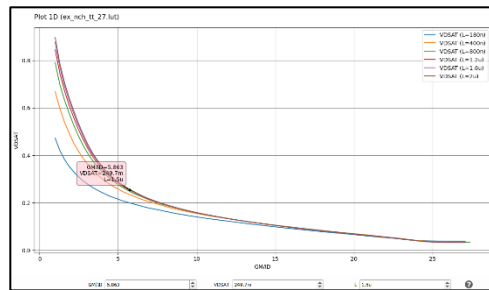
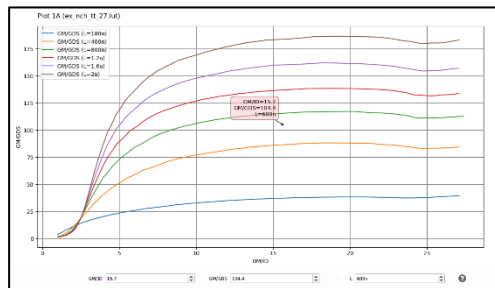
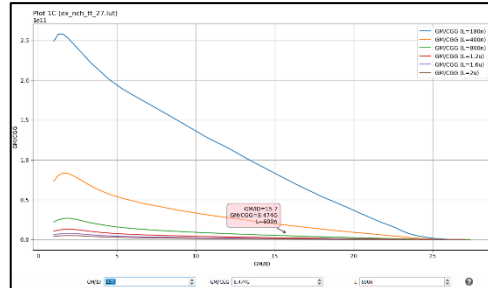
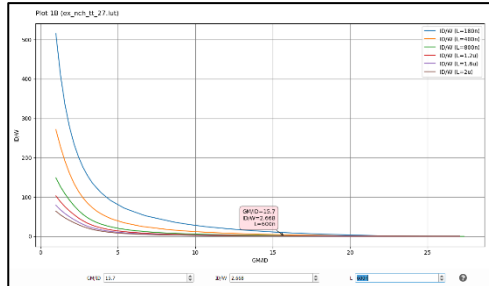


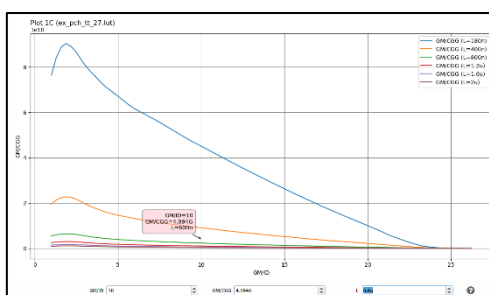
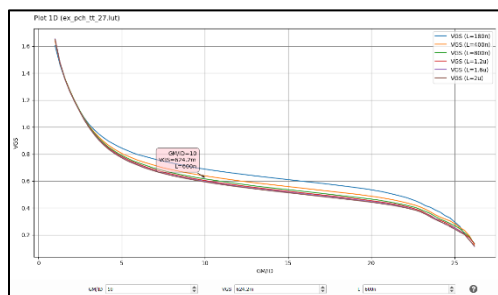
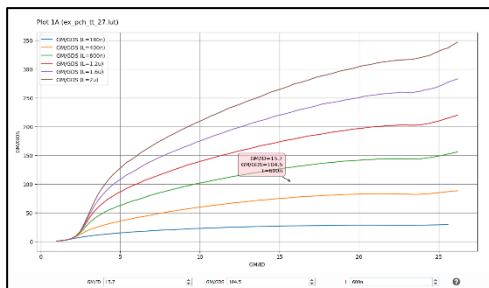
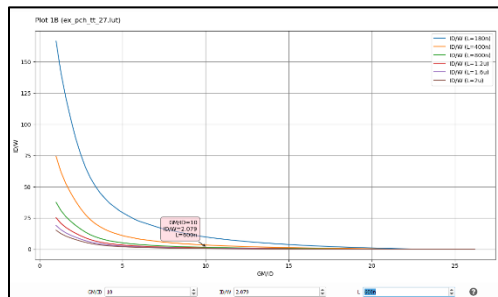
# Lab09

## Part01

### NMOS LOAD:



### PMOS LOAD:



## 1) Detailed design procedure and hand analysis.

\*  $M_1$  &  $M_2$  iP Pair &

$$\tau = \frac{t_{rise}}{2.22} = 31.53 \text{ ns}$$

$$G_{bw} = \frac{g_{m1,2}}{C_c} = 31.71$$

$$g_{m1,2} = 79.27$$

from SR,  $I_{B1} = 125 \mu A$

$$\therefore \frac{g_m}{I_D} = \frac{79.27}{6.25} = 12.6 \rightarrow \textcircled{1}$$

$$0.05 = \frac{(1 - \frac{1}{A_{vol}}) - 1}{1} \times 100$$

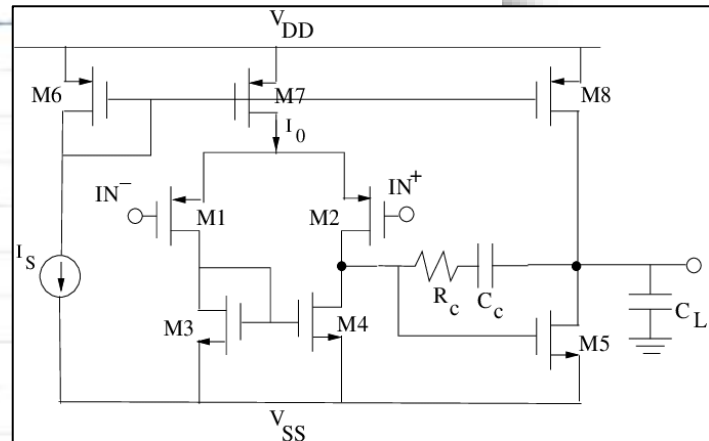
$$A_{vol} = 2000 \rightarrow \left. \begin{array}{l} \text{Gain}_1 = 2X \\ \text{Gain}_2 = X \end{array} \right\} \rightarrow \begin{array}{l} 2X^2 = 2000 \\ X = 10\sqrt{10} \end{array}$$

$$\therefore \text{Gain}_1 = 20\sqrt{10} = 36 \text{ db}$$

$$\therefore \text{Gain}_2 = 10\sqrt{10} = 30 \text{ db}$$

$$20\sqrt{10} = \frac{g_{m1,2} r_o}{2} \rightarrow g_{ds1,2} = 0.625 \mu$$

$$\therefore \frac{g_m}{g_{ds}} = 126.8 \rightarrow \textcircled{2}$$



From ① & ②  
 $L = 0.9 \mu$   
 $I_{D1} = 798.7 \mu$   
 $W_{n1} = 7.8 \mu$   
 $V_{GS1} = 566.4 \text{ mV}$

