

# 228.371 ASSIGNMENT 1

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1.

```
> t.test(gas$HeatRate,mu=9750, alternative='greater')
```

One Sample t-test

data: gas\$HeatRate

t = 3.8569, df = 31, p-value = 0.0002714

alternative hypothesis: true mean is greater than 9750

95 percent confidence interval:

10412.64    Inf

sample estimates:

mean of x

10932.44

Explain

Answer : Sample is not representative.



-2

2.

```
> t.test(gas$InletTemp, gas$ExhTemp, paired=TRUE)
```

Paired t-test

data: gas\$InletTemp and gas\$ExhTemp

t = 35.3892, df = 31, p-value < 2.2e-16

alternative hypothesis: true difference in means is not equal to 0

95 percent confidence interval:

621.139 697.111

sample estimates:

mean of the differences

659.125

Answer : P value is much smaller than 0.05, and then NULL hypothesis is rejected. The default value for NULL hypothesis is zero. So the mean reduction between InletTemp and ExhTemp exists, which value is between 621.139 and 697.111.



3.

```
> t.test(gas$Power[gas$Engine == "Advanced"],gas$Power[gas$Engine == "Traditional"],
alternative="greater")
```

#### Welch Two Sample t-test

data: gas\$Power[gas\$Engine == "Advanced"] and gas\$Power[gas\$Engine == "Traditional"]

t = 2.598, df = 21.509, p-value = 0.008297

alternative hypothesis: true difference in means is greater than 0

95 percent confidence interval:

29931.71    Inf  
sample estimates:  
mean of x mean of y  
153469.62 65017.33

What  
assumptions are  
required if your  
findings are to be  
generalised?

Answer:

on average

As shown above, p-value = 0.008297, alternative hypothesis: true difference in means is greater than 0. Hence the advanced engine have more power than the other.

-2



4

```
> t.test(InletTemp[Engine == 'Aeroderiv'],ExhTemp[Engine == 'Aeroderiv'],paired=TRUE)
```

#### Paired t-test

data: InletTemp[Engine == "Aeroderiv"] and ExhTemp[Engine == "Aeroderiv"]

t = 9.6462, df = 6, p-value = 7.11e-05

alternative hypothesis: true difference in means is not equal to 0

95 percent confidence interval:

438.0989 735.9011

sample estimates:

mean of the differences

587

```
> t.test(InletTemp[Engine == 'Advanced'],ExhTemp[Engine == 'Advanced'],paired=TRUE)
```

Paired t-test

data: InletTemp[Engine == "Advanced"] and ExhTemp[Engine == "Advanced"]

t = 66.5674, df = 12, p-value < 2.2e-16

alternative hypothesis: true difference in means is not equal to 0

95 percent confidence interval:

716.9696 765.4919

sample estimates:

mean of the differences

741.2308

```
> t.test(InletTemp[Engine == 'Traditional'],ExhTemp[Engine == 'Traditional'],paired=TRUE)
```

Paired t-test

data: InletTemp[Engine == "Traditional"] and ExhTemp[Engine == "Traditional"]

t = 51.2638, df = 11, p-value = 1.914e-14

alternative hypothesis: true difference in means is not equal to 0

95 percent confidence interval:

585.9634 638.5366

sample estimates:

mean of the differences

612.25

Answers: Three different types of turbines have three different estimated mean temperature reductions. The values are 587, 741.2308 and 612.25.

```
> anova(lm(InletTemp-ExhTemp ~ Engine))
```

Analysis of Variance Table

Response: InletTemp - ExhTemp

	Df	Sum Sq	Mean Sq	F value	Pr(>F)
Engine	2	150419	75209	11.26	0.0002405 ***
Residuals	29	193699	6679		

