

Assignment 3a - solutions

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EE114 - Power Engineering 1

Course instructor: Prof. Sandeep Anand

Scribe: Saurabh Singh

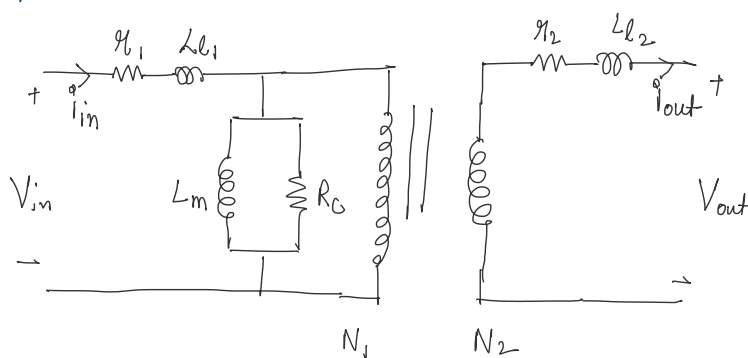
*** Answers are rounded upto 3 decimal places*

Ques 1 :-

$$N_1 = 300$$

$$N_2 = 100$$

$$\mathcal{R} = 2.5 \times 10^{-4} \text{ AT/Wb}$$

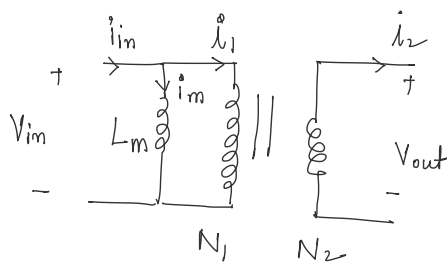


No leakage flux $\rightarrow L_{l1} = L_{l2} = 0$

No iron loss $\rightarrow R_c = 0$

No wire resistance $\rightarrow r_1 = r_2 = 0$

So the equivalent ckt is



a) $V_{in} \rightarrow 240\text{V}, 50\text{Hz supply}$

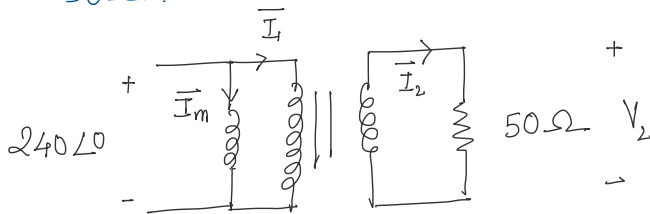
Secondary of the transformer is open circuited
 So $i_2 = 0 \Rightarrow$ Reflected i_1 on primary side is also 0. Only current that flows in the equivalent ckt of the transformer is in the magnetizing inductance branch.

$$L_m = \frac{N_1^2}{R} = \frac{300^2}{2.5 \times 10^4} = 3.6 \text{ H}$$

$$\bar{I}_m = \frac{\bar{V}_{in}}{j\omega L_m} = \frac{240}{j2\pi 50 \times 3.6}$$

$$\bar{I}_m = 0.212 \angle -90^\circ \text{ A}$$

b) Now secondary is connected to resistance of 50Ω .



$$\frac{\bar{V}_1}{\bar{V}_2} = \frac{N_1}{N_2}$$

$$\bar{V}_2 = \frac{100 \times 240 \angle 0}{300}$$

$$\bar{V}_2 = 80 \angle 0$$

$$\bar{I}_2 = \bar{V}_2 / R = 80 \angle 0 / 50 = 1.6 \angle 0 \text{ A}$$

c) Method 1:-

$$N_1 \bar{I}_1 = N_2 \bar{I}_2$$

$$\bar{I}_1 = \frac{100}{300} \times \bar{I}_2 = \frac{100}{300} \times 1.6 \angle 0$$

$$\bar{I}_1 = 0.533 \angle 0$$

$$\bar{I}_m = \bar{I}_1 + \bar{I}_m$$

$$= 0.533 \angle 0 + 0.212 \angle -90^\circ$$

$$\bar{I}_{in} = 0.574 \angle -21.69^\circ$$

★ Method 2 :-

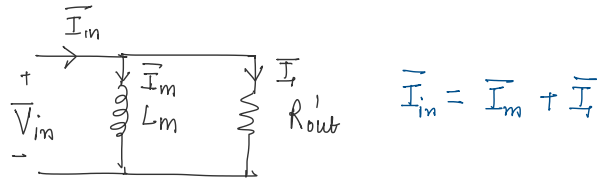
R_{out} referred to the primary side of the transformer