\*  $M_6, M_7, M_8$  tail Current Sources :-

$$V_{icm} \text{ high} < -V_{gs1} - V_{ds7} + \frac{V_{dd}}{L=1.8}$$

$\downarrow$   
1V

$$\therefore V_{ds7} = 0.234 \text{ V}$$

$$\text{from Swing } V_{dd} - 2V_{ov} = 1.4$$

$$V_{ds8} = 0.2 \text{ V} \quad \text{take this value.}$$

$$\text{from CMRR } A_{vcm} = 36.74 = -38 \text{ dB}$$

$$\therefore -38 \text{ dB} = \frac{1}{2g_{m3,4} r_{o7}} = 0.0125$$

$$\text{assume Current load } \frac{g_m}{I_D} = 10$$

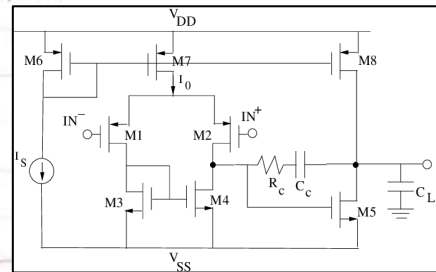
$$\therefore g_{m3,4} = 62.5$$

$$\therefore g_{ds7} = 1.5625$$

$$\text{from } V^* \rightarrow \left( \frac{g_m}{I_D} \right)_7 = \frac{2}{V^*} = 10 \quad \text{--- (1)}$$

$$\therefore g_m = 125$$

$$\rightarrow \left( \frac{g_m}{g_{ds}} \right)_7 = 80 \quad \text{--- (2)}$$



$$\begin{aligned} L &= 580 \text{ n} = 0.58 \mu \\ \frac{I_D}{W} &= 2.166 \\ W_7 &= 5.77 \end{aligned}$$

\*  $M_6, M_7$  &  $M_8$  Same  $L$  Because They come from Current mirror also same  $\frac{g_m}{I_d} = 10$

$$\begin{aligned} W_7 = 5.77 & \longrightarrow 12.5 \mu A \\ W_8 = x & \longrightarrow 47.5 \mu A \\ W_6 = x' & \longrightarrow 10 \mu A \end{aligned}$$

$$\begin{aligned} W_8 = x &= 22 \mu \\ W_6 = x' &= 4.66 \mu \end{aligned}$$

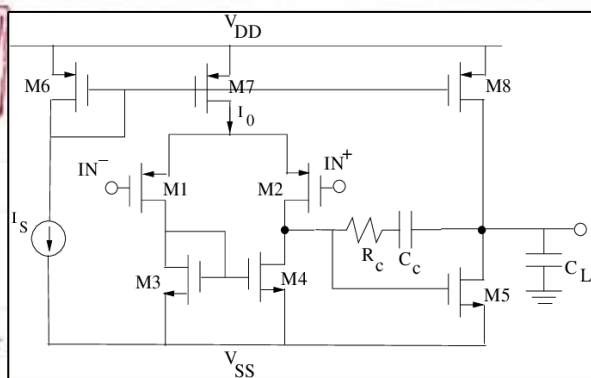
$$\begin{aligned} g_{ds7} &= 1.5625 \longrightarrow 12.5 \mu A \\ g_{ds8} &= x \longrightarrow 47.5 \mu A \end{aligned}$$

$$g_{ds8} = x = 5.93 \mu$$

\*  $M_5$

$$\frac{G_{m2}}{C_L} = \frac{4G_{m1}}{C_c}$$

$$G_{m2} = 8G_{m1} = 631.16 =$$



$$I_{B2} = 4I_{B1} \Rightarrow \text{but we have budget } \therefore I_{B2} = 47.5 \mu A$$

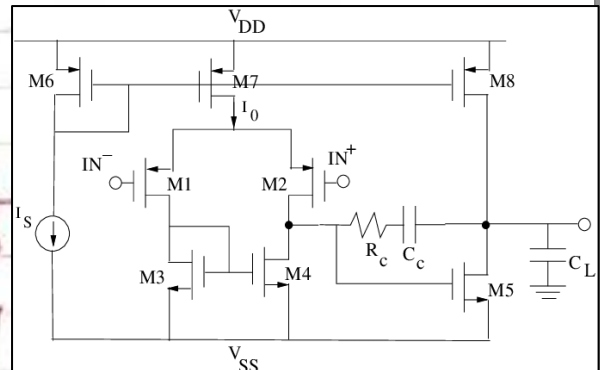
$$\frac{g_{m5}}{I_d} = 13.35 \rightarrow \textcircled{1}$$

$$Gain = g_{m5} (r_{o5} \parallel r_{o8}) = 10\sqrt{10}$$

$$g_{ds5} = 14.123 \mu$$

$$\therefore \left( \frac{g_m}{g_{ds}} \right)_5 = 45$$

$$\begin{aligned} L_5 &= 220 \text{ n} \\ \frac{I_d}{I_5} &= 12.31 \\ \frac{W}{L}_{gs} &= 619.4 \\ W_5 &= 3.85 \mu \end{aligned}$$