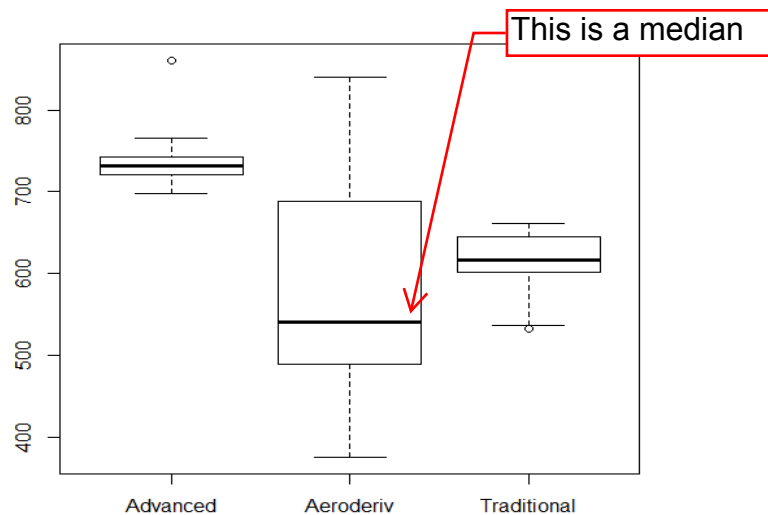
There are at least one pair of engine types that have different power.

Comment

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

```
boxplot((InletTemp - ExhTemp) ~ Engine)
```



The graph shows the mean of the heat difference between inlet and outlet is different significantly.

5.

```
> cor.test(gas$Power, gas$Airflow)
```

Pearson's product-moment correlation

data: gas\$Power and gas\$Airflow

t = 36.0711, df = 30, p-value < 2.2e-16

alternative hypothesis: true correlation is not equal to 0

95 percent confidence interval:

0.9766740 0.9945111

sample estimates:

cor

0.9886671

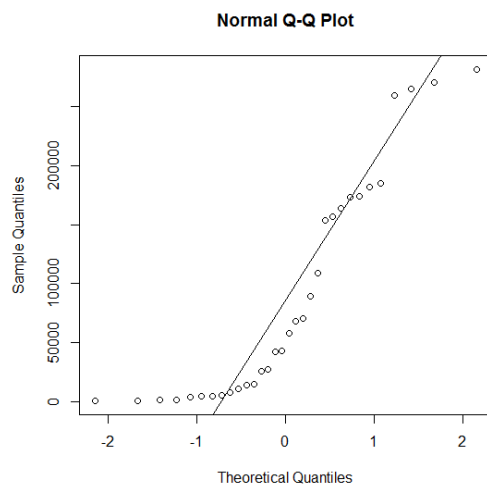
Answer: P value is less than  $2e^{-6}$ , Null hypothesis is rejected, hence this linear model is suitable for the relationship between Airflow and Power.



6

```
> qqnorm(Power)
```

```
> qqline(Power)
```



```
> t.test(Power)
```

#### One Sample t-test

data: Power

t = 5.3919, df = 31, p-value = 6.981e-06

alternative hypothesis: true mean is not equal to 0

95 percent confidence interval:

55776.87 123644.19

sample estimates:

mean of x

89710.53

```
> shapiro.test(Power)
```

#### Shapiro-Wilk normality test

data: Power

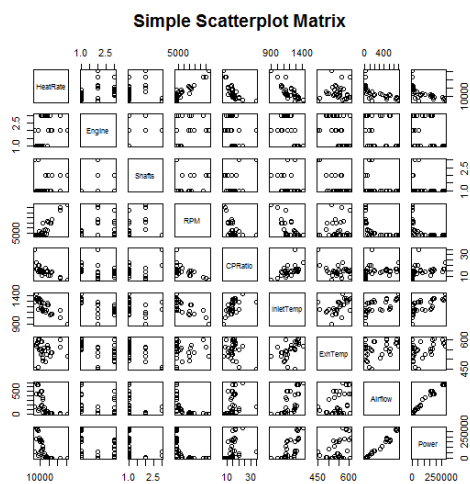
W = 0.8383, p-value = 0.0002344

Answer: As shown above the trend does not follow qqline. P value is much smaller than 0.05, so NULL hypothesis has been rejected. Null hypothesis stands for Power is normally distributed, hence this is not a normal distribution of the power of the turbines.