$$R_{out}' = R_{out} \times \left(\frac{N_1}{N_2} \right)^2$$

$$= 50 \times \left(\frac{300}{100} \right)^2$$

$$R_{out}' = 450 \Omega$$

Equivalent ckt :-



$$\vec{I}_{in} = \frac{\vec{V}_{in}}{j\omega L_m} + \frac{\vec{V}_{in}}{R_{out}}$$

$$\vec{I}_{in} = 0.212 \angle -90^\circ + 0.533 \angle 0^\circ$$

$$\vec{I}_{in} = 0.574 \angle -21.69^\circ$$

Ques 2 :-

$$f = 50 \text{ Hz}$$

$$\mu_i = 4500 \mu_0$$

$$A_c = 0.05 \text{ m}^2$$

$$l = 2 \text{ m}$$

$$N_1 = 600$$

$$N_2 = 200$$

a)

$$V_1 = 4.44 f \phi_{peak} N_1 = 4.44 f \phi_{peak} A_c N_1$$

Derivation :-

$$V = V_m \cos \omega t$$

$$e = N \frac{d\phi}{dt}$$

$$\phi = \frac{1}{N} \int e dt$$

$$\phi = \frac{V_m}{N\omega} \sin \omega t$$

$$\phi_{peak} = \frac{V_{peak}}{N\omega}$$

$$V_{peak} = N\omega \phi_{peak}$$

$$V_{rms1} = \frac{N\omega}{\sqrt{2}} \phi_{peak}$$

$$= \frac{N \times 2\pi f}{\sqrt{2}} \phi_{peak}$$

$$V_{rms1} = 4.44 N f \phi_{peak}$$

$$V_{rms1} = 4.44 \times 600 \times 50 \times 1 \times \sqrt{2} \times 0.05$$

$$= 9418.662 \text{ V}$$

$$V_{rms2} = \frac{N_2}{N_1} \times V_1 = 3139.553 \text{ V}$$

b)

$$L_m = \frac{N_1^2}{R}$$

$$R = \frac{l}{\mu A_c} = \frac{2}{4500 \times 4\pi \times 10^{-7} \times \frac{1}{0.05}}$$

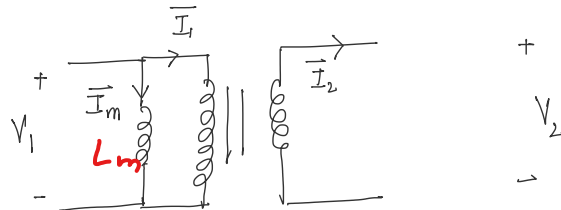
$$R = 7073.553$$

$$\alpha_m = \frac{600^2}{7073.553} = 50.894 \text{ H}$$

$$\bar{I}_m = \frac{\bar{V}_{in}}{j\omega L}$$

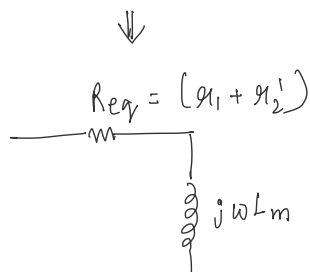
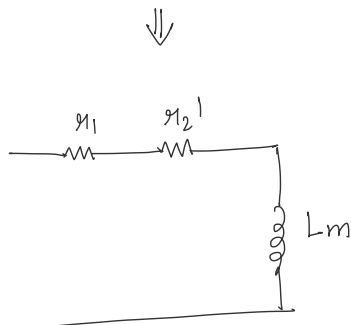
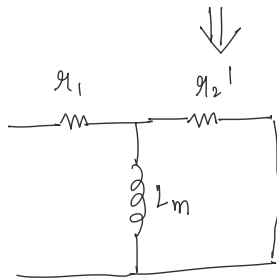
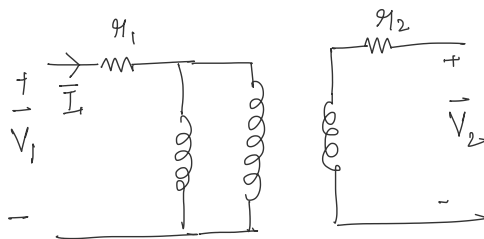
$$= \frac{9418.662}{j \times 2\pi 50 \times 50.894}$$

