



A phase-field model of dynamic fracture

CES Seminar Work WS17/18, Karsten Paul
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Agenda

- Introduction to fracture
 - Brittle and ductile fracture
- Phase-field formulation
 - Griffith's theory of brittle fracture
 - Phase-field theory
 - Energy approximation
 - Strong form
- Numerical formulation
 - Weak form
 - Spatial and temporal discretization
- Numerical result
- Summary

Cracks: Brittle and ductile fracture

- Engineering designs: reliable prediction of fracture and material failure
 - Experiments: high expense and enormous costs
 - FEM: approximate crack nucleation and propagation

Cracks: Brittle and ductile fracture

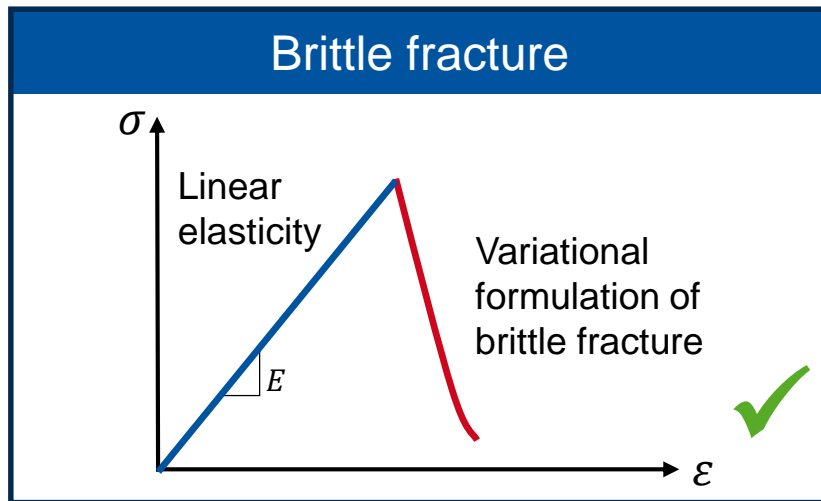
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How to model cracks?

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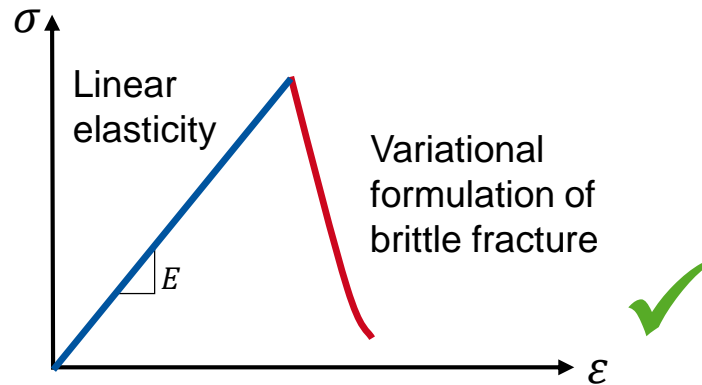


Cracks: Brittle and ductile fracture

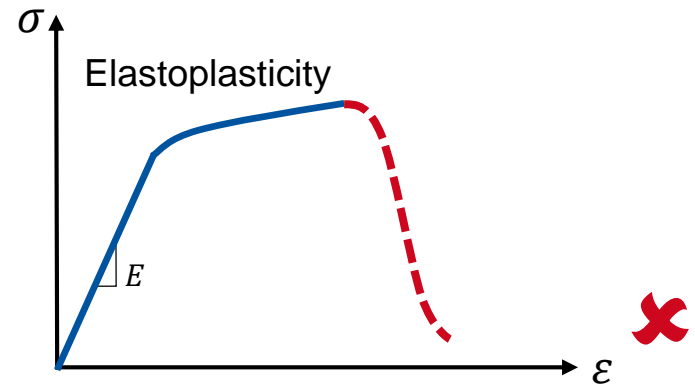
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Brittle fracture



