

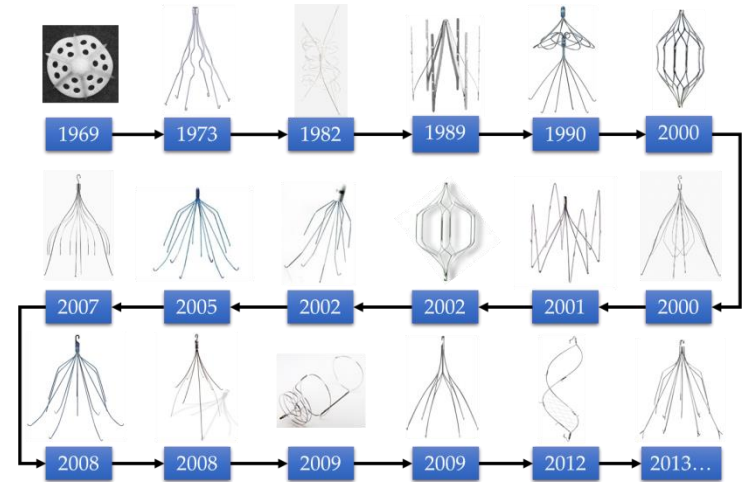
# FDA Critical Path Project

“Generation and Review of Regulatory-Grade Computational Evidence Using a Generic Inferior Vena Cava Filter”

## Summary of Preliminary FEA

# The objectives of this project are to...

- **Develop** a **generic** IVC filter
- **Predict & demonstrate:**
  - **fatigue** resistance
  - embolus-trapping efficiency
- Ideally,
  - single strut shape (simplify fatigue simulation/testing)
  - resist tilt, migration, and vein wall perforation

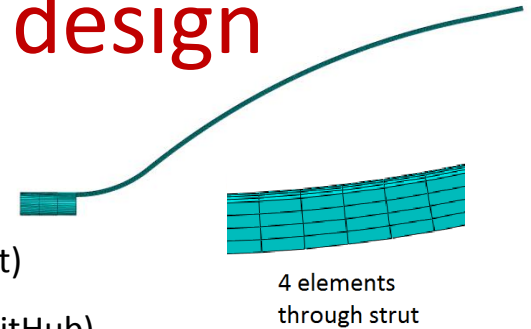


???

# FEA performed to evaluate filter design

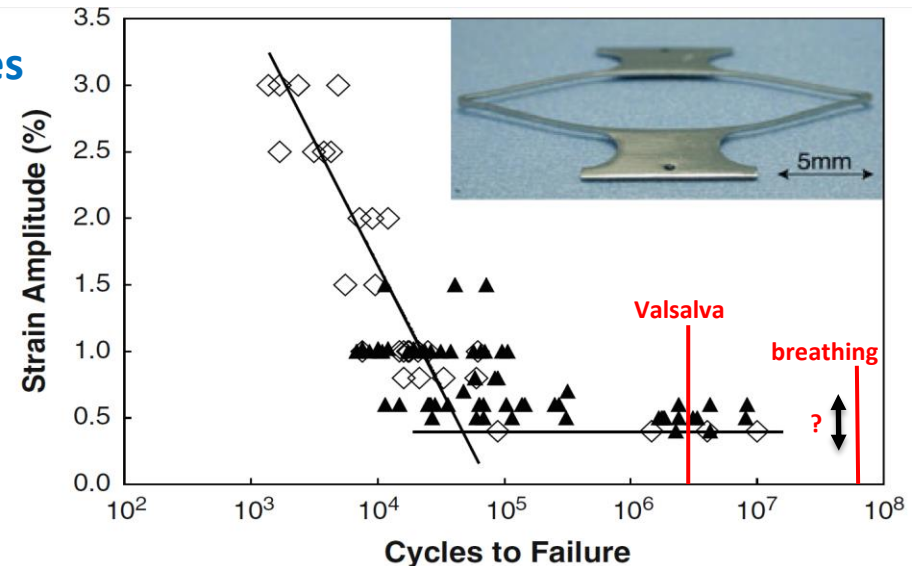
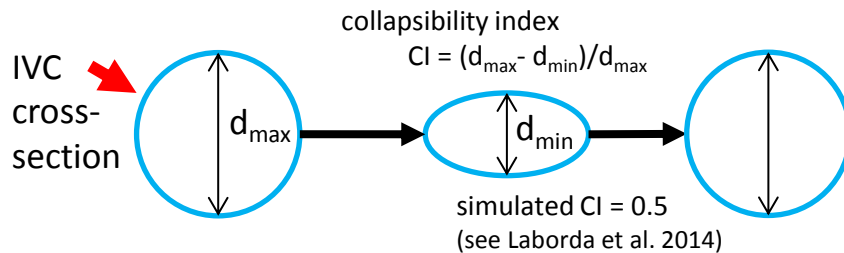
## Setup:

- ABAQUS Dynamic/Implicit (quasi-static); 10x mass scaling
- C3D8I elements (4 per strut thickness & width; ~3,000 to 6,000 per strut)
- SE508 nitinol (material properties from Craig Bonsignore's example on GitHub)



## Simulated conditions → extracted quantities

1. Sheathing → prestrain
2. Filter placement → contact force/area
3. Valsalva → mean/amplitude strain



Pelton, A. R. (2011). *J. Mater. Eng. Perform.*, 20(4-5), 613–617

## Two IVC diameters considered (human variability):

1. 14mm (3.5mm wall displacement during Valsalva)
2. 28mm (7.0mm wall displacement during Valsalva)

We assume Valsalva is the limiting loading scenario for fatigue life

# Performance goals are set for quantities extracted from FEA simulations

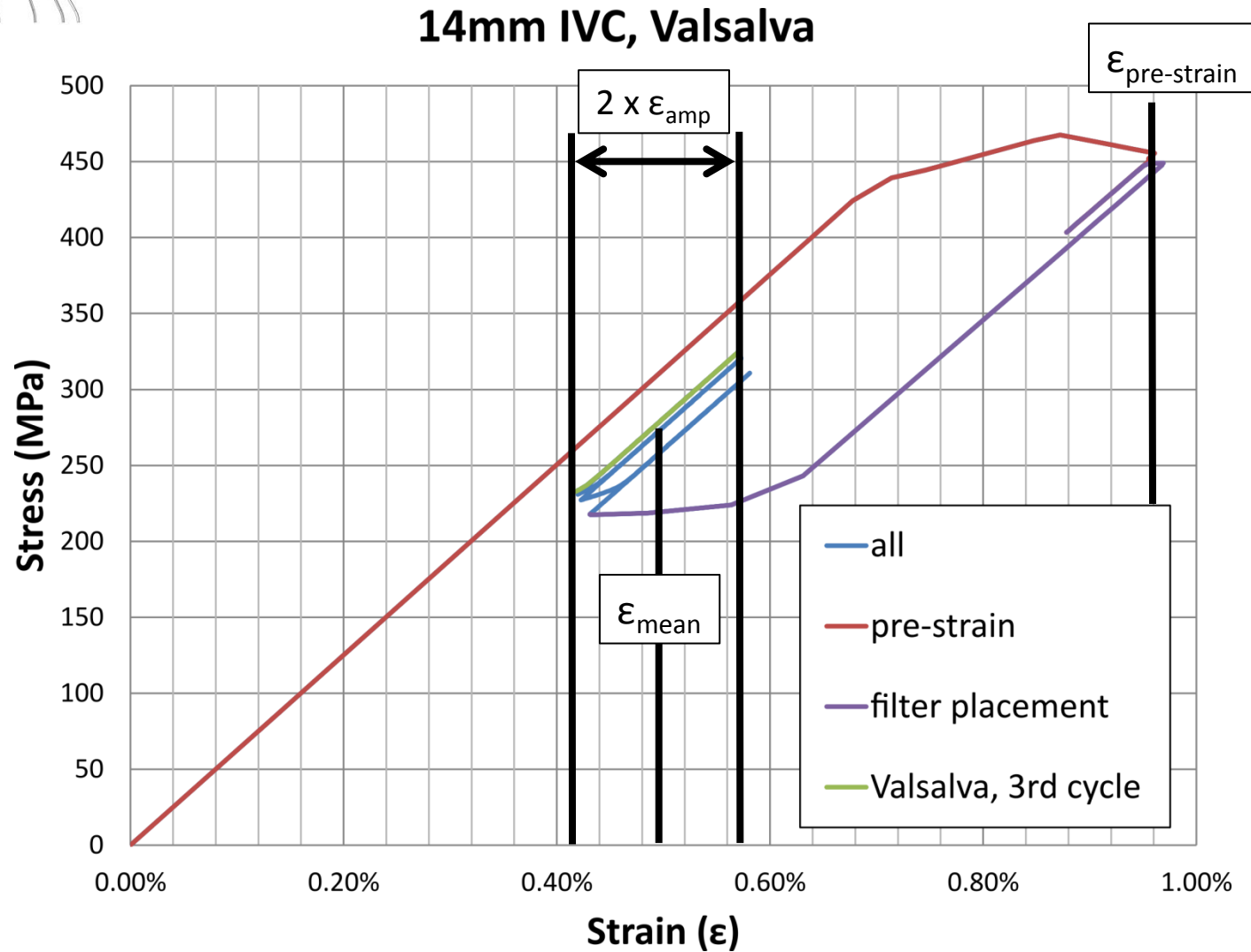
	distal end contacts wall?	prestrain (max/min prin. LE)	contact force (N) (per strut)	contact area (mm <sup>2</sup> ) (per strut)	$\epsilon$ amplitude, Valsalva (CI=0.5)	mean $\epsilon$ , Valsalva (CI=0.5)
target	yes	<6%	0.010 to 0.100	>0.05?	<0.4%	<6%