$$\bar{I}_m = 0.589 \angle -90^\circ$$



c) No iron losses $R_c = 0$
 No leakage inductance $L_{l1} = L_{l2} = 0$

Equivalent circuit



Approximate
equivalent circuit

$$X_m = j\omega L_m = j \times 2\pi \times 50 \times 80.894 \Omega$$

$$X_m = 15.99 \text{ k}\Omega$$

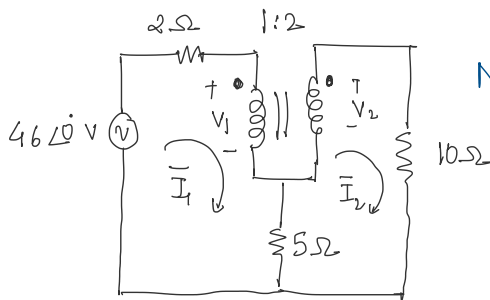
Approximately, losses in transformer at full load

$$P_{\text{loss}} = I^2 R_{\text{eq}}$$

$$2000 = 80^2 \times R_{\text{eq}}$$

$$R_{\text{eq}} = 0.3125 \Omega$$

Ques 3:-



$$N_1 \bar{I}_1 = N_2 \bar{I}_2$$

$$\bar{I}_2 = \frac{1}{2} \bar{I}_1$$

$$\frac{\bar{V}_1}{\bar{V}_2} = \frac{1}{2}$$

$$\bar{V}_2 = 2\bar{V}_1$$

Choose the current direction according to the dot convention.

Here, if we reverse the direction of current I_2 then the relation between I_1 and I_2 would be $I_1 = -I_2$.

First Loop

$$-46\angle 0^\circ + 2\bar{I}_1 + \bar{V}_1 + 5(\bar{I}_1 - \bar{I}_2) = 0$$

$$\bar{V}_1 + \frac{9}{2}\bar{I}_1 = 46\angle 0^\circ \quad \text{--- (i)}$$

$$-\bar{V}_2 + 10\bar{I}_2 + 5(\bar{I}_2 - \bar{I}_1) = 0$$

$$-2\bar{V}_1 + \frac{5}{2}\bar{I}_1 = 0$$

$$\bar{V}_1 = \frac{5}{4}\bar{I}_1 \quad \text{--- (ii)}$$

From (i) & (ii)

$$\frac{5}{4}\bar{I}_1 + \frac{9}{2}\bar{I}_1 = 46\angle 0^\circ$$

$$\bar{I}_1 = 8\angle 0^\circ \text{ A}$$

$$\bar{I}_2 = 4\angle 0^\circ \text{ A}$$

$$\begin{aligned} P_{\text{loss in } 10\Omega \text{ resistor}} &= |\bar{I}_2|^2 R \\ &= 4^2 \times 10 \\ &= 160 \text{ W} \end{aligned}$$

Ques 4.

$$P_{\text{core}_1} = 3000 \text{ W @ } 80 \text{ Hz}$$

$$P_{\text{core}_2} = 5000 \text{ W @ } 75 \text{ Hz}$$

$$\begin{aligned} P_{\text{core}} &= P_{\text{hys}} + P_{\text{eddy}} \\ &= a f B_m^{1.6} + b f^2 B_m^2 \end{aligned}$$

Assumptions

Since B_m is kept constant at both frequencies

$$P_{core} = Af + Bf^2$$

At 50 Hz $50A + 2500B = 3000$

$$75A + 5625B = 5000$$

$$A = 46.667$$

$$B = 0.267$$

@ 50 Hz $P_{phys} = 46.667 \times 50 = 2333.35 \text{ W}$
 $P_{eddy} = 0.267 \times 50^2 = 667.5 \text{ W}$

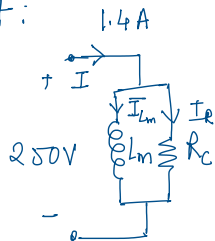
@ 75 Hz $P_{phys} = 3500.025 \text{ W}$
 $P_{eddy} = 1501.875 \text{ W}$

@ 60 Hz $P_{phys} = 2800.02 \text{ W}$
 $P_{eddy} = 961.2 \text{ W}$

Ques 5.