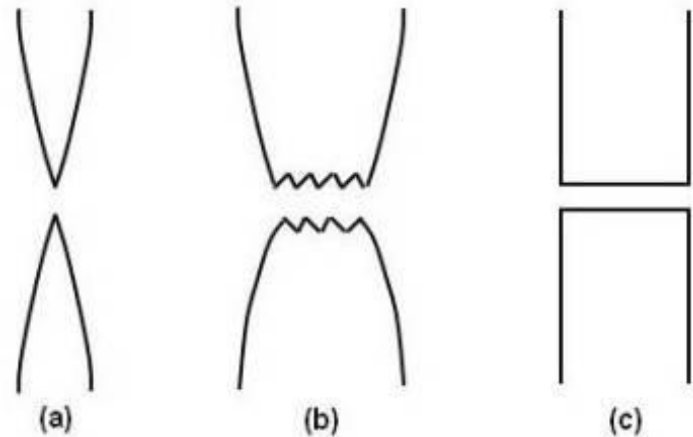
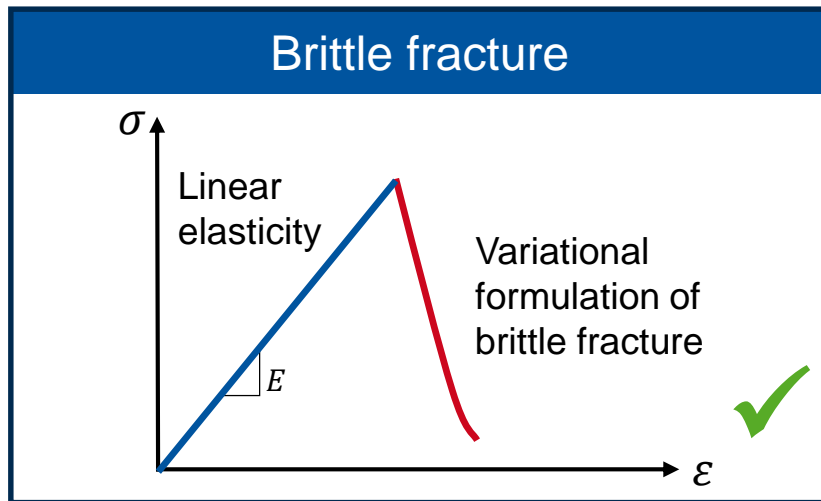
Ductile fracture



Cracks: Brittle and ductile fracture

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How to model cracks?



Macroscopic View of Fractures

K P Shah, The Handbook on Mechanical Maintenance

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How to describe the splitting of the material?

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How to describe the splitting of the material?

Sharp interface models

- Insert **discontinuities** into the body
 - Enrich displacement field
Cohesive segments method
$$\mathbf{u}(x, t) \approx \sum_A (N_A(x) \mathbf{u}_A(t) + \dots)$$
 - Mesh handling
Virtual crack closure technique
- Great drawback: 3D

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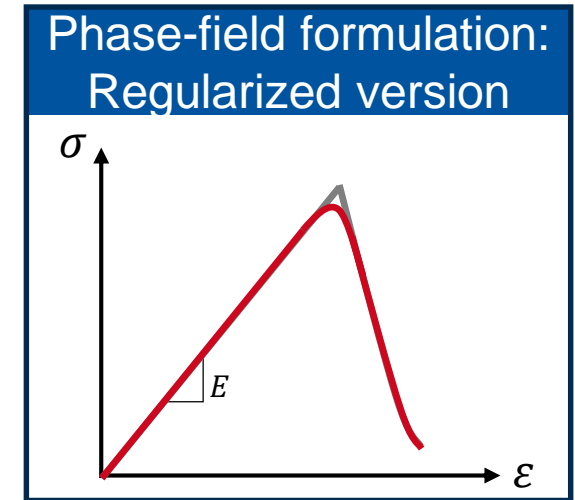
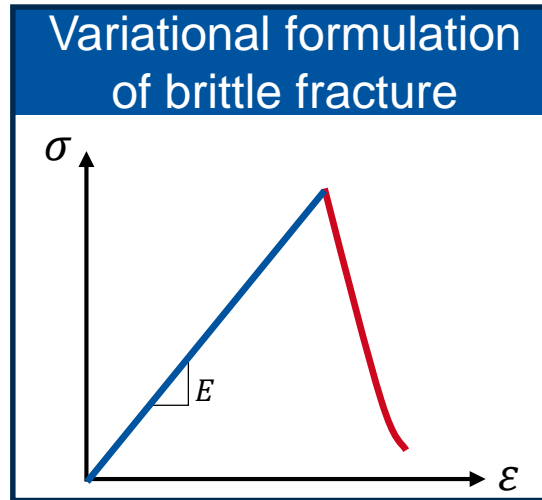
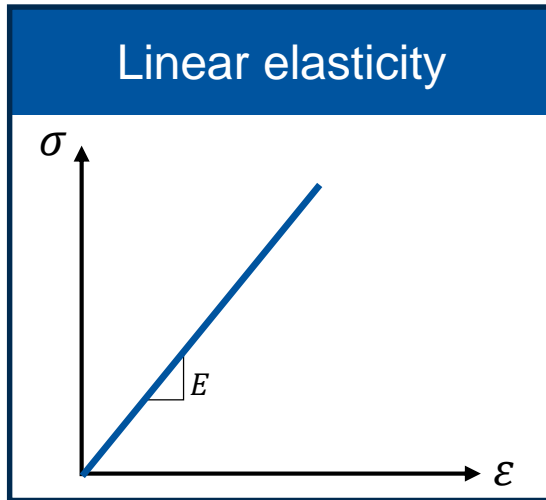
- Insert **discontinuities** into the body
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Diffuse interface models

