**Virtual Quality Control Robot Electrical Design**

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**Abstract**

A driver circuit designed to be placed on a printed circuit board is developed to control the speed and direction of four motors that attach to the arms and gripper of a quality control robot. Each motor requires its own driver circuit in order to operate independently. A driver circuit consists of a dual-input H-bridge that is used to control the speed and direction of the motor. This PCB is then mounted on the base of the robot and connects to the four motors, with one placed at each joint. An optical encoder is selected to measure rotation angle and this information is sent to the system’s controller.

This report introduces the relevant nomenclature and describes an overview of the system electronics in Section 1. The motor selection process is reviewed in Section 2, and Section 3 describes the circuit design in detail. Section 4 presents the step response and model that will be used in subsequent steps of the design. Section 5 outlines the PCB configuration, followed by a look at the 3D model of the board in Section 6. Finally, Section 7 describes the encoder selection process and additional resources are presented in Appendix A.

**Nomenclature**

SCARA Selective Compliance Assembly Robot Arm

PCB Printed Circuit Board

OP AMP Operational Amplifier

GBP Gain Bandwidth Product

BJT Bipolar Junction Transistor

NPN Negative-Positive-Negative

PNP Positive-Negative-Positive

TF Transfer Function

CPT Counts Per Turn

1. **Electrical System Overview**

Before designing the driver circuits, power source and microcontroller constraints are reviewed. An Arduino Leonardo is used which has a +5V rail. This means that an H-bridge is required for the motors to rotate in both directions. In order to keep the overall system frame small and inexpensive, one common power supply spanning from -18V to +18V is used. Thus, there is no need for multiple sources or stepping voltages up or down. A linear model is made to approximate the transfer function of the circuit for this virtual system. An optical encoder is used to measure position; this information is sent to the arduino for appropriate PID response.

1. **Motor Selection**

The motor that was chosen is a balance of several parameters. Ideally the motor must be lightweight, small, minimize power consumption, and have a nominal torque that is able to support the remaining joints and gripper. As per Maxon motor’s drive.tech page [1], motors with precious metal brushes have a higher terminal capacitance, making them more responsive to sudden changes in voltage. Having a higher terminal capacitance also prevents increased no load currents and mitigates the motor temperature rise during operation. Fast response to change in voltage and reduced temperature are desirable parameters for our system.

The SCARA robot will be lifting small and lightweight objects and since the overall design is small, we are able to use the same motor at each joint and to control the gripper. The motor is an 18V Maxon DCX 22S Precious Metal Brush DC motor. The motor is 34mm long with a 22 mm diameter enclosure, and the shaft has a diameter of 3mm. The motor’s max speed is 12400 rpm and has a stall torque of 14.5 mNm. The motor can be found on page 89 of the Maxon™ Motor catalog [2]. The motor is shown in Fig. 1

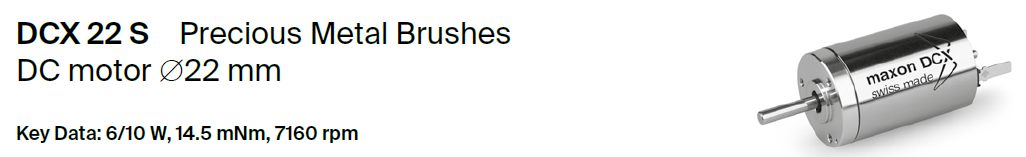


Figure 1: Maxon Motor

1. **Circuit Design**

The motor must operate in both the forward and reverse directions for a full range of motion with 3.5 degrees of freedom. An H-bridge circuit is used with two input ports that connect to the Arduino for directional control. The logic used to control the motor is shown in Table 1.

