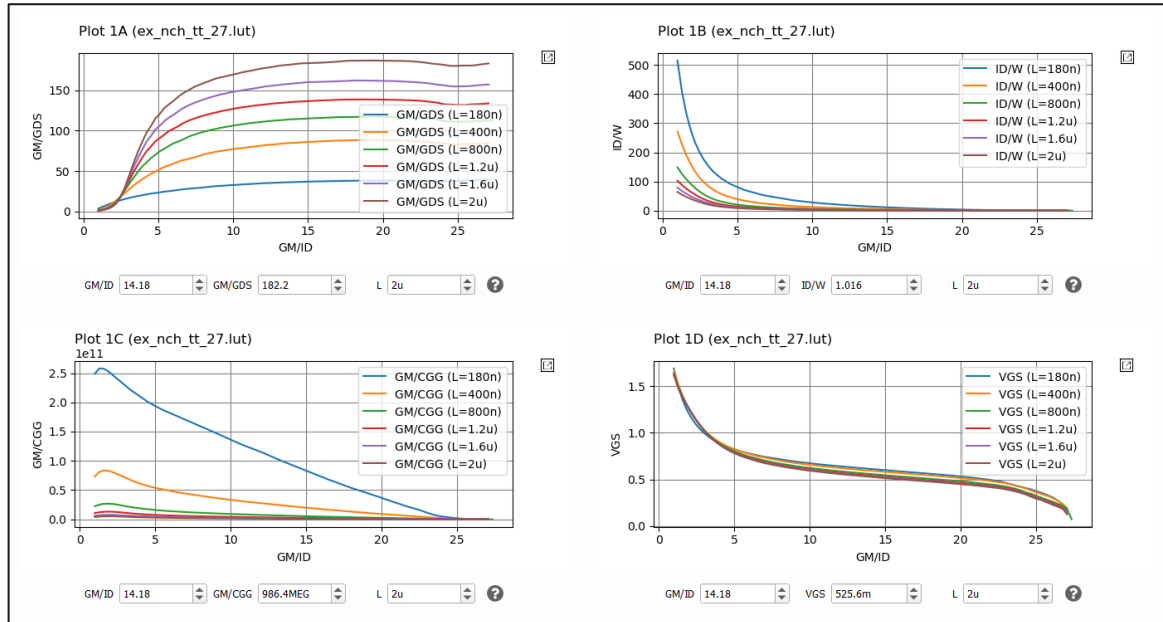


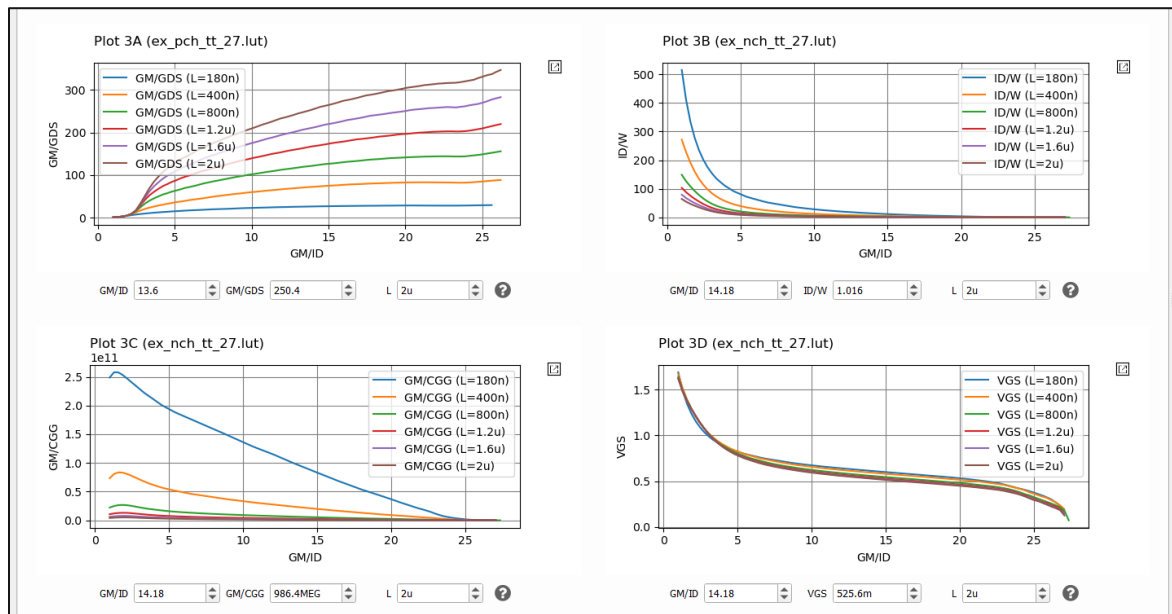
Lab 11 (Mini Project 02)