OC test:

LV side :-



$$P_{oc} = 105 \text{ W}$$

$$\frac{V^2}{R_c} = 105 \text{ W}$$

$$R_c = \frac{250^2}{105}$$

$$R_c = 595.238 \Omega$$

$$I_R = \frac{250}{595.238} = 0.42 \text{ A}$$

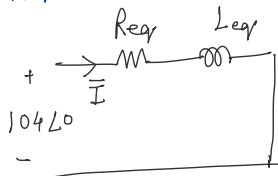
$$I^2 = I_R^2 + I_{Lm}^2$$

$$I_{Lm} = \sqrt{I^2 - I_R^2} = \sqrt{1.4^2 - 0.42^2} = 1.336 \text{ A}$$

$$1.336 = \frac{250}{X_m} \Rightarrow X_m = 187.126 \Omega$$

SC test :-

HV side



$$P_{cu} = 320 \text{ W} \Rightarrow \begin{cases} 8^2 \times R_{eq} = 320 \\ R_{eq} = 5 \Omega \end{cases} \quad \left. \begin{array}{l} \text{Referred to LV} \\ R_{eq} = 0.05 \Omega \end{array} \right\}$$

$$I = \frac{104}{(R_{eq}^2 + X_{eq}^2)^{1/2}}$$

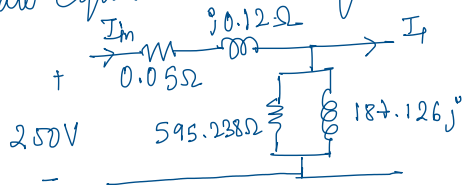
$$8 = \frac{104}{\sqrt{5^2 + X_{eq}^2}}$$

$$64 = \frac{104^2}{5^2 + X_{eq}^2}$$

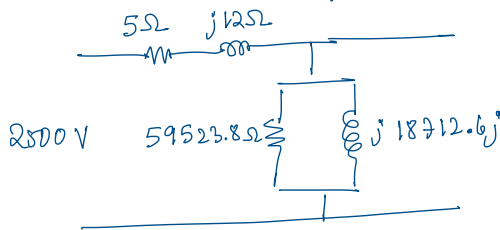
$$X_{eq} = \sqrt{\frac{104^2}{64} - 5^2} = 12 \Omega$$

Referred to LV
 $R_{eq} = 0.12 \Omega$

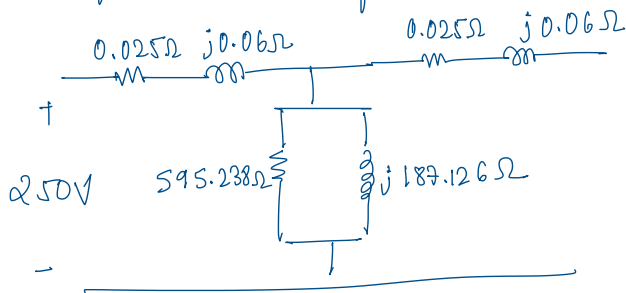
Approximate equivalent ckt referred to LV side



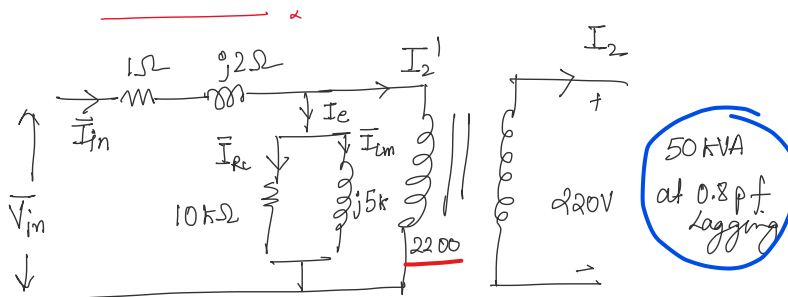
Approximate equivalent ckt referred to HV side