7

```
pairs(HeatRate~Engine+Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power,data=gas,
main="Simple Scatterplot Matrix")
```



Answer: RPM and InletTemp are the numeric variables are useful as linear regression predictor.

8.

```
> summary(lm(HeatRate ~ RPM))
```

Call:

```
lm(formula = HeatRate ~ RPM)
```

Residuals:

Min	1Q	Median	3Q	Max
-1424.64	-404.31	-36.18	351.38	1575.73

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	9.238e+03	1.689e+02	54.70	< 2e-16 ***
RPM	1.901e-01	1.384e-02	13.74	1.77e-14 ***

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1



Residual standard error: 652.9 on 30 degrees of freedom

Multiple R-squared: 0.8628, Adjusted R-squared: 0.8583

F-statistic: 188.7 on 1 and 30 DF, p-value: 1.772e-14

Answer : p value is 1.777e-14 and Multiple R-squared: 0.8628 which is close to 1, hence these two data sets fit to a linear model.

9.

```
> summary(lm(HeatRate ~ InletTemp))
```

Call:

```
lm(formula = HeatRate ~ InletTemp)
```

Residuals:

Min	1Q	Median	3Q	Max
-1989.23	-847.72	-33.47	547.72	2864.75

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	24798.940	1958.107	12.665	1.43e-13 ***
InletTemp	-11.501	1.616	-7.115	6.50e-08 ***

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 1075 on 30 degrees of freedom

Multiple R-squared: 0.6279, Adjusted R-squared: 0.6155

F-statistic: 50.63 on 1 and 30 DF, p-value: 6.498e-08

Answer : Multiple R-squared: 0.6279, hence InletTemp is ok, but RPM is a better choice.

10.

```
> summary(lm(HeatRate~InletTemp*RPM))
```

Call:

```
lm(formula = HeatRate ~ InletTemp * RPM)
```

Residuals:

Min	1Q	Median	3Q	Max
-1510.85	-217.73	84.35	208.47	1176.65

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	1.438e+04	1.778e+03	8.088	8.33e-09 ***
InletTemp	-3.957e+00	1.421e+00	-2.785	0.0095 **
RPM	1.711e-01	1.037e-01	1.651	0.1100
InletTemp:RPM	-2.007e-05	9.584e-05	-0.209	0.8356

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 563.3 on 28 degrees of freedom

Multiple R-squared: 0.9047, Adjusted R-squared: 0.8945

F-statistic: 88.62 on 3 and 28 DF, p-value: 2.103e-14

Answer : the interaction term was not required.

Why?

11.

```
> summary(lm(formula = HeatRate ~ Shafts + RPM + CPRatio + InletTemp + ExhTemp + Airflow + Power))
```

Call:

```
lm(formula = HeatRate ~ Shafts + RPM + CPRatio + InletTemp + ExhTemp + Airflow + Power)
```

Residuals:

Min	1Q	Median	3Q	Max
-991.83	-215.47	-62.23	193.12	954.98

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	1.168e+04	2.196e+03	5.318	1.86e-05 ***
Shafts	4.559e+01	2.146e+02	0.212	0.8335
RPM	1.082e-01	2.282e-02	4.741	8.02e-05 ***
CPRatio	-1.619e+01	4.058e+01	-0.399	0.6935
InletTemp	-6.337e+00	2.283e+00	-2.776	0.0105 *
ExhTemp	1.156e+01	5.436e+00	2.126	0.0440 *
Airflow	9.665e-01	3.260e+00	0.296	0.7694
Power	-4.860e-03	8.253e-03	-0.589	0.5615

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 441.6 on 24 degrees of freedom

Multiple R-squared: 0.9498, Adjusted R-squared: 0.9351

F-statistic: 64.86 on 7 and 24 DF, p-value: 4.793e-14

Comment on the significance

12.