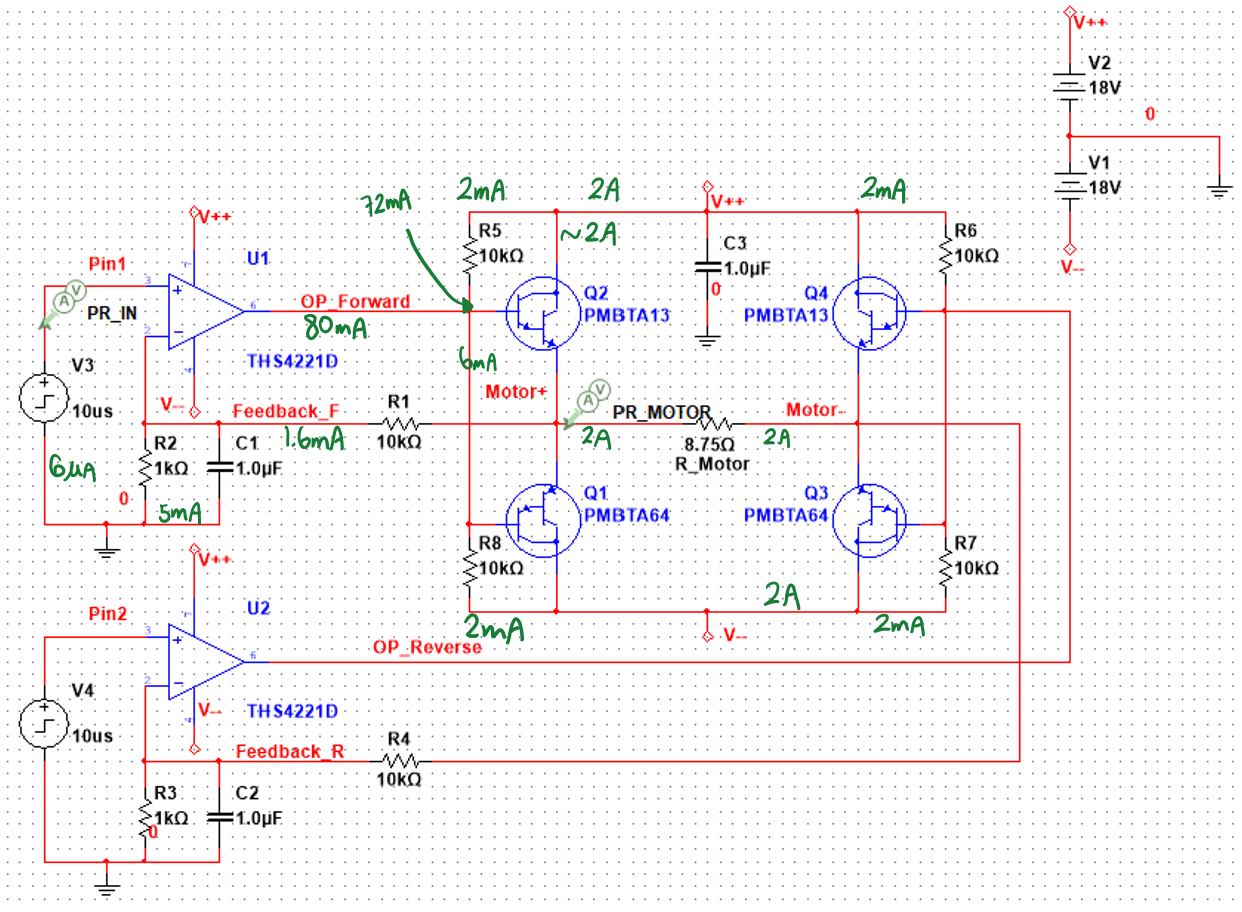
|  |  |  |
| --- | --- | --- |
| **Pin 1** | **Pin 2** | **Direction** |
| High | Low | Forward |
| Low | High | Reverse |
| Low | Low | Stopped |
| High | High | Stopped |

Table 1: Directional Control from Arduino Pins

The motor is modelled using the terminal resistance found in the Maxon Motor Catalog, with a value of 8.75 Ω. Two op amps are connected to the input pins from the Arduino and connected to ±18 V to increase the voltage before it reaches the motor. Two THS4221D op amps were chosen due to their fast response and low distortion [3]. This op amp has a GBP of 120 MHz and a slew rate of 990 µV/s, which give it an extremely fast response and as a result a straightforward transfer function estimate.