- $V_{gs}$  of 2<sup>nd</sup> input stage should follow  $V_{gs}$  of 1<sup>st</sup> stage current mirror so

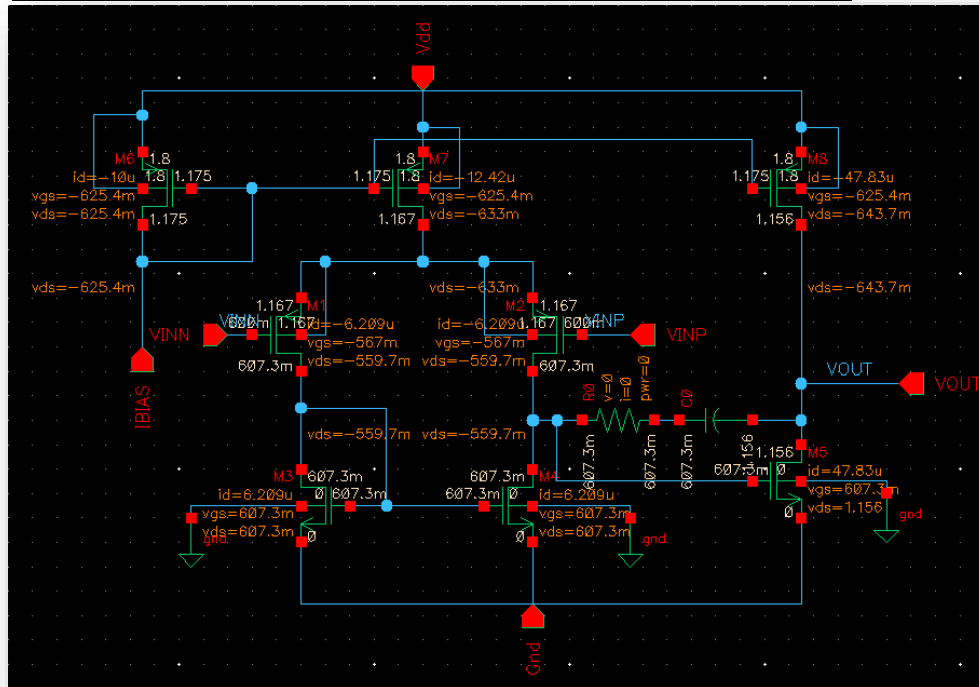
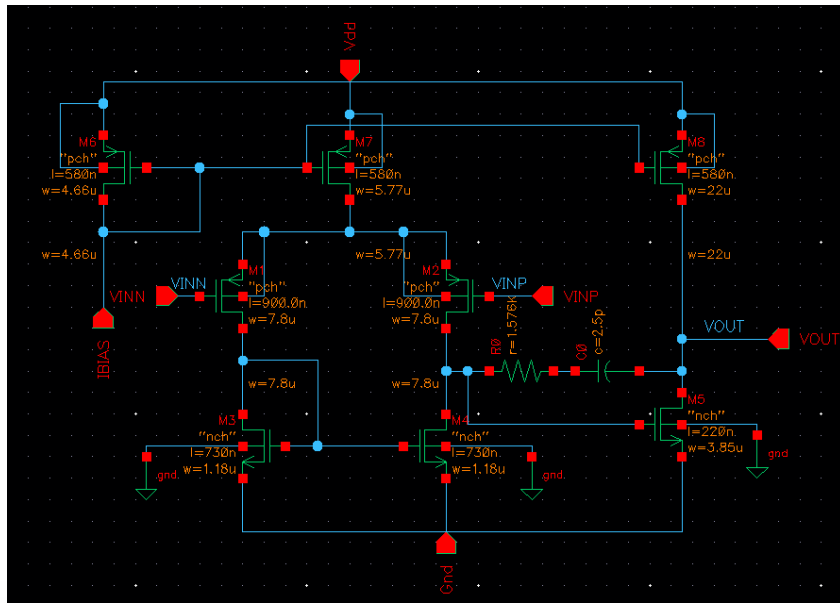
$$V_{gs_{3,4}} = 619 \text{ mV}, g_{ds} = 0.62 \mu \text{ and } I_d = 6.25 \mu$$

$$\text{From ADT } L = 730 \text{ n}, W = 1.18 \mu$$

$$G_m/I_d = 10.27 > 10 \text{ Condition satisfied}$$

- $R_z = 1/G_{m2} = 1.567 \text{ kohm}$

Parameter	W	L	Gm	ID	Gm/ID	Vov	V*
Input Pair M0&M1	7.8u	0.9u	79.27u	6.25u	12.6	15.25m	160.18m
Tail CS M7	5.77u	580n	125u	12.5u	10	195.19m	200.74m
Current Mirror M6	4.66u	580n	100u	10u	10	195.19m	200.74m
CM Load M3&M4	1.18u	730n	82.62u	6.25u	10.27	200.33m	151.56m
2 <sup>nd</sup> input M5	3.58u	220n	628u	47.5u	13.35	139.85m	151.56m
Output Load M8	22u	580n	475u	47.5u	10	195.19m	200.74m



- Yes, current and gm and vgs are exactly equal for both branches
- 1<sup>st</sup> stage output should be close to  $V_{DD}/3$  Well Defined
- 2<sup>nd</sup> stage should be close to  $V_{DD}/2$  iLL Defined so output higher by  $\Delta I R_0$