Answer: According to beta values, when predictor variables of Shaft, CPRatio, InletTemp, Power increase, the response variable decrease with each particular ratio.

by how much?

13.

```
> summary(lm(HeatRate~InletTemp+RPM))
```

Call:

```
lm(formula = HeatRate ~ InletTemp + RPM)
```

Residuals:

Min	1Q	Median	3Q	Max
-1529.9	-243.1	83.9	208.5	1168.8

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	1.457e+04	1.504e+03	9.688	1.35e-10 ***
InletTemp	-4.123e+00	1.158e+00	-3.561	0.0013 **
RPM	1.497e-01	1.633e-02	9.169	4.55e-10 ***

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 553.9 on 29 degrees of freedom

Multiple R-squared: 0.9046, Adjusted R-squared: 0.898

F-statistic: 137.4 on 2 and 29 DF, p-value: 1.605e-15

```
> summary(lm(HeatRate~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power))
```

Call:

```
lm(formula = HeatRate ~ Shafts + RPM + CPRatio + InletTemp +  
    ExhTemp + Airflow + Power)
```

Residuals:

Min	1Q	Median	3Q	Max
-991.83	-215.47	-62.23	193.12	954.98

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	1.168e+04	2.196e+03	5.318	1.86e-05 ***
Shafts	4.559e+01	2.146e+02	0.212	0.8335
RPM	1.082e-01	2.282e-02	4.741	8.02e-05 ***
CPRatio	-1.619e+01	4.058e+01	-0.399	0.6935
InletTemp	-6.337e+00	2.283e+00	-2.776	0.0105 *
ExhTemp	1.156e+01	5.436e+00	2.126	0.0440 *
Airflow	9.665e-01	3.260e+00	0.296	0.7694
Power	-4.860e-03	8.253e-03	-0.589	0.5615

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 441.6 on 24 degrees of freedom  
Multiple R-squared: 0.9498, Adjusted R-squared: 0.9351  
F-statistic: 64.86 on 7 and 24 DF, p-value: 4.793e-14

Quote value

Answer: Applying least squared theory, 7-predictor has smaller Residual standard error. Hence it has better predictive than the 2-predictor model.



14.

```
> summary(lm(HeatRate~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power))
```

Call:

```
lm(formula = HeatRate ~ Shafts + RPM + CPRatio + InletTemp +  
    ExhTemp + Airflow + Power)
```

Residuals:

Min	1Q	Median	3Q	Max
-991.83	-215.47	-62.23	193.12	954.98

Coefficients:

	Estimate	Std. Error	t value	Pr(> t )
(Intercept)	1.168e+04	2.196e+03	5.318	1.86e-05 ***
Shafts	4.559e+01	2.146e+02	0.212	0.8335
RPM	1.082e-01	2.282e-02	4.741	8.02e-05 ***
CPRatio	-1.619e+01	4.058e+01	-0.399	0.6935
InletTemp	-6.337e+00	2.283e+00	-2.776	0.0105 *
ExhTemp	1.156e+01	5.436e+00	2.126	0.0440 *
Airflow	9.665e-01	3.260e+00	0.296	0.7694
Power	-4.860e-03	8.253e-03	-0.589	0.5615

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 441.6 on 24 degrees of freedom

Multiple R-squared: 0.9498, Adjusted R-squared: 0.9351

F-statistic: 64.86 on 7 and 24 DF, p-value: 4.793e-14

Answer: As shown above, it means 94.98% variation.

The model explains 94% of the variation in the HeatRate of the turbines.

15.

This means that some part of the model is useful. It does not say that this model is the best model.

P value is  $4.793e-14$ , much less than 0.01, Null hypothesis is rejected. Hence this model is good to predicate HeatRate.