Two PMBTA13 NPN Darlington Transistors [4] were used in combination with two PMBTA64 PNP Darlington Transistors [5]. These BJTs have a high voltage gain and deliver the necessary current for the motor, which has a stall current of 2.06 A. Feedback resistors are connected to the op-amp, and an optimal gain with minimum overshoot was found with R1 = 10 kΩ and R2 = 1 kΩ. Additional 10 kΩ pull-up and pull-down resistors are added to reduce the sensitivity of the circuit. The circuit is shown in Figure 2. The step voltage sources are used to model the input from the Arduino pins. Currents at each connection are measured using the probing tool. As an additional feature, bypass capacitors were added to limit noise in the feedback path and the overall response improved with less overshoot in the transients.

Figure 2: Driver Circuit



1. **Driver Response and Linearization**

The driver circuit in Figure 2 gives two different responses, depending on the inputs to the step sources, which correspond to the inputs in Table 1 above. The transient responses of the motor operating in the forward and reverse directions are shown in Figures 3 and 4A, respectively.

The reverse direction’s voltage is taken as a differential voltage across the motor and as a result there is slight overshoot and settling before reaching a final value that is just above 16 V, which will suffice for our load and speed requirements when using the 18 V motor. The effect of the bypass capacitors can be observed by analyzing Figure 4B in the Appendix, where the response has a greater settling time.

Analysis of the transient plot indicates that the selected op amp gives a fast response with appropriate voltage gain for our 18 V motor. Figure 5 in Appendix A presents the near steady-state values of the motor’s voltage and current, which are similar to and approaching the motor’s stall torque and nominal voltage.

Figure 4: Driver Circuit Transient in Reverse Direction

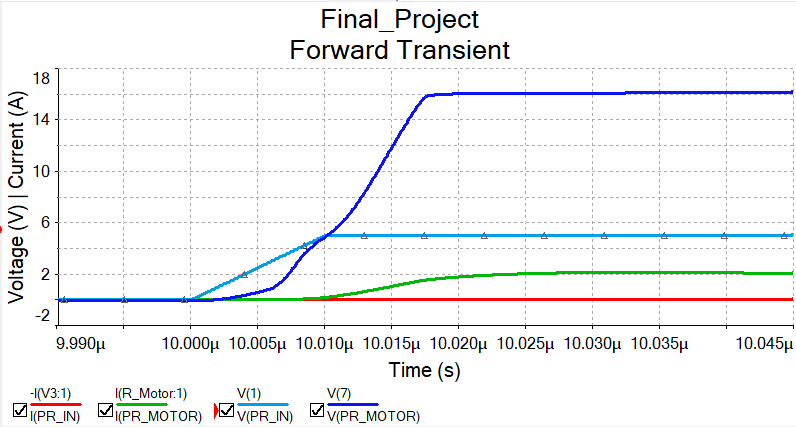
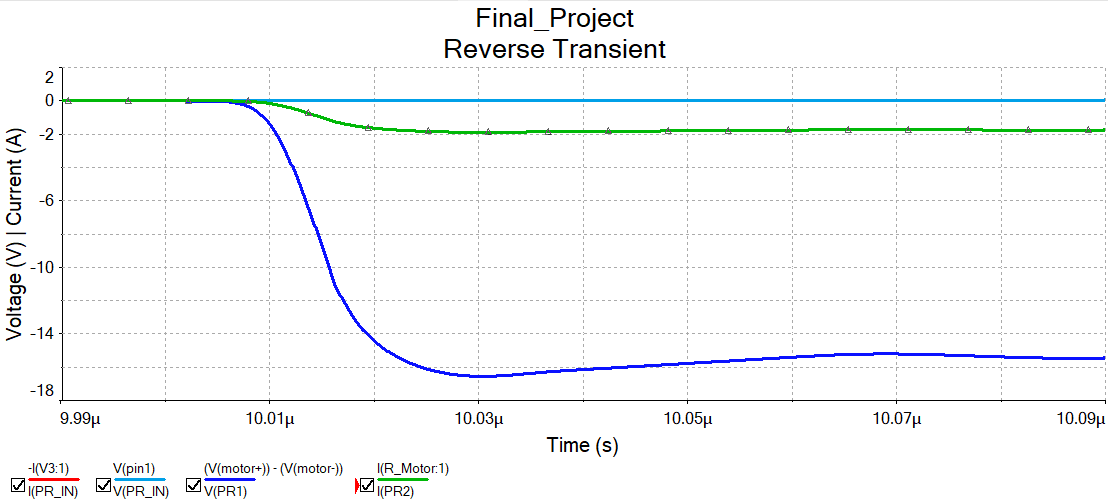