- Phase-field methods
 - Model interfaces between different phases
 - Smooth transition
 - No discontinuities

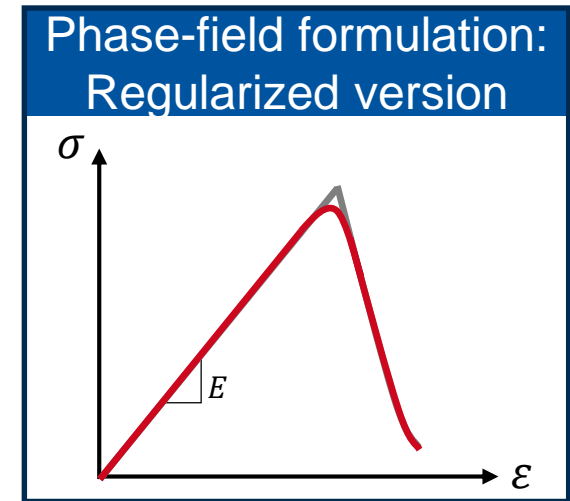
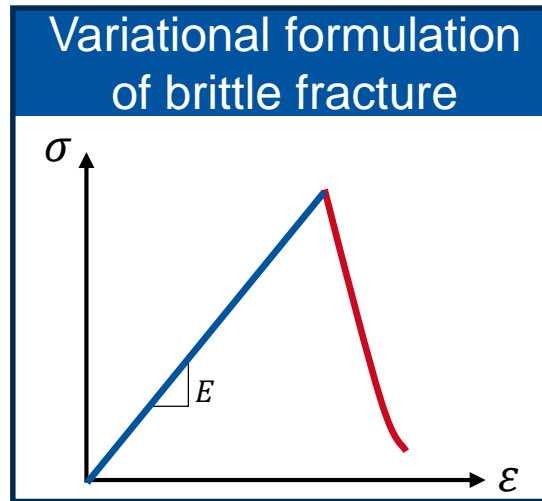
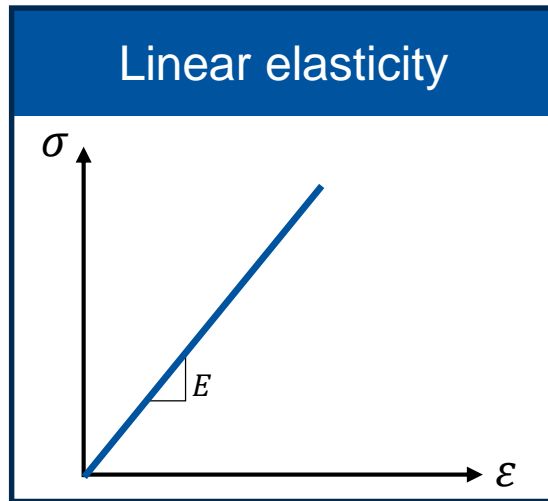
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Phase-field formulation



