

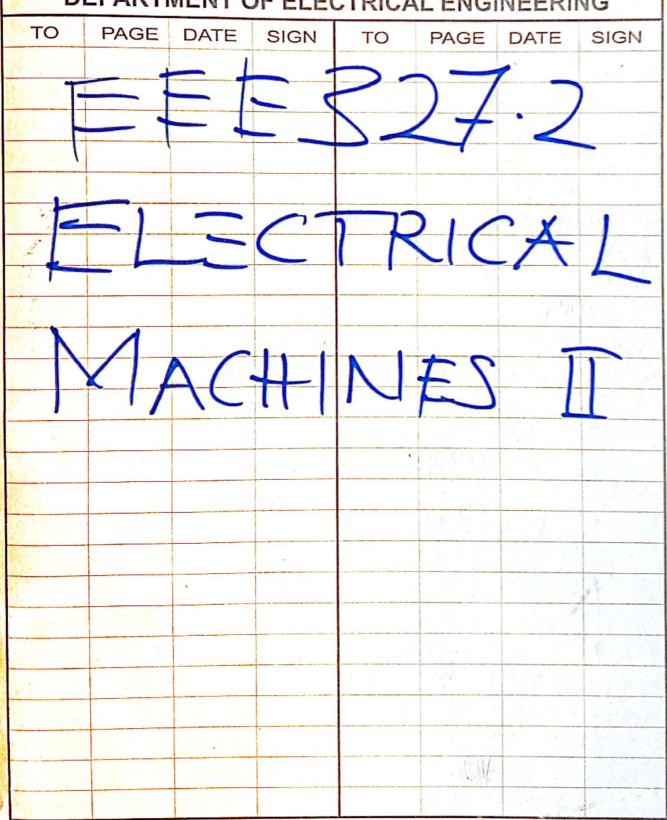




NIGERIA MARITIME UNIVERSITY, OKERENKOKO, DELTA STATE, NIGERIA

FILE TITLE

FACULTY OF ENGINEERING DEPARTMENT OF ELECTRICAL ENGINEERING



is found on the rotating part, referred to as the rotor. The armature winding of a DC machine consists of many cirls connected together to form a closed loop. As the rotor rotates a mechanical contact (split ring commutator) is used to supply current to the armature winding.

Synchronous and DC machines typically have two sets of windings. Apart from the armature windings they have a second set of windings which carry DC current and which produce the main operating flux in the machine. This second winding is typically called field winding. While the field windings of a synchronous machine is found on the rofor that of the DC machine is found on the stator. Since the field windings of the Synchronous machine is found on the rofor current must be supplied winding by means of a rofating mechanical contact (slip rings). Since permanent magnets also produce DC magnetic flux they can be used in place of field windings.

The stator and votor of votating machines is made of magnetic material (mostly electrical steel) and the windings are placed in slots on the stator and votor structures. The magnetic materials used are of very high relative permeabilities and serve the following purposes;

- 1. They maximize the coupling between stator and rotor
- 2. They increase the magnetic energy availably in the coupting field for electromechanical energy conversion.
- 3. They also help the machine designer to shape and distribute the magnetic fields to suit each particular machine

The time varying plux present in the armature structures induces eddy currents in the armature structure. The effect of eddy currents can enginificantly reduce the machine performance. These eddy currents are reduced by building the armature structure from thin laminations of electrical steel which are insulated from each other

In some machines such a variable reluctance machines and stepper motors, there are no windings on the rotor. The operation of such machines depend on the non-uniformity of air-gap relictance associated with variations in the position of the rotor in relation to the time varying currents applied to their stator windings. In such machines since both the stator and rotor are subjected to time varying magnetic flux both may require laminations to reduce eddy current effects.

1.2. Introduction to AC Machines

Traditionally. AC machines fall into one of two categories: Synchronous or induction. It would be seen that a major distinguishing feature between these two categories of AC machines is that in synchronous machines rotor winding currents are supplied directly from the stationary frame through a votating contact whereas in induction machines rotor currents are induced into the rator windings by a combination of the time varying stafor currents and the motion of the notor relative to the stator.

Synchronous Machines

To understand the performance and operation of a synchronous machine, let us consider a very much simplified two-pole salient pole sychronous generator shown in figure 1.1.