Figure 3: Driver Transient Response in Forward Direction

Using the results obtained from the transient response of the driver circuit, we can use MATLAB to estimate the appropriate transfer function. This method is preferred as it allows for accurate estimations and quick turnaround time when iterating designs. The estimated driver TF is then used in a model of DC motor as shown in Figure 6. The estimated transfer function using the **tfest** MATLAB function is shown in Figure 7 in Appendix A, with a fit above 90% using a second order estimation. A step response of the model using only a P controller is shown in Figure 8.

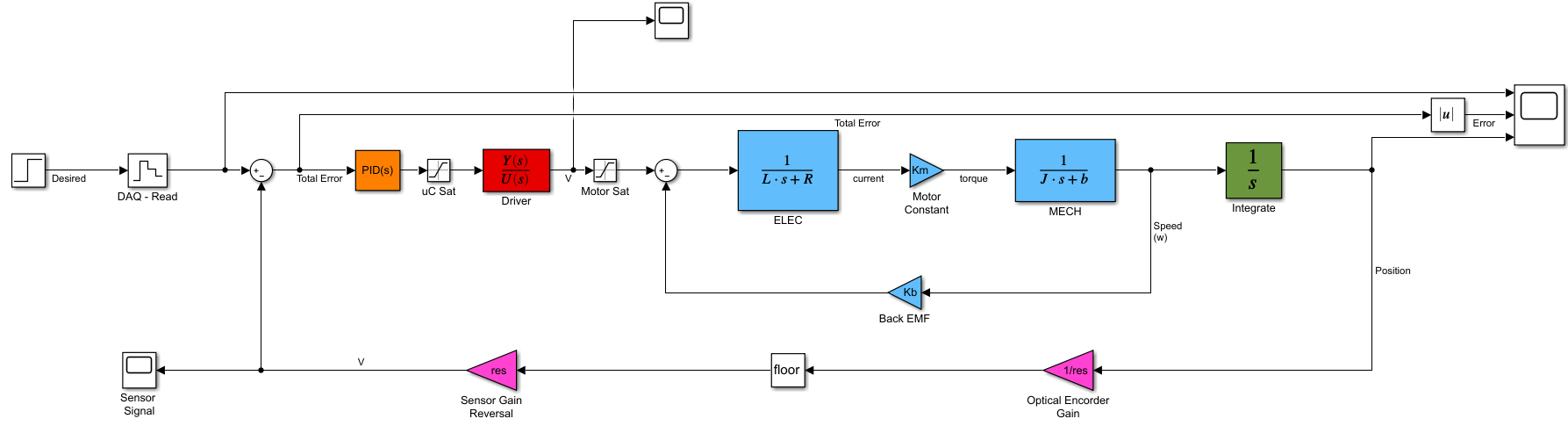


Figure 6: Motor Linear Simulink Model with Driver Circuit TF in Red

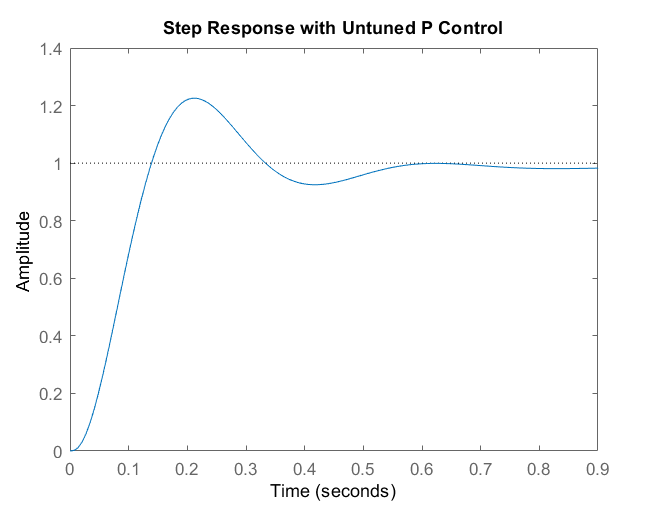


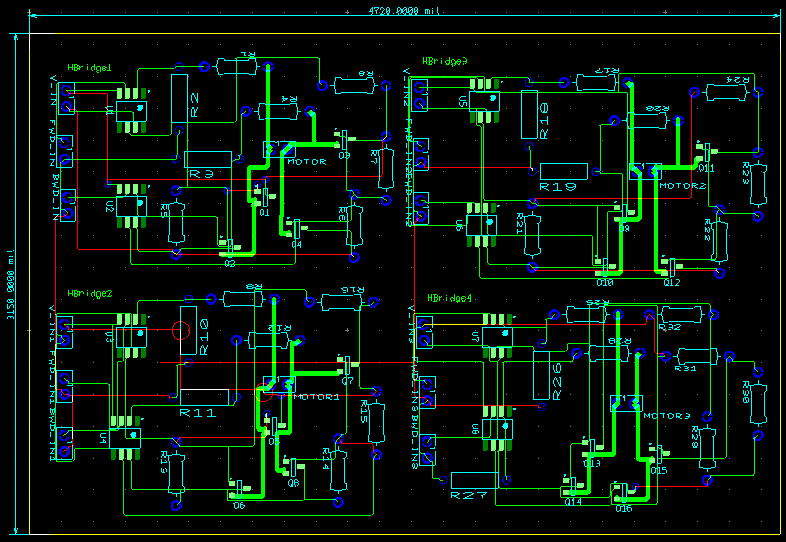
Figure 8: Linear Model Step Response with P Control Only

1. **PCB Configuration**

The PCB contains four H-bridge driver circuits, one for each motor. Since the circuits are identical, a similar approach was taken when laying out the four different drivers. An emphasis was placed on reducing board size and limiting the number of vias for ease of manufacturing.

As shown in the driver circuit in Figure 2, each node and input was probed and max current was recorded. The corresponding trace sizes can then be calculated for our PCB. Common manufacturing guides indicate that on the lower end, thickness of PCBs are 1-2 oz/ft^2 of copper. For 2oz of copper, spacing between traces of 8 mils is recommended [6]. When calculating trace width, the official DigiKey trace width calculator was used, which complies with IPC221 standards, and is sufficient for this application [7, 8]. An example of trace width calculation is shown in Figure 9 in Appendix A. The largest trace width was found to be 40 mils for 2 amps of current. These thick traces are connected between the power supply and the motors. All other traces carry current below 100 mA and therefore a trace width of 5 is appropriate and within manufacturing constraints when creating a PCB. The 2D drawing of the PCB is shown in Figure 10 and the 3D Ultiboard drawing is shown in Figure 11.

