

1. In the magnetic circuit of Fig. 1, the coil F₂ is supplying 500 AT in the direction indicated. Find the AT that the coil F₁ must provide to produce a flux of 4 mWb in the airgap. The relative permeability of the core is 4500.

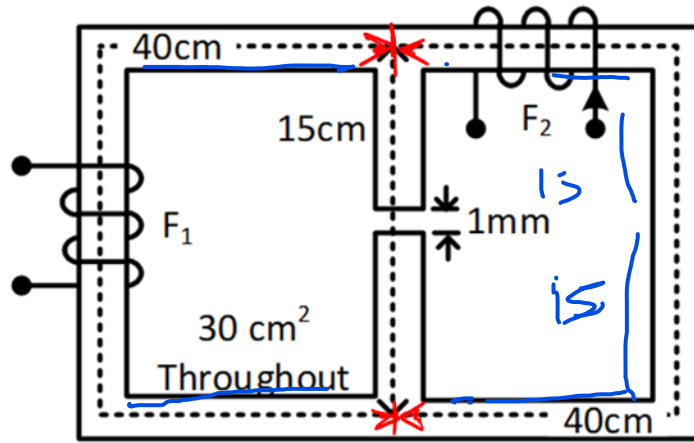


Figure 1

Q1

$$\text{Reluctance of } 40 \text{ cm long core} = \frac{l}{\mu_0 \mu_r A} = \frac{40 \times 10^{-2}}{4\pi \times 10^{-7} \times 4500 \times 30 \times 10^{-4}}$$

$$\therefore R_1 = R_2 = 23.58 \times 10^3$$

$$\text{Reluctance of airgap} = \frac{l \times 10^{-3}}{4\pi \times 10^{-7} \times 30 \times 10^{-4}} = 265 \times 10^3 = R_4$$

$$\text{Reluctance of central limb} = \frac{(15 - 0.1) \times 10^{-2}}{4\pi \times 10^{-7} \times 4500 \times 30 \times 10^{-4}} = 8.78 \times 10^3 = R_3$$

Now, flux in the airgap is 4 mWb

$$\begin{aligned} \therefore \text{MMF drop in central limb} &= \phi (R_3 + R_4) \\ &= 4 \times 10^{-3} (8.78 + 265) \times 10^3 \\ &= 1095.12 \text{ AT} \end{aligned}$$

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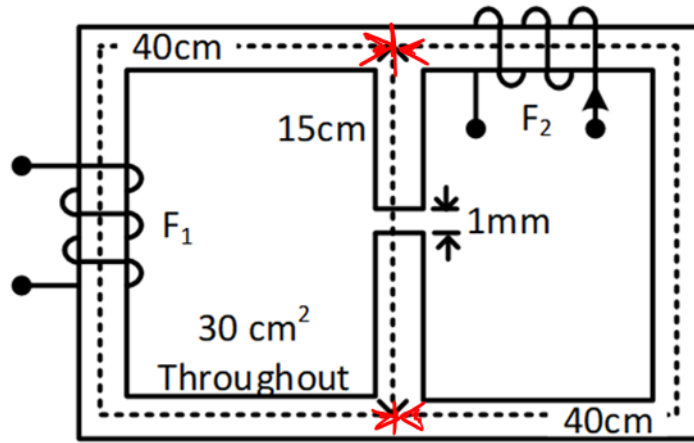
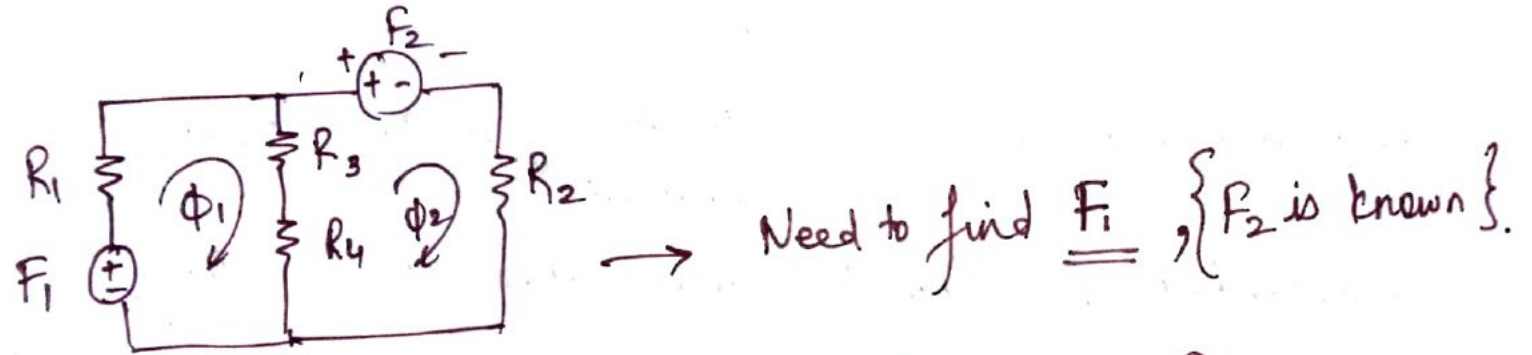