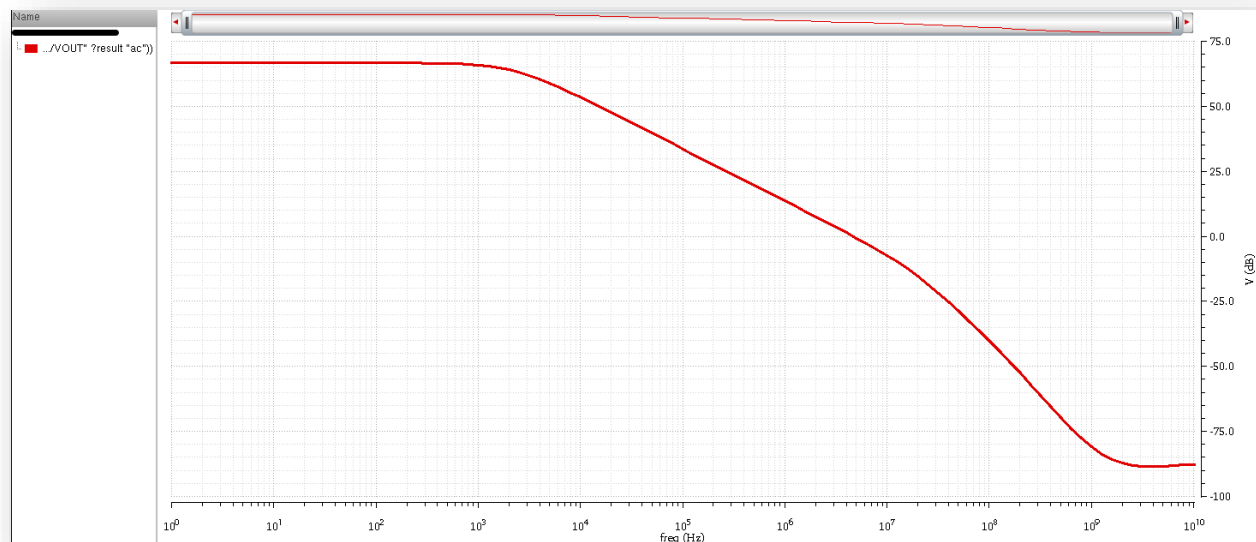
1	
vid	0.000
/VOUT (V)	1.156
/I0/net18 (V)	607.3E-3

## 1) Diff small signal ccs:

Test	Output	Nominal	Spec	Weight	Pass/Fail
ITI_ANALOG2:Labo9_TB:1	ymax(dB20(v("/VOUT" ?result...	66.53			
ITI_ANALOG2:Labo9_TB:1	ymax(mag(v("/VOUT" ?result...	2.121k			
ITI_ANALOG2:Labo9_TB:1	unityGainFreq(v("/VOUT" ?r...	4.685M			
ITI_ANALOG2:Labo9_TB:1	bandwidth(v("/VOUT" ?result...	2.241k			
ITI_ANALOG2:Labo9_TB:1	gainBwProd(v("/VOUT" ?res...	4.764M			

- diff gain (in dB) vs frequency.

**66.52db**



Parameter	Hand	Simulation
Gain	2000	2121
GBW	5M	4.76M
BW	2500	2241

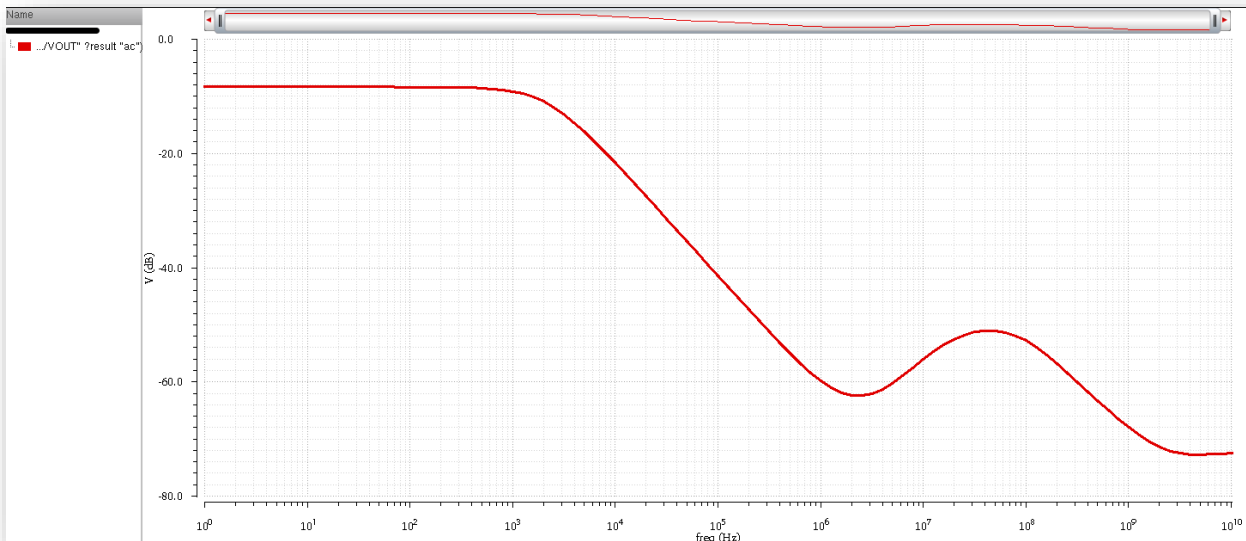
- GBW and BW less than calculated due to parasitics.