Figure 10: 2D Ultiboard Drawing of PCB



1. **SolidWorks PCB Model**

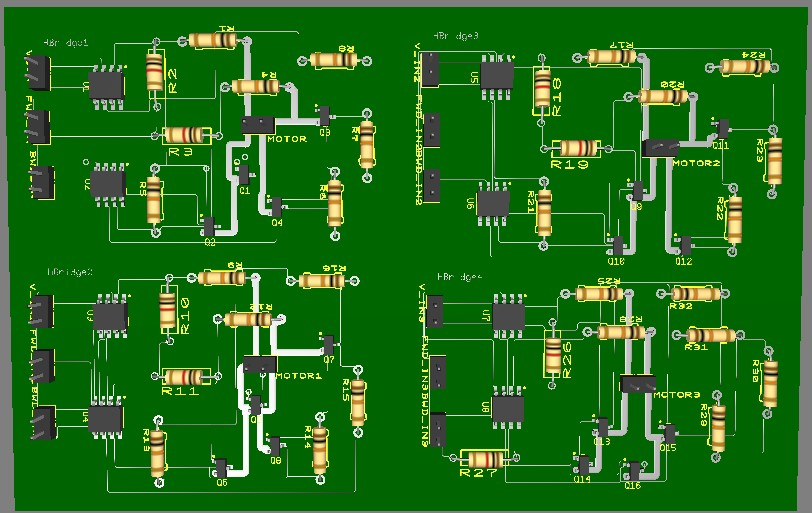


Figure 11: 3D Ultiboard Model of PCB

The PCB model is exported to SolidWorks as a 3D CAD model. The PCB may then be placed on the enclosure of the SCARA robot and connected to the arduino output pins. The dimensions of the board are 120mm x 80mm. The SolidWorks model is shown in Figure 12. The size of the 4 H-bridge PCB is comparable to the 2 H-bridge L298N as shown in Figure 13 in Appendix A. The L298N is a similar H-Bridge PCB that is commonly used for similar applications. This size comparison reinforces the small scale of the custom driver circuit.

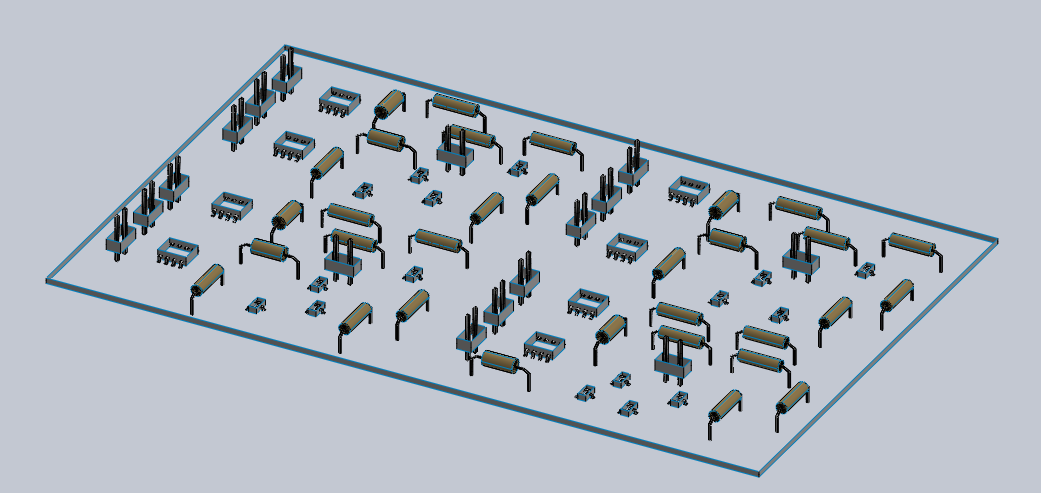
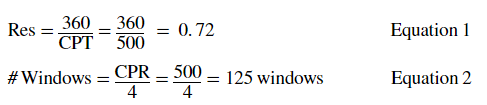


Figure 12: SolidWorks shell model of PCB

1. **Encoder Selection**

Each motor position is measured by an optical encoder. The model chosen is a Maxon HEDS 5540 500 CPT, 3-Channel encoder. The part number is 110511 and has a 3mm shaft opening diameter. This motor was chosen because it is a quadrature encoder with relatively low resolution, giving us a good sampling rate of the position of each motor. Additionally, it is cheaper and easier to find than other alternatives.

The encoder dimensions are 30mm x 18.3mm. The CPT = 500 and is defined as being four times the number of pulses per revolution [9]. The CPT is used to find the resolution and number of windows in the encoder, as shown in Eq. 1 and 2.



The sensor introduces noise into our system and since the measurements are discrete, the value that we are reading is not exact, as indicated by the “floor” block in our Simulink Model in Figure 6. An encoder can then be mounted onto each of the motors to measure their individual positions for feedback into the Arduino. An image of the encoder is shown in Figure 13 and the part can be found on page 471 of the Maxon Motors Catalog.