16.

```
> lm1<-lm(HeatRate~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power)
```

```
> hatvalues(lm1)
```

```

  1    2    3    4    5    6    7    8
0.4284616 0.3252555 0.1641741 0.7507745 0.5133682 0.4849646 0.2036465 0.1885726
  9   10   11   12   13   14   15   16
0.1761790 0.2563977 0.2641164 0.2880030 0.3192141 0.1678053 0.1670899 0.2168007
 17   18   19   20   21   22   23   24
0.2168691 0.1559862 0.3693915 0.1646246 0.1452208 0.1148014 0.4081885 0.1573087
 25   26   27   28   29   30   31   32
0.1635554 0.1737555 0.1835541 0.1591480 0.2287911 0.1181886 0.2243930 0.1013998
```

```
> which((hatvalues(lm1)/mean(hatvalues(lm1))>2))
```

4 5

4 5

Answer: two of leverages more than twice the mean leverage. But there is no enough evidence to prove 4,5 are significantly influential.



17.

Applying stepwise algorithm:

```
> m1<-lm(HeatRate~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power)
```

```
> m0<-lm(HeatRate~1, data = swiss)
```

```
> m2<-step(m0,scope=~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power,
direction="both")
```

Start: AIC=478.32

HeatRate ~ 1

Start with the multiple regression model and reduce

	Df	Sum of Sq	RSS	AIC
+ RPM	1	80446795	12788995	416.75

```

+ InletTemp 1 58543841 34691949 448.68
+ CPRatio 1 45683457 47552333 458.77
+ Airflow 1 39749292 53486498 462.53
+ Power 1 38757766 54478024 463.12
<none> 93235790 478.32
+ Shafts 1 2105658 91130131 479.59
+ ExhTemp 1 32823 93202967 480.31

```

Step: AIC=416.75

HeatRate ~ RPM

	Df	Sum of Sq	RSS	AIC
+ CPRatio	1	4995085	7793910	402.90
+ InletTemp	1	3891445	8897550	407.14
+ Shafts	1	950016	11838979	416.28
+ Power	1	853856	11935139	416.54
<none>			12788995	416.75
+ Airflow	1	392791	12396204	417.75
+ ExhTemp	1	4980	12784015	418.74
- RPM	1	80446795	93235790	478.32

Step: AIC=402.9

HeatRate ~ RPM + CPRatio

	Df	Sum of Sq	RSS	AIC
+ InletTemp	1	1866842	5927068	396.14
+ Power	1	1318310	6475600	398.97
+ Airflow	1	1091714	6702196	400.07
+ ExhTemp	1	835555	6958355	401.27
<none>			7793910	402.90
+ Shafts	1	234852	7559058	403.92



- CPRatio 1 4995085 12788995 416.75  
 - RPM 1 39758423 47552333 458.77

Step: AIC=396.14

HeatRate ~ RPM + CPRatio + InletTemp

	Df	Sum of Sq	RSS	AIC
+ ExhTemp	1	523560	5403508	395.18
<none>			5927068	396.14
+ Power	1	319598	5607470	396.36
+ Airflow	1	308565	5618503	396.43
+ Shafts	1	33628	5893440	397.96
- InletTemp	1	1866842	7793910	402.90
- CPRatio	1	2970482	8897550	407.14
- RPM	1	19804634	25731702	441.12

Step: AIC=395.18

HeatRate ~ RPM + CPRatio + InletTemp + ExhTemp

	Df	Sum of Sq	RSS	AIC
+ Power	1	699396	4704112	392.74
+ Airflow	1	651517	4751991	393.07
- CPRatio	1	93602	5497110	393.73
<none>			5403508	395.18
- ExhTemp	1	523560	5927068	396.14
+ Shafts	1	1206	5402302	397.17
- InletTemp	1	1554848	6958355	401.27
- RPM	1	11111263	16514770	428.93