## 2)CM small signal ccs:

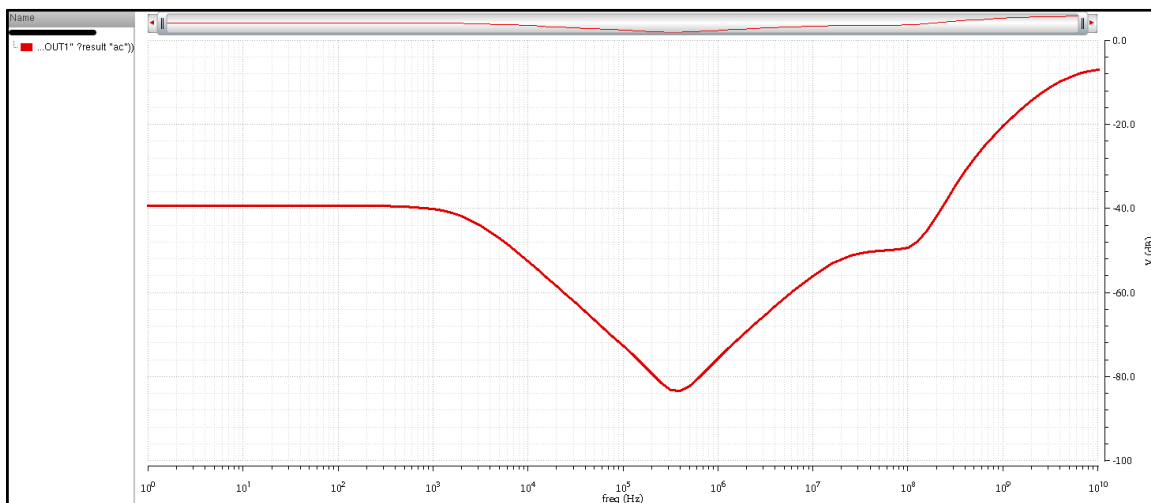
- CM gain in dB vs frequency.