Figure 13: Maxon Motors Encoder and Pulse Diagram

**References**

[1] Maxon Drive.Tech, <https://drive.tech/en/stream-content/precious-metal-vs-graphite-brushes>

[2] Maxon Motor Catalog,

<https://online.flippingbook.com/view/1042987/89/>

[3] OP AMP Datasheet

[https://www.ti.com/lit/ds/symlink/ths4221.pdf](https://www.ti.com/lit/ds/symlink/ths4221.pdf?ts=1618265823794&ref_url=https%253A%252F%252Fwww.ti.com%252Fproduct%252FTHS4221%253Futm_source%253Dgoogle%2526utm_medium%253Dcpc%2526utm_campaign%253Dasc-null-null-GPN_EN-cpc-pf-google-wwe%2526utm_content%253DTHS4221%2526ds_k%253DTHS4221%2526DCM%253Dyes%2526gclid%253DCj0KCQjw38-DBhDpARIsADJ3kjnHKA-FAz7-_aFnizxdG3OdNK8p6aCJLJnCz_y97E_iSaVWWaVX-UoaAkeGEALw_wcB%2526gclsrc%253Daw.ds)

[4] NPN Transistor Datasheet

<https://assets.nexperia.com/documents/data-sheet/PMBTA13_PMBTA14.pdf>

[5] PNP Transistor Datasheet

<https://assets.nexperia.com/documents/data-sheet/PMBTA64.pdf>

[6] Standard Copper Thickness for PCBs

<https://pcbprime.com/pcb-tips/how-thick-is-1oz-copper/>

[7] DigiKey Trace Width Calculator

<https://www.digikey.ca/en/resources/conversion-calculators/conversion-calculator-pcb-trace-width>