Part1: gm/id Design chart

Nmos



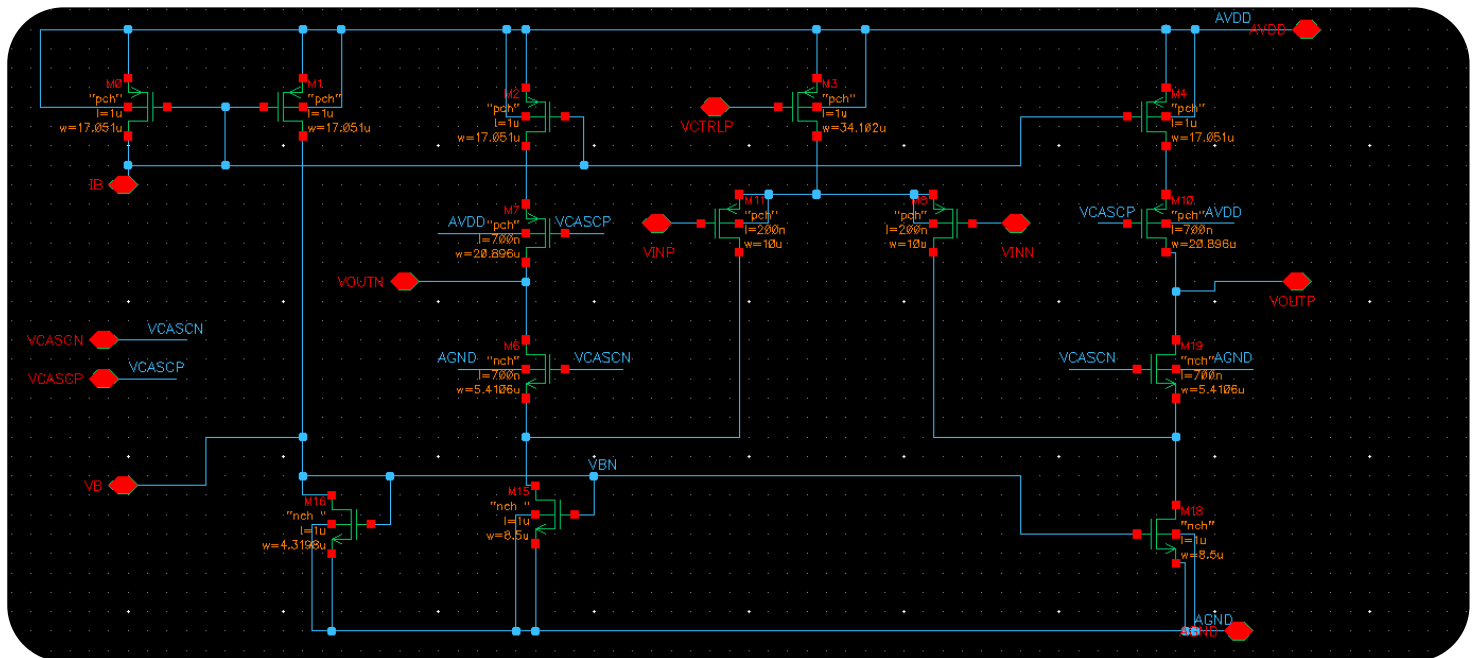
Pmos



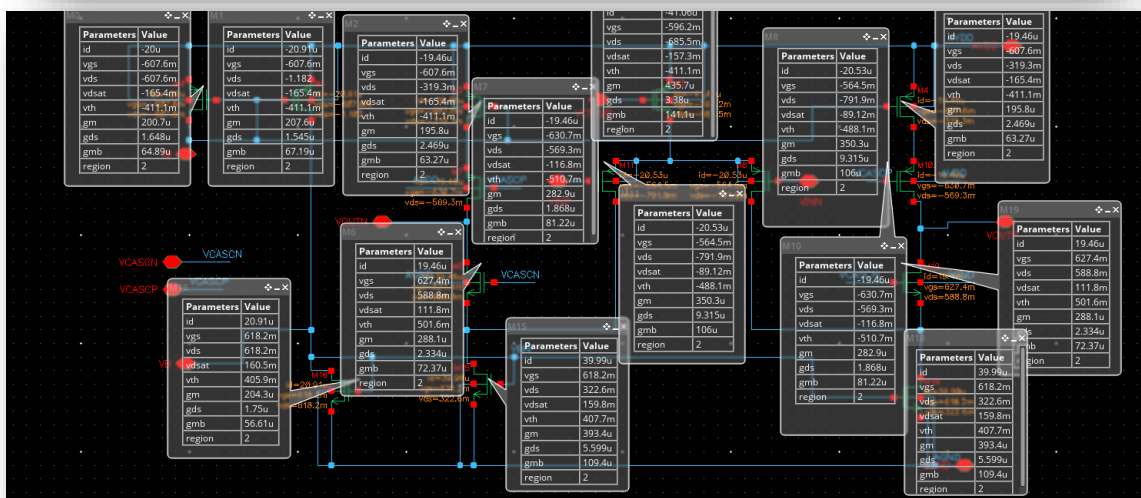
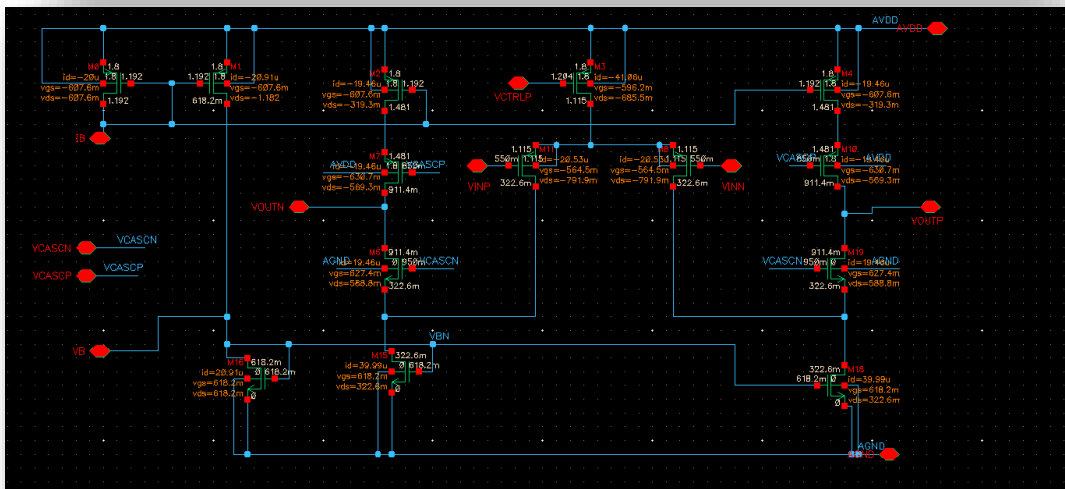
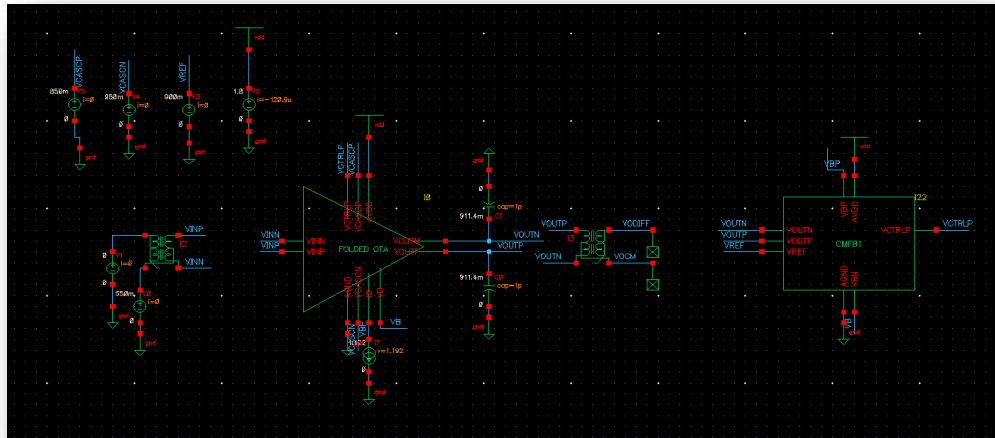
Part2: OTA Design

| Parameter | Gm/id | id | L | W | VGS | V* |
|-------------|-------|-----|------|---------|---------|---------|
| M8&M11 | 17 | 20u | 0.2u | 10u | 572.78m | 118.39m |
| M0&M1&M2&M4 | 10 | 20u | 1u | 17.051u | 609.12m | 201m |
| M3 | 10 | 40u | 1u | 34.102u | 609.12m | 201m |
| M7&M10 | 15 | 20u | 0.7u | 20.895u | 649.3m | 131m |
| M6&M19 | 15 | 20u | 0.7u | 5.4106u | 643.2m | 134.25m |
| M15&,18 | 10 | 40u | 1u | 8.5u | 614m | 200m |
| M16 | 10 | 20u | 1i | 4.32u | 615m | 200.76m |

- gm/id of input pair = 17 instead of 15 , L of cascade = 0.7 instead of 0.5 to meet specs.



1) Schematic of the OTA and bias circuit with DC node voltages:



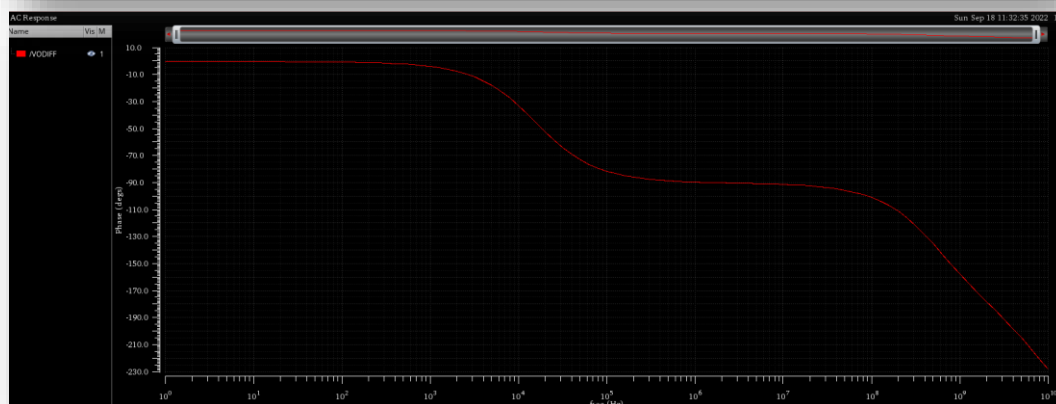
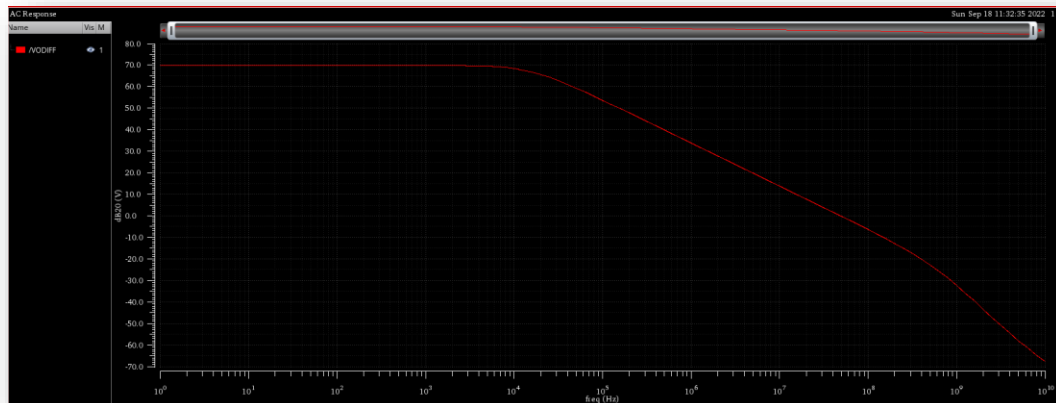
- $V_{OCM}=911.4m$

- V_{CTRLP}

| | |
|--------------------------------------|-------------------|
| v("/VCTRLP" ?result "dcOp")-v("/V... | |
| M | v("/VCT...p") (V) |
| 1 1.000 | 11.42E-3 |

- Relation: they exactly equal because we use VCCS with gain=1

2) Diff small signal ccs:



| Test | Output | Nominal |
|------------|--------------------------------|---------|
| lab11:TB:1 | /VODIFF | |
| lab11:TB:1 | ymax(mag(VF("/VODIFF"))) | 3.214k |
| lab11:TB:1 | dB20(ymax(mag(VF("/VODIFF...)) | 70.14 |
| lab11:TB:1 | gainBwProd(VF("/VODIFF")) | 50.06M |
| lab11:TB:1 | unityGainFreq(VF("/VODIFF")) | 49.89M |
| lab11:TB:1 | phaseMargin(VF("/VODIFF")) | 84.64 |