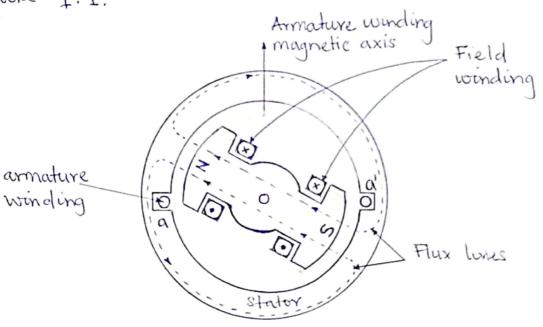


Fig. 1.1. Schematie view of a simplified, two-pole single phase synchronous genenerator.

As seen in figure 1.1 the armature winding of a synchronous machine is mostly found on the stator and the field winding is placed on the rotor. The field winding is excited by DC conducted to it by means of stationary Carbon brushes which contact rotating slip rings. It is practically more advantageous to have the low power, single phase field winding on the rotor white the high power, multi-phase armadure winding is placed on the stator.

Figure 1.1. shows the cross-section of the armature winding consisting of a single cost of N-turns, represented by two cost sides a and a on the inner surface of the stator.

The votor is turned at a constant speed by a source of mechanical power connected to the shaft. Since armature we winding is assumed to be open circuited the flux in this machine is produced by the field winding alone.

The ideal model of this machine assumes a sinusotolal distribution of magnetic flux in the air gap as soon in figure 1.2(a).

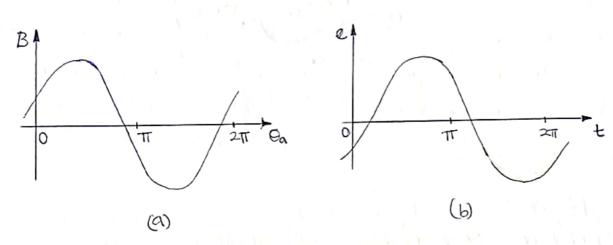


Fig. 1.2. (a) Space distribution of flux density
(b) Waveform of the corresponding generated voltage
for the single phase generator of figure 1.1.

As the refer retates, the flux linkages of the armature winding change with time. Assuming a sinusoidal flux distribution and constant refer speed, the resultant induced voltage, e, will be sinusoidal as shown in figure 1.2(b). Thus it is seen that the voltage included in the coil completes a cycle for each revolution of the two-pole machine of fig. 1.1. Its frequency in Hz (cycles per second) is same as the speed of the votor in revolutions per second. The elec-

trical frequency of the generated voltage is thus synchronized with the mechanical speed of voltation, hence the name "Synchronous" machine. It is therefore seen, for example, that a two-pole synchronous machine must revolve at 3000 revolutions per minute to produce a 50 Hz voltage-

In practice most synchronous machines have more than two poles. When a machine has more than two poles, it is convenient to concentrate on a single pole pair bearing in mind that the electric, magnetic and mechanical conditions of every other pole pair are repetitions of those for the pair under consideration. Fig. 1.3 precents a four pole single phase synchronous generator.

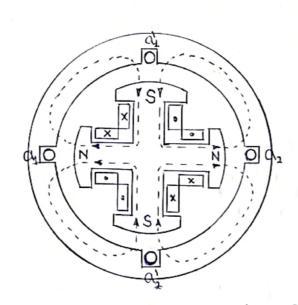


Fig. 1.3. Schematic of a simple, four-pole, single phase synchronous generator

As seen in figure 1.3 the field coils are connected so that the poles are of alternate polarity. In this arrangement there are two complete wavelengths, or cycles per complete revolution of the field as illustrated by figure 1.4. The armature windings now contains two coils as a and as, as, connected in series by their end connections. As seen in figure

1.4 the generated voltage now goes through two complete eycle per verofution of the rotor. The frequency in hertz will-thus be troice the nuchanical speed in revolutions per second.