Exact equivalent ckt referred to LV side



Ques 6



$$S_{out} = |V_{out}| \times |I_2|$$

$$50 \times 10^3 = 220 \times I_2$$

$$|I_2| = 227.273$$

$$\cos^{-1}(0.8) = 36.87^\circ$$

$$I_2 = 227.273 \angle -36.87^\circ \text{ A}$$

$$I_2' = \frac{N_2}{N_1} \times I_2$$

$$= \frac{220}{2200} \times 227.273 \angle -36.87^\circ$$

$$\bar{I}_2' = 22.727 \angle -36.87^\circ$$

$$\begin{aligned} a) \quad I_{\text{iron loss}} &= V^2/R_c \\ &= \frac{2200^2}{10 \times 10^3} = 484 \text{ W} \end{aligned}$$

$$I_{R_c} = \frac{2200}{10 \times 10^3} = 0.22$$

$$I_{L_m} = \frac{2200}{j \times 5 \times 10^3} = -j0.44 \quad \boxed{\bar{I}_e = I_{R_c} + I_{L_m}} \quad \bar{I}_e = 0.22 - j0.44 \quad \textcircled{C}$$

$$b) \quad \bar{I}_1 = \bar{I}_e + \bar{I}_2' = 23.168 \angle -37.414^\circ$$

$$P_{cu} = 23.168^2 \times 1 = 536.756 \text{ W}$$

$$d) \quad \bar{V}_i = 2200 + 23.168 \angle -37.414^\circ [1 + 2j]$$

$$\bar{V}_i = 2246.669 \angle 0.58^\circ$$

$$\boxed{S_{in} = |\bar{V}_i| |\bar{I}_i|} = 2246.669 \times 23.168$$

$$S_{in} = 52050.823 \text{ W}$$

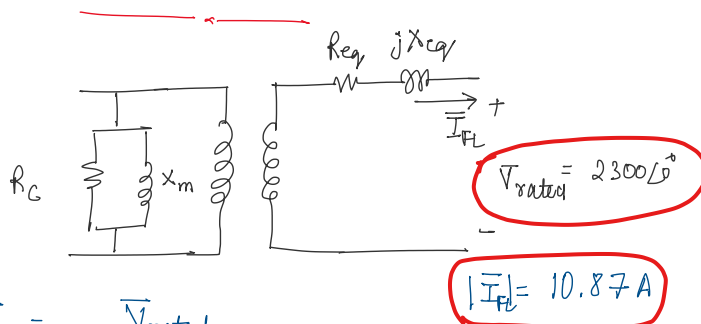
$$\boxed{P_{in} = \text{Re} \{ \bar{V}_i \bar{I}_i^* \}} = \text{Re} \{ 2246.669 \times 23.168 \angle 0.58^\circ + 37.414^\circ \}$$

$$P_{in} = 41019.967 \text{ W}$$

$$\text{input pf} = \frac{P_{in}}{S_{in}} = \frac{41019.967}{52050.823}$$

$$= 0.788$$

Ques 7.



$$\bar{V}_{FL} = \bar{V}_{rated}$$

$$\bar{V}_{NL} = \bar{V}_{rated} + n \bar{I}_p (R_{eq} + jX_{eq})$$

$$= \bar{V}_{rated} + n \bar{I}_{FL} (R_{eq} + jX_{eq})$$

$$= \bar{V}_{rated} + n |\bar{I}_{FL}| R_{eq} (\cos \theta + j \sin \theta) + n |\bar{I}_{FL}| X_{eq} (\cos \theta + j \sin \theta)$$

$$= V_{rated} + x |\bar{I}_{FL}| (R_{eq} \cos \theta - X_{eq} \sin \theta) + j |\bar{I}_{FL}| x (R_{eq} \sin \theta + X_{eq} \cos \theta)$$

$$|\bar{V}_{NL}| = \sqrt{\left[V_{rated} + x |\bar{I}_{FL}| (R_{eq} \cos \theta - X_{eq} \sin \theta) \right]^2 + \left[|\bar{I}_{FL}| x (R_{eq} \sin \theta + X_{eq} \cos \theta) \right]^2}$$