- Hand Anaalysis

Gain= GM8*ROUT

$ROUT = ro_{10} * (ro_4(gm_{10} + gmb_{10}) + 1) // ro_{19} * ((gm_{19} + gmb_{19})(ro_{18} // ro_1) + 1) = 79.48M // 10.78M = 9.492M$

Gain=9.492M*350.3u=3.325k

Gain(db)=70.436

Bandwidth= $\frac{1}{2\pi * Rout * CL} = 16.77k$

GBW=16.77k*3.325k=55.76M

UGF=55.76M

$PM = 90 - \tan^{-1}\left(\frac{w_u}{w_{p2}}\right) = 90 - \tan^{-1}\left(\frac{w_u}{\frac{gm_6 + gmb_6}{(css_6 + cdd_{11} + cdd_{15})}}\right) = 90 - \tan^{-1}\left(\frac{50M}{3.37G}\right) = 89.06$

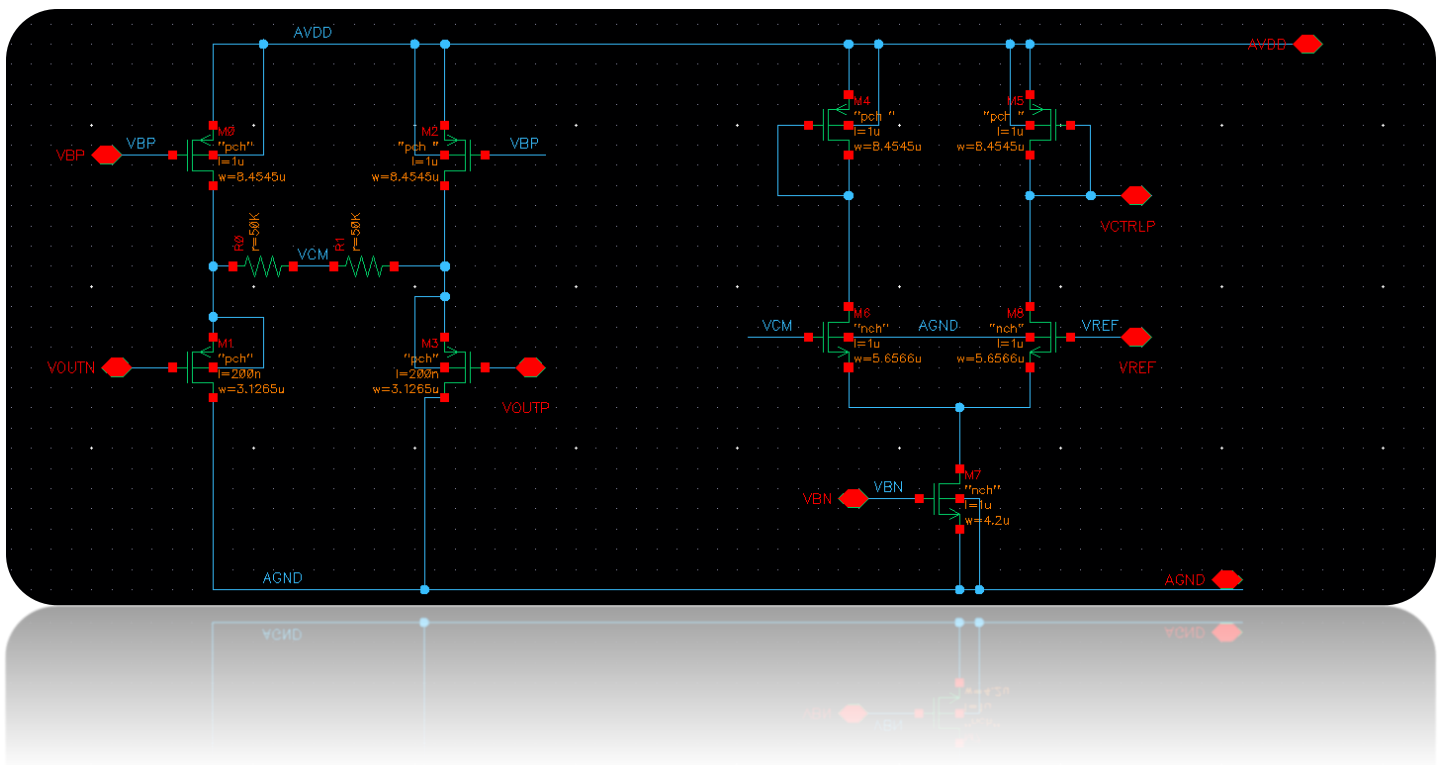
$C_{ss6} = 81.18fF, C_{dd11} = 14.1fF, cdd_{15} = 11.64fF$

| Parameter | Hand analysis | Simulation |
|-----------|---------------|------------|
| Gain | 3.325k | 3.214k |
| Gain(db) | 70.436 | 70.14 |
| Bandwidth | 16.77k | 15.54k |
| GBW | 55.76M | 50.06M |
| UGF | 55.76M | 49.89M |
| PM | 81.87 | 89 |

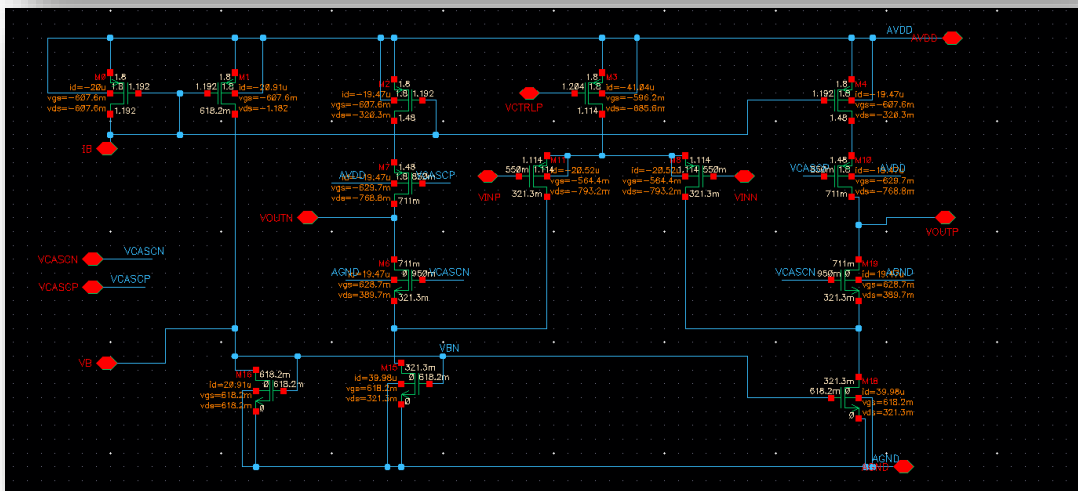
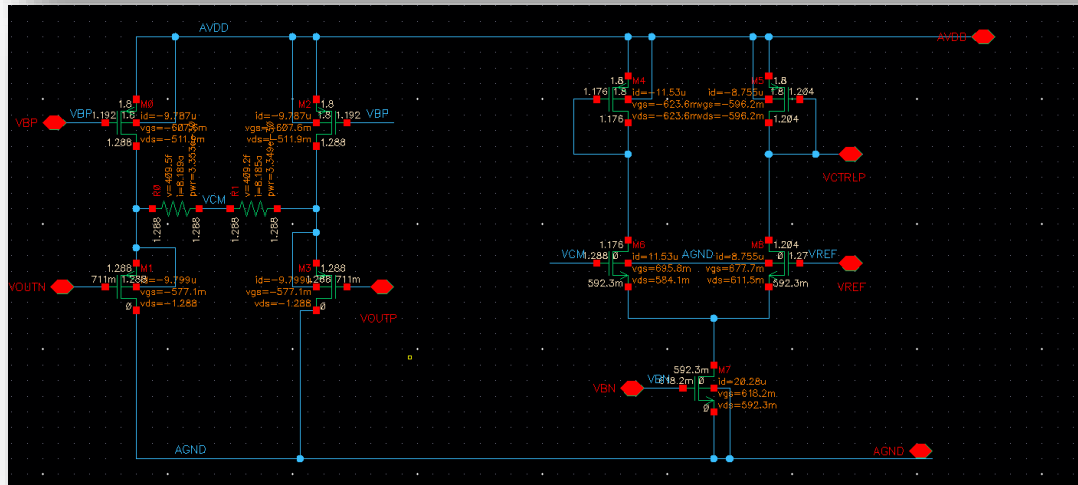
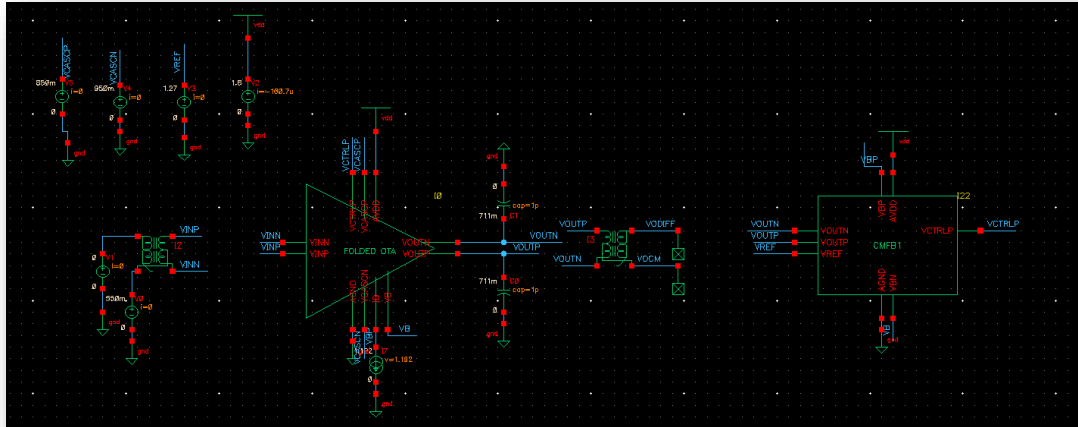
PART 4: Open-Loop OTA Simulation (Actual CMFB)

