

# LOCAL AND GLOBAL STRESS ANALYSIS



## Ship Data

Lenght (m):

Breadth (m):

Depth (m):

Draft (m) : 7.462686567164179

Block Coeffic:

Lightweight (ton):

Deadweight (ton):

Displacement (ton) : 12628

Stiffener Distance (mm):

Girder Distance (mm) :

DAF

- ▶ Draft:  $D = \frac{\nabla}{L*B*CB*\rho}$
- ▶ Displacement:  $\nabla = Lw + Dw$
- ▶ DAF = Dynamic Amplification Factor
- ▶ Stiffener distance = s
- ▶ Girder distance = l
- ▶ Normal stress:  $\sigma = 160 \text{ MPa}$

# SHIP DATA

### Local Strength of Bottom Plating

Pressure (N/mm<sup>2</sup>): 0.0975509328358209

#### Stiffener

Section Modulus (cm<sup>3</sup>): 156.8436092000933

Inertia (cm<sup>4</sup>): 1783

Profile (mm) : 160x9

#### Girder

Section Modulus (cm<sup>3</sup>): 15492.307520988807

#### Plate

Plate Thickness (mm): 8.642189129637547

Equivalent Plate Thickness (mm): 10.699331986780404

Inertia (mm<sup>4</sup>): 3547541842416.8228

Section Modulus (cm<sup>3</sup>): 506791.69177383184

▶ Pressure:  $P = \rho * g * D * \frac{DAF}{1000}$

#### ▶ Stiffener

▶ Section Modulus:  $Z = \frac{P * s * l^2}{12 * \sigma} * \frac{1}{1000}$

▶ Inertia and Profile from Table 1

#### ▶ Girder

▶ Section Modulus :  $Z_g = \frac{P * l * B^2}{10 * \sigma} * \frac{1}{1000}$

#### ▶ Plate

▶ Thickness:  $t = \frac{s}{2} \sqrt{\frac{P}{\sigma}}$

▶ Equivalent Thickness:  $t_{eq} = t + \frac{A_{profile}}{s}$

▶ Neutral Axis:  $NA = \frac{L}{ST} * 2 * 1000$

▶ Inertia:  $I = \frac{l}{2} * t_{eq} * NA^2 * 2 + \frac{1}{12} \frac{L}{ST} * t_{eq}^3$

▶ Section Modulus:  $Z_{plat} = \frac{I}{NA} * \frac{1}{1000}$

# LOCAL STRENGTH

## Global Strength

Ship Divisions (tanks): 8

Number of tanks with load: 4

Buoyancy (ton/m): 112.75

Lightweight Distributed (ton/m): 53.57142857142857

Deadweight Distributed (ton/m): 118.35714285714286

The deadweight is distributed in the outer tanks in bow and stern.

► Ship divisions: Ship equally divided in number of tanks (ST).

► Tanks with load: Paired number of tanks in each end of the ship (LT)

►  $Bouyancy = \frac{\nabla}{L}$

►  $LW \text{ distributed} = \frac{LW}{L}$

►  $DW \text{ distributed} = \frac{DW}{L * \frac{LT}{ST}}$

# GLOBAL STRENGTH DATA

### Resulting Load

Load Full Tanks (ton/m): -59.17857142857143

Load Empty Tanks (ton/m): 59.17857142857143

Established conditions: Always hogging.

Maximum Force (N\*m): 1657

Maximum Moment (MN\*m): 463.96

### DNV Rules

Wave Coefficient ( $C_w$ ) : 8.172273870249207

Stillwater Bending Moment (kN\*m): 253606.91918153374

Wave Bending Moment (kN\*m): 287097.917401594

Worst case scenario, seagoing condition.

# GLOBAL STRENGTH DATA

## ► Resulting load

►  $L_{full} = Buoyancy - LW_d - DW_d$

►  $L_{empty} = Buoyancy - LW_d$

► Always hogging condition, loaded tanks on the sides of the ship

►  $F_{max}$  and  $M_{max}$  from applying resulting loads to the ship

## ► DNV rules

►  $C_w$ : Table in pag 53.

►  $M_{so} = C_w * L^2 * B * (0.1225 - 0.015 * C_b)$  Pag 69.

►  $M_{wo} = 0.19 * C_w * L^2 * B * C_b$  Pag 70

### Strenght Evaluation

Stillwater Bending Moment (kN\*m): 463960

Total Bending Moment (kN\*m): 751057.917401594

Midship Section Modulus (cm<sup>3</sup>): 429175.9528009108

**Conclusion: Plate holds**

### ► *Strength evaluation*

► *Comparison between DNV rules and values obtained in Resulting load*

► *Maximum value is used*

►  $M_{tot} = M_{so} + M_{wo}$

►  $Z_{midship} = \frac{M_{tot}}{175}$

### ► *Conclusion*

► *Check:  $Z_{plat} > Z_{midship}$*

# GLOBAL STRENGTH DATA