[8] IPC2221A Generic Standard on Printed Board Design

<https://www.ipc.org/TOC/IPC-2221A.pdf>

[9] CPR and PPR Definitions

<https://www.cuidevices.com/blog/what-is-encoder-ppr-cpr-and-lpr>

**Appendix A**

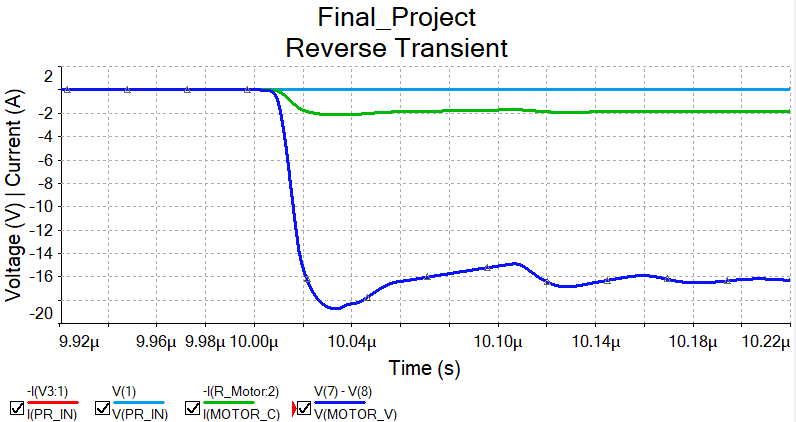


Figure 4B: Driver Circuit Transient in Reverse Direction without Capacitor