Figure 1



$$F_1 - \Phi_1 R_1 - (\Phi_1 - \Phi_2)(R_3 + R_4) = 0 \quad \dots \textcircled{1}$$

and

$$0 - (\Phi_2 - \Phi_1)(R_3 + R_4) - F_2 - \Phi_2 R_2 = 0 \quad \dots \textcircled{2}$$

$$\Phi_1(R_1 + R_3 + R_4) - \Phi_2(R_3 + R_4) = F_1$$

$$-\Phi_1(R_3 + R_4) + \Phi_2(R_2 + R_3 + R_4) = -F_2$$

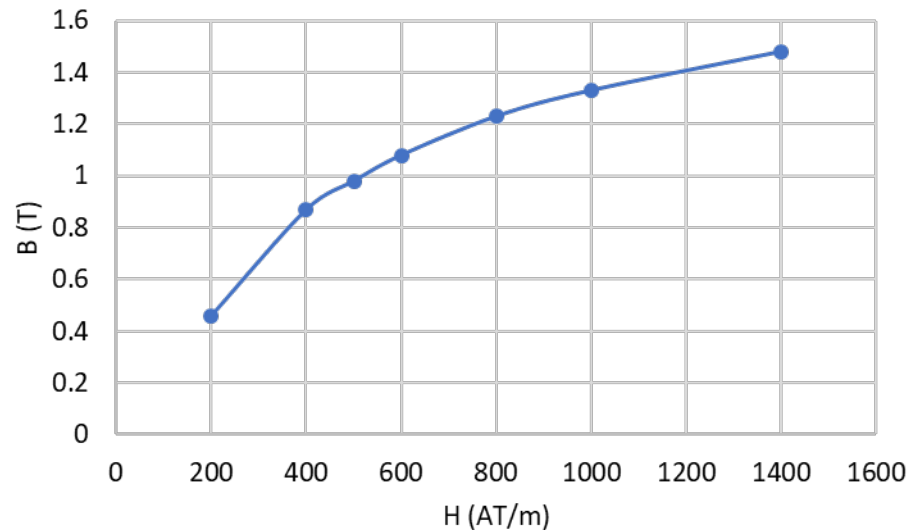
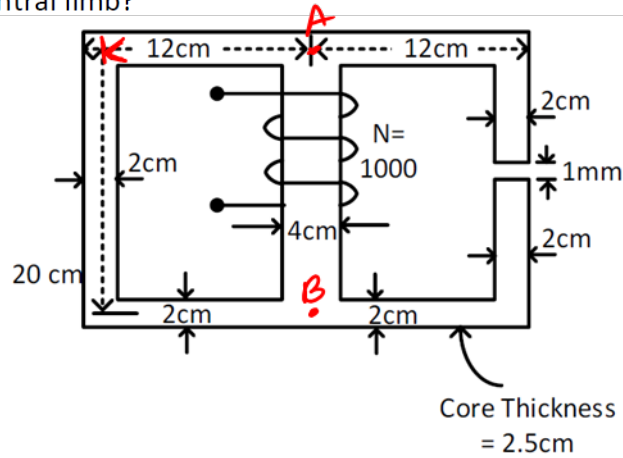
solve to get Φ_1 , Φ_2 , and F_1 .