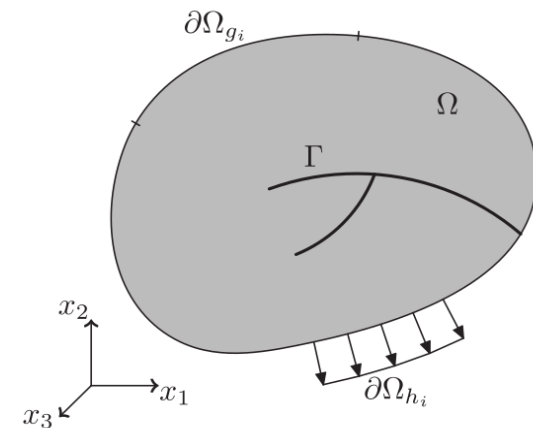
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Phase-field formulation



Notation and assumptions

- Small deformation and deformation gradients
- Isotropic linear elasticity
- Body Ω with boundary $\partial\Omega$
- *Fracture surface* Γ
- Dirichlet BC $\mathbf{u} = \mathbf{g}$ on $\partial\Omega_{g_i}$
- Neumann BC $\mathbf{t} = \mathbf{h}$ on $\partial\Omega_{h_i}$



Griffith's theory and phase-field theory

- Elastic energy density: $\Psi_e(\boldsymbol{\varepsilon}) = \frac{1}{2} \lambda \operatorname{tr}(\boldsymbol{\varepsilon})^2 + \mu \boldsymbol{\varepsilon} : \boldsymbol{\varepsilon}$
- Critical fracture energy density: G_c *Energy necessary to create a unit area of fracture surface*

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Recall: Hamilton's principle

Motion of mechanical system: $J(q, \dot{q}) = \int_{t_0}^{t_1} L(q, \dot{q}, t) dt \xrightarrow{!} \text{stationary point}$

Lagrangian (here): $L(\mathbf{u}, \dot{\mathbf{u}}, t) = \int_{\Omega} \left(\frac{1}{2} \rho \dot{\mathbf{u}} \dot{\mathbf{u}} - \Psi_e(\boldsymbol{\varepsilon}) \right) d\Omega - \int_{\Gamma} G_c d\Gamma$

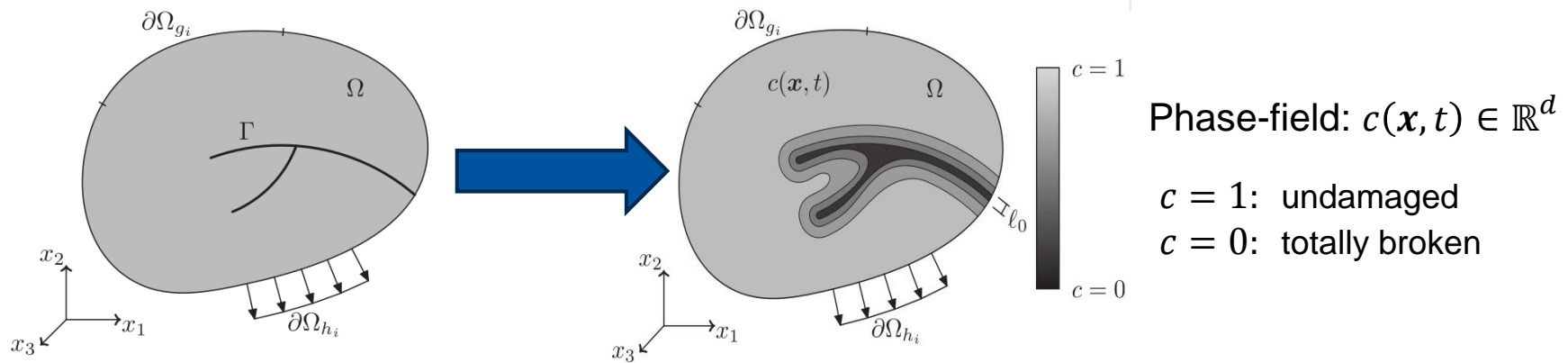
➡ Euler-Lagrange equation to find minimizer