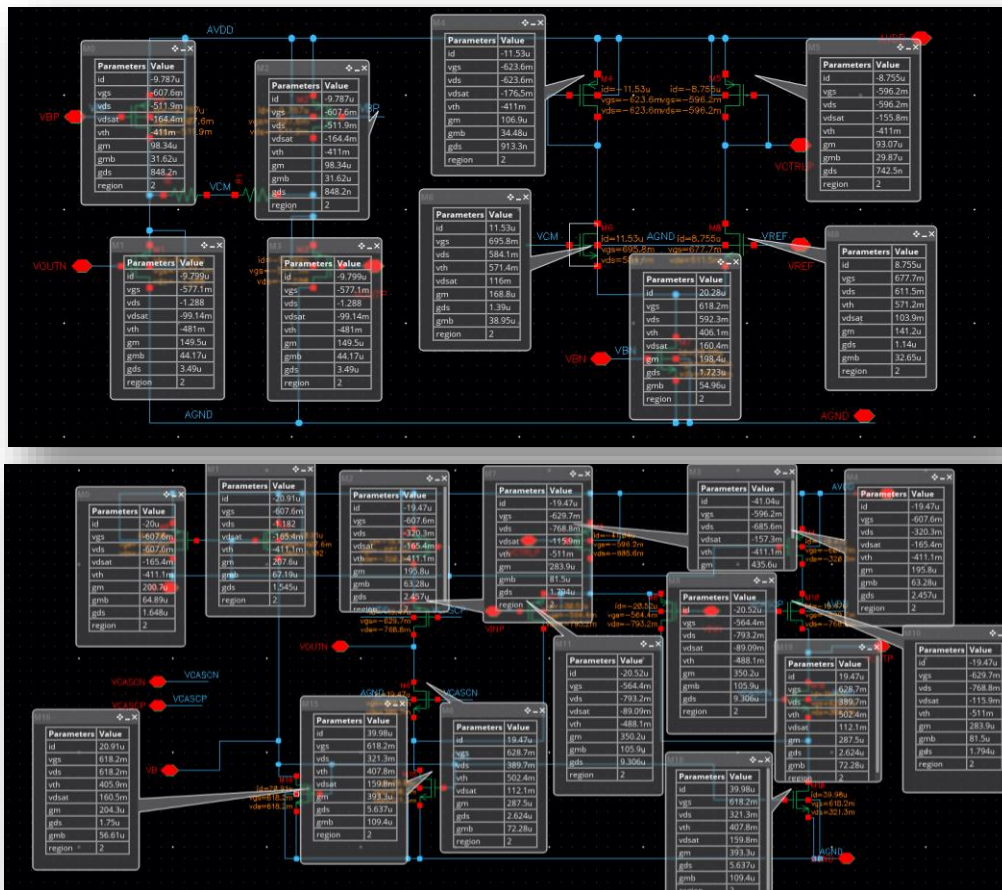
| Parameter | Gm/id | Id | W | L | VGS | V* |
|-------------|-------|-----|--------|----|---------|---------|
| M0&M2&M5&M4 | 10 | 10u | 8.45u | 1u | 608.67m | 200.97m |
| M1&M3 | 15 | 10u | 3.126u | 1u | 597.36m | 134.3m |
| M6&M8 | 15 | 10u | 5.656u | 1u | 535.09m | 134.06m |
| M7 | 10 | 20u | 4.2u | 1u | 614.04m | 200.83m |

- $V_{OUTmax} = V_{DD} - V^* - |V_{GSP}| = 1.8 - 200.97m - 597.36m = 1.0175V$
- $V_{OUTmin} = v^* + v^* = 134.35m + 200.76m = 0.3351V$
- $V_{REF} = \text{middle value} + |V_{GSP}| = 1.27V$



1) Schematic of the OTA and CMFB circuit with DC node voltages and transistors OP parameters (i_d , v_{gs} , v_{ds} , v_{dsat} , v_{th} , g_m , g_{ds} , region) clearly annotate





- **VOCM=711m**

| | | |
|---|-------|-----------------------------------|
| V | | v("I22/VCM") ?result "dcOp")-v("V |
| 1 | 1.270 | 18.10E-3 |

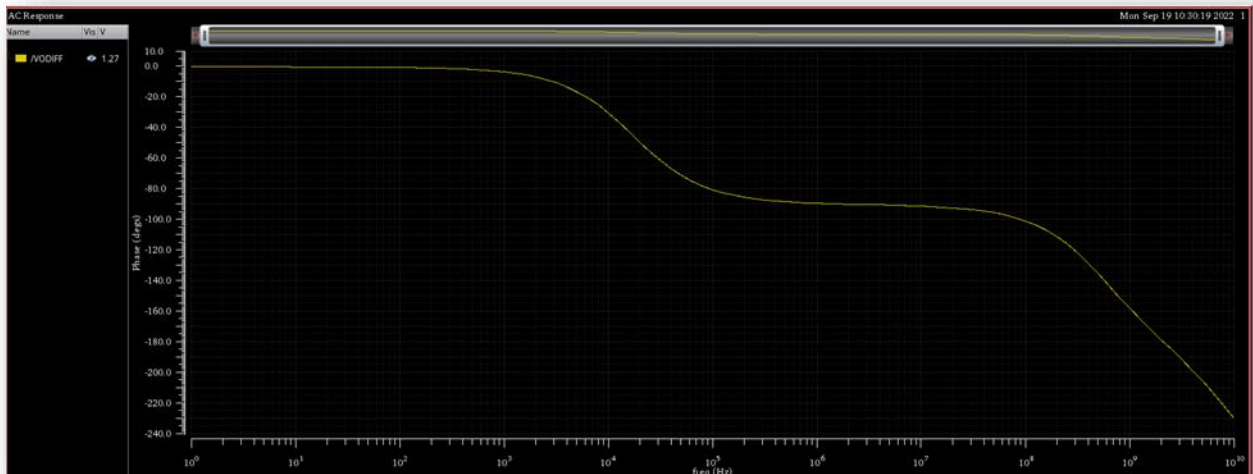
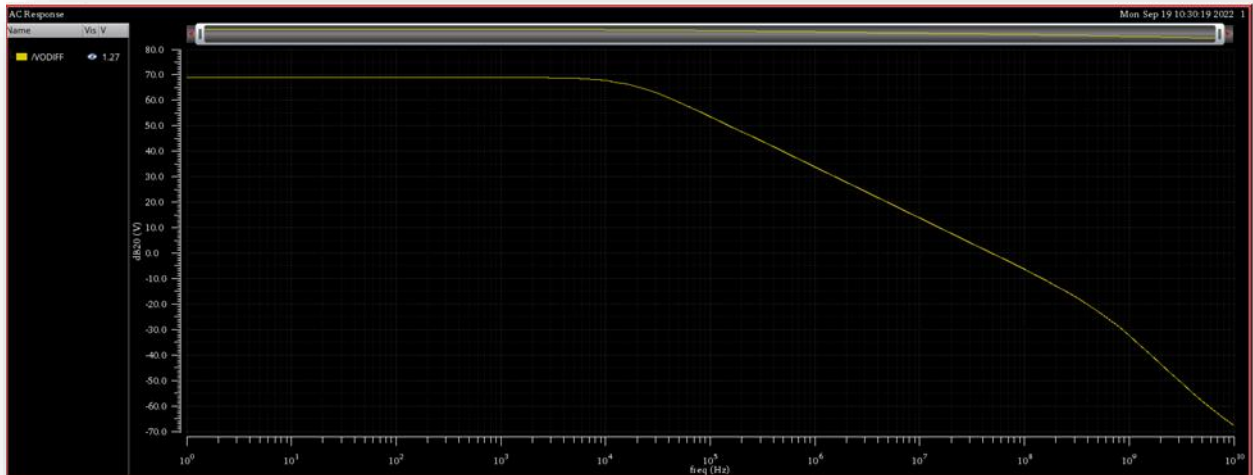
| | | |
|--------|-------|---------------------------------|
| Output | | v("VCTRLP" ?result "dcOp")-v("V |
| 1 | 1.270 | 11.47E-3 |


| | | |
|-------------|-------|----------------------------------|
| Ratio= 633m | | (v("VCTRLP" ?result "dcOp")-v("V |
| 1 | 1.270 | 633.7E-3 |

