EdgeColor','k');
95
96 hPend1 = plot3([0 0],[0 0],[0 0],'-','LineWidth',6,'Color',[0.2 0.8 0.2]);
97 hPend2 = plot3([0 0],[0 0],[0 0],'-','LineWidth',6,'Color',[0.2 0.2 0.8]);
98 hM1 = plot3(0,0,0,'o','MarkerSize',8,'MarkerFaceColor',[1 0 0],'MarkerEdgeColor','k');
99 hM2 = plot3(0,0,0,'o','MarkerSize',8,'MarkerFaceColor',[0 0 1],'MarkerEdgeColor','k');
100 camlight; lighting gouraud;
101
102
103 doSaveVideo = true;
104 videoFile = 'DIPC_3D.mp4';
105 if doSaveVideo
106     v = VideoWriter(videoFile,'MPEG-4');
107     v.FrameRate = frameRate;
108     v.Quality = 100;
109     open(v);
110 end
111
112 fprintf('Animating %d frames (%.1f s @ %d fps)\n', length(t), t(end)-t(1), frameRate);
113 hWait = waitbar(0,'Animating...','Name','DIPC Animation Progress');
114
115 for k = 1:length(t)
116     xk = xc(k);
117     p1 = [p1x(k), p1y(k), z_offset1];
118     p2 = [p2x(k), p2y(k), z_offset2];
119     hinge = [xk, CART_H, 0];

```

```

120      set(cart_patch,'Vertices',cart_base_verts + [xk 0 0]);
121      set(hPend1,'XData',[hinge(1),p1(1)],'YData',[hinge(2),p1(2)],'ZData',[hinge(3),p1(3)]);
122      set(hPend2,'XData',[p1(1),p2(1)],'YData',[p1(2),p2(2)],'ZData',[p1(3),p2(3)]);
123      set(hM1,'XData',p1(1),'YData',p1(2),'ZData',p1(3));
124      set(hM2,'XData',p2(1),'YData',p2(2),'ZData',p2(3));
125      xlim([xk-1.2, xk+1.2]);
126      drawnow;
127      frame = getframe(fig);
128
129      if doSaveVideo
130          writeVideo(v, frame);
131      end
132
133      if mod(k,ceil(length(t)/100))==0
134          waitbar(k/length(t),hWait,sprintf('Animating... %d%%',round(100*k/length(t))));
135      end
136
137 end
138
139
140 if doSaveVideo
141     close(v);
142     fprintf('◆ Video saved to: %s\n', fullfile(pwd, videoFile));
143 end
144 if ishandle(hWait), close(hWait); end
145 disp('Animation complete.');
146
147 function dx_aug = aug_dynamics(~,x_aug,K,L,A,B,C,x_e,u_e,params)
148     x_real = x_aug(1:6); z = x_aug(7:12);
149     u_dev = -K*z; u = u_e + u_dev;
150
151     try
152         if exist('compute_D','file')==2 && exist('compute_C','file')==2 &&
153         exist('compute_G','file')==2
154             Dm =
155             compute_D(x_real(1),x_real(2),x_real(3),params.M,params.m1,params.m2,params.l1,params.l2);
156             Cm =
157             compute_C(x_real(1),x_real(2),x_real(3),x_real(4),x_real(5),x_real(6),params.m1,params.m2,params.
158             l1,params.l2);
159             Gv =
160             compute_G(x_real(1),x_real(2),x_real(3),params.m1,params.m2,params.l1,params.l2,params.g);
161             qd = x_real(4:6);
162             qdd = Dm\eye(3)*u - Cm*qd - Gv;
163             dx_real = [qd; qdd];
164         else
165             x_dev = x_real - x_e;
166             dx_real = A*x_dev + B*(u - u_e);
167         end
168     catch
169         x_dev = x_real - x_e;
170         dx_real = A*x_dev + B*(u - u_e);
171     end
172
173     x_dev = x_real - x_e;
174     y_real_dev = C*x_dev;
175     y_est_dev = C*z;
176     dz = A*z + B*u_dev + L*(y_real_dev - y_est_dev);
177     dx_aug = [dx_real; dz];
178 end
179

```