very small w.r.t first term as it has V_{rated} added to it

$$|\bar{V}_{NL}| \approx V_{rated} + x |\bar{I}_{FL}| (R_{eq} \cos \theta - X_{eq} \sin \theta)$$

if lagging $|\bar{V}_{NL}| = V_{rated} + x |\bar{I}_{FL}| (R_{eq} \cos \theta + X_{eq} \sin \theta)$

if leading $|\bar{V}_{NL}| = V_{rated} + x |\bar{I}_{FL}| (R_{eq} \cos \theta - X_{eq} \sin \theta)$

$$\begin{aligned} \text{Voltage Regulation} &= \frac{|\bar{V}_{NL}| - |\bar{V}_{FL}|}{|\bar{V}_{FL}|} \\ &= \frac{x |\bar{I}_{FL}| (R_{eq} \cos \theta \pm X_{eq} \sin \theta)}{V_{rated}} \end{aligned}$$

Let $R = Z_{eq} \cos \phi$
 $X_{pu} = Z_{eq} \sin \phi$

$$= \frac{x |\bar{I}_{FL}| Z_{eq} [\cos \theta \cos \phi \pm \sin \theta \sin \phi]}{V_{rated}}$$

$$\text{Voltage regulation} = \frac{x |\bar{I}_{FL}| Z_{eq} [\cos \theta \cos \phi \pm \sin \theta \sin \phi]}{V_{rated}}$$

in case of lagging load

$$\text{Voltage regulation} = \frac{x |\bar{I}_{FL}| Z_{eq} [\cos(\theta - \phi)]}{V_{rated}}$$

For maximum regulation $x = 1$
 $\& \theta = \phi$

in case of leading load

$$\text{Voltage regulation} = \frac{x |\bar{I}_{FL}| Z_{eq} [\cos(\theta + \phi)]}{V_{rated}}$$

Voltage regulation will always be better (less) for leading load as compared to lagging load

For our question :-

$$Z_{base} = \frac{2300^2}{25 \times 10^3} = 211.6$$

$$\theta = \phi = \tan^{-1} \left(\frac{X_{eq}}{R_{eq}} \right) = \tan^{-1} \left(\frac{2}{1} \right) = 51.34^\circ$$

$$pf \text{ of load} = 0.625 \text{ lagging}$$

$$\text{regulation} = Z_{pu} = \frac{\sqrt{16+25}}{211.6} = 0.03026$$

$$= 3.026\%$$

Ques 8 :-

$$P_{core} = \frac{V_{rated}^2}{R_c}$$

$$R_c = \frac{V_{rated}^2}{P_{core}} = \frac{240^2}{100} = 576 \Omega$$

$$P_{cu} = \left(\frac{I_{rated}}{2}\right)^2 R_{eq}$$

$$60 = \frac{41.667^2}{2} \times R_{eq}$$

$$R_{eq} = 0.138 \Omega$$

$$I_{rated} = \frac{10 \times 10^3}{240}$$

$$= 41.667$$

$$\eta = \frac{P_{out}}{P_{out} + P_{loss}}$$

$$P_{out} = V_{out} I_{out} \cos \phi$$

$$= 240 \times 41.667 \times 0.8$$

$$P_{out} = 8000.064$$

$$P_{loss} = P_{core} + P_{cu} = 100 + 239.587$$

$$= 339.587$$

$$\eta = 95.93\%$$

Ques 9.

$$P_{core} = 200W$$

$$P_{cu} = I^2 R_{eq}$$

$$= (\alpha I_{rated})^2 R_{eq}$$

$$0.8^2 \times P_{cu}^{rated} = 500$$

$$P_{cu}^{rated} = 781.25W$$

$$\eta = \frac{P_{out}}{P_{out} + P_{core} + \alpha^2 P_{cu}^{rated}}$$

$$(i) \quad \eta = \frac{5 \times 10^3 \times 0.8}{5 \times 10^3 \times 0.8 + 200 + 0.25^2 \times 781.25} = 94.144\%$$

$$(ii) \quad \eta = \frac{10 \times 10^3 \times 0.9}{10 \times 10^3 \times 0.9 + 200 + 0.5^2 \times 781.25} = 95.792\%$$