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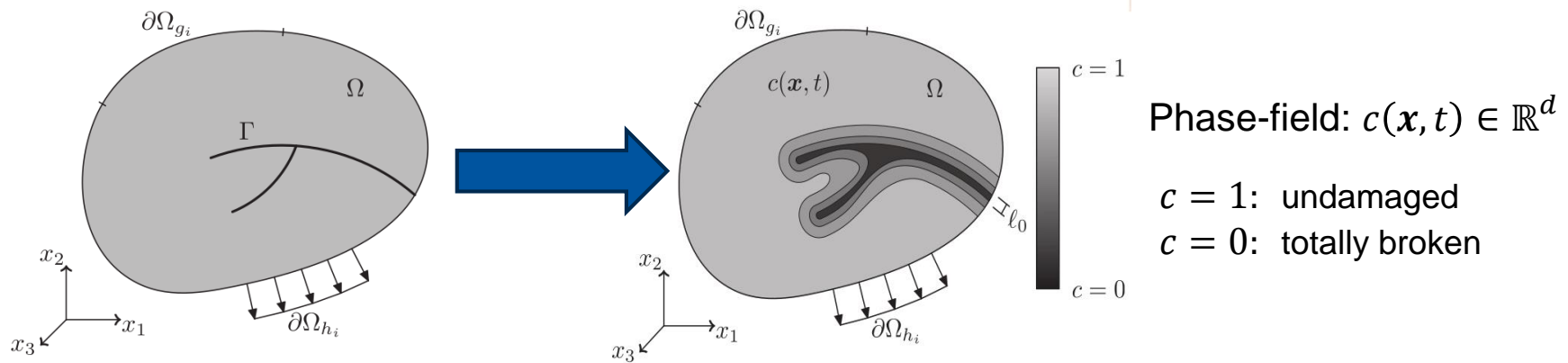
Griffith's theory and phase-field theory

Approximation of the fracture surface



Griffith's theory and phase-field theory

Approximation of the fracture surface



- Phase-field:

- Approximation:

$$\int_{\Gamma} G_c d\Gamma \approx \int_{\Omega} G_c \Gamma_{c,n} d\Omega$$

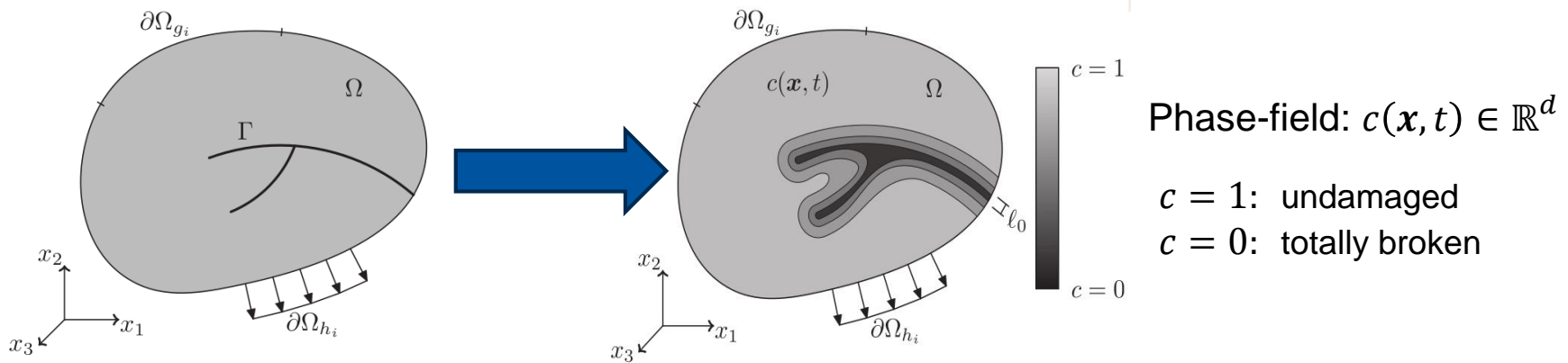
- Crack density functional:

$$\Gamma_{c,2} = \frac{1}{4l_0} [(c-1)^2 + 4l_0^2 |\nabla c|^2]$$

$$\Gamma_{c,4} = \frac{1}{4l_0} [(c-1)^2 + 2l_0^2 |\nabla c|^2 + l_0^4 (\Delta c)^2]$$