- the CM level at the output=0.71V, we force Vcm to equal VREF-VGSP=0.7
- the relation between them= CM gain of 5t-OTA which equal

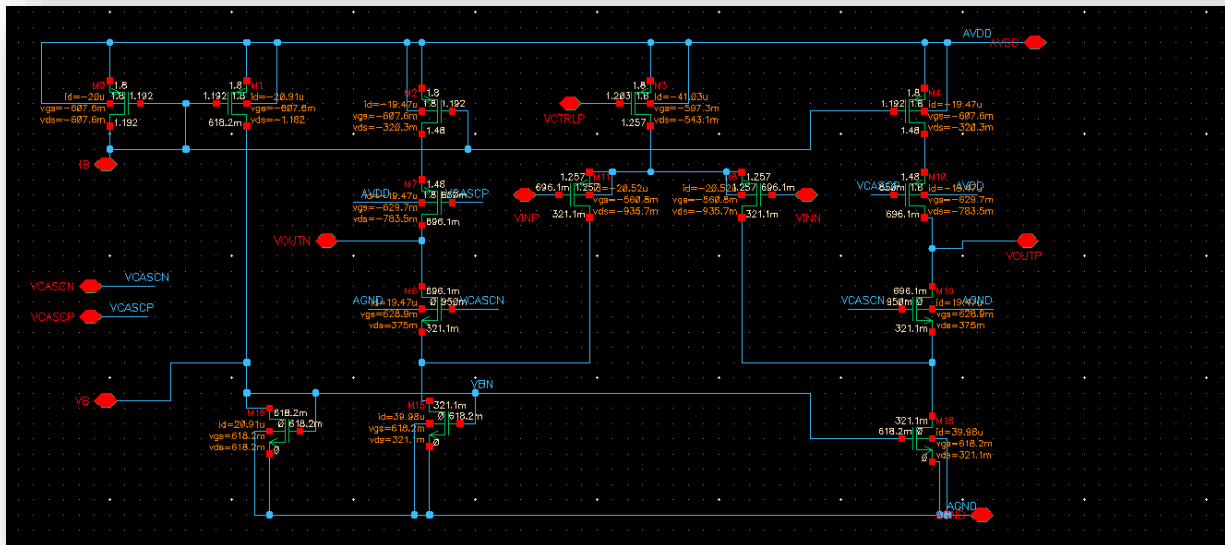
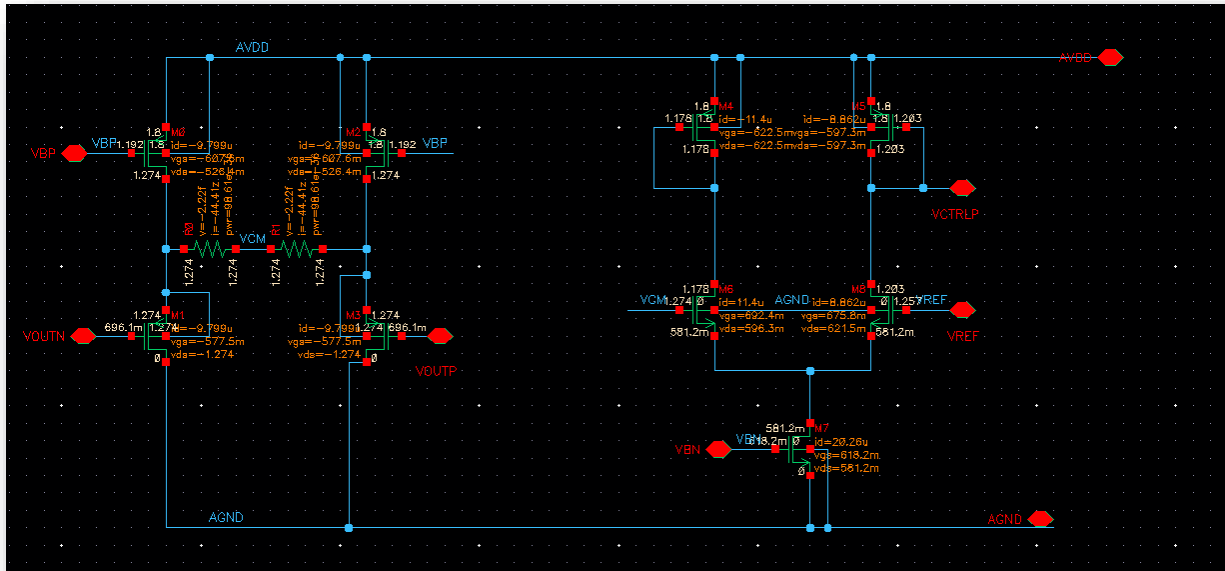
$$\text{to } \frac{1}{2(gm5+gmb5)RSS} = \frac{1}{2(93.07u+29.87u)*(\frac{1}{1.723u})} = 7m$$

2) Diff small signal ccs:



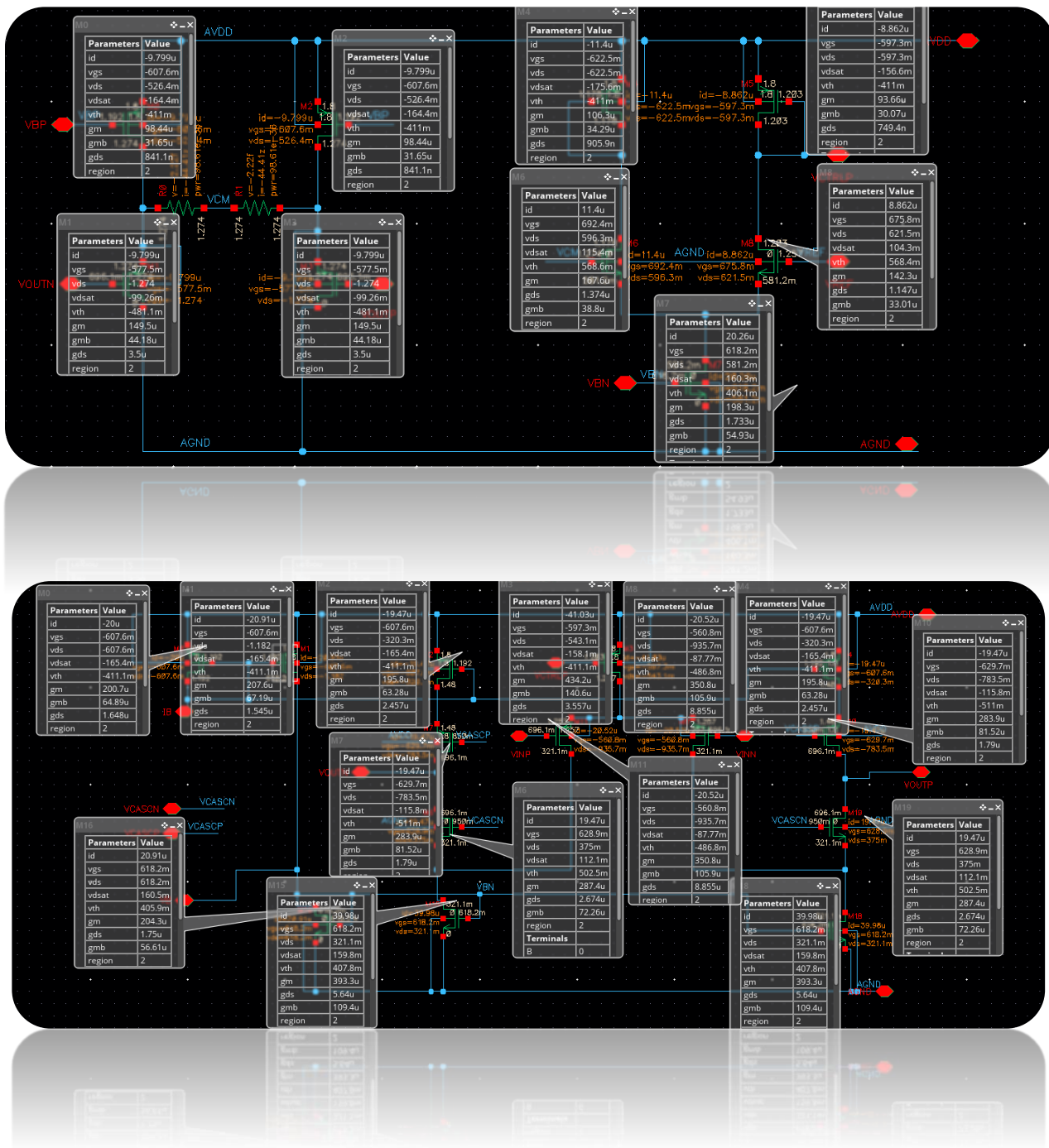
| Test | Output | Nominal |
|------------|---|---|
| lab11:TB:1 | /VODIFF |  |
| lab11:TB:1 | y _{max} (mag(VF("/VODIFF"))) | 2.903k |
| lab11:TB:1 | dB20(y _{max} (mag(VF("/VODIFF...)) | 69.26 |
| lab11:TB:1 | bandwidth(VF("/VODIFF") 3 "l... | 17.21k |
| lab11:TB:1 | gainBwProd(VF("/VODIFF")) | 50.07M |
| lab11:TB:1 | unityGainFreq(VF("/VODIFF")) | 49.8M |
| lab11:TB:1 | phaseMargin(VF("/VODIFF")) | 84.63 |