$$(iii) \quad \eta = \frac{20 \times 10^3}{20 \times 10^3 + 200 + 781.5 \times 1^2} = 95.323\%$$

$$(iv) \quad \eta = \frac{10 \times 10^3 \times 0.8}{10 \times 10^3 + 200 + 781.5 \times 1^2} = 95.291\%$$

$$0.8 \times 10 \times 10^3 + 200 + 781.5 \times 0.5$$

Fraction of rated load at which efficiency is maximum (at upf)

$$\eta = \frac{x P_{\text{rated}}}{x P_{\text{rated}} + P_{\text{core}} + x^2 P_{\text{cu}}}$$

$$\frac{d\eta}{dx} = \frac{(x P_{\text{rated}} + P_{\text{core}} + x^2 P_{\text{cu}}) P_{\text{rated}} - x P_{\text{rated}} (P_{\text{rated}} + 2x P_{\text{cu}})}{(x P_{\text{rated}} + P_{\text{core}} + x^2 P_{\text{cu}})^2}$$

$$x P_{\text{rated}} + P_{\text{core}} + x^2 P_{\text{cu}} - x P_{\text{rated}} - 2x^2 P_{\text{cu}} = 0$$

$$x = \sqrt{\frac{P_{\text{core}}}{P_{\text{cu}}}} = \sqrt{\frac{200}{781.25}} = 50.596\%$$

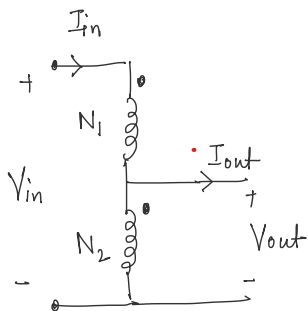
At 0.8 pf lagging & $x \times P_{\text{rated}}$ loading

$$\eta = \frac{x \times S_{\text{rated}} \cos \theta}{x \times S_{\text{rated}} \cos \theta + P_{\text{core}} + x^2 P_{\text{cu}}}$$

$$\eta_{\text{max}} \text{ at } x = \sqrt{\frac{P_{\text{core}}}{P_{\text{cu}}}} = 50.596\%$$

$$\eta_{\text{max}} = 95.291\%$$

Ques 10 :-



$$P_{\text{out}} = 5 \text{ kW at upf}$$

$$V_{\text{out}} = 115 \text{ V}$$

$$V_{\text{in}} = 230 \text{ V}$$

a) Voltage transformation ratio ($V_{\text{HV}}/V_{\text{LV}}$)

$$= \frac{V_{\text{in}}}{V_{\text{out}}} = \frac{230}{115} = 2$$

b)

$$P_{\text{out}} = V_{\text{out}} I_{\text{out}} \cos \theta$$

$$5 \times 10^3 = 115 \times I_{\text{out}}$$

$$I_{\text{out}} = 43.478 \text{ A}$$

c)

Assuming ideal transformer

assuming new winding

$$V_{in} I_{in} = V_{out} I_{out}$$

$$I_{in} = \frac{115}{230} \times 43.478$$

$$I_{in} = 21.739 \text{ A}$$

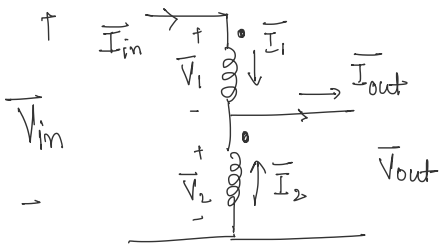
d) Given Number of turns in primary side $N_1 + N_2 = 400$

$$\frac{V_{in}}{V_{out}} = \frac{N_1 + N_2}{N_2}$$

$$\frac{230}{115} = \frac{400}{N_2}$$

$$N_2 = 200 \rightarrow \text{No of turns in secondary}$$

e)