$$\Phi_1 = 28.98 \text{ mWb}, \Phi_2 = 25 \text{ mWb}, F_1 = 1778 \text{ AT}$$

2. For the magnetic circuit shown in Fig. 2, the points of magnetization curve are as follows:

| | | | | | | | |
|----------|------|------|------|------|------|------|------|
| H (AT/m) | 200 | 400 | 500 | 600 | 800 | 1000 | 1400 |
| B (T) | 0.46 | 0.87 | 0.98 | 1.08 | 1.23 | 1.33 | 1.48 |

Calculate the exciting current required to create a flux of 0.25 mWb in the airgap. What is the flux in the central limb?



$$\text{Reluctance of airgap} = \frac{l \times 10^{-3}}{\mu_0 \mu_r \times 2 \times 2.5 \times 10^{-4}} = 15.9 \times 10^5$$

flux through this airgap is ~~0.25~~ 0.25 mWb.

$$\Rightarrow \text{AT required} = 0.25 \times 10^{-3} \times 15.9 \times 10^5 \approx 398 \text{ AT} = F_g$$

$$\text{length of right limb } l_{AB} = 12 + 12 + 20 - 0.1 \text{ cm} = 43.9 \text{ cm}$$

$$\text{flux density in right limb} = \frac{0.25 \times 10^{-3}}{2 \times 2.5 \times 10^{-4}} = 0.5 \text{ Wb/m}^2$$

$$\text{Corresponding } H \text{ (from B-H curve data)} \approx 220 \text{ AT/m}$$

$$\therefore \text{'AT' required } F_{AB} = 220 \times \text{length of limb} = 220 \times 0.439 = 96.58$$

$$\approx 97 \text{ AT}$$

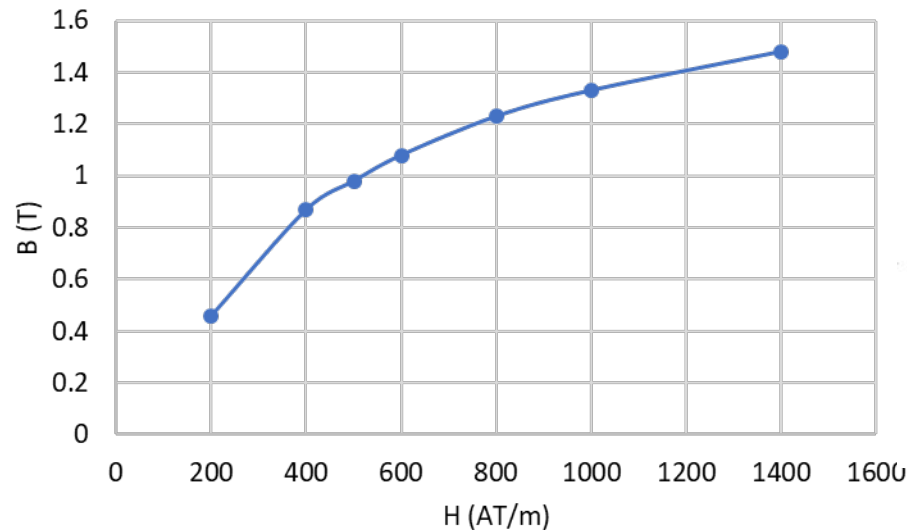
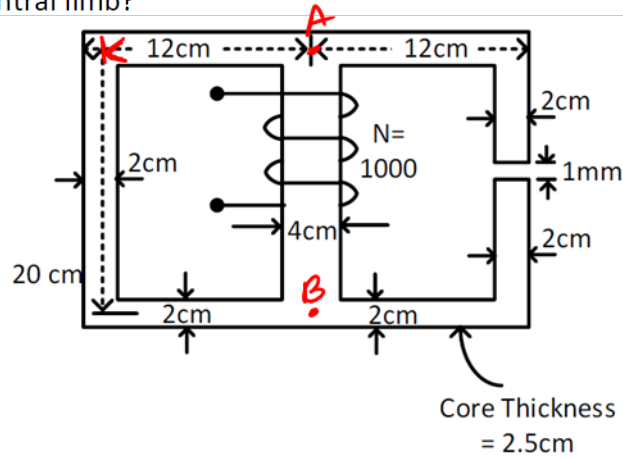
$$\therefore \text{Total 'AT' required for right limb}$$

$$= 97 + 398 = 495 \text{ AT}$$

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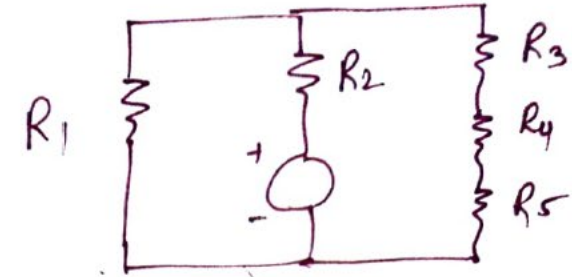
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Calculate the exciting current required to create a flux of 0.25 mWb in the airgap. What is the flux in the central limb?