-8.4db this gain after multiplying by 2<sup>nd</sup> stage gain = 30db



Parameter	Hand	Simulation
Gain	-38db	-39.34db

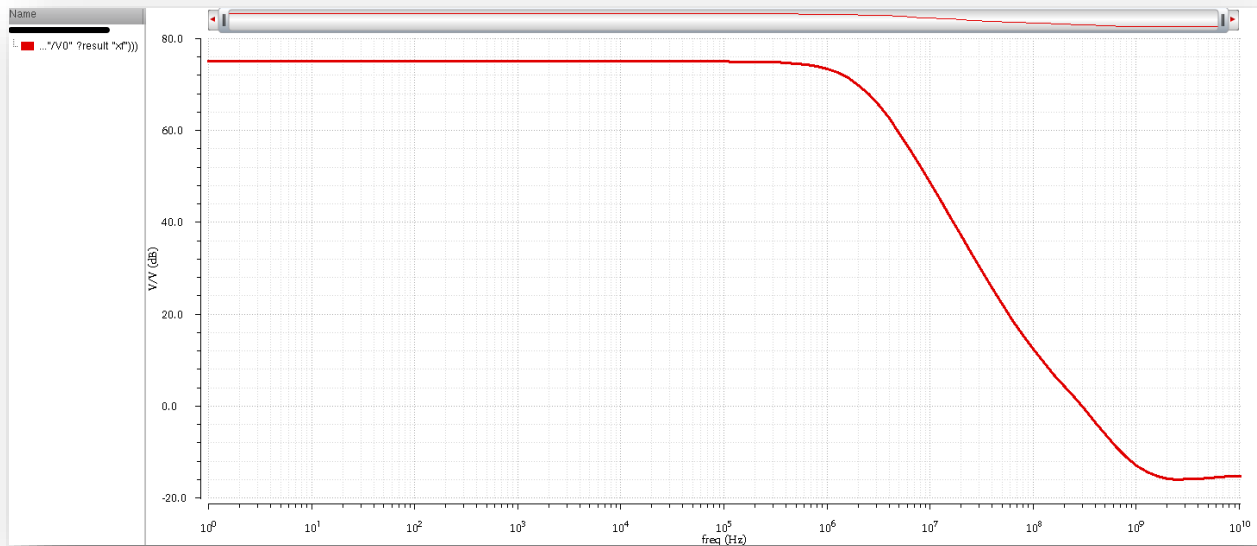
- At the first stage



### 3) (Optional) CMRR:

- CMRR in dB vs frequency

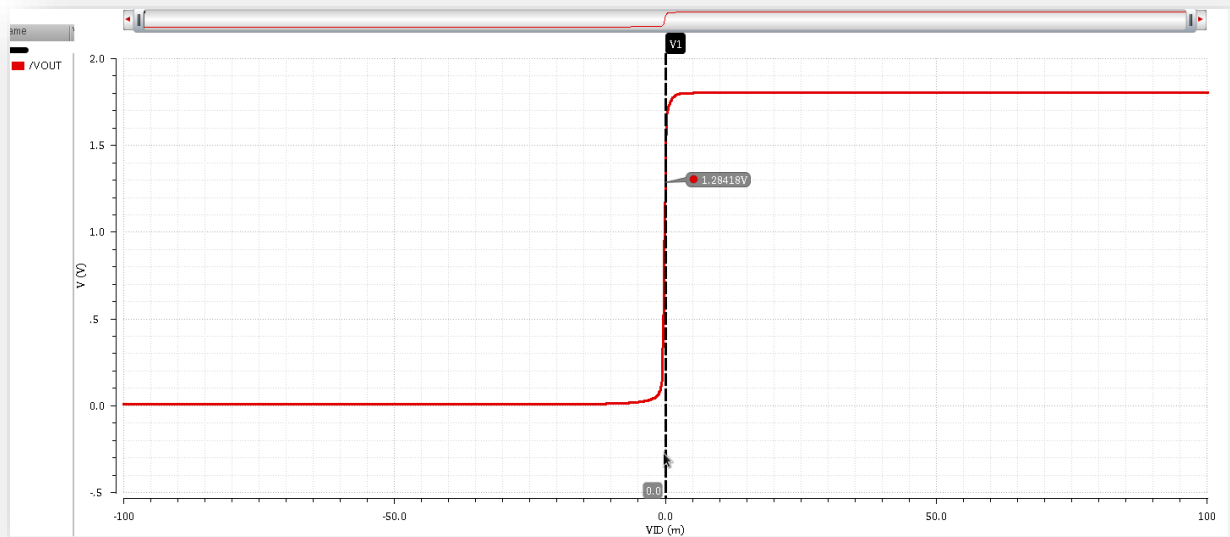
75db



Parameter	Hand	Simulation
CMRR	74db	75db

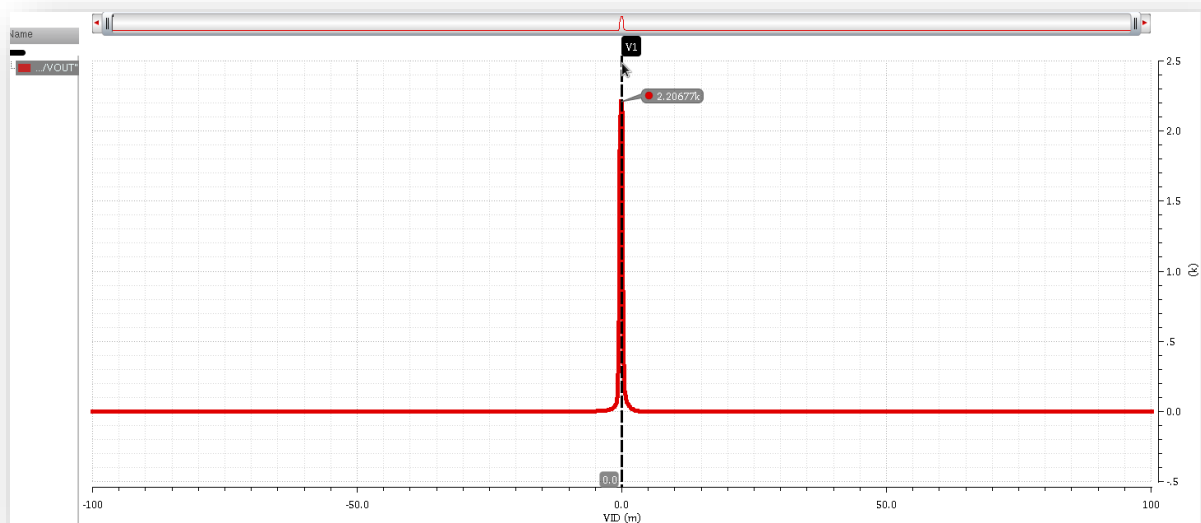
$$CMRR = A_{vd} = 36db - (-38db)$$
$$A_{vcm} = 74db$$