$$I_{out} = I_1 + I_2$$

$$I_2 = I_{out} - I_1$$

$$I_{out} = 43.478 \text{ A}$$

$$I_{in} = I_1 = 21.739 \text{ A}$$

$$\Rightarrow I_2 = 21.739 \text{ A}$$

Power transformed in the windings and supplied to load

$$= \bar{V}_1 \cdot \bar{I}_1 \text{ or } \bar{V}_2 \bar{I}_2$$

$$= 115 \times 21.739$$

$$= 2.5 \text{ kW} = \bar{V}_2 \cdot \bar{I}_2$$

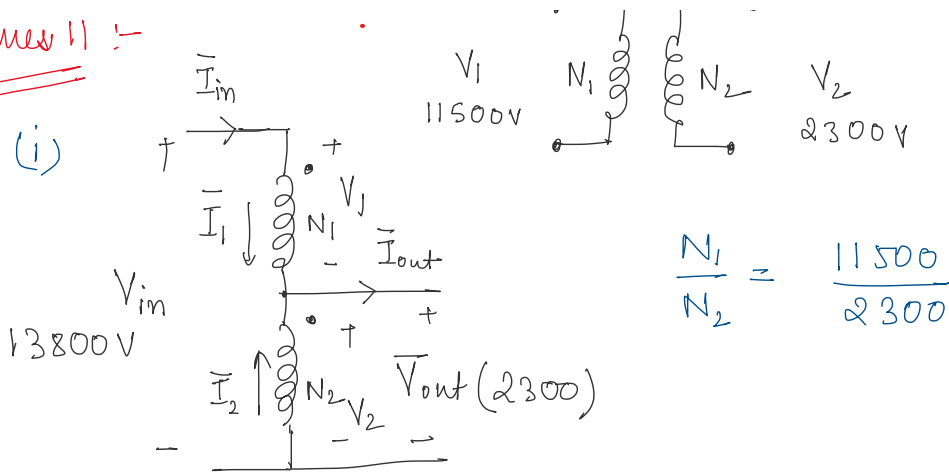
Rest of the output power is conducted directly from the supply to the load

$$= 5 \text{ kW} - 2.5 \text{ kW}$$

$$= 2.5 \text{ kW}$$

Ques 11 :-

(i)



$$\frac{N_1}{N_2} = \frac{11500}{2300}$$

$$\frac{I_1}{I_2} = \frac{N_2}{N_1}$$

For 2 winding configuration

$$V_2 I_2 = V_{out} I_2 = S_{1\phi}$$

For auto transformer

$$V_{out} \times I_{out} = S_{Auto}$$

$$S_{Auto} = V_{out} \times (I_1 + I_2)$$

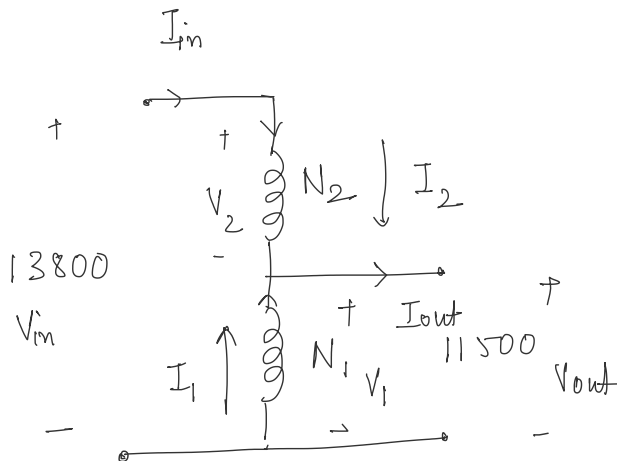
$$= V_{out} \times \left(\frac{N_2}{N_1} + 1 \right) I_2$$

$$S_{Auto} = S_{1\phi} \left(1 + \frac{N_2}{N_1} \right)$$

$$= 100\text{kVA} \left(1 + \frac{2300}{11500} \right)$$

$$= 120\text{kVA}$$

(ii)



$$S_{1\phi} = V_1 I_1$$

$$\begin{aligned} S_{Auto} &= V_1 (I_1 + I_2) \\ &= V_1 \left(I_1 + \frac{N_1}{N_2} I_1 \right) \\ &= V_1 I_1 \left(1 + \frac{N_1}{N_2} \right) \\ &= S_{1\phi} \left(1 + \frac{N_1}{N_2} \right) \\ &= 100 \left(1 + \frac{11500}{2300} \right) \\ &= 600 \text{ kVA} \end{aligned}$$