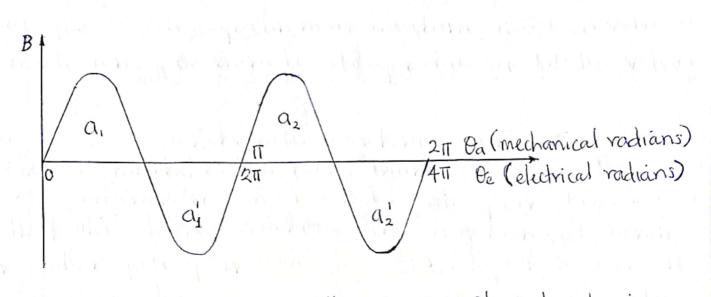


Fig. 1.4. Space distribution of the air-gap flux density in an ideal. four-pole, single phase synchronous generator

It is convenient to express angles in electrical degrees or electrical radians rather than in physical units. The relationship between electrical radians and mechanical radians is gotten by noting that one complete pair of poles volation or one cycle of flux distribution equals 360 electrical degrees or 211 electrical radians. Since there are no. of poles/2 complete wavelengths, or cycles in one complete revolution, it follows that

Flectrical degrees,
$$O_e = \binom{no. of poles}{2} O_a$$
 1.1

Where Da is the spacial angle (in mechanical degrees). This same relationship holds for all angular measurements in a multipole machine. The electrical units equivalent will be equal (no, of poles/2) times the equivalent spacial values. From the waveform of induced voltage in a multipole machine it is seen that the cost voltage passer through a complete cycle every time a pair

of poles sweeps by, or (no. of poles/2) times each revolution. The electrical frequency of the induced voltage in a synchronous machine is therefore

$$f = \left(\frac{n_0 \cdot q \text{ poles}}{2}\right) \frac{n}{60} \text{ Hz}$$
 1.2

Where n is the mechanical speed in revolutions per minute, and n/60 is the speed in revolutions per second. The electrical frequency in radians per second is given as

Where Wm is the mechanical speed in radians per second.

The refor of a synchronous machine can be constructed in two main forms; sattient or projecting poles, having concentrated windings (Figures 1.1 and 1.3) and nonsalient poles or cylind rical refor, having distributed windings as illustrated in

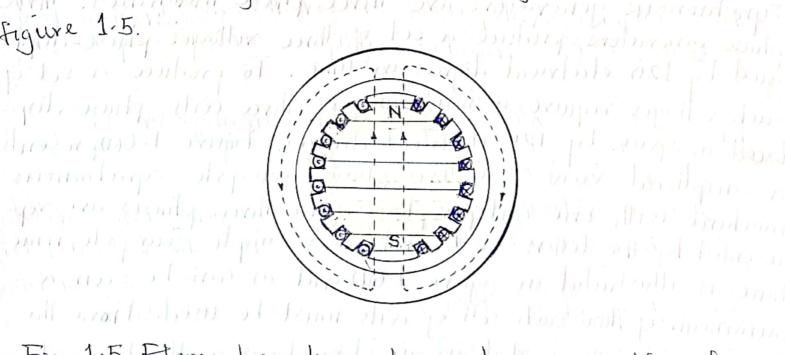


Fig. 1.5. Etementary two-pole synchronous machine, showing Cylindrical rotor having distributed windings.

As seen in figure 1.5 the cost sides are arranged into multiple slots around the rotor surface. This distributed arrangement produces an approximately sinusoidal distribution of flux around the our gap.

Most power systems in the world operate at either 50 or Most prover systems in the world operate at either 50 or Gotts frequency. Power generating systems (such as hydroelectric generators) which employ hydraulic turbines that operate at tric generators) which employ hydraulic turbines that perests would require a relatively large number relatively low speeds would require a relatively large number of pole to achieve the desired frequency. Such generators there fore make use of salient-pole rolors. Steam and gas turbines fore make use of salient-pole rolors. Steam and gas turbines on the other hand operate best at relatively high speeds and such systems commonly make use of two or four-pole cylindrical rotors.

Three Phase Synchronous Machines

The discussion so few has centered on single phase synchronous machines. However, most of the worlds power systems are three phase machines. Three synchronous generators are three phase machines. Three phase generators produce a set of three voltages phase-displaced by 120 electrical degrees in time. To produce a set of such voltages require a minimum of three costs, phase displaced in space by 120 electrical degrees. Figure 1.60 presents a simplified view of a three phase, two-pole synchronous machine with one cost per phase. The three phases are represented by the letters a, b and c. A simple four pole machine is thustvated in figure 1.6(b) and as can be seen a minimum of two such sets of costs must be used. From the foregoing it follows that in an elementary multipole machine the number of sets of costs is given by half the number of potes.