## 4) (Optional) Diff large signal ccs:



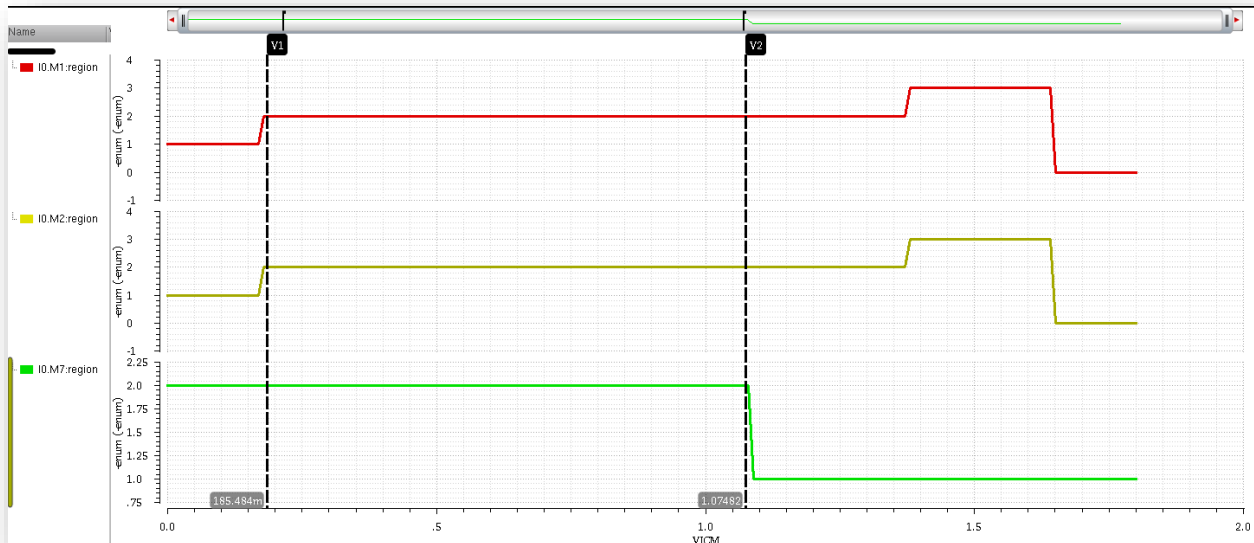
- equal values

	vid	/VOUT (V)
1	0.000	1.285

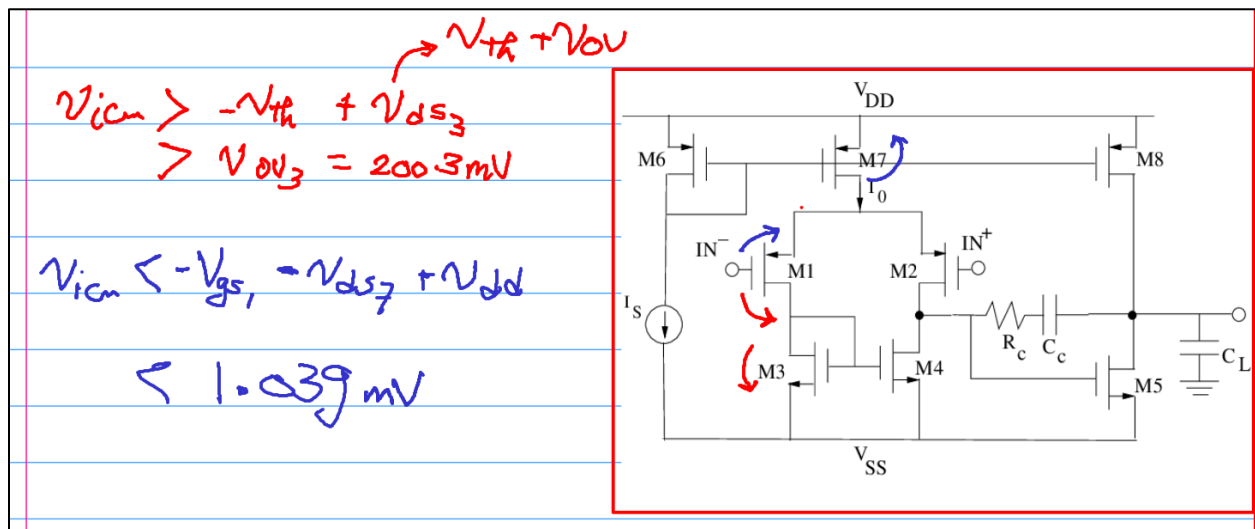


- $\sim$  equal the  $A_{vd}$

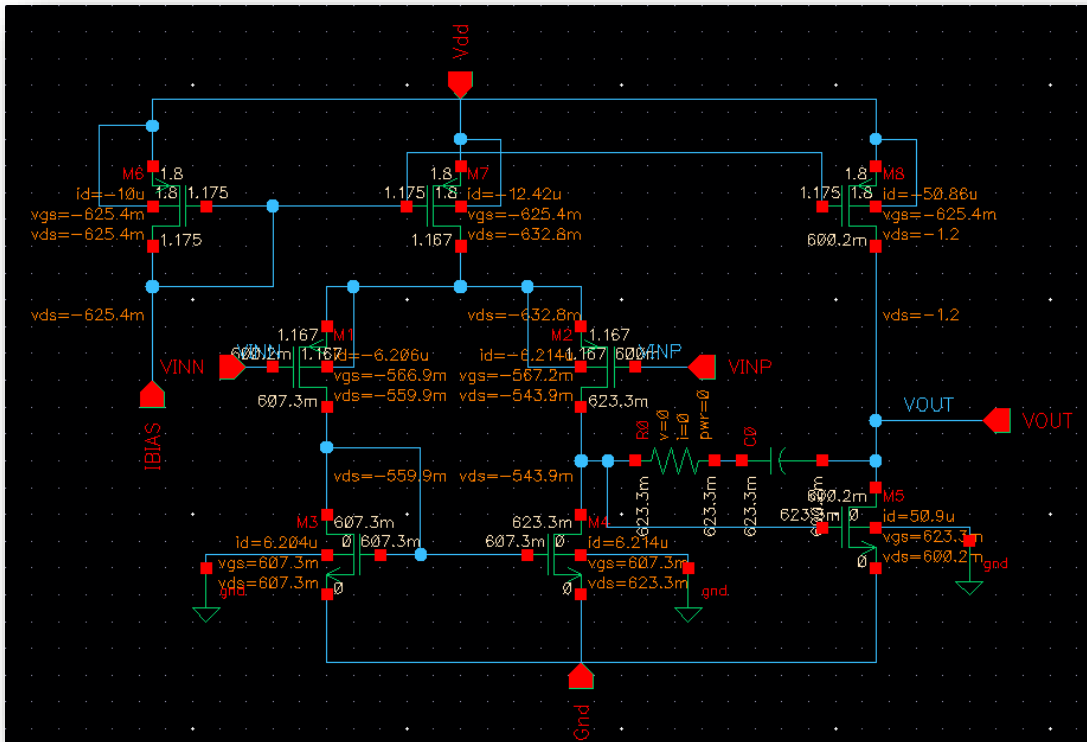
## 5) CM large signal ccs (region vs VICM):



Simulation	0.185	1.07
Hand	0.203	1.039

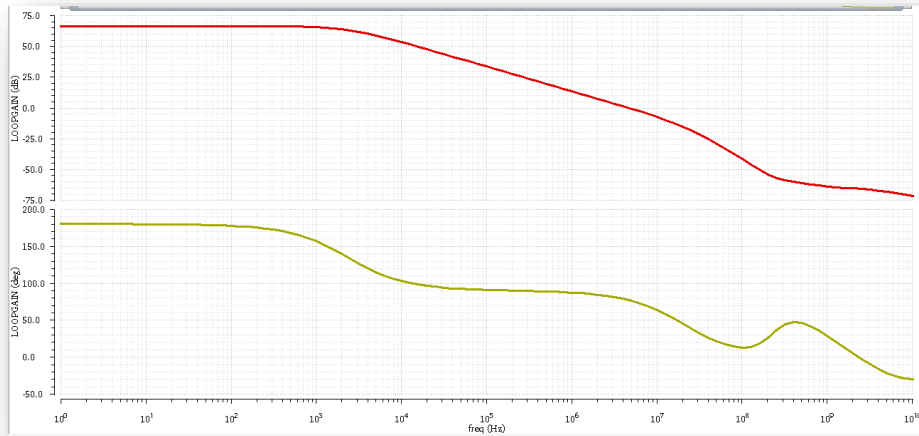


## PART 4: Closed-Loop OTA Simulation



- Dc voltages not equal in input terminals due to the error of the feedback system
- DC voltage at the output of the first stage not exactly equal to the value in the open-loop simulation due to diff in  $V_{icm}$
- current (and gm) in the input pair not exactly equal there is difference due to the mismatch in input pair

## 2) Loop gain:



Test	Output	Nominal
ITI_ANALOG2:Labo9_TB2:1	bandwidth(getData("loopGain...	2.341k
ITI_ANALOG2:Labo9_TB2:1	unityGainFreq(getData("loop...	4.684M
ITI_ANALOG2:Labo9_TB2:1	gainBwProd(getData("loopGa...	4.757M
ITI_ANALOG2:Labo9_TB2:1	ymax(mag(getData("loopGain...	2.027k

- Values are equal to those from open loop gain because  $\beta=1$
- $LG = \beta \times A_{OL} = A_{OL}$

- gainMargin(dB)=65.475506  
gainMarginFreq(Hz)=2.3205746e+09  
phaseMargin(Deg)=77.390461  
phaseMarginFreq(Hz)=4631467.5