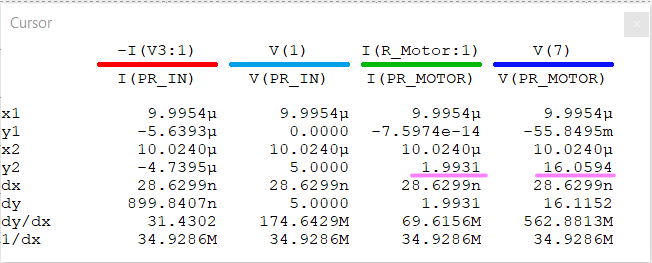


Figure 5: Transient Near Steady-State Values

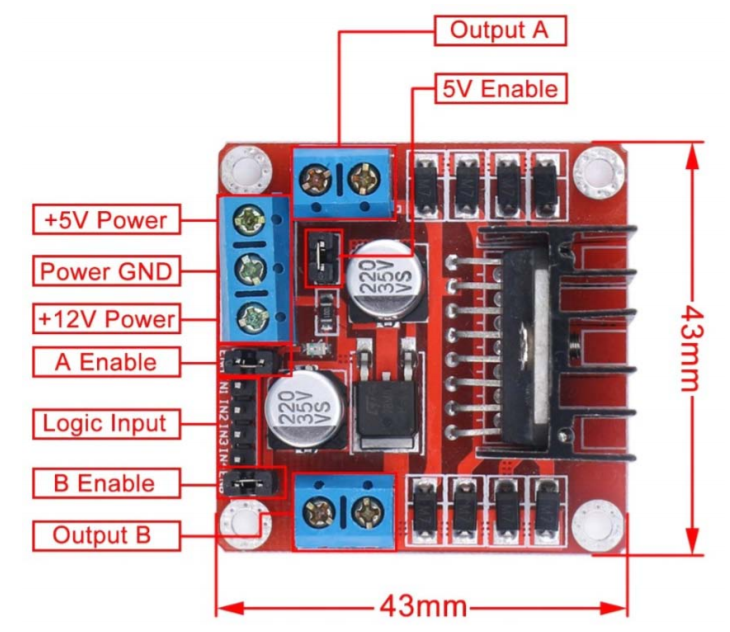


Figure 12: L298N Dual H-Bridge PCB

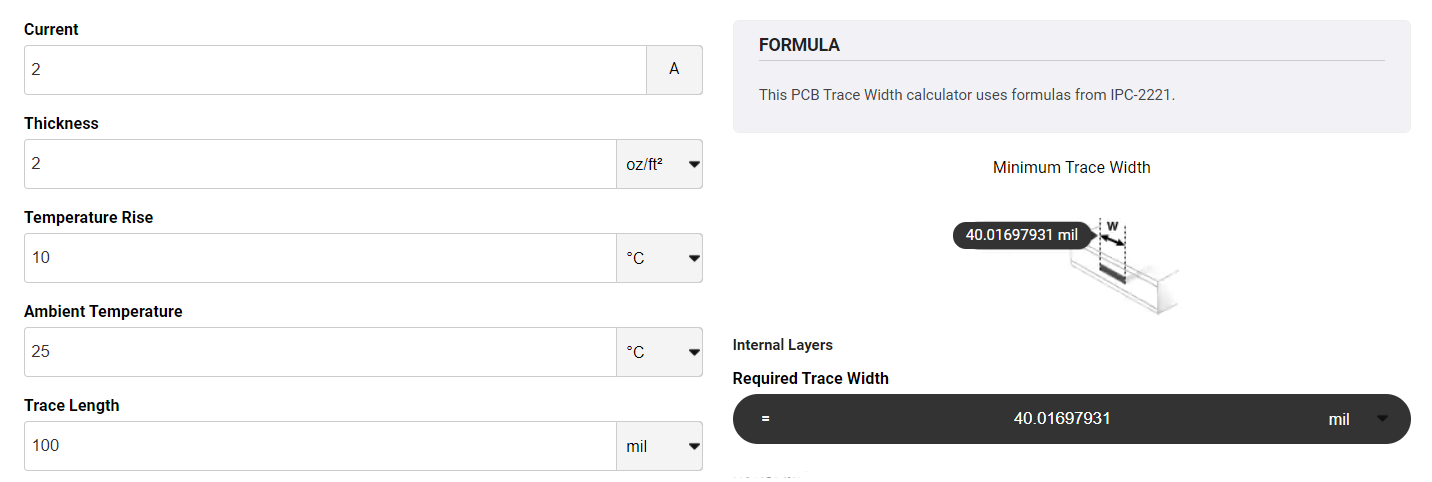


Figure 9: DigiKey Trace Width Calculator

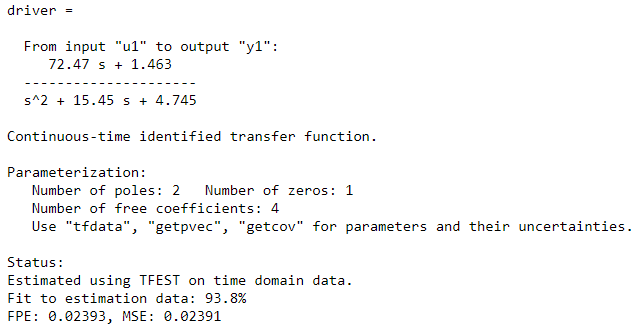


Figure 7: Driver Transfer Function