*\*to avoid plastic deformation during sheathing*



# Stress-strain history diagram

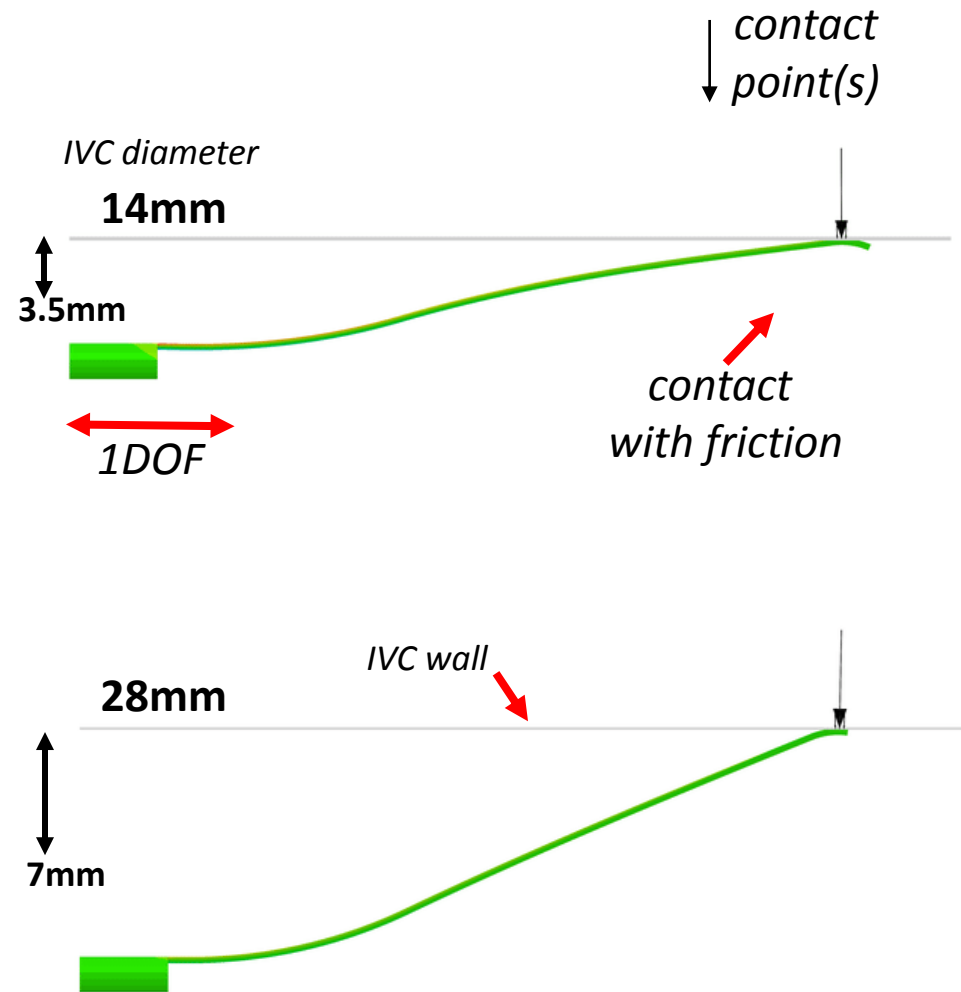
(Rev1)