Step: AIC=392.74

HeatRate ~ RPM + CPRatio + InletTemp + ExhTemp + Power

	Df	Sum of Sq	RSS	AIC
- CPRatio	1	38144	4742256	391.00
<none>			4704112	392.74
+ Airflow	1	14173	4689939	394.65
+ Shafts	1	5840	4698272	394.70
- Power	1	699396	5403508	395.18
- ExhTemp	1	903358	5607470	396.36
- InletTemp	1	1656870	6360982	400.40
- RPM	1	6797549	11501660	419.35

Step: AIC=391

HeatRate ~ RPM + InletTemp + ExhTemp + Power

	Df	Sum of Sq	RSS	AIC
<none>			4742256	391.00
+ CPRatio	1	38144	4704112	392.74
+ Airflow	1	27094	4715162	392.82
+ Shafts	1	445	4741811	393.00
- Power	1	754854	5497110	393.73
- ExhTemp	1	4145633	8887889	409.10
- InletTemp	1	6735273	11477529	417.29
- RPM	1	7413766	12156023	419.12

Answer: My reduced model is HeatRate vs CPRatio, RPM ,InletTemp.



Fit and comment

18.

```
> full_model <- lm(HeatRate~Shafts+RPM+CPRatio+InletTemp+ExhTemp+Airflow+Power)
> reduced_model <- lm(HeatRate~CPRatio+RPM+InletTemp)
> anova(full_model,reduced_model)
```

Analysis of Variance Table

Model 1: HeatRate ~ Shafts + RPM + CPRatio + InletTemp + ExhTemp + Airflow +  
Power

Model 2: HeatRate ~ CPRatio + RPM + InletTemp

	Res.Df	RSS	Df	Sum of Sq	F	Pr(>F)
1	24	4681132				
2	28	5927068	-4	-1245936	1.597	0.2075

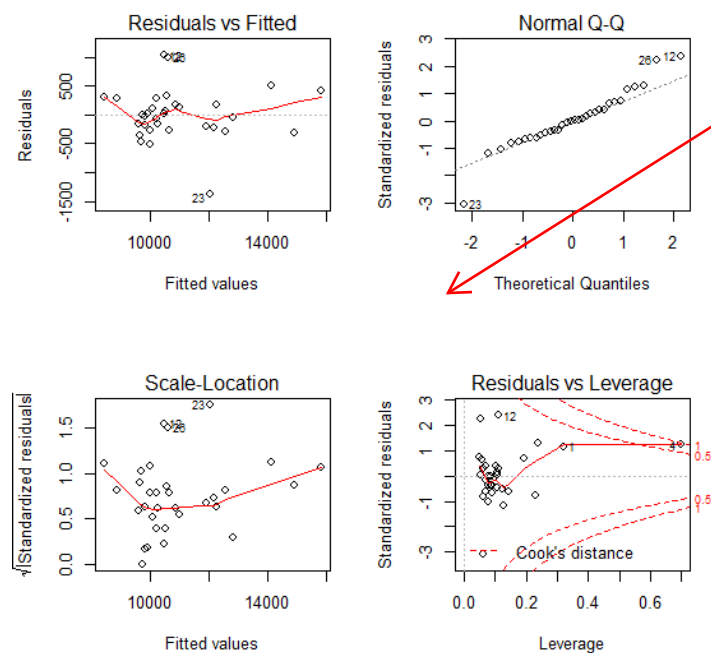
sufficient

Answer: reduced model is better.

19.

```
> par(mfrow=c(2,2))
> plot(reduced_model)
```

The graph generated:



Comment

20.

```
> vif(reduced_model)
CPRatio    RPM InletTemp
1.561515 2.076288 2.124232

> which(cooks.distance(reduced_model)>1)
named integer(0)

> vif(reduced_model)
CPRatio    RPM InletTemp
1.561515 2.076288 2.124232
```

Answer: as shown above, cooks distance is less than 1 and vif less than 10. Hence, nothing to worry about.