- **PART 5: Closed Loop Simulation (AC and STB Analysis)**

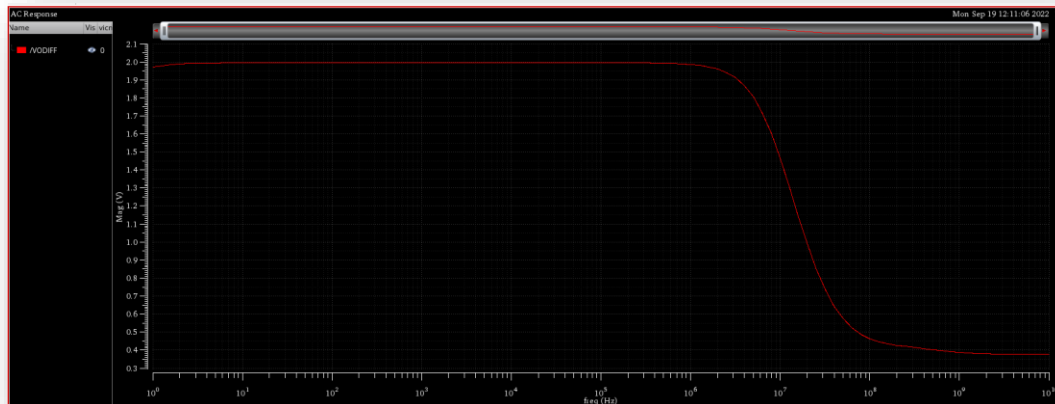


- CM level at the OTA output = 696.1mV , as we adjusted vref at this level thus Vocm should be equal to Vref to minimize the input error.
- CM level at the OTA input = 696.1mV, we put vicm= 0.55 V but since we are using high resistance in the feedback 1T the input node follow the output voltage .

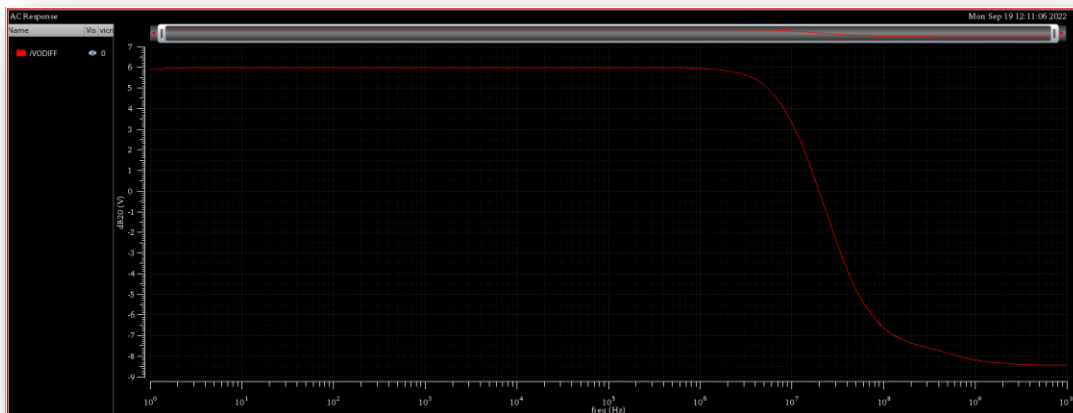
- Dc op



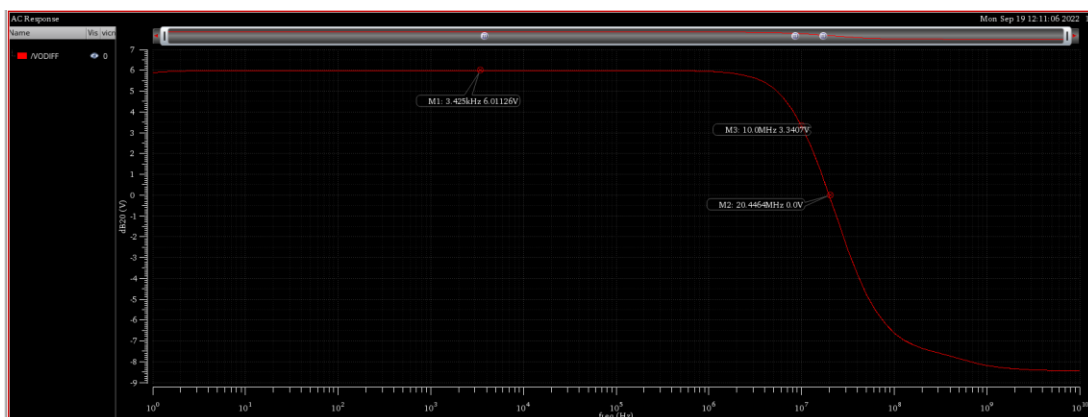
2) Differential closed-loop response:




- Gain(db)

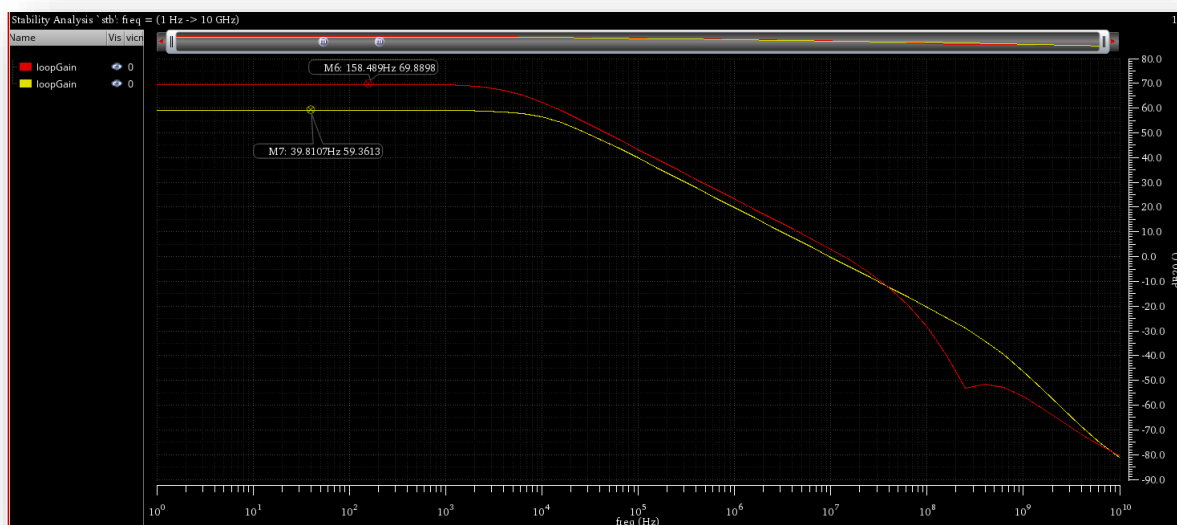
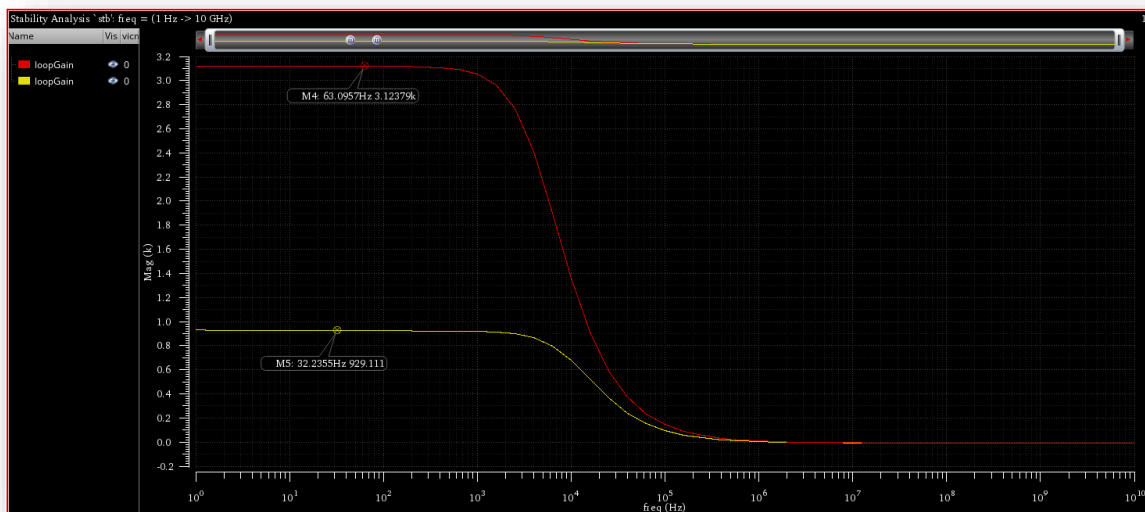