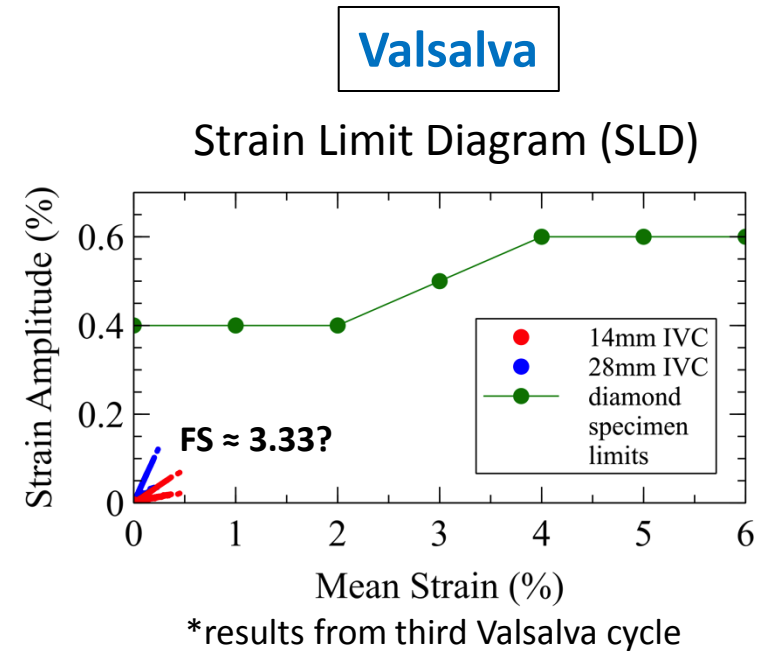
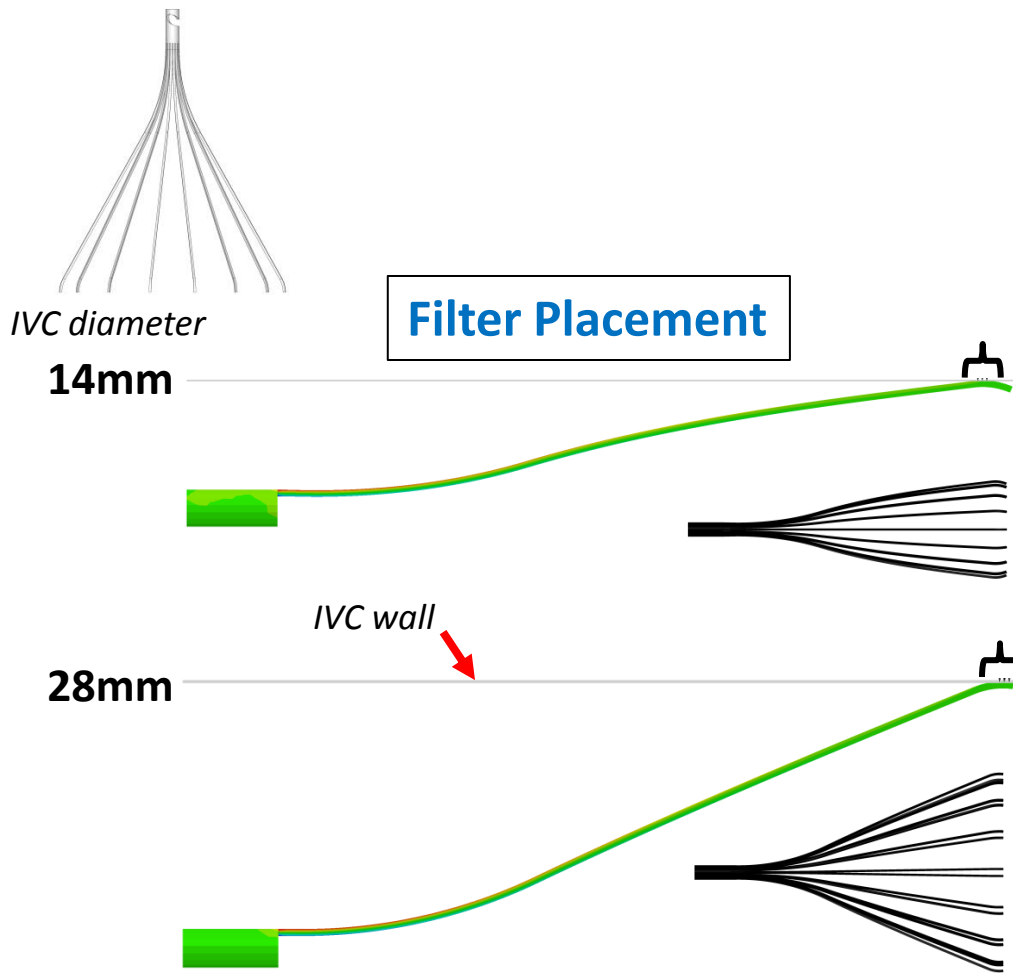