' R_1 ' is in parallel with $(R_3 + R_4 + R_5)$

\Rightarrow 'AT' required to create a flux of 0.25 mWb in the airgap (also in the right limb) = 'AT' across R_1



\therefore Length of left limb = $12 + 12 + 20 = 44$ cm

\therefore H in left limb ~~is~~ $= \frac{495}{0.44} = 1125$ AT/m

$\rightarrow B \cong 1.38$ Wb/m² (from BH curve)

$\therefore \phi$ (flux) in Left limb = $1.38 \times 2 \times 2.5 \times 10^{-4} = 0.69$ mWb

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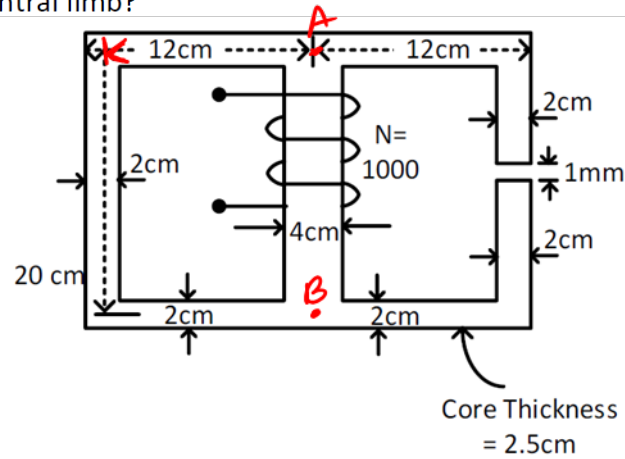
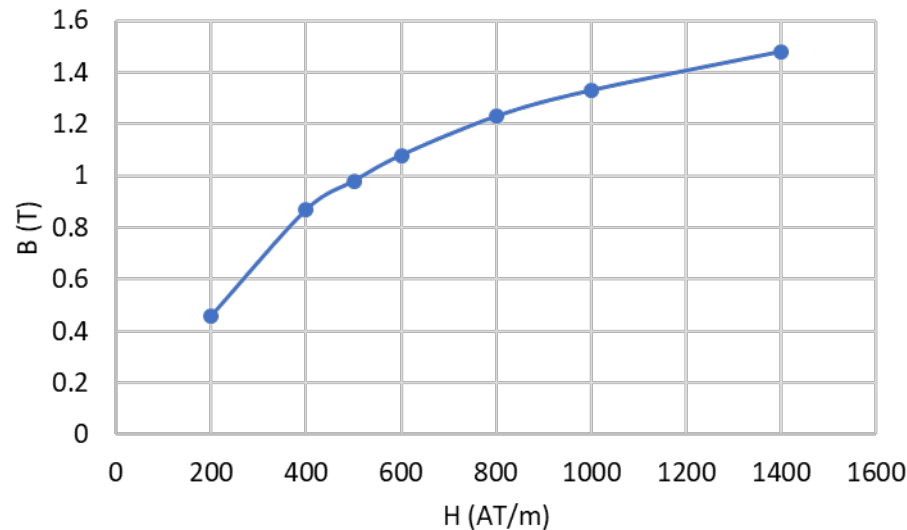


Figure 2



$$\therefore \phi \text{ (flux) in Left limb} = 1.38 \times 2 \times 2.5 \times 10^{-4} = 0.69 \text{ mWb}$$

$$\therefore \phi \text{ in central limb} = 0.69 + 0.25 = \cancel{0.00094} = 0.94 \text{ mWb.}$$

$$\therefore 'B' \text{ in central limb} = \frac{0.94 \times 10^{-3}}{4 \times 2.5 \times 10^{-4}} = 0.94 \text{ T}$$