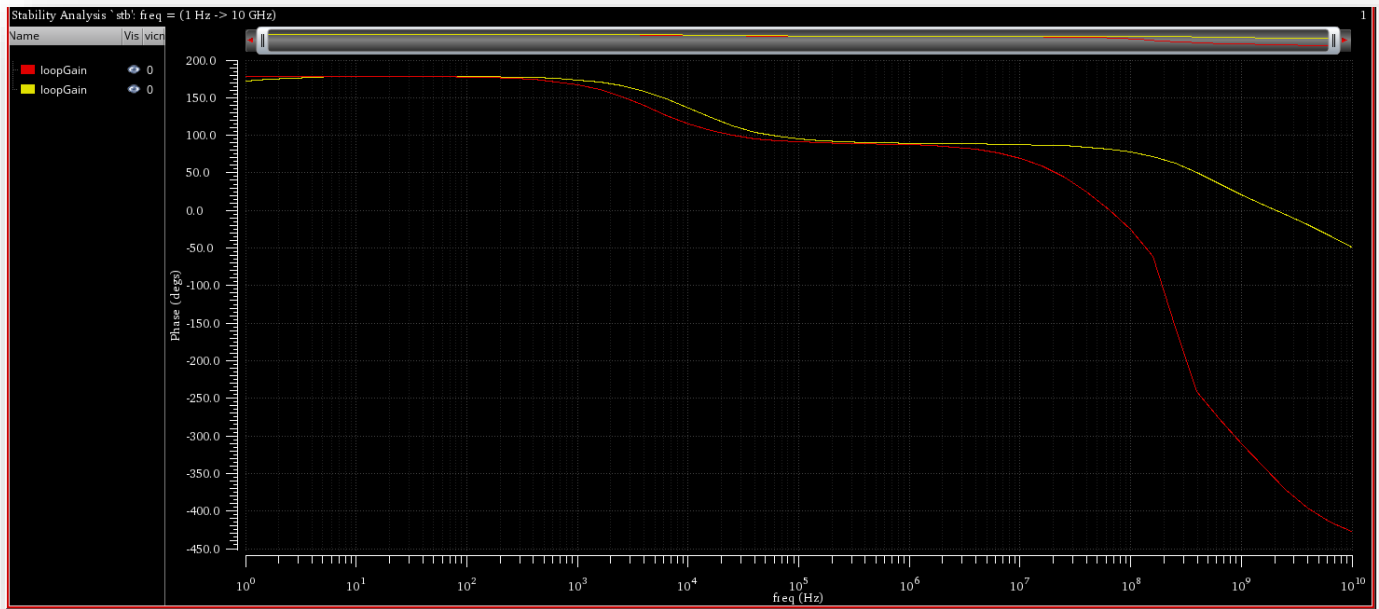
- Use Measures or cursors to calculate circuit parameters (DC gain, CL BW, CL GBW)



| Test | Output | Nominal |
|---------------|---------------------------------|---|
| lab11:part5:1 | /VODIFF |  |
| lab11:part5:1 | ymin(mag(VF("/VODIFF"))) 1 | 1.998 |
| lab11:part5:1 | dB20(ymin(mag(VF("/VODIFF...))) | 6.011 |
| lab11:part5:1 | bandwidth(VF("/VODIFF") 3 "l... | 11.2M |
| lab11:part5:1 | gainBwProd(VF("/VODIFF")) | 22.15M |
| lab11:part5:1 | unityGainFreq(VF("/VODIFF")) | 19.85M |

3) Differential and CMFB loops stability (STB analysis):





• Phase margin

| /phaseMargin x | |
|----------------|-----------------|
| vicm | /phase... (Deg) |
| 1 0.000 | 63.39 |

| gainBwProd(value(mag(getData | |
|------------------------------|---------|
| Expression | Value |
| 1 gainBwProd(v... | 10.15E6 |

| /phaseMargin x | |
|----------------|-----------------|
| vicm | /phase... (Deg) |
| 1 0.000 | 88.96 |

| gainBwProd(value(mag(getData | |
|------------------------------|---------|
| Expression | Value |
| 1 gainBwProd(v... | 15.40E6 |

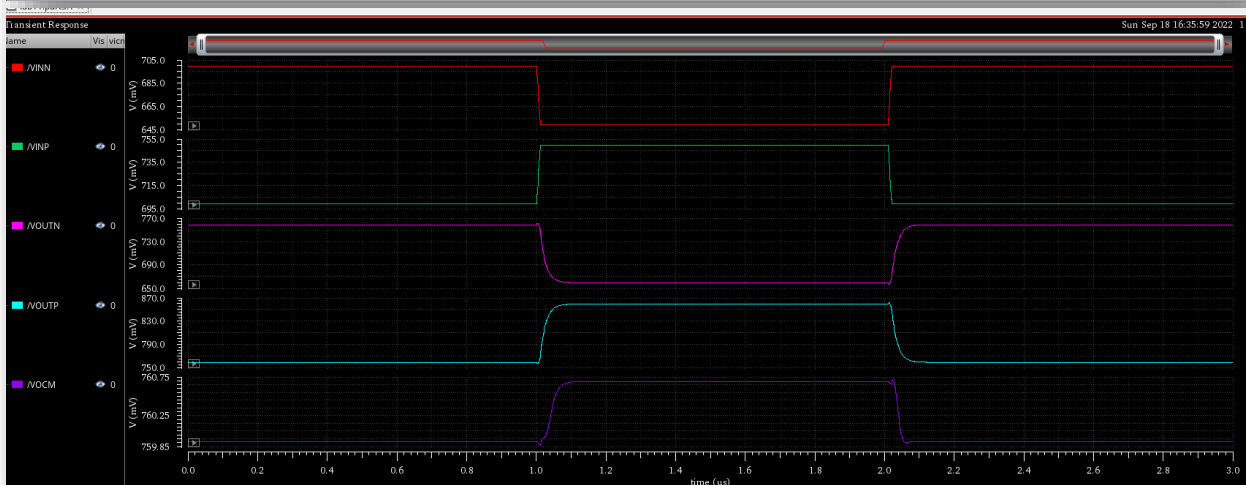
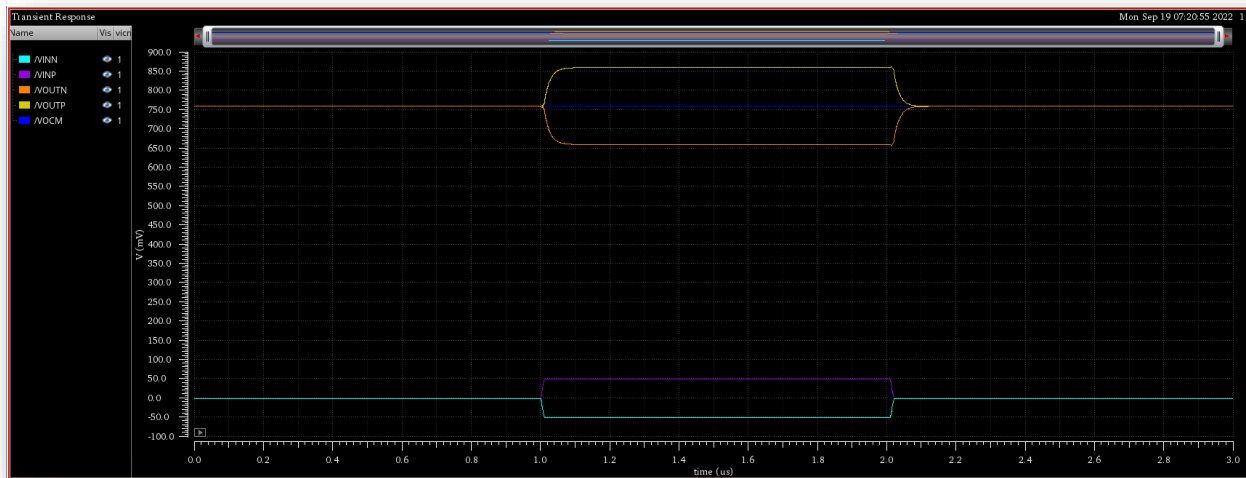
- GBW diff < GBW CM , PM diff> PM CM
- Compare DC LG and GBW of the diff loop with those obtained from open-loop simulation. Comment

| Parameter | Diff LG | Diff Open loop |
|-----------|----------|----------------|
| DC gain | 59.36 db | 69.26 db |
| GBW | 10.15M | 50.07M |