# Valsalva (fatigue loading) (Rev1)

*\*FEA simulations of Valsalva shown for reference; note that the contact point between the IVC wall and the filter strut changes as the strut deforms*



# Results summary (Rev1)



IVC diameter	distal end contacts wall?	prestrain (max/min prin. LE)	contact force (N) (per strut)	contact area (mm <sup>2</sup> ) (per strut)	$\epsilon$ amplitude, Valsalva (CI=0.5)	mean $\epsilon$ , Valsalva (CI=0.5)
<i>14mm</i>	<i>yes</i>	<i>0.80%</i>	<i>0.028</i>	<i>0.018</i>	<b>0.07%</b>	<i>0.45%</i>
<i>28mm</i>	<i>yes</i>	<i>0.80%</i>	<i>0.010</i>	<i>0.018</i>	<b>0.12%</b>	<i>0.24%</i>

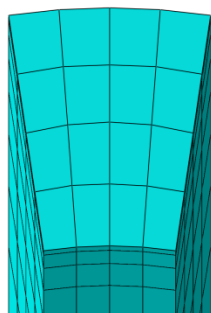


# Mesh refinement

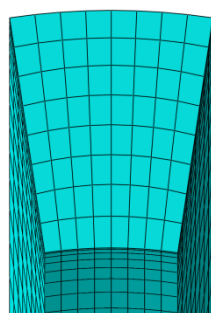
## (Rev1)

IVC diamter	distal end contacts wall?	prestrain (max/min prin. LE)	contact force (N) (per strut)	contact area (mm <sup>2</sup> ) (per strut)	$\epsilon$ amplitude, Valsalva (CI=0.5)	mean $\epsilon$ , Valsalva (CI=0.5)
<i>coarse</i> (4x4)	<i>yes</i>	<i>0.80%</i>	<i>0.0096</i>	<i>0.018</i>	<b>0.121%</b>	<i>0.24%</i>
<i>medium</i> (8x8)	<i>yes</i>	<i>0.92%</i>	<i>0.0096</i>	<i>0.0048</i>	<b>0.134%</b>	<i>0.26%</i>
<i>fine</i> (12x12)	<i>yes</i>	<i>1.04%</i>	<i>0.0102</i>	<i>0.0050</i>	<b>0.139%</b>	<i>0.27%</i>