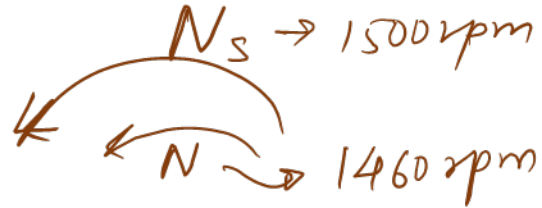
$$\therefore 'H' \text{ (from BH curve)} \rightarrow 450 \text{ AT/m}$$

$$\therefore \text{AT required} = 450 \text{ AT/m} \times \text{length of central limb} \\ = 450 \times 0.2 = 90 \text{ AT}$$

$$\therefore \text{Total AT} = 90 + 494 = 584 \text{ AT}$$

$$\therefore \text{Exciting coil current} = \frac{584}{1000} = 0.584 \text{ A}$$

3. A 4-Pole, 50 Hz, 3 phase induction motor delivers full load torque at 1460 rpm. The speed of the stator field relative to the rotor is 40 rpm and of the rotor field relative to the rotor is 40 rpm.



4. A 3 phase, 400 V, 1460 rpm, 50 Hz, 100 HP, 4-pole induction motor is to be operated from 3 phase, 40 Hz supply. In order to maintain the airgap flux constant, the value of the supply voltage should be 320. This control technique is known as V/f control.

reduced to $\frac{40}{50} \times 400$



5. If the electromotive force in the stator of an 8 pole induction motor has a frequency of 50 Hz, and that in the rotor 1.5 Hz, at what speed is the motor running and what is the slip?

$$N_s = \frac{120f}{P} = 750 \text{ rpm}, \quad * \text{ slip frequency, } f_s = S \cdot f$$

$$\Rightarrow S = \frac{1.5}{50} = 0.03 \quad \downarrow 3\%$$

$$S = \frac{N_s - N}{N_s}$$

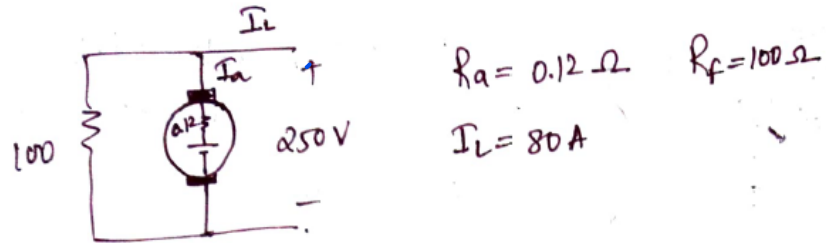
$$\Rightarrow N = N_s (1 - S)$$

$$= 750 (0.97)$$

$$= 727.5 \text{ rpm}$$

6. A shunt machine, connected to 250 V mains, has an armature resistance (including brushes) of 0.12 ohm, and the resistance of the field circuit is 100 ohm. Find the ratio of the speed as a generator to the speed as a motor, the line current in each case being 80 A. (1.08)

Q6.



Motor: $I_f = \text{field current} = \frac{250}{100} = 2.5 \text{ A}$
 $(I_L = I_a + I_f) \therefore I_a = 80 - 2.5 \text{ A} = 77.5 \text{ A}$
 $\therefore E_b = 250 - I_a \cdot R_a = 250 - 77.5 \times 0.12$
 $= 240.7 \text{ V}$

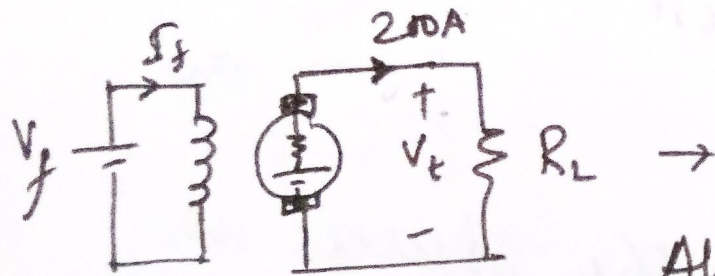
Generator: field current = 2.5 A
 $(I_a = I_L + I_f) \therefore I_a = I_L + I_f = 82.5 \text{ A}$
 $\therefore E_g = 250 + I_a R_a = 250 + 82.5 \times 0.12$
 $= 259.9$

Now, since field current is same for both cases,

$$\frac{N_{\text{generator}}}{N_{\text{motor}}} = \frac{E_g}{E_b} = \frac{259.9}{240.7} \approx 1.079$$

7. A separately excited generator, when running at 1200 rpm, supplies 200 A at 125 V to a circuit of constant resistance. What will be the current when the speed is dropped to 1000 rpm if the field current is unaltered? Armature resistance: 0.04 ohm, total drop at brushes: 2 V, ignore the effect of armature reaction.