21.

```
> poly1<-lm(HeatRate~poly(InletTemp,1,row=T))
> poly2<-lm(HeatRate~poly(InletTemp,2,row=T))
> poly3<-lm(HeatRate~poly(InletTemp,3,row=T))
> anova(poly1,poly2)
```

Analysis of Variance Table

Model 1: HeatRate ~ poly(InletTemp, 1, raw = T)

Model 2: HeatRate ~ poly(InletTemp, 2, raw = T)

	Res.Df	RSS	Df	Sum of Sq	F	Pr(>F)
1	30	34691949				
2	29	28960612	1	5731337	5.7391	0.02327 *

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

```
> anova(poly1,poly3)
```

Analysis of Variance Table

Model 1: HeatRate ~ poly(InletTemp, 1, raw = T)

Model 2: HeatRate ~ poly(InletTemp, 3, raw = T)

```

Res.Df  RSS Df Sum of Sq  F Pr(>F)
1    30 34691949
2    28 28358735  2  6333214 3.1265 0.05949 .
---
Signif. codes:  0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

> anova(poly2,poly3)

Analysis of Variance Table

```

Model 1: HeatRate ~ poly(InletTemp, 2, raw = T)

Model 2: HeatRate ~ poly(InletTemp, 3, raw = T)

```

Res.Df  RSS Df Sum of Sq  F Pr(>F)
1    29 28960612
2    28 28358735  1  601877 0.5943 0.4472

```

Adding  $x^3$  does not significantly improve

-1

Answer: 0.02327 is smallest one. Hence the model with degree 2 is the best model.

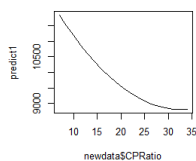
significant

22.

```

> poly2<-lm(HeatRate~poly(CPRatio,RPM,degree=2,raw=TRUE))
> newdata<-data.frame(RPM=rep(4500,19),CPRatio=seq(7,35,1.5))
> predict1<-predict.lm(poly2,newdata)
> plot(newdata$CPRatio,predict1,type='l')