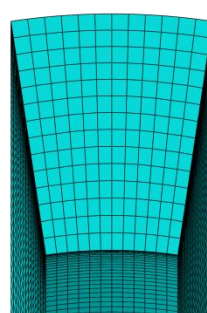
**GCI: -2.81%**



**coarse**



**medium**



**fine**

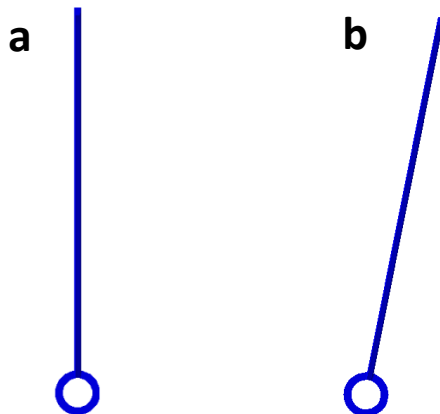




# Eccentric loading of filter strut

(Rev1)

	IVC diamter	distal end contacts wall?	prestrain (max/min prin. LE)	contact force (N) (per strut)	contact area (mm <sup>2</sup> ) (per strut)	$\epsilon$ amplitude, Valsalva (CI=0.5)	mean $\epsilon$ , Valsalva (CI=0.5)
a	28mm	yes	0.80%	0.010	0.018	<b>0.12%</b>	0.24%
b	28mm	yes	0.80%	0.0086	0.0091	<b>0.14%</b>	0.26%

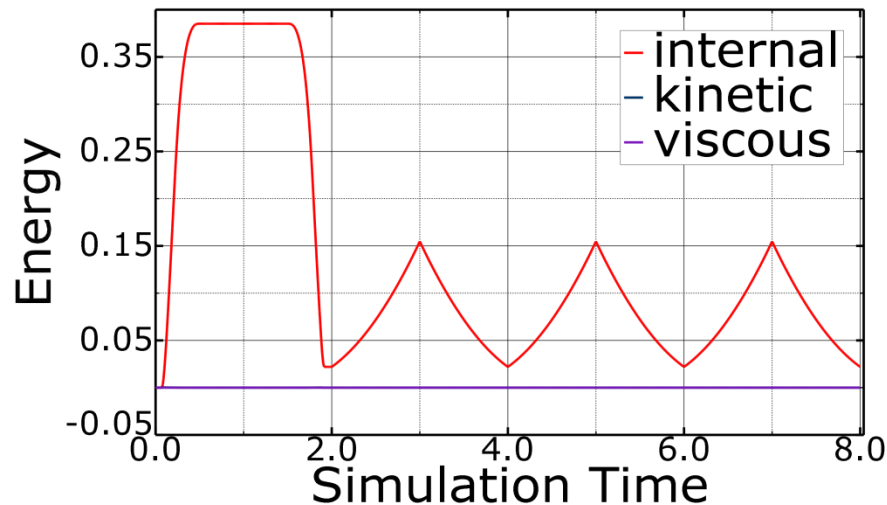




# Static/Implicit vs. Dynamic/Implicit (Rev1)

	IVC diamter	distal end contacts wall?	prestrain (max/min prin. LE)	contact force (N) (per strut)	contact area (mm <sup>2</sup> ) (per strut)	$\epsilon$ amplitude, Valsalva (CI=0.5)	mean $\epsilon$ , Valsalva (CI=0.5)
Static/Imp	28mm	yes	0.798%	0.00884	0.0182	<b>0.122%</b>	0.239%
Dynamic/Imp	28mm	yes	0.797%	0.00959	0.0182	<b>0.121%</b>	0.238%

Dynamic/Imp



*\*Simulations were performed using Abaqus Standard, Dynamic/Implicit to increase stability of contact interactions. Simulations performed using Static/Implicit yield similar results, but do not converge in some cases.*