(166)



At 1200 rpm. $V_t = 125\text{V}$, $I_a = 200\text{A}$
 $\therefore R_L = \frac{125}{200} = 0.625\ \Omega$

Also, $E = V_t + \text{Brush drop} + I_a R_a$
 $= 125 + 2 + 200 \times 0.04 = 135\text{V}$.

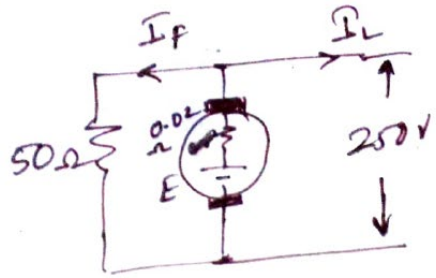
Now, field is unchanged & speed is dropped to 1000 rpm.
 using $E = k\phi\omega$, we get, $\frac{E_2}{E_1} = \frac{N_2}{N_1}$ $N: \text{rpm}$.

$\therefore E_2 = 135 \times \frac{1000}{1200} = 112.5\text{V}$.

$\therefore I_a \Big|_{\text{case 2}} = \frac{E_2 - \text{brush drop}}{\frac{0.625}{R_L} + \frac{0.04}{R_a}} = \frac{112.5 - 2}{0.665} = \underline{\underline{166.2\text{A}}}$.

8. A shunt generator delivers 50 kW at 250 V and 400 rpm. The armature and field resistance are 0.02 ohm and 50 ohm, respectively. Calculate the speed of the machine running as a shunt motor and taking 50 kW input at 250 V. Allow 1 V per brush for contact drop and neglect armature reaction. (382 rpm)

Q8.



$$R_a = 0.02 \Omega, R_f = 50 \Omega$$

$$\text{At 400 rpm, } P_{\text{out}} = 50 \text{ kW,} \\ V_{\text{out}} = 250 \text{ V}$$

$$I_f = 5 \text{ A,}$$

$$I_L = \frac{50000 \text{ W}}{250 \text{ V}} = 200 \text{ A}$$

In generating mode,

$$I_a = I_L + I_f = 205 \text{ A}$$

$$\therefore E_g = 250 + \underbrace{(2 \text{ V})}_{\text{Brush drop}} + \underbrace{205 \times 0.02}_{I_a \cdot R_a} = 256.1 \text{ V}$$

In motoring mode,

$$I_a = I_L - I_f = 195 \text{ A}$$

$$\therefore E_b = 250 - 2 \text{ V} - (195 \times 0.02) = 244.1 \text{ V}$$

Since I_f is same in both modes,

$$\frac{N_{\text{motor}}}{N_{\text{generator}}} = \frac{E_b}{E_g} = \frac{244.1}{256.1}$$

$$\Rightarrow N_{\text{motor}} = \frac{244.1}{256.1} \times 400 = 381 \text{ rpm}$$

9. A separately excited DC motor rotates at 1200 rpm when armature terminal voltage is 200 V and armature current is 1 A. The armature resistance is 1 ohm, field winding voltage is 100 V, and the field winding resistance is 100 ohm. Now, the motor is required to rotate at 1250 rpm, with armature current of 1 A, but the armature terminal voltage cannot be increased beyond 200 V. How to achieve the required speed? Give relevant details.

We know that, $E = k\phi\omega$ & $\phi \propto V_{\text{field}}$.

$$\therefore \frac{E_1}{\phi_1 \omega_1} = \frac{E_2}{\phi_2 \omega_2} \quad \text{or} \quad \frac{E_1}{V_{f1} N_1} = \frac{E_2}{V_{f2} N_2}$$

Since E remains unchanged at 1200 & 1250 rpm,
field voltage has to be reduced to increase the speed.

$$\therefore V_{f2} = \frac{N_1 \cdot V_{f1}}{N_2} = \frac{1200}{1250} \times 100 = \underline{\underline{96 \text{ V}}} \rightarrow$$