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Energy approximation and strong form

Coupling phase-field and kinematics

$$\Psi_e(\boldsymbol{\varepsilon}, c) = \underbrace{g(c)\Psi_e^+(\boldsymbol{\varepsilon})}_{\text{Tensile}} + \underbrace{\Psi_e^-(\boldsymbol{\varepsilon})}_{\text{Compressive}}$$

$$g(c) = m(c^3 - c^2) + 3c^2 - 2c^3 \quad \triangleq \text{Crack growth driven by development of elastic strains}$$

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Strong form: Governing equations (abbreviated)

- Local form of the linear momentum balance: $\nabla \cdot \boldsymbol{\sigma} + \mathbf{b} = \rho \ddot{\mathbf{u}}$
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Strong form: Governing equations (abbreviated)

- Local form of the linear momentum balance: $\nabla \cdot \boldsymbol{\sigma} + \mathbf{b} = \rho \ddot{\mathbf{u}}$
- Phase-field evolution, 2nd order theory: $\frac{2l_0 H}{G_c} g'(c) + c - 4l_0^2 \Delta c = 1$
- Phase-field evolution, 4th order theory: $\frac{2l_0 H}{G_c} g'(c) + c - 2l_0^2 \Delta c + l_0^4 \Delta(\Delta c) = 1$
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Weak form (abbreviated)

Weak form: Multiply with variation and integrate by parts

Find $\mathbf{u}(t)$ and $c(t)$ s.t. \forall variations \mathbf{w} and q :

$$(\rho \ddot{\mathbf{u}}, \mathbf{w})_{\Omega} + (\boldsymbol{\sigma}, \nabla \mathbf{w})_{\Omega} = (\mathbf{h}, \mathbf{w})_{\partial\Omega_h} + (b, \mathbf{w})_{\partial\Omega_g}$$

$$\left(\frac{2l_0 H}{G_c} g'(c) + c, q \right)_{\Omega} + (4l_0^2 \nabla c, q)_{\Omega} = (1, q)_{\Omega} \quad , \text{ for } n = 2$$

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+ BC + IC, $(\cdot, \cdot)_{\Omega} : L^2$ inner product

- FE approximation: $\mathbf{u}(\mathbf{x}, t) \approx \mathbf{u}^h(\mathbf{x}, t) = \sum_{A=1}^n N_A(\mathbf{x}) \mathbf{u}_A(t)$
 - Semidiscrete Galerkin form analogue

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Spatial and temporal discretization

Recall

- Crack density functional: $\Gamma_{c,4} = \frac{1}{4l_0} [(c - 1)^2 + 2l_0^2 |\nabla c|^2 + l_0^4 (\Delta c)^2]$
- Term in the weak form: $(l_0^4 \Delta c, q)_\Omega$
➡ 2^{nd} -order continuous derivatives of c required

Spatial and temporal discretization

Isogeometric Analysis (IGA)

- Splines (e.g. NURBS) used for geometric domain and analysis
- Exact representation of geometries
- Smooth basis (FEA: continuous but not smooth basis)
- More accurate stress representation

Spatial and temporal discretization

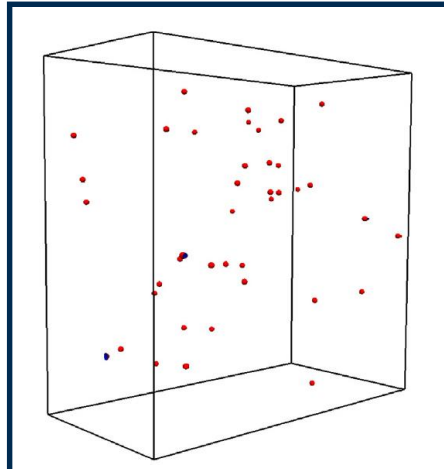
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Generalized- α scheme

- Implicit
- Newton-iteration required
- 2^{nd} -order accuracy for optimal parameters