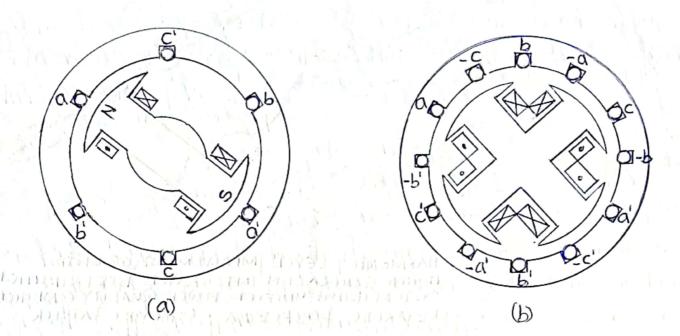


Fig. 1.6. Simplified schematics of three-phase generators (a) two-pole (b) four-pole

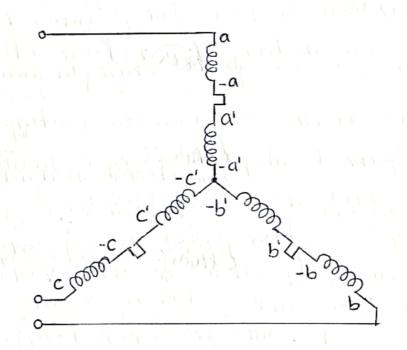


Fig. 1-7. Star (Y) connection of the windings.

As seen in figure 1.7 the two costs in each phase are connected in series so that their voltages add and the three phases are then connected in star (Y). However since the cost voltages in each phase are some a pavallel connection is possible and the three phases can also be connected in Δ (delta.

When a synchronous generator is supplying power to a load current will flow through it armature windings to the load. This amasture current creates a rotating magnetic field in the air gap which rotates at synchronous speed. The interaction between this armature flux and the field flux results in an electromechanical torque due to their tendency to align. This electromechanical torque is the mechanism through which the synchronous generator converts mechanical to electrical energy. In a generator this electromechanical torque opposes rotation of the votor and external mechanical torque must be applied from a prime mover to maintain rotation.

In the operation of a synchronous motor, on the other, hound while alternating current is supplied to the armature winding on the stator, DC excitation is supplied to the field windings located on the rotor. The current flowing in the armature creates a magnetic field which rotates at synchronous speed. The DC current flowing in the field windings also creates a rotating magnetic field. The interaction between the stator and rotor fields creates an electromechanical torque which causes rotation in the rotor.

To produce a steady electromechanical torque the magnetic fields produced in the stator and votor must be of constant amplitude and stationary relative to each other. This steady state speed in a synchronous motor is determined by the number of poles and frequency of the armature current.

Therefore, a synchronous mofor which is operated from a constant frequency AC source will produce a steady electromechanical torque which in turn translates to a constant steady-state speed in the votor.

Induction Machines

The induction machine presents a second type of AC machine. Like in the sychronous machine the effetor winding is excited by AC. However, in contrast to the synchronous machine afternating current also flows in the rotor of an induction machine, but by induction (transformer action). The induction machine may thus be regarded as a generalized transformer in which electric power is transformed between stator and rotor with a change in frequency and a flow of mechanical power

At this point it is worthy of note that induction machines are commonly deployed as induction motors and seldom used as generators. This is because the performance of the induction gen is unsatisfactory for most applications. However, recently it was found well suited for wind power application and it may also be used as a frequency chan-

In construction, the induction motor windings are essentially the same as those of a synchronous machine. However, the rotor windings are electrically short-circulted and frequently have no external connections, since

current is induced by transformer action from the stator winding

As in a synchronous motor, the armature flux in the induction motor leads that of the rotor thus producing an electromagnetic torque. However, unlike the synchronous machine the rotor of the induction machine not rotate synchronously. Induction motors, thus operate at speeds less than synchronous mechanical speeds. Figure 1.8 presents a typical speed-torque characteristic of an induction motor.

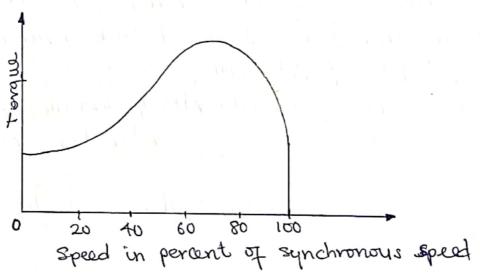


Figure 1.8. Typical induction motor speed-torque characteristics.

the straight and a second second