- As $\beta = 1/3 \rightarrow \text{Diff LG} = 1/3 * \text{AOL} = 59.36\text{db}$
- $\text{GBW} = \text{gain} * \text{BW}$, as gain decreases by factor 1/3 so GBW decreases by 1/3

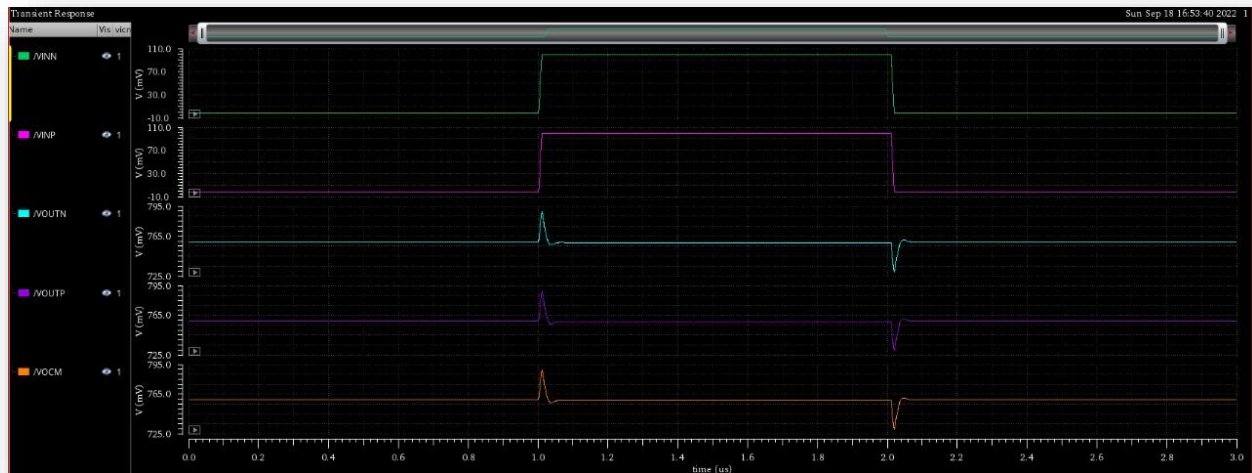
PART 6: Closed Loop Simulation (Transient Analysis)

1) Differential and CMFB loops stability (transient analysis):



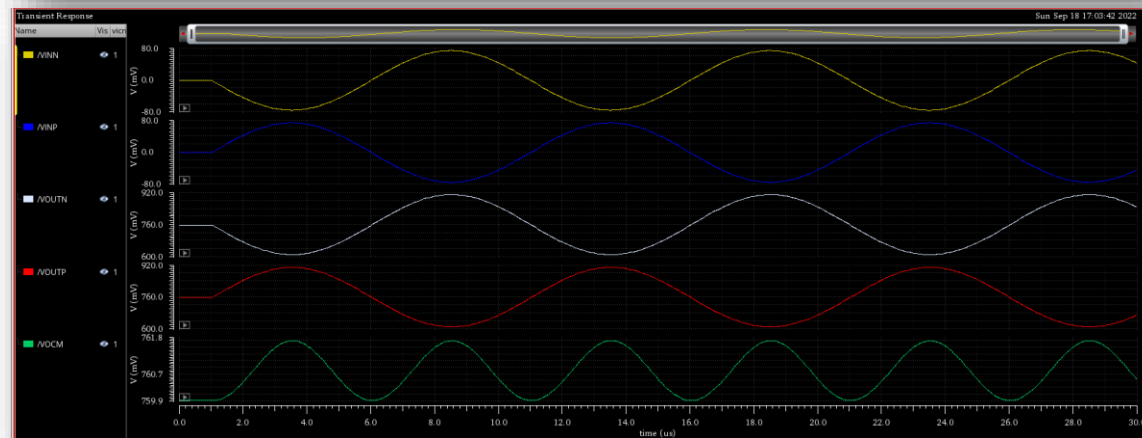
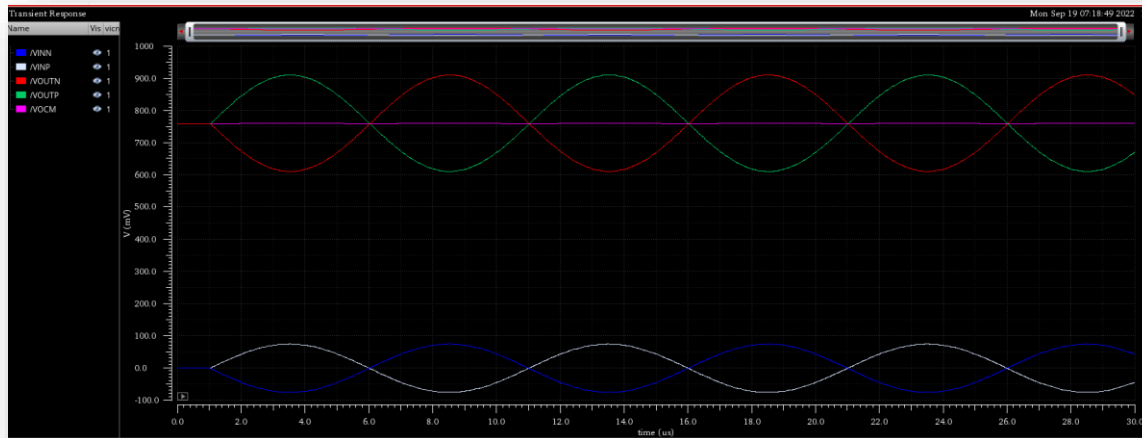
- No, ringing in time domain , yes both are stable

- Set differential input to zero and apply the same previous pulse at the balun CM input

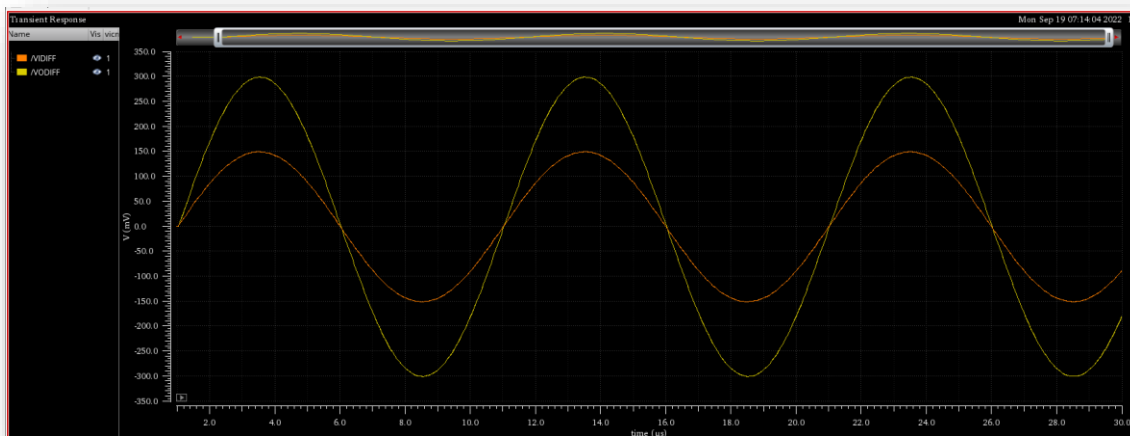


- Yes there are CM ringing in time domain , since CM PM in stp analysis = 63.3 which is smaller than 67 so the CM is underdamped.

2) output swing



- Voutdiff vs vindiff



| peakToPeak(value(getData("/VINDIFF"))) 1 | | peakToPeak(value(getData("/VOUTDIFF"))) 1 | |
|--|----------|---|----------|
| Expression | Value | Expression | Value |
| 1 peakToPeak(v... | 599.3E-3 | 1 peakToPeak(v... | 300.0E-3 |