```

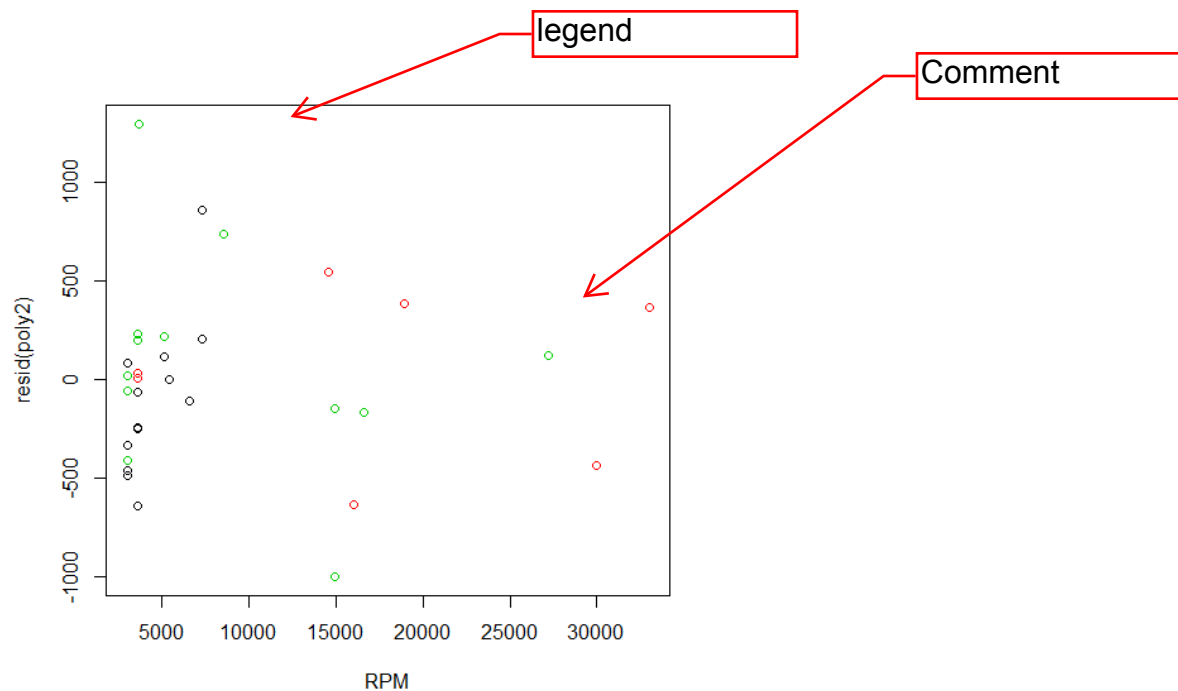


Answer: When RPM equals to 4900 rpm, and CPRatio is between 7 and 35.



23.

```
> plot(RPM,resid(poly2),col=Engine)
```



24.

```
> poly_with_engine<-lm(HeatRate~poly(CPRatio,RPM,degree=2,raw=TRUE)+Engine)
```

```
> summary(poly_with_engine)
```

Call:

```
lm(formula = HeatRate ~ poly(CPRatio, RPM, degree = 2, raw = TRUE) +  
    Engine)
```

Residuals:

Min	1Q	Median	3Q	Max
-1048.15	-256.65	3.56	181.36	1138.72

Coefficients:

	Estimate	Std. Error	t value
(Intercept)	1.171e+04	2.242e+03	5.221
poly(CPRatio, RPM, degree = 2, raw = TRUE)1.0	-1.768e+02	1.884e+02	-0.939
poly(CPRatio, RPM, degree = 2, raw = TRUE)2.0	2.213e+00	3.517e+00	0.629

```
poly(CPRatio, RPM, degree = 2, raw = TRUE)0.1 1.851e-01 2.053e-01 0.901
poly(CPRatio, RPM, degree = 2, raw = TRUE)1.1 -3.942e-03 1.015e-02 -0.388
poly(CPRatio, RPM, degree = 2, raw = TRUE)0.2 -1.859e-07 3.413e-06 -0.054
EngineAeroderiv          2.862e+02 3.371e+02 0.849
EngineTraditional        3.109e+02 2.578e+02 1.206
```

Pr(>|t|)

```
(Intercept)          2.38e-05 ***
poly(CPRatio, RPM, degree = 2, raw = TRUE)1.0 0.357
poly(CPRatio, RPM, degree = 2, raw = TRUE)2.0 0.535
poly(CPRatio, RPM, degree = 2, raw = TRUE)0.1 0.376
poly(CPRatio, RPM, degree = 2, raw = TRUE)1.1 0.701
poly(CPRatio, RPM, degree = 2, raw = TRUE)0.2 0.957
EngineAeroderiv        0.404
EngineTraditional      0.240
```

Not significant

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 511.3 on 24 degrees of freedom

Multiple R-squared: 0.9327, Adjusted R-squared: 0.9131

F-statistic: 47.51 on 7 and 24 DF, p-value: 1.548e-12

Answer: p value: 1.548e-12, hence adding Engine improved this model.

25.

```
> another_poly_with_engine <- lm(HeatRate~poly(CPRatio,RPM,degree=2,raw=TRUE)*Engine)
```

```
> anova(another_poly_with_engine,poly_with_engine)
```

Analysis of Variance Table

Model 1: HeatRate ~ poly(CPRatio, RPM, degree = 2, raw = TRUE) \* Engine

Model 2: HeatRate ~ poly(CPRatio, RPM, degree = 2, raw = TRUE) + Engine

	Res.Df	RSS	Df	Sum of Sq	F	Pr(>F)
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1	14	2218234				
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2 24 6275250 -10 -4057016 2.5605 0.05284 .

---

Signif. codes: 0 '\*\*\*' 0.001 '\*\*' 0.01 '\*' 0.05 '.' 0.1 ' ' 1



Comment