Three-dimensional crack propagation over time

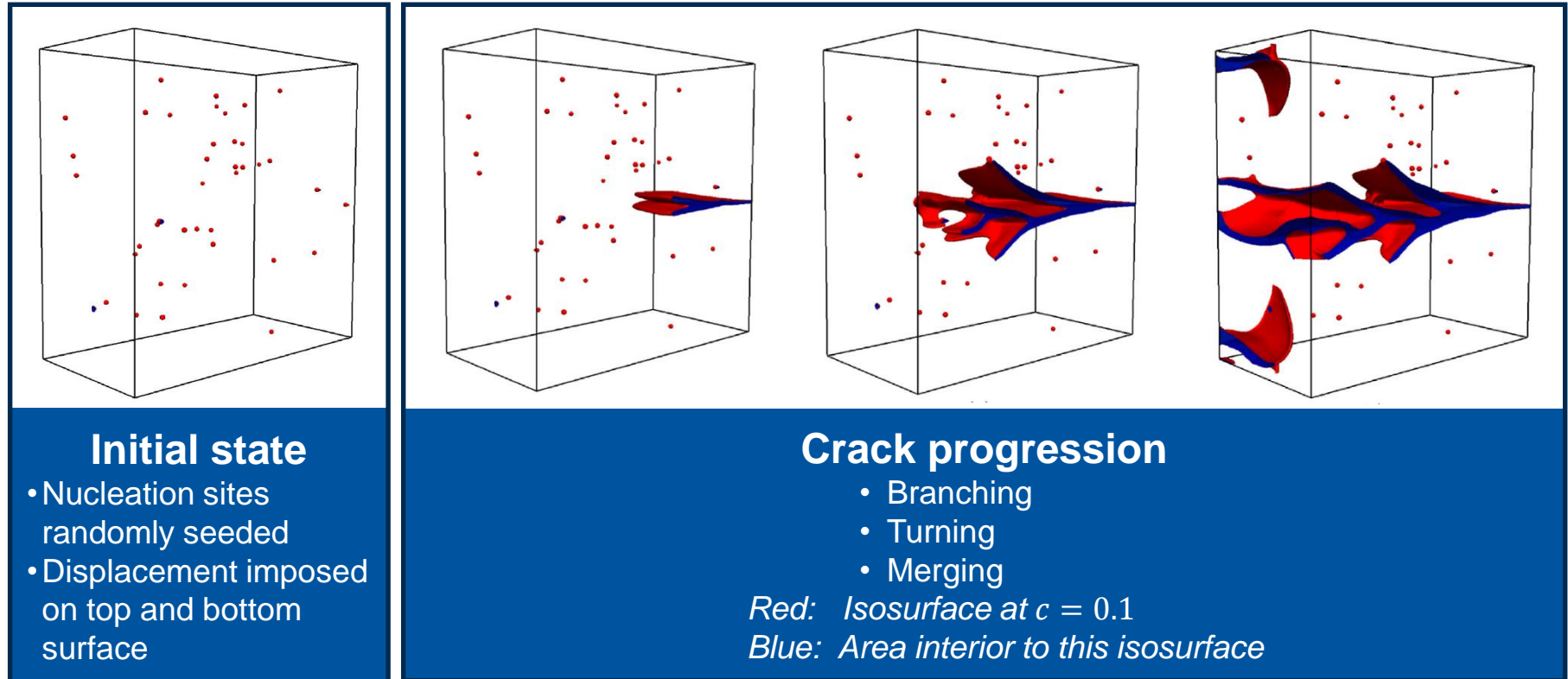


Initial state

- Nucleation sites randomly seeded
- Displacement imposed on top and bottom surface

Borden, M.J., Hughes, T.J.R., Landis, C.M., Verhoosel, C.V: A higher-order phase-field model for brittle fracture: Formulation and analysis within the isogeometric analysis framework, Computer Methods in Applied Mechanics and Engineering 273 (2014), pages 100-118

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Phase-field method: Models and benefits

- General differences:

Quasi-static	Dynamic
2^{nd} -order-	4^{th} -order phase-field theory
Brittle fracture	Ductile fracture
Small deformations	Large deformations
Elasticity	Elastoplasticity

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 - Additional PDE coupled to stress equilibrium

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- Phase-field:
 - Smooth transition
 - Additional PDE coupled to stress equilibrium
- Benefits:
 - 2D to 3D
 - Crack not a function of the geometry
 - No numerical tracking of crack

**Thank you
for your attention**