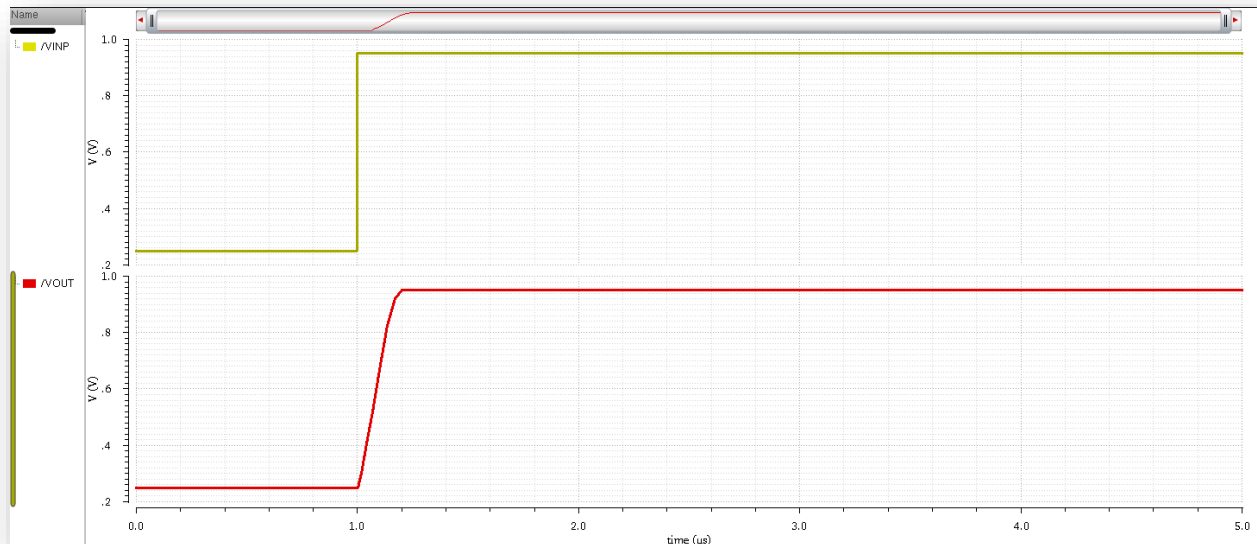
$$PM = 90 - \tan^{-1} \left( \frac{gm_0}{\frac{C_c}{gm_7}} \right) = 75.83$$

- $PM = 77.4^\circ$  > 70 condition satisfied

$LG = PA_{OL} = A_{OL} = 2000$ ( $\beta=1$ )
$GBW = LG \times BW = 5 \text{ MHz}$
$\rightarrow$ same BW of open loop $\beta$ is frequency independent

Parameter	Hand	Simulation
Gain	2000	2300
GBW	5M	4.757M
BW	2500	2027

### 3) Slew rate:

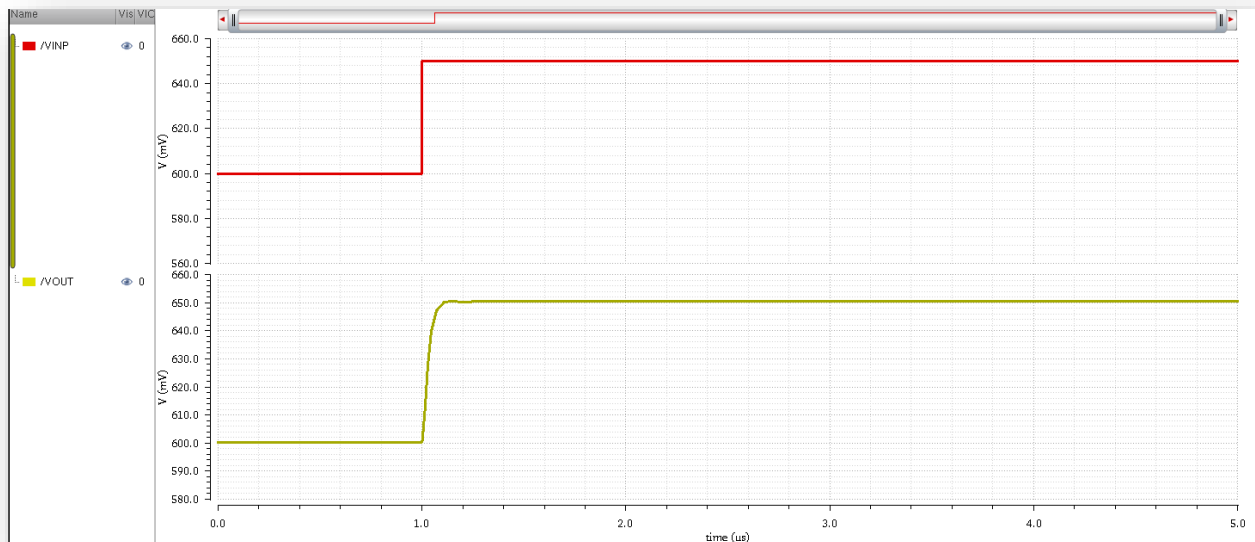


ITI_ANALOG2:Labo9_TB2:1	slewRate(v("/VOUT" ?result "...	4.205M
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Parameter	Hand	Simulation
Slew rate	$I_d/C_c = 5\text{M}/\mu\text{s}$	4.2M/ $\mu\text{s}$

- Could be better with using smaller  $C_c$  , hence BW1 and GBW increases and PM dec slightly since second stage pole is not **changed** (CL dependent not  $C_c$  ,  $C_c$  just make the output node LIN and hence  $W_{p2}$  go outwards).

## 4) Settling time:



ITI\_ANALOG2:Labo9\_TB2:1    riseTime(v("/VOUT" ?result "t...    54.88n

$$\tau_{rise} = \frac{2.22}{\mu g^p} = \frac{2.22}{2\pi \times 5M} = 70.6 nS$$

Parameter	Hand	Simulation
Rise time	70.6nS	54.88nS

No ringing since we have  $PM = 77$  , the system is critically damped